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AUS DER KAISERLICH-KÖNIGLICHEN HOF- UND STAATSDRUCKEREI.

1887.

IIA Lib.

CANON DER FINSTERNISSE.

VON

HOFRATH PROF. TH. RITTER V. OPPOLZER,

WIRKLICHEM MITGLIEDE DER KAISERLICHEN AKADEMIE DER WISSENSCHAFTEN.

Mit 160 Tafeln.

VORGELEGT IN DER SITZUNG DER MATHEMATISCH-NATURWISSENSCHAFTLICHEN CLASSE AM 25. OCTOBER 1885.

Einleitung.

Durch meine "Syzygientafeln für den Mond" (Publication der astronomischen Gesellschaft XVI., Leipzig, Engelmann 1881) und meine "Tafeln zur Berechnung der Mondesfinsternisse" (im XLVII. Bande der Denkschriften der math.-naturw. Classe der kais. Akademie der Wissenschaften zu Wien) habe ich Hilfsmittel dargeboten, welche die Berechnung der näheren Umstände jeder Sonnen- oder Mondfinsterniss ohne allzu grosse Arbeit ermöglichen; die in diesen Tafeln eingeführten Abkürzungen sind derart beschaffen, dass dadurch in der Genauigkeit der Resultate keine nennenswerthe Einbusse zu befürchten ist.

Obwohl sich die Bestimmung einer Finsterniss auf Grund dieser Hilfsmittel sehr einfach gestaltet, so sehien es mir doch, dass die Berechnung der Elemente aller Finsternisse, die sieh innerhalb eines für unsere gegenwärtigen Zwecke hinreichend umfassenden Zeitraumes ereignet haben oder ereignen werden, eine Arbeit sei, welche für die Wissenschaft einen bleibenden Werth behalten wird, wenn auch die Grundlagen dieser Rechnungen durch die Fortschritte der Theorie in der Zukunft vielleicht nicht unerhebliche Verbesserungen erfahren werden. Von diesem Standpunkte aus wird die nunmehr vorliegende Berechnung der Elemente und der Hilfsgrössen für 8000 Sonnenfinsternisse und 5200 Mondfinsternisse, die ich mit grossen materiellen Opfern zu Stande gebracht habe, jedenfalls für alle künftigen Untersuchungen als Richtschnur benützt werden können; mit Rücksicht auf diesen mir vorschwebenden Zweck habe ich mir erlaubt, der Sammlung den Titel "Canon" vorzusetzen. Es dürfte daher wohl gerechtfertigt erscheinen, dass dieser Canon, um seinem Titel gerecht zu werden, innerhalb des von ihm in Betracht gezogenen Zeitraumes alle überhaupt möglichen Finsternisse anführe, wenn auch von dem grössten Theile derselben wohl niemals Gebrauch gemacht werden wird.

Was oben in Bezug auf zuktinftige Verbesserung der Grundlagen gesagt wurde, ist theilweise noch vor Abschluss dieser Arbeit eingetreten; Herr F. K. Ginzel hat in seinen schönen Untersuchungen über historische Finsternisse, welche, auf meine Syzygientafeln und auf einige damals schon fertiggestellte Theile des vorliegenden Canons gegründet, in drei Abhandlungen in den Sitzungsberichten der math.-naturw. Classe der kais. Akademie der Wissenschaften erschienen sind (Band LXXXV, II. Abth., Märzheft, LXXXVIII, II. Abth., Juliheft, LXXXIX, II. Abth., Märzheft), und welche in Folge der Bedeutung der erlangten Resultate von der Pariser Akademie durch die Ertheilung des Valz'schen Preises für das Jahr 1884 ausgezeichnet wurden, gezeigt, dass die von mir in den Syzygientafeln angeführten empirischen Correctionen noch erheblicher Verbesserungen fähig seien, und hat in der dritten der oben genannten Abhandlungen die von ihm für dieselben gewonnenen Resultate mitgetheilt. Es müsste daher erwünscht erscheinen, den Canon auf die Ginzel'schen empirischen Correctionen zu gründen, statt auf jene, welche die Syzygientafeln und die Tafeln zur Berechnung der Mondesfinsternisse angeben; jedoch war dies nicht mehr möglich, denn die vorliegende Arbeit war bereits grossen Theils fertiggestellt, bevor Ginzel's Untersuchungen ihren Abschluss fanden. Da indessen durch diese neuen Correctionen, insbesondere für historische Finsternisse, nur in seltenen Fällen halbwegs beträchtlich

veränderte Resultate erhalten werden, so wird man schliessen können, dass dieser dem Canon schon gegenwärtig anhaftende Mangel ihn doch seines Werthes nicht beraubt; doch wird es sich empfehlen, falls eine Finsterniss aus älterer Zeit mit ganz besonderer Genauigkeit gerechnet werden soll, auf diese eben erwähnten Correctionen Rücksicht zu nehmen; um aber die hiezu erforderliche Neuberechnung der Elemente der Finsternisse zu umgehen, beabsichtigt Dr. R. Schram in der nächsten Zeit der kais. Akademie Hilfstafeln vorzulegen, welche in einfacher Weise die hiefür erforderlichen, an die Zahlen des Canons anzubringenden Verbesserungen angeben.

Bezüglich der Zeitgrenzen, die im Detail durch die Einrichtung der Syzygientafeln bedingt wurden, schien es für die nächsten Zwecke kaum nöthig, wesentlich über das Jahr 1200 v. Chr. Geb. zurückzugreifen; anderseits wurden die Rechnungen, um gegenwärtig schon ein Bild für die Zukunft zu entwerfen, bis in das 22. Jahrhundert unserer Zeitrechnung ausgedehnt; die Finsternisse des 20. Jahrhunderts hat Herr Dr. E. Mahler (Denkschriften der kais. Akademie der Wissenschaften, Band XLIX) auf Grund dieser Zahlen näher ausgeführt.

Der Canon in seiner vorliegenden Gestalt soll hauptsächlich dem Historiker bei seinen schwierigen ehronologischen Untersuchungen behilflich sein. Die zahlreichen Nachrichten über Sonnen- und Mondfinsternisse, die sich aus dem Alterthum und Mittelalter erhalten haben, geben in Verknüpfung mit anderen bistorischen Thatsachen ein werthvolles Material zur Ordnung der Chronologie ab; ja, ich glaube nicht allzuviel zu behaupten, wenn ich die Meinung ausdrücke, dass diese Notizen fast allein es ermöglichen, die Chronologie des Alterthums überhaupt in erträgliche Ordnung zu bringen. Die richtige Beurtheilung von Finsternissnachrichten ist indessen keine leichte, da für jeden Fall zumeist mehrere Finsternisse nachgewiesen werden können, welche der Überlieferung genügen, weshalb anderweitige, meist als Nebenumstände zu bezeichnende Angaben von Seite der Historiker herangezogen werden müssen, um mit einiger Wahrscheinlichkeit die thatsächlich gemeinte Finsterniss herauszufinden. Wenn auch die werthvolle Arbeit Pingre's in der Art de vérifier les dates den Historikern hier sehon eine Leitung gegeben hat, so dürfte doch der vorliegende Canon, der, wie es im Fortschritte der Wissenschaft begründet ist, wesentlich genauere Zahlen und diese selbst in grösserer Vollständigkeit vorführt, ihnen um so willkommener sein, weil die beigegebene Iconographie, deren Verwendung weiter unten erläutert wird, sie in den Stand setzt, sich das bezügliche Material, sofern es sich um bedeutende Finsternisse handelt, ganz ohne Rechnung selbst herauszusuchen. Es wird dadurch dem Historiker die Möglichkeit der Entscheidung geboten, ob für seine Frage nur eine oder ob mehrere Finsternisse in Betracht kommen; und seine daran sich knüpfenden Forschungen können daher auf breiterer Basis aufgebaut werden. Will man die näheren Umstände einer Sonnenfinsterniss für einen bestimmten gegebenen Ort mit Genauigkeit ermitteln, so lässt sieh wohl eine kleine Rechnung nicht umgehen, die dem Historiker im Allgemeinen schwer fallen dürfte; es wird aber jedem Astronomen oder auch überhaupt jedem mit der Anwendung mathematischer Formeln vertrauten Maune leicht möglich sein, diese Rechnungen durchzuführen, wenn er nur die hiezu nöthigen, den im Canon enthaltenen Hilfsgrössen angepassten Formeln zur Verfügung hat. Aus dem letzteren Grunde habe ich, besonders da eine solche Formelsammlung keinen allzugrossen Raum beansprucht, eine vollständige Zusammenstellung der für die erwähnten Zwecke nöthigen Formeln, die sich der nunmehr so ziemlich allgemein angenommenen Hansen'schen Theorie der Sonnenfinsternisse der Hauptsache nach anschliessen, beigegeben; übrigens gibt auch hier die von Dr. R. Schram in den Denkschriften der Wiener kais, Akademie (Band LI) publicirte Abhandlung: "Tafeln zur Berechnung der näheren Umstände der Sonnenfinsternisse", wenn es sich darum handelt, ein genähert richtiges Resultat zu erlangen, die Hilfsmittel an die Hand, die für den Historiker erforderlichen Rechnungen auf einen so einfachen Mechanismus zu reduciren, dass dieselben leicht bei sehr mässiger Übung selbst von Personen, denen der Calcul sonst fern liegt, bewältigt werden können. Man kann daher die eben erwähnten Schram'schen Tafeln als überaus werthvolle Ergänzung zum vorliegenden Canon betrachten.

Der Werth einer Arbeit wie der vorliegenden beruht hauptsächlich auf ihrer Verlässlichkeit, weshalb ich besondere Massnahmen ergriffen habe, um die Richtigkeit der in dem Canon enthaltenen Zahlen, so weit dies überhaupt bei einer solch umfassenden calculatorischen Arbeit erreichbar ist, und so weit es die zu Grunde

gelegten Tafeln gestatten, verbürgen zu können; ich glaube die Behauptung zuversichtlich aussprechen zu dürfen, dass sich in dem Canon nur sehr wenige Fehler vorfinden werden. Es wird erwünseht sein, hier die zu diesem Zwecke ergriffenen Massregeln auseinanderzusetzen. Die Einrichtung der Syzygientafeln bringt es mit sich, dass die Arbeit in gewisse Abschnitte, Cyclen, eingetheilt ist; innerhalb eines solchen Cyclus können die Argumente für alle möglicherweise stattfindenden ekliptischen Syzygien durch successive Addition der entsprechenden Zuwächse der Argumente der Reihe nach erhalten werden, und am Schlusse eines solchen Cyclus wird die Übereinstimmung der so erhaltenen Argumente mit dem Resultate der directen Rechnung eine gute Pritfung für die Richtigkeit aller Argumentwerthe innerhalb des ganzen Cyclus abgeben. Auf diese Weise kann sich daher jeder Rechner selbst nahezu völlige Bürgschaft für die correcte Durchführung dieses so wichtigen Abschnittes seiner Arbeit verschaffen; da aber trotzdem noch der Fall denkbar ist, dass innerhalb eines Cyclus in demselben Argumente vielleicht mehrere Fehler begangen wurden, die sich im Schlussresultate zufälligerweise ausgleichen, so wurde auch dieser Theil der Rechnung durch eine zweite, unabhängig durchgeführte Rechnung geprüft. Mit Hilfe der so gewonnenen Argumente wurden durch eine doppelte, von zwei Rechnern in völlig unabhängiger Weise ansgeführte Operation die Elemente der Sonnenfinsternisse mittelst der Syzygientafeln (mit Zuziehung der daselbst gegebenen empirischen Correctionen), jene der Mondfinsternisse mittelst der Tafeln zur Berechnung der Mondesfinsternisse ermittelt, dann beide Rechnungen sorgfältig wiederholt verglichen und erst nach Verbesserung der auftretenden Differenzen bis zur völligen Übereinstimmung der beiderseitigen Zahlen, die letzten Stellen nicht ausgenommen, abgeschlossen. Mit dieser Arbeit ist zugleich die Bestimmung der Mondfinsternisse fast vollendet; für die Sonnenfinsternisse war aber die Ermittlung weiterer Hilfsgrössen und für die centralen Finsternisse besonders die Bereehnung der Hauptpunkte der Centralität sehr wünschenswerth, durch welche Zusätze eben die Zahlen des Cauons im erhöhten Masse brauehbar werden. Auch hiebei ist eine doppelte, unabhängige Rechnung als erstes Erforderniss zur Erreichung einigermassen vertrauenswürdiger Resultate betrachtet worden, doch konnte man diese doppelte Rechnung, besonders wegen der historisch wichtigen, centralen Finsternisse nicht gentigen lassen, da von beiden Rechnern bisweilen die gleichen Zeichen- und Quadrantenfehler gemacht worden sein konnten, die dann übereinstimmende und doch fehlerhafte Resultate zu Tage gefördert hätten. Um auch hiefür die nöthige Sicherheit zu schaffen, wurde zuletzt mit Hilfe geeignet construirter Hilfstafeln, welche mittelst der Argumente B, L und $\log \Delta L$ die auf den rechts liegenden Seiten des Canons eingetragenen Hilfsgrössen in leichter Weise und verhältnissmässig grosser Annäherung direct finden lassen, die Bestimmung der Hauptpunkte der Centralität und der anderen Hilfszahlen nochmals vorgenommen, und die so gewonnenen Resultate mit den früheren verglichen; ein grösserer Fehler konnte nunmehr nicht leicht der Aufmerksamkeit entgehen. In der That erwies sich diese Controle, welche von Herrn Strobl durchgeführt und von Herrn Ginzel revidirt wurde, nicht zwecklos, da dieselbe noch einige, wenn auch nicht erhebliche Incorrectheiten aufdeckte. Ich meine daher, dass auf diese Weise meinerseits Alles geschehen ist, um den Zahlen des Canons eine mit Recht zu fordernde Authenticität zu geben.

Die Herstellung des Canons, welcher 121 Cyclen umfasst, bedurfte des Zusammenwirkens mehrerer Rechner, und es dürfte hier der geeignete Ort sein, in übersichtlicher Weise den Antheil hervorzuheben, welchen jeder Rechner an diesem grossen Werke genommen hat. Bei der folgenden statistischen Zusammenstellung war ich, um derselben durch allzuviel Details nicht eine ungebührliche Ausdehnung zu geben, oft genöthigt, nur den Hauptantheil, den ein Rechner an einem Abschnitte genommen hat, zu notiren; ausserdem muss ich hier der unermüdlichen Thätigkeit des Herrn F. K. Ginzel in besonderer Weise Erwähnung thun, der bei der Revision der Resultate und deren Richtigstellung im Vereine mit mir einen wesentlichen Antheil an der Vollendung der Arbeit hat, ohne dass dies in dem folgenden Schema bemerkbar ist.

Nr. des Cyclus	Reck do Elem	er	Rec d Hi grö	er	Nr. des Cyclus	Recl de Elem	er	d Hi	hner er lfs- ssen	Nr. des Cyclus	Rech de Elem	er	d Hi	hn er er Ifs- ssen	Nr. des Cyclus	Reel de Elem	er	H	ehner ler ilfs- issen
1 2 3 4 5	M. M. M. M. M.	St. St. St. St.	My. My. My. My. My.	Seh. Seh. Seh. Seh. Seh.	31 32 33 34 35	M. M. M. M. M.	St. St. St. St.	My. My. My. My. My.	Seh. Seh. Seh. Seh. Seh.	61 62 63 64 65	M. M. M. M. M.	st. st. st. st.	M. M. M. My. M.	Seh. Seh. Seh. Seh. Seh.	91 92 93 94 95	M. M. M. M. M.	SE S	M. M. M. M. M.	Sch. Sch. Sch. Sch.
6 7 8 9	M. M. M. M. H.	St. St. St. K.	My. My. My. My. H.	Seh. Seh. Seh. Seh. Hz.	36 37 38 39 40	M. M. M. M. M.	St. St. St. St.	My. My. My. My. My.	Sch. Sch. Sch. Sch. Sch.	66 67 68 69	M. M. M. M.	St. St. St. St.	My. My. My. My. My.	Sch. Sch. Sch. Sch.	96 97 98 99 100	M. M. M. M.	St. St. St. St.	M. M. M. M.	Seh. Seh. Seh. Seh.
11 12 13 14 15	И. Н. А. М. М.	St. St. II. St. St.	П. Н. Н. П.	Sch. Sch. Sch. Sch.	41 42 43 44 45	M. M. M. M. M.	St. St. St. St.	My. My. My. My. My.	Sch. Sch. Sch. Sch.	71 72 73 74 75	M. M. M. M. M.	St. St. St. St.	My. My. My. M.	Sch. Sch. Sch. Sch.	101 102 103 104 105	M. M. M. M. M.	St. St. St. St. St.	M. M. M. M. M.	Sch. Sch. Sch. Sch. Sch.
16 17 18 19 20	M. M. M. R. Sch.	St. St. St. Sch. St.	II. H. II. G.	Sch. Sch. Sch. Sch.	46 47 48 49 50	G. G. G. M. M.	St. St. St. St.	G. G. M. M.	Sch. Sch. Sch. Sch.	76 77 78 79 80	M. M. M. M. M.	St. St. St. St.	M. M. M. M. M.	Seh. Seh. Seh. Seh.	106 107 108 109 110	M. M. M. M. M.	St. St. St. St.	M. M. M. M. M.	Sch. G. Sch. Sch. Sch.
21 22 23 24 25	К. G. G. G. M.	Sch. M. St. St. St.	G. G. G. G. My.	Sch. Sch. Sch. My. Sch.	51 52 53 54 55	M. M. M. M. M.	St. St. St. St.	M. M. M. M. M.	Sch. Sch. Sch. Sch.	81 82 83 84 85	M. M. M. M.	St. St. St. St.	M. M. M. M. M.	Sch. Seh. Seh. Sch. Seh.	111 112 113 114 115	M. M. M. M.	St. St. St. St.	M. M. M. M. M.	Sch. Sch. Sch. Sch. Sch.
26 27 28 29 30	M. M. M. M. M.	St. St. St. St. St.	My. My. My. My. My.	Seh. Seh. Seh. Seh.	56 57 58 59 60	M. M. M. M. M.	St. St. St. St.	M. M. M. M.	Sch. Sch. Sch. Sch.	86 87 88 89 90	M. M. M. M. M.	St. St. St. St. St.	M. M. M. M.	Sch. Sch. Sch. Sch. Sch.	116 117 118 119 120	M. M. M. M. M.	St. St. St. St.	M. M. M. M. M.	Sch. Sch. Sch. Sch.
															121	M.	St.	M.	Sch.

Namen der Rechner:

 $\begin{array}{lll} A. \equiv \mathrm{Dr. \ Ferd. \ Anton.} & M. \equiv \mathrm{Dr. \ Ed. \ Mahler.} \\ G. \equiv F. \ K. \ Ginzel. & My. \equiv \mathrm{Dr. \ M. \ Wilh. \ Meyer.} \\ H. \equiv \mathrm{Dr. \ E. \ Freih. \ v. \ Haerdtl.} & R. \equiv H. \ Freih. \ v. \ Rülling. \\ Hz. \equiv \mathrm{Dr. \ Norb. \ Herz.} & Sch. \equiv \mathrm{Dr. \ Bernh. \ Schwarz.} \\ K. \equiv \mathrm{Dr. \ Frz. \ K\"uhnert.} & St. \equiv \mathrm{Josef \ Strob \ l.} \end{array}$

Die Berechnung der Mondfinsternisse haben die Herren F. K. Ginzel und Josef Strobl in zwei von einander unabhängigen Rechnungen durchgeführt.

Ich glaube auch hier hervorheben zu müssen, dass ich, um den gewiss sehr sachgemässen Beschlüssen der Washingtoner Conferenz des Jahres 1884 bezüglich der Zählung der geographischen Längen und der Zeit Rechnung zu tragen, bei allen Längenangaben die östlichen positiv, die westlichen negativ angesetzt und den Greenwicher Meridian als Ausgangsmeridian betrachtet habe. Die Zeitangaben sind durchaus als Weltzeit zu nehmen, welche mit der bürgerlichen mittleren Greenwicher Zeit zusammenfällt. Ich will hoffen, dass die Gegner der Weltzeit hieraus nicht die Unbrauchbarkeit des vorliegenden Canons ableiten werden; gerade hier wird jene Zeiteinrichtung, die der bürgerlichen angepasst ist, wesentliche Vortheile aufweisen.

Schliesslich habe ich auch jener Massnahmen zu gedenken, welche ergriffen wurden, um die Drucklegung der gewonnenen Resultate möglichst correct durchzuführen; dabei hatte ich mich der besonderen Fürsorge des

Directors der k. k. Hof- und Staatsdruckerei Hofrathes A. v. Beck zu erfreuen, wofür ich demselben zu grossem Danke verpflichtet bin. Die erste Correctur wurde mit dem Originalmanuscripte gelesen, welches aus den beiderseitigen Rechnungen fertiggestellt worden war und durch mehrfache Vergleichungen gesichert erschien; die zweite Correctur wurde mit den Zahlen der einen, die dritte mit jenen der anderen Rechnung direct gelesen. Bei dieser umfassenden und mühevollen Arbeit bin ich in aufopferungsvoller Weise von Herrn Alois Steinmaszler unterstützt worden; ich erlaube mir, ihm an dieser Stelle meinen Dank auszusprechen; desgleichen muss ich hier der eifrigen Mithilfe des Herrn Josef Strobl Erwähnung thun, sowie der des Herrn Dr. Franz Kühnert; bei der Correctur der ersten Druckbogen wirkte überdies in sehr erspriesslicher Weise Herr F. K. Ginzel mit. Um aber ganz sicher zu sein, dass nicht etwa ein Versehen bei der Fertigstellung der Druckplatten für die definitiven Abzüge vorgefallen sei, haben die Herren Dr. R. Schram und Dr. E. Mahler nochmals die Aushängebogen einer vollständigen Controle unterzogen; die Fehler, welche bei derselben bemerkt wurden, waren meist nicht einem Übersehen bei den früheren Correcturen zuzuschreiben und beschränken sich grösstentheils auf Beschädigungen, welche die Ziffern durch die Druckoperation erfahren hatten. Im Ganzen blieben zwei Fehler in den Zahlenangaben, welche bei den früheren Correcturen übersehen worden waren; gewiss ein sehr befriedigendes Resultat. Das Fehlerverzeichniss ist am Schlusse des Textes angeführt und zeigt eine allerdings grössere Anzahl von Fehlern, die sich jedoch in anderer Weise in die Tafeln eingeschlichen haben; ausserdem wird man häufigere Correcturen in den ersten drei Bogen bemerken, doch sind diese Fehler eigentlich nicht als solche zu betrachten, sondern erklären sich aus dem Umstande, dass man anfänglich alle Finsternisse, die nicht central erscheinen, zu den partiellen gezählt hatte; über die schärfere, später eingeführte Trennung berichtet die für die E-Columne gegebene Erläuterung. Ich meine daher, dass demnach die Correctheit des vorliegenden Canons selbst hochgespannten Forderungen im vollsten Masse genügen werde.

I.

Canon der Sonnenfinsternisse.

Erläuterung der im Canon der Sonnenfinsternisse angeführten Zahlenwerthe.

Der Canon der Sonnenfinsternisse enthält die Elemente und die Hilfsgrössen aller Finsternisse, welche sich zwischen dem Datum:

- 1207 November 10 (julianisch) und 2161 November 17 (gregorianisch)

ereignen. Als Grundlage hiezu dienten meine eingangs erwähnten Syzygientafeln, durch deren Einrichtung die Zeitgrenzen im Detail bedingt wurden, mit Hinzuziehung der dort gegebenen empirischen Correctionen. Zufolge der Abzählung der Gattung der Finsternisse findet man, dass in einem julianischen Jahrhunderte durchschnittlich 237.5 Sonnenfinsternisse stattfinden, von denen für die Erde überhaupt 83.8 partiell, 77.3 ringförmig, 10·5 ringförmig-total und 65·9 total sind. Die Anordnung der Zahlen in dem Canon der Sonnenfinsternisse ist so getroffen, dass mit Ausnahme der letzten Columne die linke Seite die Elemente, die rechte Seite die Hilfsgrössen enthält.

Die Columnen jeder link en Seite sind:

- 1. Columne. Nr., enthält die fortlaufende Nummer der Finsternisse.
- 2. Columne. T, gibt dem Wesen nach die Weltzeit der wahren ekliptischen Conjunction und zerfällt in drei Subcolumnen: Die erste enthält das Datum, wie die Überschrift darstellt, bis zum October 1582 in julianischer, von da ab in gregorianischer Zählung; die zweite Subcolumne gibt den zum Datum gehörigen Tag der julianischen Periode und wurde hauptsächlich deshalb angesetzt, um mittelst dieser Zahl auf etwaige andere Kalenderzählungen mit Hilfe der Schram'schen Hilfs-

tafeln für Chronologie (im XLV. Bd. der Denkschriften der math.-naturw. Classe der kais. Akad. der Wissensch. in Wien) in bequemer Weise übergehen zu können. Ein weiterer, allerdings nicht wesentlicher Vortheil der Angabe der zum Datum gehörigen julianischen Tage besteht darin, dass man dadurch im Stande ist, den Wochentag des vorgesetzten Datums zu bestimmen. Dividirt man nämlich die dem Datum entsprechende Tageszahl der julianischen Periode durch sieben, so ist der Tag ein:

	Montag, v	venn	der	\mathbf{Rest}	Ο,
	Dienstag,	"	27	22	1,
Seef 32	Mittwoch,	27	"	27	2,
•	Donnerstag	, ,,	"	"	3,
	Freitag,	27	77	27	4,
	Samstag,	27	17	"	5,
	Sonntag,	"	77	22	6 ist.

Die dritte Subcolumne gibt in Stunden, Minuten und deren Decimaltheilen die Weltzeit (bürgerliche Greenwicher Zeit) der wahren ekliptischen Conjunction.

- 3. Columne. L', ist die zur Zeit der wahren Conjunction stattfindende scheinbare L\u00e4nge der Sonne und des Mondes.
- 4. Columne. Z, ist die Zeitgleichung in Einheiten des Grades; wollte man dieselbe in Einheiten der Zeitminute erhalten, so hätte man sie vorher mit 4 zu multiplieiren. Die Zeitgleichung ist durchaus im Sinne "mittlere wahre Zeit" angesetzt und gibt also die Correction an, die man zur wahren Zeit algebraisch hinzulegen muss, um die mittlere zu erhalten.
- 5. Columne. ε, stellt die zur Zeit der Finsterniss stattfindende Schiefe der Ekliptik dar.
- 6. Columne. P, gibt die Grösse P, welche in Verbindung mit $\log p$ aus der achten Columne durch die Formel $B = p \sin P$ die Grösse $B = \frac{\sin (b b')}{\sin (\pi \pi')}$ finden lässt, in welch' letzterer Formel b und b' beziehungsweise die Mond- und Sonnenbreiten, π und π' die zugehörigen Parallaxen bezeichnen. B ist der Werth der von Hansen mit Q bezeichneten Coordinate des Schattenkreismittelpunktes für den Moment der wahren Conjunction.
- 7. Columne. Q, enthält die Grösse Q, welche in Verbindung mit $\log q$ aus der zehnten Columne durch die Formel $\Delta B = q \cos Q$ die Grösse ΔB oder die stündliche Änderung des oben B genannten Ausdruckes darstellt.
- · 8. Columne. log p, siehe unter 6. Columne.
- 9. Columne. $\log \Delta L$, gibt den \log der stündlichen Änderung des Ausdruckes $\frac{\cos b \sin(L-L')}{\sin(\pi-\pi')}$, in welchem L und L' die scheinbaren Mond- und Sonnenlängen vorstellen. Es ist dies die stündliche Änderung der von Hansen mit P bezeichneten Coordinate des Schattenkreismittelpunktes, welch' letztere selbst für den Moment der wahren Conjunction gleich Null ist.
- 10. Columne. $\log q$, siehe unter 7. Columne.
- 11. Columne. u'_a , ist der Halbmesser des Schattenkreises in der durch den Mittelpunkt der Erde senkrecht auf die Axe des Schattenkegels gelegten Ebene in Einheiten des Erdhalbmessers.
- 12. Columne. $\log f_a$, gibt den log des Bogens, welcher dem Erzeugungswinkel des Schattenkegels entspricht.
- . 13. Columne. log γ, enthält den log der Grösse γ, welche Grösse selbst sich in der dritten Columne der rechten Seite vorfindet.

Die Columnen der rechten Seite sind:

- 1. Columne Nr., enthält wieder die fortlaufende Nummer der Finsterniss, um die Zusammengehörigkeit der Ziffern beider Seiten zu sichern.
- 2. Columne. μ, enthält den Stundenwinkel der wahren Sonne unter dem Meridian von Greenwich zur Zeit der grössten Phase der Finsterniss.

- 3. Columne. 7, gibt die kleinste Entfernung des Erdmittelpunktes von der Axe des Schattenkegels in Einheiten des Erdhalbmessers.
- 4. Columne. log n, gibt den log. der stündlichen Bewegung des Schattencentrums auf der Durchschnittslinie der relativen Mondbahn mit der durch den Mittelpunkt der Erde senkrecht auf die Schattenkegelaxe gelegten Ebene in Einheiten des Erdhalbmessers.
- 5. Columne. G, gibt die Hilfsgrösse G.
- 6. Columne. K, gibt die Hilfsgrösse K.
- 7. Columne, log sin g, gibt die Hilfsgrösse log sin g.
- 8. Columne. log sin k, gibt die Hilfsgrösse log sin k.
- 9. Columne, log cos g, gibt die Hilfsgrösse log cos g.
- \cdot 10. Columne, log cos k, gibt die Hilfsgrösse log cos k.
- · 11. Columne. log sin d', gibt den log, sin, der Sonnendeelination zur Zeit der wahren Conjunction.
- · 12. Columne. log cos δ' , gibt den log, cos, desselben Winkels.
- . 13. Columne. N', gibt den Winkel an, welchen die relative Mondbahn zur Zeit der wahren Conjunction mit dem Declinationskreise bildet.

Die zur Berechnung der vorstehenden Hilfsgrössen nöthigen Formeln sind:

$$B = p \sin P$$
 $\Delta B = q \cos Q$
 $\sin \delta' = \sin I I \sin \varepsilon$ $\tan A = \cos I I \tan \varepsilon$

 δ' als Sonnendeelination und h sind stets innerhalb der Grenzen 0° bis ± 90 ° zu nehmen, also $\cos \vartheta'$ und $\cos h$ stets positiv; $\cos \vartheta'$ lässt sich immer aus $\sin \vartheta'$ mit Sicherheit bestimmen.

$$n \sin N_1 = \Delta L$$

$$n \cos N_1 = \Delta B.$$

Der Quadrant von $N_{\rm f}$ ist so zu bestimmen, dass n positiv gefunden wird.

$$\gamma = B \sin N_1$$
.

Bezeichnet man mit d die in Decimaltheile des Tages umgesetzte Weltzeit, so bestimmt sich die Hilfsgrösse ρ , nach der Formel:

$$\mu = 360 . d - Z - \frac{15}{n} B \cos N_1 \pm 180^\circ;$$

ferner ist noch zu berechnen:

$$N' = N_1 - h$$

$$\sin g \sin G = \sin \delta' \sin N'$$
 $\sin k \sin K = \sin N'$
 $\sin g \cos G = \cos N'$ $\sin k \cos K = \sin \delta' \cos N'$
 $\cos g = \cos \delta' \sin N'$ $\cos k = \cos \delta' \cos N'$.

Die Quadranten von G und K werden so bestimmt, dass sin g und sin k immer positiv sind. Somit erscheint der Zusammenhang der auf der rechten Seite des Canons vor dem stark ausgezogenen Verticalstrich stehenden Hilfsgrössen mit den Sonnenfinsternisselementen dargestellt.

Die 14. Columne enthält in drei Subcolumnen, deren jede wieder in zwei weitere zerfällt, die Angabe der drei Hauptpunkte der Centralität. Die erste Subcolumne gibt die von Greenwich gezählte geographische Länge (östlich positiv, westlich negativ) und Breite desjenigen Punktes, an welchem die Centralität bei Sonnenaufgang, die zweite jenen Ort, für den die Centralität im Mittag, die dritte jenen, an welchem die Centralität im Momente des Sonnenunterganges stattfindet. Für Finsternisse, die auf der Erde überhaupt nur partiell sind, liegt es in der Natur der Sache, dass für dieselben keine derartigen Punkte vorhanden sind; für die partiellen Finsternisse sind also an Stelle der geographischen Coordinaten nur Striche gesetzt. Striche finden sich übrigens auch in selteneren Fällen an Mittagspunkten der Centralität. Manche Finsternisse haben nämlich die Eigenschaft, dass für dieselben kein reeller Mittags- oder auch Mitternachtspunkt entsteht, wesshalb der zweite Ort eine Lücke zeigt; dann sind aber die beiden den Aufgangs- und Untergangscolumnen zugewiesenen Coordinaten entweder beide Aufgangs- oder beide Untergangspunkte. Um dies anzeigen zu können, ohne die Anordnung der Zahlen zu verschieben, sind jene Untergangspunkte, welche in die Aufgangscolumne gestellt wurden, in Klammern gesetzt, ebenso jene Aufgangspunkte, die in der Untergangscolumne stehen. Erscheinen also in der Untergangscolumne die Angaben der geographischen Coordinaten geklammert, so sind beide Punkte Aufgangspunkte, sind dagegen die Zahlen der Aufgangspunkte in Klammern gefasst, so sind beide Punkte Untergangspunkte. Ferner haben manche Finsternisse keinen Mittagspunkt, wohl aber einen Mitternachtspunkt, d. h. man sieht für den angegebenen Ort die Finsterniss um Mitternacht. Solche Punkte sind in die Columne des Mittagspunktes eingetragen, aber in Klammern gefasst; die Einklammerung eines Mittagspunktes zeigt also, dass er eigenflich ein Mitternachtspunkt ist.

Die 15. Columne F, charakterisirt die Gattung der Finsterniss überhaupt, und zwar bezeichnet:

p = partielle Finsterniss,

(p) =in Folge der Abplattung unsichtbare Finsterniss,

r = ringförmige, centrale Finsterniss,

(r) = ringförmige, nicht centrale Finsterniss,

t =totale, centrale Finsterniss,

(t) = totale, nicht centrale Finsterniss,

r-t = ringförmig-totale, centrale Finsterniss.

* zeigt au, dass die drei Hauptpunkte der betreffenden Finsterniss vollständig in das Gebiet der beigegebenen Karten fallen.

Die Berechnung der Centralitätspunkte in Columne 14 gesehah in einer genäherten Weise mit Vernachlässigung der Erdabplattung; die dadurch erlangte Genauigkeit ist für den vorliegenden Zweek, nämlich für die allgemeine Charakterisirung des Curvenganges der Centrallinie völlig ausreichend. Für die Bestimmung des Mittagspunktes der Centralität hat man zuerst:

$$\sin(\varphi_m - \delta') = \frac{\gamma}{\sin N'}.$$

 $(\varphi_m - \delta')$ wird innerhalb der Grenzen O° bis ± 90 ° angenommen, so dass $\cos(\varphi_m - \delta')$ stets positiv ist. Findet sich $\pm \sin(\varphi_m - \delta') > 1$, so ist kein reeller Mittags- oder Mitternachtspunkt vorhanden. Bereelnet man nun φ_m aus $(\varphi_m - \delta')$ mittelst:

$$\varphi_m = (\varphi_m - \delta') + \delta',$$

so kann der Fall eintreten, dass $\varphi_m > \pm 90^{\circ}$ wird, dann setzt man statt φ_m seine Ergänzung zu $\pm 180^{\circ}$, das obere Zeichen gilt für φ_m positiv, das untere für φ_m negativ. In beiden Fällen ist der gefundene Punkt ein Mitternachtspunkt und erscheint im Canon in Klammern gesetzt.

Die geographische Länge des Mittagspunktes findet sich nach der Formel:

$$\lambda_m = -\mu - \frac{15}{n} \cos N' \sin (\varphi_m - \delta'),$$

ist aber in jenen Fällen, wo $\varphi_n > \pm 90^\circ$ gefunden wurde, um $\pm 180^\circ$ zu vermehren, gehört dann zu einem Mitternachtspunkt und erscheint im Canon in Klammern gesetzt.

Die geographischen Coordinaten der Aufgangs- und Untergangspunkte der Centralität werden mittelst der folgenden Formeln bestimmt:

$$\sin W = \gamma, \qquad \tau' = \frac{15}{n} \cos W$$

W innerhalb der Grenzen 0° bis ±90°, also cos W stets positiv.

Aufgangspunkt. Untergangspunkt.
$$tg \ t_a = \frac{tg (N'+W)}{\sin \delta'}$$

$$tg \ t_a = \frac{tg (N'+W)}{\sin \delta'}$$

$$tg \ t_a = \frac{tg (N'-W)}{\sin \delta'}$$

$$sin \ t_a \ muss \ mit \ sin \ (N'-W) \ gleich \ bezeichnet \ sein.$$

$$sin \ \varphi_a = -\cos \delta' \cos (N'+W)$$

$$sin \ \varphi_a = \cos \delta' \cos (N'+W)$$

$$\tau_a = \mu - \tau'$$

$$\lambda_a = t_a - \tau_a.$$

$$\lambda_u = t_u - \tau_u.$$

Ist in der 15. Columne das Symbol r oder t geklammert, also (r) oder (t) angesetzt (der Fall (r-t) kommt in den vorliegenden 8000 Finsternissen überhaupt nicht vor), so erhalten die in der 14. Columne stehenden Zahlen eine etwas andere Bedeutung. Es sind nämlich die so bezeichneten Finsternisse solche, die zwar nirgends für die Erde central werden, jedenfalls aber die Grösse von 12 Zoll erreichen. Für diese Finsternisse sind die angesetzten Punkte demmach nicht für die Centrallinie zu verstehen, sondern es gelten für die auf der nördlichen Hemisphäre sichtbaren Finsternisse die Punkte der südlichen zwölfzölligen Curve, für diejenigen auf der südlichen Hemisphäre dagegen jene der nördlichen zwölfzölligen Curve. Im Allgemeinen werden sich diese zwölfzölligen Curven ähnlich wie jene der Centralität verhalten, und es wird meist, aber nicht immer, der Mittags- oder Mitternachtspunkt fehlen. Die bezüglichen Unterscheidungsmerkmale sind ähnlich wie früher gewählt; ist kein Mittagspunkt, wohl aber ein Mitternachtspunkt vorhanden, so erscheint die Angabe in der Columne des Mittags eingeklammert, fehlt aber ein solcher ganz, und sind demnach die Punkte Aufgangsoder Untergangspunkte, so ist im ersten Falle die in der Untergangscolumne stehende geographische Position, im anderen Falle jene in der Aufgangscolumne geklammert. Die Rechnung für diese nicht sehr häufigen Fälle ist der Consequenz halber für eine rein sphärische Erde, und zwar in der folgenden Weise durchgeführt.

Zuerst bestimmt man
$$u'_i$$
 nach: $u'_i = 0.5473 - u'_o$.

Bezeichnet man den absoluten Werth von u'_i dadurch, dass über den betreffenden Buchstaben ein positives Zeichen gesetzt wird, und setzt dann $\gamma = u'_i = \sin W$, wobei der obere Werth gilt, wenn γ positiv, der untere, wenn γ negativ ist, so wird W zwischen den Grenzen 0° bis $\pm 90^{\circ}$ anzunehmen sein, und man hat dann:

$$\tau' = \frac{15}{n} \cos W$$

$$\operatorname{tg} t_a = \frac{\operatorname{tg} (N' + W')}{\sin \delta'}$$

$$\sin t_a \text{ ungleich bezeichnet mit } \sin (N' + W)$$

$$\sin \varphi_a = -\cos \delta' \cos (N' + W)$$

$$\tau_a = \mu - \tau'$$

$$\lambda_a = t_a - \tau_a$$

$$\sin (\varphi_m - \delta') = \frac{\sin W}{\sin N'}$$

$$\lambda_m = -\mu - \frac{15}{n} \cos N' \sin (\varphi_m - \delta').$$

Auch hierbei ist natürlich zu beachten, dass wenn $\varphi_m > \pm 90^\circ$ wird, man statt φ_m seine Ergänzung zu $\pm 180^\circ$ zu nehmen und das zugehörige λ_m um $\pm 180^\circ$ zu vermehren hat. Es gehören dann wieder φ_m und λ_m einem Mitternachtspunkte an und erscheinen im Canon in Klammern gesetzt.

Zufolge der Syzygientafeln hat man für die Grenzen der Finsternisse anzunehmen:

$$B = p \sin P$$
.

- 1) B < 1.0048, so ist die Finsterniss central,
- 2) $1 \cdot 0048 < B < 1 \cdot 0073 + u'_a$, so ist die Finsterniss nicht central,
- 3) $1 \cdot 0073 + u_a' < B$, so ist die Finsterniss unmöglich.

Für die Grenzen zwischen Totalität und Ringförmigkeit erhält mau:

- 4) $u'_a < 0.5473$, so ist die Finsterniss total,
- 5) $0.5479 < u'_a < 0.5519$, so ist die Finsterniss ringförmig-total,
- 6) $0.5519 < u'_a$, so ist die Finsterniss ringförmig.

Zu diesen durch die Syzygientafeln gegebenen Grenzen, welche für die kugelförmige Erde gelten, wären die folgenden Bemerkungen zu machen. Zunächst ist in der Gleichung 2) nach einer Bemerkung des Dr. Robert Schram statt des Ausdruckes "partiell" das Wort "nicht central" gewählt worden, da es möglich ist, dass an sich nicht centrale Finsternisse in allerdings seltenen Fällen doch total oder ringförmig sein können. Für solche Finsternisse, bei denen der absolute Werth von γ mit Rücksicht auf die Abplattung der Erde zwischen den Grenzen 0·9970 und 1·0300 eingeschlossen ist, wurde die Entscheidung in der folgenden Weise vorgenommen:

 $u'_a < 0.5473$ and $0.9970 < \frac{+}{\gamma} + u'_a < 1.5447$, so ist die Finsterniss total, aber nicht central (t). $0.5473 < u'_a < 0.5519$ and $0.9970 < \frac{+}{\gamma} < 0.4501 + u'_a$, so ist die Finsterniss ringförmig-total, aber nicht central (r - t). $u'_a > 0.5519$ and $0.9970 < \frac{+}{\gamma} < 0.4501 + u'_a$, so ist die Finsterniss ringförmig, aber nicht central (r).

Für alle nicht centralen Finsfernisse also, die aber stellenweise doch total oder ringförmig erscheinen können, sind die analogen Bezeichnungen in Klammern eingesetzt und sind, wie schon oben bei Erläuterung der 14. Columne hervorgehoben wurde, die Hauptpunkte der 12zölligen Phase gerechnet.

Bezüglich der für ringförmig-totale Finsternisse aufgestellten Grenzbestimmungen wäre zu bemerken, dass innerhalb dieser Grenzen wohl ein Übergang von der Ringförmigkeit in die Totalität stattfinden kann, aber nicht muss. Das Kriterium, ob in der That für eine vorgelegte Finsterniss die Bezeichnung v-t beizubehalten oder nur r anzusetzen sei, findet sich leicht, wie folgt:

$$\log f_i = 9_n 9978 + \log f_a$$

$$u_i' = 0.5478 - u_a'$$

$$\frac{u_i}{f_i} < \cos W.$$

Ist diese Ungleichung erfüllt, so erscheint in der That die Finsterniss in den Enden der Centralzone ringförmig, gegen ihre Mitte hin total; ist aber diese Bedingung nicht erfüllt, so bleibt die Finsterniss an allen Orten ringförmig. Dementsprechend sind alle Finsternisse, für welche die obigen Grenzbestimmungen r-t ergaben, näher untersucht und eventuell auf die Bezeichnung r zurückgeführt worden.

Die Bestimmung der Hauptpunkte der Centralität gilt für eine kugelförmige Erde. Zufolge der Abplattung der Erde werden einige wenige Finsternisse, für welche die obigen Grenzbestimmungen die Bezeichnung p finden lassen, völlig unsichtbar. Dieser Fall kann nur eintreten, wenn γ zwischen 1·5200 und 1·5800 liegt, und wenn $\gamma > 0$ ·9970 + u'_a wird. Diese Finsternisse wären daher eigentlich aus dem Canon auszuscheiden gewesen; sie sind aber der Consequenz halber beibehalten worden, nur wurde der Buchstabe p in Klammern gesetzt. Die mit (p) bezeichneten Finsternisse finden also zufolge einer genaueren Rechnung nicht statt.

Die den Buchstaben beigefügten Sternehen finden ihre nähere Erläuterung bei den Karten, nur soll gleich hier hervorgehoben werden, dass der Zusatz eines Sternehens den Hinweis enthält, dass alle drei Punkte in das Gebiet einer Karte fallen, welche die gesammte nördliche Hemisphäre und den Gürtel vom Äquator bis zu 30° südlicher Breite zur Darstellung bringt.

Da bei der Grenzbestimmung für den Eintritt einer Sonnenfinsterniss auf die Säcularglieder und auf die Einführung einer empirischen Correction keine Rücksicht genommen wurde, so wäre es bei einer Combination

von ausserordentlichen Umständen immerhin möglich, dass eine oder die andere Finsterniss bei Berücksichtigung derselben vorhanden ist, während sie ohne Rücksichtnahme auf dieselben als nicht eintretend bezeichnet werden muss. Ein wesentlicher Nachtheil kann aber hieraus um so weniger entstehen, als es sich hier bloss um Finsternisse handelt, deren Eintreten nur mit Hilfe grösserer optischer Hilfsmittel constatirt werden kann, und zwar nur in der Nähe des Horizontes in Gegenden, die den Polen der Erde verhältnissmässig naheliegen. Übrigens sind die Finsternisse innerhalb der Zeitgrenzen des Canons in dieser Richtung untersucht worden, und es hat sieh hiebei keine Correctur der Angaben des Canons als erforderlich erwiesen.

Zusammenstellung der Formeln zur Berechnung der näheren Umstände der Sonnenfinsternisse.

Ich gebe hier noch eine ausführliche Zusammenstellung aller zur Ermittlung der wichtigsten Umstände einer Finsterniss nöthigen Formeln, dem Wesen nach Hansen's Theorie der Sonnenfinsternisse entsprechend (Theorie der Sonnenfinsternisse und verwandter Erscheinungen. Abhandl. d. kgl. sächs. Ges. d. Wiss. IV.), doch sind an manchen Orten einige für die vorliegenden Zwecke als zulässig zu bezeichnende Abkürzungen eingeführt und hie und da zweckmässige Abänderungen vorgenommen worden.

I. Ermittlung der Umstände einer Sonnenfinsterniss für die Erde überhaupt.

a) Gemeinsame Hilfsgrössen und Formeln zur Bestimmung der Grenzeurven.

Angenommene Abplattung der Erde
$$e = \frac{1}{299 \cdot 153}$$
.

$$D = \delta' + \xi' \sin \delta' \cos \delta'$$

$$\log \xi' = 9 \cdot 2830$$

$$v = -\xi' \cos y \cos k \qquad \sin C = \xi \cos y, \qquad e = \cos C$$

$$\log \xi = 8 \cdot 9122 \qquad \sin C = \xi \cos k, \qquad e' = \cos C'.$$

 $\zeta' \sin \delta' \cos \delta'$ und ν werden in Einheiten des Grades erhalten.

Der grösste Theil der nachstehenden Formeln reducirt die Grössen zur Bestimmung der geographischen Coordinaten, für welche die gestellten Bedingungen eintreten, auf die folgenden drei Winkelgrössen H, ψ und W. Um das betreffende Formelsystem nicht mehrmals ansetzen zu müssen, führe ich dasselbe bier an, webei die Kenntniss der drei Grössen H, ψ und W vorausgesetzt wird. Mit diesen Grössen lässt sich die geographische Breite φ und die östliche Länge λ vom Greenwicher Meridian, wie folgt, berechnen:

$$\operatorname{tg} H' = \frac{\operatorname{tg} H}{\operatorname{cos} (N' - W)}.$$

Die Wahl des Quadranten von $\operatorname{tg} H'$ kann nach Gutdünken vorgenommen werden.

$$\operatorname{tg} t = \frac{\cos H' \operatorname{tg} (N' - W)}{\sin (H' - D)}.$$

$$\sin t \operatorname{mit} \sin (N' - W) \operatorname{gleich} \operatorname{bezeichnet}.$$

$$\operatorname{tg} \varphi_1 = \operatorname{cotg} (H' - D) \operatorname{cos} t$$

$$\varphi = \varphi_1 + (\varphi - \varphi_1).$$

$$(\varphi - \varphi_1) \operatorname{mit} \operatorname{dem} \operatorname{Argumente} \varphi_1 \operatorname{aus} \operatorname{der} \operatorname{folgenden} \operatorname{Hilfstafel} \operatorname{I}.$$

$$\tau = \mu + \frac{15}{n} e' \operatorname{cos} (W - \nu) + \frac{15}{n} u' \operatorname{cos} \psi$$

$$\lambda = t - \tau.$$

Alle Winkel erscheinen in Einheiten des Grades; τ ist der Stundenwinkel der Sonne für den Hauptmeridian bei Eintritt der betreffenden Phase, t der entsprechende Stundenwinkel für den Ortsmeridian. Beide können nach Tafel V p. XXX in Zeit verwandelt werden; u' ist entsprechend den vorangehenden Annahmen zu wählen, also für die äusseren Berührungen u'_a , für die inneren u'_b .

		_							
Н	i	1	ťa	1	Ω	f	O.	T	

<u>-</u> φ ₁	$\perp (\varphi - \varphi_1)$	土91	$\perp (\varphi - \varphi_1)$		<u>-</u> (9 — 91)	±φ1	± (φ — φ₁)	±φ1	$-1-(\varphi-\varphi_1^r)$	<u></u> φ ₁	上(941)	<u>:L:</u> φ ₁	⊥ (φ — φ₁
0° 1 2 3 4 5 6 7 8 9 10 11 12	0°000 003 007 010 013 017 020 023 026 030 033	13° 14 15 16 17 18 19 20 21 22 23	0°042 045 048 051 054 056 059 062 064 067 069	26° 27 28 29 30 31 32 33 34 35 36 37 38	0°076 078 080 081 083 085 086 088 089 090 091	39° 40 41 42 43 44 45 46 47 48 49 50	0°094 094 095 096 096 096 096 096 095 095	52 53 55 55 55 57 58 59 60 60 60 60 60	0°093 092 091 090 089 088 086 085 083 081 079	65 66 67 68 69 77 73 74 75 76 77	0°073 071 069 067 064 062 059 056 054 051 048	78° 79 80 81 82 83 84 85 86 89 90	0°039 036 033 030 026 023 020 017 013 010

β) Bestimmung des ersten und letzten Berührungspunktes des Halbschattens.

Die Aufsuchung der Punkte auf der Erdoberstäche, für welche der Eintritt der Finsterniss überhaupt zuerst und zuletzt wahrgenommen wird, bedarf einer indirecten Lösung, doch lässt sich dem Verfahren eine Form geben, dass an eine Wiederholung der Rechnung bei den hier gesteckten Genauigkeitsgrenzen nicht geschritten zu werden braucht.

Daraus finden sich zwei Werthe für $(W_1 + \nu)$; für jeden dieser Werthe ist die folgende Rechnung durchzuführen:

Der Quadrant von ψ_1 bestimmt sich daraus, dass ψ_1 nahe 360° — $(W_1 + \nu)$ sein muss. Das Zeichen von cos ψ wird, so lange dieser Werth nicht sehr klein ist, die Entscheidung bringen, ob man es mit dem Anfange oder Ende der Finsterniss zu thun hat:

Wird aber $\cos \psi$ sehr klein, so kann diese Regel unrichtig werden; entscheidend ist das Zeichen des Ausdruckes:

$$y = nk \cos \psi + \sin (\psi + W) \sin D$$

$$\log k = 0.5820,$$
für den Anfang ist y negativ
für das Ende ist y positiv.

Setzt man nun:

$$\rho = W_1 + \nu - (360^{\circ} - \psi_1), \dots$$

so wird ρ stets ein sehr kleiner Winkel sein, und man hat:

$$W + v = W_1 + v + \frac{u'_a}{1 + u'_a} \rho$$

$$\psi = \psi_1 - \frac{u'_a}{1 + u'_a} ,$$

in welcher Formel man ohne wesentliche Ungenauigkeit den Factor von ρ gleich $\frac{1}{3}$ setzen darf. Mit diesen Werthen von W und ψ findet sich:

in welchem Ausdrucke $\cos(\psi + W)$ meist der Einheit gleich gesetzt werden darf. H wird stets ein kleiner negativer Bogen sein. Die Benützung des Formelsystemes B) (p. XIII) führt dann zur Kenntniss der Orte, an denen die erste und letzte Berührung des Schattenkegels stattfindet. Der Unterschied der beiden Werthe von τ , die zum Anfange und Ende gehören, gibt in Graden die Zeitdauer der Finsterniss in wahrer Zeit.

Wollte man jene Punkte finden, an welchen die Finsterniss zuerst aufängt und zuerst aufhört vollständig gesehen zu werden, welche Punkte der inneren Bertihrung des Halbschattenkegels entsprechen, so hätte man zu setzen:

und ähnlich wie in den vorstehenden Formeln vorzugehen. ψ_i wird der Gleichung 2) entsprechend bestimmt, nur ist die Wahl von ψ_i so vorzunehmen, dass sieh ψ_i und $W_1 + \nu$ nahe zu 180° ergänzen. Dann setzt man:

Die Berechnung dieser ziemlich unwichtigen Punkte kann wohl meist gespart bleiben. In allen jenen Fällen, wo der Schattenkegel über die Erde wegstreicht, wird dieses Punktepaar imaginär.

γ) Bestimmung der Punkte, in welchen die nördliche und südliche Grenzeurve der partiellen Finsterniss von der westlichen und östlichen berührt wird.

Die Aufsuchung dieser vier Punkte bedarf auch einer indirecten Lösung, doch wird meist keine wiederholte Rechnung nöthig sein. Die Lösung kann für ein Punktepaar imaginär werden, was man leicht erkennt, wenn sin $(W+\nu)>1$ wird. Dieser Umstand findet darin seine Erklärung, dass der Halbschatten den Erdkörper nicht völlig trifft, sondern mit einem Theile nördlich oder stidlich von der Erde verbeistreift.

Bertthrungspunkte mit der

nördlichen Grenzeurve: stidlichen Grenzeurve: $\sin\left(W_1 + \nu\right) = \frac{\gamma + i t_a'}{e}.$ $\sin\left(W_1 + \nu\right) = \frac{\gamma - i t_a'}{e}.$

Für beide Werthe der Winkel, welche dem Sinus entsprechen, ist folgende Rechnung durchzuführen:

$$\log k = 0.5820$$

$$\begin{split} \operatorname{tg} \psi &= \frac{nk + \sin D \sin W_1}{\sin D \cos W_1} \\ &= \sin D \cos W_1 \\ &= \sin$$

Stimmt W_2 mit W_4 nicht hinreichend überein, so muss die Rechnung wiederholt werden, da aber die gemachte Näherungsannahme sin $\psi = \pm 1$ der Wahrheit stets sehr nahe kommt, so wird eine solche Wiederholung selten nöthig sein.

$$\sin H = f_a \sin W - r$$
 $\log r = 7.9822;$
 $\sin H = -f_a \sin W - r$
 $r = -1.0.009599.$

Mit den Werthen von H, W und ψ werden die geographischen Coordinaten nach den Formeln B) (p. XIII) gefunden.

δ) Bestimmung der westlichen und östlichen Grenzeurve der partiellen Finsterniss.

Entweder:
$$\sin (W+\nu) = \frac{\gamma}{e} + \frac{u'_a}{e} \sin \psi$$
oder:
$$\sin \psi = \frac{e}{u'_a} \sin (W+\nu) - \frac{\gamma}{u'_a}.$$

Die erste der beiden Formeln wird man benützen, wenn seinem absoluten Werthe nach sin $\psi > \sin(W+\nu)$, die zweite, wenn $\sin \psi < \sin(W+\nu)$ ist. Der Grenzwerth von $\sin(W+\nu)$, bei welchem ein Wechsel der Formeln zweckmässig vorgenommen wird, findet sich durch die Relation:

$$\sin(W+\nu) = \frac{\gamma}{e + u'_{\alpha}}$$

Das obere Zeichen gilt, wenn man sich sin $(W+\nu)$ mit sin ψ gleich bezeichnet vorstellt, das untere, wenn sie ungleich bezeichnet sind. Im ersteren Falle wird unter Umständen der Werth für die Grenze imaginär, es wird dann nur ein Grenzwerth in Betracht kommen; sind beide Werthe reell, so werden zwei in Erwägung zu ziehen sein. Substituirt man in die erste der obigen Formeln einen beliebigen Werth von ψ oder in die zweite einen beliebigen Werth von $(W+\nu)$, so erhält man für den correspondirenden Bogen $(W+\nu)$ oder beziehungsweise ψ ; da die Bestimmung durch einen Sinus erfolgt, zwei Annahmen; mit beiden ist die Rechnung weiter zu führen. Unter Umständen (der Halbschatten projieirt sich nicht ganz auf den Erdkörper) wird man für die Sinus grössere Werthe als die Einheit finden, also auf imaginäre Lösungen geführt; jene Bögen, welche diese Lösungen bedingen, sind auszuschliessen. Im Falle, dass ψ und $(W+\nu)$ die ganze Peripherie durchlaufen können, ohne Imaginäres in den Formeln 1) zu bedingen, bildet sowohl die westliche als auch die östliche Grenzeurve eine geschlossene, ovalförmige Linie. Sind aber imaginäre Lösungen vorhanden, so vereinigen sich die östliche und westliche Grenze zu einem achterförmigen Curvenzuge.

Im Allgemeinen wird ein negativer Werth von $\cos \psi$ dem Anfang der Finsterniss, ein positiver dem Ende entsprechen; ist aber $\cos \psi$ klein, so ist die Entscheidung bedingt durch das Zeichen von y in:

$$y = uk \cos \psi + \sin (\psi + W) \sin D$$

log $k = 0.5820$;

negative y entsprechen dem Anfang, positive dem Ende der Finsterniss. Rechnet man den Curvenzug, so wird die regelmässig fortschreitende Rochnung auch ohne dieses Kriterium leicht die Entscheidung bringen, umsomehr, da die Berührungspunkte der westlichen und östlichen mit der stidlichen und nördlichen Grenzeurve bekannt sind. Die westliche Grenzeurve verbindet die Orte, die den Beginn und das Ende der Finsterniss bei Sonnenaufgang, die östliche jene, welche diese Phasen bei Sonnenuntergang sehen.

Die Ermittlung der geographischen Coordinaten geschieht nach B) (p. XIII).

s) Die Curve der grössten Phase im Horizont.

u' und f erhalten verschiedene Werthe je nach der Grösse der Finsterniss, die in Zollen i angegeben werden soll. Setzt man:

$$\frac{1}{6} \left(u'_a - 0 \cdot 27365 \right) = \Delta u$$

$$\overline{9 \cdot 2208} f_a = \Delta f,$$

so sind die Werthe, die zu einer Phase von i Zoll gehören:

Hiebei witre zu bemerken, dass bei strenger Befolgung der vorstehenden Formeln bei ringförmigen Sonnenfinsternissen die Curve von 12 Zoll nördlich thatsächlich stidlicher verläuft als die Curve von 12 Zoll stidlich, und dass eben diese Curven mit einem Theile (bis zu 10·7 Zoll) den Nachbareurven gewissermassen übereinander gelagert erscheinen. Projicirt sich der Schattenkegel nicht ganz auf die Erde, so werden für gewisse Werthe von u' die späteren Ausdrücke imaginär; dieselben sind auszuschliessen. Die folgende Rechnung ist eine indirecte, doch sind die Näherungsannahmen so genau, dass eine Wiederholung der Rechnung kaum nöthig wird.

Nördliche Curve. Sudliche Curve.
$$\sin (W_1 + \nu) = \frac{\gamma + u'}{e}.$$

$$\sin (W_1 + \nu) = \frac{\gamma - u'}{e}.$$

Für beide Bögen, die zu dem Sinus gehören, ist die folgen le Rechnung auszuführen; der eine Bogen gehört zur grössten Phase im Herizent bei Sennenuntergang, der andere zu der bei Sennenaufgang.

$$E = \sin D - f \cos D \sin N'$$

$$E = \sin D + f \cos D \sin N'$$

$$F = E + r \cos D \cos (N' - W_1)$$

$$\log r = 7.9822$$

$$\log k = 0.5820;$$

$$tg \psi = \frac{nk + e'F \sin (W_1 - \nu)}{eF \cos (W_1 + \nu)}$$

$$\sin \psi \text{ stets positiv}$$

$$\sin \psi \text{ stets negativ}$$

$$\sin (W_2 + \nu) = \frac{\gamma}{e} + \frac{v'}{e} \sin \psi.$$

$$E = \sin D + f \cos D \sin N'$$

$$F' = E + r \cos D \cos (N' - W_1)$$

$$\log r = 7.9822$$

$$eF \cos (W_1 - \nu)$$

$$\sin \psi \text{ stets negativ}$$

$$\sin \psi \text{ stets negativ}$$

$$\sin (W_2 + \nu) = \frac{\gamma}{e} + \frac{v'}{e} \sin \psi.$$

 W_2 wird mit W_1 meist schon eine gentigende Übereinstimmung zeigen; wäre dies nicht der Fall, so müsste die Rechnung mit dem Werthe $(W_2 + \nu)$ wiederholt werden.

$$\sin H = f \sin W - r \qquad | \sin H = -f \sin W - r
\log r = 7.9822; \quad r = +0.009599.$$

Mit den Werthen H, W und ψ werden die geographischen Goordinaten nach den Formeln B) p. XIII gefunden.

Die Curve der grössten Phase erfährt zwischen den nördlichen und sudlichen zu i=12 gehörenden Punkten eine Unterbrechung; natürlich gilt diese Bemerkung nur von centralen Finsternissen. Die Punkte für die Phase von 0 Zoll brauchen nicht berechnet zu werden, sie fallen mit den in γ) (p. XV) berechneten Punkten zusammen.

Streicht der Schattenkegel theilweise an der Erde vorbei, so wird sich eine der obigen Grenzeurven zu einem Punkte zusammenziehen, den ich mit dem Namen Grenzpunkt bezeichnen will; dieser Punkt ist für die bildliche Darstellung des Curvenganges der grössten Phase im Horizont von Wichtigkeit.

Man findet denselben leicht aus den folgenden Gleichungen, wobei natürlich in einem gegebenen Falle nur ein System in Anwendung kommt, und zwar:

wenn
$$\gamma$$
 positiv: wenn γ negativ:

 $W+\nu = 90^{\circ}$ $\psi = 270^{\circ}$
 $\psi = 90^{\circ}$ $\psi = 270^{\circ}$
 $u' = e - \gamma$ $u' = e + \gamma$
 $i = 6 \frac{u'_a - u'}{u'_a - 0 \cdot 27365}$ $i = 6 \frac{u'_a - u'}{u'_a - 0 \cdot 27365}$
 $f = f_a - i\Delta f$
 $tg H = f - r$
 $log r = 7 \cdot 9822$; $r = +0 \cdot 009599$.

Mit den Werthen H, W und ψ werden die geographischen Coordinaten nach B) (p. XIII) gefunden. Will man jene Orte kennen, für welche die völlige Contralität zur Zeit des Sonnenaufganges oder Sonnenunterganges stattfindet, so hat man:

$$\sin (W+\nu) = \frac{\gamma}{e}$$

$$\tan H = -r$$

$$\log r = 7.9822$$

$$\cos \psi = 0,$$

und rechnet mit den Werthen von H, W, ψ die geographischen Coordinaten nach B) (p. XIII). Die Ermittlung dieser Punkte mit Vernachlässigung der Abplattung und Refraction erweist sich zur Beurtheilung der Umstände einer Finsterniss hinlänglich genau. Die diesbezüglichen Formeln sind sehon p. XI mitgetheilt worden.

ζ) Ermittlung der nördlichen und südlichen Curve einer gegebenen Grösse.

Die Rechnung ist zwar indirect, aber es lassen sich Formeln außtellen, welche so hinreichende Annähe rungen ergeben, dass man die Rechnung als direct bezeichnen kann. In diesem Abschnitte treten zunächs Formeln auf, die sich wesentlich von den Hansen'schen unterscheiden, hauptsächlich dadurch, dass anstat des als unabhängige Variable gewählten Stundenwinkels der Sonne der Winkel E eintritt, der wesentlich Vortheile, besonders für jene Curven, die nahe dem Pole verlaufen, darzubieten scheint. Die Rechnung wird durch diese neuen Formeln zwar etwas umständlicher, gewinnt aber an Sicherheit und Übersichtlichkeit ferner finden keine Ausnahmsfälle statt. Da aber Hansen's Formeln in der überwiegenden Anzahl der Fäll sieher angewendet werden können, und denselben der Vortheil einer kürzeren Rechnung zukommt, so hab ich weiter unten auch diese ausführlich aufgenommen. Es ist hier nicht der Ort, auf die Ableitung de früher erwähnten Formelsystemes einzugehen, welches sich übrigens in meiner Abhandlung: "Über de Venusdurchgang des Jahres 1874" (Sitzber. 28. April 1870), den dortigen Verhältnissen angepasst, angegebe und abgeleitet findet.

Die Grössen f und u' werden nach s) 1) und 2) (p. XVI und XVII) ermittelt; man erhält zunächst di erforderlichen Hilfsgrössen durch die folgenden Formeln, bei deuen die oberen Zeichen für die nördlichen die unteren für die südlichen Grenzeurven gelten:

$$\sin g' \sin G' = \sin g \sin G \mp f \cos \delta', \qquad \beta = \frac{15}{n} (1-c) \cos k$$

$$\sin g' \cos G' = \sin g \cos G, \qquad \alpha_1 = (1-c)f \sin \delta'$$

$$\cos g' = \cos g \pm f \sin \delta', \qquad \log (1-c) = 9 \cdot 9985$$

$$\operatorname{tg} \rho = -\frac{\operatorname{tg} g'}{(1-c)};$$
Iranten zu nehmen.

 ρ stets im vierten Quadranten zu nehmen.

$$\sin W' = \gamma \pm u';$$

cos W', aus sin W' bestimmt, wird stets positiv genommen.

$$\sin C' = \zeta \cos g', \qquad \log \zeta = 8.9122 - 10;$$

 $\cos C'$, aus $\sin C'$ bestimmt, wird stets positiv genommen.

Hierauf bestimmt man für alle Curven gemeinsam:

$$\operatorname{tg} \Phi = \frac{\cos k}{\sin \delta'}, \sin \Phi \text{ gleichbezeichnet mit } \cos k;$$

$$\sin \omega = \frac{\sin \delta'}{\sin k}, \operatorname{daraus } \cos \omega, \operatorname{dem } \operatorname{man } \operatorname{stets } \operatorname{das } \operatorname{positive Vorzeichen } \operatorname{ertheilt.}$$

Nun nimmt man eine Anzahl von in passenden Intervallen (etwa 30°) gewählten Werthen eines willkürlichen Winkels F vor, welche den Bedingungen, dass

genügen. Für die Grenzwerthe von E wird die Finsterniss sehr nahe im Horizonte stattfinden, für den Mittelwerth bei der gegebeuen Grösse in nahezu maximaler Höhe. Für jeden der so gewählten Werthe von Fberechnet man:

$$v \sin V = \cos \omega \cos (\Phi - F) v \cos V = \sin y \cos (K - G).$$

Es beginnen nun jene Rechnungen, welche für jede einzelne Curve durchzuführen sind. Setzt man zunächst:

$$\sin C' = \xi \cos g', \qquad \log \xi = 8.9122 - 10$$

$$\cdot e = \cos C', \\
\cos \rho = \frac{1 - e}{e} \cos g', \quad \log (1 - e) = 9.9985 - 10$$

$$\sin \rho = -\frac{1}{e} \sin g' \\
tg \psi = \frac{nk + v \sin k \sin (W' - V)}{\sin g \sin k' \cos W'}$$

$$\log k = 0.5820,$$

und bestimmt für jeden Punkt in jeder Curve φ_t und t nach den folgenden Formeln:

The Curve
$$\varphi_1$$
 and t nach den folgenden Forment:

$$b \sin B = \cos W \cos E'$$

$$b \cos B = \sin W$$

$$\sin \varphi_1 = b \cos (\rho - B)$$

$$\cos \varphi_1 \sin (G' + t) = b \sin (\rho - B)$$

$$\cos \varphi_1 \cos (G' + t) = \cos W \sin E',$$

we deutiger Weise erhaltenen Werthen von t und φ_1 weiter:

so rechnet man mit den derart in unzweideutiger Weise erhaltenen Werthen von t und φ_i weiter:

$$\beta_{1} = f \cos \delta' \cos t$$

$$u = u' - \alpha_{1} \sin \varphi_{1} - \beta_{1} \cos \varphi_{1}$$

$$\tau = \mu + \beta \sin \varphi_{1} - \frac{15}{n} \sin k \cos (K+t) \cos \varphi_{1} + \frac{15}{n} u \cos \psi$$

$$\lambda = t - \tau$$

$$\varphi = \varphi_{1} + (\varphi - \varphi_{1})$$

 $(\varphi - \varphi_1)$ mit dem Argumente φ_1 aus der Hilfstafel I., p. XIV.

Will man Hansen's Formeln bentitzen, die im allgemeinen bequemer sind, besonders, wenn man nur eine Curve berechnen will, so hat man in der folgenden Weise vorzugehen.

Die Rechnung ist indirect; die Grössen f und u' werden nach ϵ) 1) und 2) (p. XVI und XVII) ermittelt. Man erhält für jeden Werth von i zunächst die folgenden Hilfsgrössen, wobei die oberen Zeichen für die nördlichen, die unteren für die südlichen Grenzeurven gelten:

$$\sin g' \sin G' = \sin g \sin G \mp f \cos \delta', \qquad \alpha = (1-c)\cos g'$$

$$\sin g' \cos G' = \sin g \cos G, \qquad \beta = \frac{15}{n}(1-c)\cos k$$

$$\cos g' = \cos g \pm f \sin \delta', \qquad \alpha_1 = (1-c)f \sin \delta'$$

$$\log (1-c) = 9 \cdot 9985.$$

Die bei den weiter unten folgenden Formeln erforderlichen Hilfsgrössen k und K sind allen Curven gemeinsam und bereits bei der Rechnung der Elemente bestimmt.

Die Rechnung dieser Curven wird sich verschieden gestalten; man wird zwei Fälle zu unterscheiden haben, je nachdem $\gamma \pm u'$ seinem absoluten Werthe nach kleiner oder grösser ist als α . In dieser Gleichung ist für u' das obere Zeichen zu nehmen, wenn man die nördliche, das untere, wenn man die südliche Curve berechnen will. Bei den unten folgenden Rechnungen wird der Zeichenunterschied durch die Formeln selbst (Multiplication mit $\sin \psi$) eingeführt. Der zweite Fall hat für Finsternisse, deren nördliche und südliche Grenzcurven gleichzeitig reell sind, keine Bedeutung.

Erster Fall:
$$(\gamma \pm u')$$
 absolut $< \alpha$.

Für jede Curve der angegebenen Verfinsterungsgrösse rechnet man für eine passende Anzahl von Stundenwinkeln die unten angesetzten Formelsysteme durch. Hiebei sind die Stundenwinkel des westlichen Zweiges der Curve der grössten Phase (grösste Phase bei Sommenaufgang) als untere Grenze zu betrachten, von der man durch 360° aufsteigend zur oberen Grenze, welche die Stundenwinkel der grössten Phase bei Sounenuntergang für die gegebene Verfinsterungsgrösse darstellt, gelaugt; innerhalb dieser Grenzen kann der Stundenwinkel jeden beliebigen Werth annehmen.

bigen Werth annehmen.

$$\eta = \sin g' \sin (G' + t), \qquad \Theta = \sin k \sin (K + t)$$
 $\eta_1 = \sin g' \cos (G' + t), \qquad \Theta_1 = \frac{15}{n} \sin k \cos (K + t).$

sind bei allen Curven für dieselben Stundenwinkel

Die Grössen Θ und Θ_4 sind bei allen Curven für dieselben Stundenwinkel identisch.

$$a \sin A = \eta$$
$$a \cos A = \alpha;$$

a wird stets positiv angenommen.

Nun beginnt die indirecte Rechnung.1

$$\sin (\varphi_1' - A) = \frac{\gamma \pm u'}{a}$$

Das obere Zeichen für die nördlichen Curven, das untere Zeichen für die südlichen Curven.

$$tg \psi = \frac{nk - \Theta \cos \varphi_1'}{\eta_1 \cos \varphi_1'}$$

$$\log k = 0.5820$$

 $\sin \psi$ wird für nördliche Curven positiv, $\sin \psi$ wird für stidliche Curven negativ.

¹ Der Bogen (φ'₁-A) ist so zu bestimmen, dass dem Zeichen des Sinus entsprochen wird. Es ergeben sich aber hierbei zwei Bögen. Wenn von diesen nur einer brauchbar ist, so ist es derjenige, für welchen cos $(\varphi_1'-A)$ mit sin (K+t) gleich bezeichnet ist. Es können aber unter Umstünden beide Bögen brauchbaren Punkten angehören. Entscheidend ist die Regel, dass nur ein solcher Werth von φ_1 brauchbar sein kann, für welchen der Ausdruck cos δ' cos φ_1 cos $t+\sin\delta'$ $(1-c)\sin\varphi_1$

Mit dem Werthe von ψ rechnet man:

wodurch meist ein ausreichend genauer Werth von φ_1 gefunden ist. Sollte man eine weitere Verbesserung für wünschenswerth halten, so wird die Rechnung nach den Formeln 3) mit Ausschluss der ersten Formel einen verbesserten Werth von ψ abgeben, der in 4) eine neue Annäherung gibt; dieses Verfahren ist fortzusetzen, bis die genütgende Übereinstimmung zwischen dem Anfang- und Endwerthe hergestellt ist, doch wird, wie sehon gesagt, eine derartige Wiederholung meist nicht nöthig; auch kann, wenn man eine Reihe von Curvenpunkten rechnet, durch die Differenzwerthe ein sehr nahe richtiger Schluss auf den folgenden Werth von ψ gemacht werden.

$$\beta_{1} = f \cos \delta' \cos t$$

$$u = u' - \alpha_{1} \sin \varphi_{1} - \beta_{1} \cos \varphi_{1}$$

$$\tau = \mu + \beta \sin \varphi_{1} - \Theta_{1} \cos \varphi_{1} + \frac{15}{n} u \cos \psi$$

$$\lambda = t - \tau$$

$$\varphi = \varphi_{1} + (\varphi - \varphi_{1})$$

$$(\varphi - \varphi_{1}) \text{ mit dem Argument } \varphi_{1} \text{ aus der Hilfstafel I, p. XIV.}$$

$$Z \text{ weiter Fall: } (\gamma \pm u') \text{ absolut } > \alpha.$$

In diesem Falle geben die für die grösste Plase im Horizont geltenden Stundenwinkel keine sieheren Grenzwerthe, indem für die Zone der Sichtbarkeit sowohl grössere als auch kleinere Stundenwinkel gelten, als dies durch diese Grenzen angedeutet wird. Für die Stundenwinkel, die zwisehen den Grenzen liegen, welche die grösste Phase im Horizont gibt, wird man das für den ersten Fall gegebene Verfahren anwenden, nun aber die Stundenwinkel so wählen, dass man von der unteren Grenze (Stundenwinkel der grössten Phase bei Sonnenaufgang) absteigend zur oberen Grenze (Stundenwinkel der grössten Phase bei Sonnenuntergang) gelangt. Die Rechnung der Punkte der grössten Phase im Horizont und die oben durchgeführte Rechnung wird für die betreffenden Punkte auf der Erdoberfläche gewisse geographische Breiten finden lassen. Um den fehlenden Verlauf der Curve zu berechnen, wird man für die Zwischenwerthe der diese Liteken umgrenzenden geographischen Breiten passende Annahmen machen und nach folgenden Formeln rechnen:

wobei man wieder für die nördliche Grenzeurve in der ersten Annäherung sin $\psi = +1$, für die stidliche sin $\psi = -1$ setzt.

Man erhält zwei Werthe für den Stundenwinkel, beide sind in Rechnung zu ziehen, falls nicht einer derselben sehon in das durch die früheren Rechnungen ermittelte Gebiet der Stundenwinkel fällt.

$$\Theta = \sin k \sin (K+t)$$

$$\eta_1 = \sin g' \cos (G'+t)$$

$$\tan \psi = \frac{nk - \Theta \cos \varphi_1}{\eta_1 \cos \varphi_1}$$

$$\log k = 0.5820$$

$$\sin \psi \text{ positiv für die nördlichen Curven,}$$

$$\sin \psi \text{ negativ für die stidlichen Curven.}$$

positiv wird. Unter Umständen können aber für φ_1 Werthe zum Vorschein kommen, die grösser sind als $\pm 90^\circ$. Man hat dann diese Bögen in den folgenden Formeln beizubehalten und erst am Schlusse der Rechnung, um auf die gewöhnliche Zählung der geographischen Coordinaten überzugehen, die gefundene Länge um $\pm 180^\circ$ zu ändern und anstatt φ_1 die Ergänzung von φ_1 zu $\pm 180^\circ$ anzunehmen. Siehe hierüber auch "Beitrag zur Hansen'sehen Theorie der Sonnenfinsternisse" von Dr. Robert Schram (Sitzber. der kais. Akad. d. Wiss. in Wien, Bd. XCII, II. Abth. Decemberheft1885), wo sich auch Tafeln für die jedesmaligen Grenzen, innerhalb deren φ_1 zu nehmen ist, vorfinden.

Mit ψ berechnet man den Werth sin (G'+t) nochmals und erhält hiedurch meist eine ausreichende Näherung; man kann eventuell dieses Verfahren wiederholen. Aus φ_1 erhält man φ auf die bekannte Weise mittelst der Hilfstafel I, p. XIV.

$$u = u' - \alpha_1 \sin \varphi_1 - f \cos \theta' \cos t \cos \varphi_1$$

$$\tau = \mu + \beta \sin \varphi_1 - \frac{15}{n} \sin k \cos (K + t) \cos \varphi_1 + \frac{15}{n} u \cos \psi$$

$$\lambda = t - \tau.$$

n) Curve der Centralität.

Hat man die nördliche und südliche Grenzeurve für die Phase von 12 Zoll gereehnet, so bedarf man kaum noch der Bestimmung der Linie der Centralität, indem die zu demselben Stundenwinkel gehörenden Werthe von λ und φ in diesen beiden Grenzeurven zum Mittel vereinigt, die entsprechenden Punkte geben. Soll aber die Curve der Centralität direct gerechnet werden, so wird man zunächst die Hilfsgrössen:

$$\pi = \frac{\sin g}{(1-e)\cos g'}, \quad \sigma = \frac{15(1-e)}{n}\cos k, \quad \log 15(1-e) = 1\cdot 1746$$

$$\log 15 = 1\cdot 1761$$

$$\log \frac{1}{1-e} = 0\cdot 0015$$

bestimmen und hierauf für verschiedene passend gewählte Stundenwinkel t die folgenden Formeln 2) durchrechnen; bei der Wahl der Stundenwinkel wird man darauf Rücksicht zu nehmen haben, dass man die Rechnung nicht für Punkte führt, für die sieh die Centralität unter dem Horizonte zeigen würde, wobei die drei Hauptpunkte der Centralität als gute Leitung dienen werden.

$$tg A = \pi \sin (G + t); \quad \cos A \text{ stets positiv.}$$

$$\sin (\varphi_1 - A) = \rho \cos A$$

$$\varphi = \varphi_1 + (\varphi - \varphi_1)$$

$$(\varphi - \varphi_1) \text{ aus Hilfstafel I, p. XIV.}$$

$$\tau = \mu - \sigma \sin \varphi_1 - \omega \cos (K + t) \cos \varphi_1$$

$$\lambda = t - \tau.$$

Ist $\pm \gamma > \alpha$, so wird man ühnlich wie im Capitel ζ) für gewisse Theile der Curve nicht t, sondern φ_1 als Argument wählen und rechnen:

$$\sin (\alpha' + t) = \frac{\alpha}{\sin g} \operatorname{tg} \varphi_1 - \frac{\gamma}{\sin g} \sec \varphi_t,$$
woraus zwei Werthe für t resultiren; τ berechnet man hierauf nach:
$$\tau = \mu - \sigma \sin \varphi_1 - \omega \cos (K + t) \cos \varphi_1$$

$$\lambda = t - \tau.$$

Es kann auch von Interesse sein, die Dauer der Totalität oder Ringförmigkeit 7 zu bestimmen; man erhält dieselbe mit hinreichender Näherung in Zeitminuten für einen bestimmten Stundenwinkel für die Centralität mit Benützung der bereits ermittelten Zahlen:

$$u = u'_{i} - (1 - c)f_{i} \sin \delta' \sin \varphi_{1} - f_{i} \cos \delta' \cos \varphi_{1} \cos t$$

$$\log (1 - c) = 9 \cdot 9985$$

$$\tau' = \frac{k'u}{nk - \cos \varphi_{1} \sin k \sin (K + t)}$$

$$\log k' = 2 \cdot 6612$$

$$\log k = 0 \cdot 5820.$$

¹ Über die Wahl des Bogens (φ_1 —A) vergl. Anmerkung p. XX und XXI.

Ist u positiv, so ist die Finsterniss total, ist u negativ, ringförmig; dementsprechend wird τ' , positiv gefunden, die Dauer der Totalität, negativ, jene der Ringförmigkeit angeben. Für Finsternisse, die theilweise ringförmig sind, hat die Kenntniss des Punktes Interesse, wo die Ringförmigkeit in die Totalität übergeht; nam wird leicht jenen Werth durch Rechnung einiger passend gewählter Standenwinkel finden, für die u=o wird.

i) Grenzeurven der Totalität und Ringförmigkeit.

Wenn auch die Berechnung der Grenzeurven der Totalität und Ringförmigkeit aus den Formeln für die Bestimmung der nördlichen und stidlichen Curve von 12 Zoll (vergl. Capitel ζ) (p. XVIII ff.) resultirt, so dürfte es doch passend sein, für diesen Specialfall directe Formeln zusammenzutragen und dabei zulässige Abkürzungen einzuführen. Man setzt:

$$\rho' = -f_i \cos \delta',$$
 $\omega = \frac{15}{n} \sin k$
 $\sigma = -\frac{15}{n} (1 - c) \cos k,$ $\log 15 (1 - c) = 1 \cdot 1746.$

Für die folgende Rechnung hat man zwei Fälle, welche Trennung nachstehend durchgeführt ist, um die Grenzeurven entsprechend ihrer Bezeichnung finden zu lassen [vergl. Bemerkung im Capitel ζ) p. XXI].

Nürdliche Grenze der Totalität, stidliche Grenze der Ringfürmigkeit. $\pi' = (1-c)\{\cos a + f \cdot \sin \delta'\}$

$$\pi' = (1 - c)\{\cos g + f_i \sin \delta'\}$$

$$\log (1 - c) = 9 \cdot 9985$$

$$a \sin A = \sin g \sin (G + t) + \rho' \cos t$$

$$a \cos A = \pi'$$

$$a \text{ stets positiv}$$

$$\sin (\varphi_1 - A) = \frac{\gamma + u_i'}{a}$$

Stidliche Grenze der Totalität, nördliche Grenze der Ringförmigkeit.

$$\pi' = (1-c)\{\cos g - f_i \sin \delta'\}$$

$$\log (1-c) = 9 \cdot 9985$$

$$a \sin A = \sin g \sin (G+t) - \rho' \cos t$$

$$a \cos A = \pi'$$

$$a \text{ stots positiv}$$

$$\sin (\varphi_1 - A) = \frac{\gamma - u_i'}{a}$$

$$K+t) \cos \varphi_1$$

 $\tau = \mu - \sigma \sin \varphi_1 - \omega \cos (K + t) \cos \varphi_1$ $\lambda = t - \tau$ $\varphi = \varphi_1 + (\varphi - \varphi_1)$

 $(\varphi-\varphi_1)$ mit dem Argumente φ_1 aus der Hilfstafel I, p. XIV.

z) Bestimmung der westlichen und östlichen Grenzeurven der inneren Ränderberührung. Diese Curven bilden, sehr seltene Fälle ausgenommen, kleine ovalförmige Ringe. Man rechnet:

Curven bilden, sehr seltene Fälle ausgenommen, kleine ovalförmige kinge. Man reenner.

entweder:
$$\sin{(W+\nu)} = \frac{\gamma}{e} + \frac{u_i'}{e} \sin{\psi},$$
oder:
$$\sin{\psi} = \frac{c}{u_i'} \sin{(W+\nu)} - \frac{\gamma}{u_i'}.$$

Die erste Formel wird man benützen, wenn seinem absoluten Werthe nach $\sin \psi > \sin (W + \nu)$ wird, die zweite, wenn $\sin \psi < \sin (W + \nu)$; bei der Kleinheit von u_i' wird meist, wenn $\frac{\gamma}{e}$ nicht zufällig sehr nahe der Einheit kommt, die erste Formel allein zur Anwendung gelangen. ψ wird mit den seltensten Ausnahmen die ganze Peripherie durchlaufen können, $\sin (W + \nu)$ aber in Folge der Kleinheit von u_i' sehr beschränkt sein. Man wird für passend gewählte Intervalle die Werthe von $\sin (W + \nu)$ leicht berechnen; beide zu diesen Sinus gehörenden Bögen haben Giltigkeit und sind der weiteren Rechnung zu Grunde zu legen:

$$tg H = -f_i \cos (\psi + W) - r
log r = 7.9822, r = +0.009599.$$

Mit den Werthen von ψ, H, W, werden die geographischen Coordinaten nach den Formeln B) p. XIII ermittelt. Die Berührungspunkte der Curve der grössten Phase im Horizont trennen jene Abschnitte der Curve, welche den Anfang und das Ende der Finsterniss bezeichnen.

II. Bestimmung der Hauptumstände einer Sonnenfinsterniss für einen gegebenen Ort.

λ = östliche Länge des Ortes von Greenwich in Graden und Decimaltheilen des Grades (westliche Längen negativ gezählt).

 $\varphi = \text{geographische Breite}.$

Mittelst der Hilfstafel I_{\bullet} , p. XIV bildet man für den Ort die excentrische Polhöhe φ_{\bullet} (φ_{\bullet} ist dem absoluten Werthe nach stets kleiner als φ) und berechnet:

$$\xi = \cos \varphi_1, \qquad \eta = (1 - e) \sin \varphi_1, \qquad \log (1 - e) = 9.9985.$$

A) Zeit und Grösse der grössten Phase.

$$L = \lambda + \mu + \frac{15}{n} \eta \cos k$$

$$K' = K + L$$

$$a = -\frac{15}{n} \xi \sin k$$

$$\operatorname{tg} \tau' = \frac{a \cos K'}{l + a \sin K'}.$$

l ist mit dem Argumente τ aus der folgenden Tafel II zu entlehnen; die Rechnung ist daher eine indirecte. Man setzt beim ersten Versuche log t=1.7581, erhält hieraus einen genäherten Werth von τ' , der zur Entnahme eines genaueren Werthes von 1 beutitzt wird. Die Rechnung ist zu wiederholen, bis keine Änderung in den Zahlen auftritt; es wird selten nöthig sein, über die zweite Näherung hinauszugehen.

Hilfstafel II.

τ'	$\log t$	τ'	log t	r'	log l
0° 1 2 3 4 5 6 7 8 9	1.7581 o 1.7581 +1 1.7582 +1 1.7583 +2 1.7585 +2 1.7587 +2 1.7589 +3 1.7592 +3 1.7595 +4 1.7593 +4 1.7603	10° 11 12 13 14 15 16 17 18 19 20	1.7603 x.7608 x.7608 +5 x.7619 +6 x.7625 x.7635 x.7638 x.7645 x.7653 x.7653 x.7653 x.7653 x.7665	20° 21 22 23 24 25 26 27 28 29 30	1'7670 1'7679+9 1'7688+10 1'7698+10 1'7709+11 1'7720+11 1'7743+12 1'7743+13 1'7768+13

Ist der wahre Werth von τ' ermittelt, so findet man weiter:

$$t_0 = \tau' + L$$

$$\log z = 9 \cdot 4180$$

$$m' \sin M' = -z \xi \sin g \cos (G + t_0)$$

$$m' \cos M' = n - z \xi \sin k \sin (K + t_0)$$

$$t = t_0 + \frac{15}{m'} \sin M' \{ \gamma - \gamma \cos g + \xi \sin g \sin (G + t_0) \}$$

$$\tau = t - \lambda.$$

Der Werth t ist für den vorgelegten Ort der Stundenwinkel der Sonne für die Zeit der grössten Phase, τ der Stundenwinkel der Sonne unter dem Meridian von Greenwich für diesen Zeitpunkt; beide können in Zeit verwandelt werden nach Tafel V, pag. XXX.

Die grösste Phase ist für den gegebenen Ort sichtbar (über dem Horizont), sobald der Ausdruck $\sin \delta' \sin \varphi + \cos \delta' \cos \varphi \cos t$ innerhalb der Grenzen — 0·01 und + 1·00 liegt.

$$\pm m \!=\! \frac{\gamma \!-\! \gamma\cos g \!+\! \xi\sin g\sin \left(G \!+\! t\right)}{\cos M'}.$$

Das obere Vorzeichen gilt, wenn der Ausdruck rechts vom Gleichheitszeichen positiv ist, in welchem Falle der nördliche Theil der Sonnenscheibe verfinstert wird, das untere, wenn er negativ ist, in welchem Falle der südliche Theil der Sonnenscheibe verfinstert wird; mist also stets positiv zu nehmen. Die Grösse der Phase selbst findet sich daraus:

Grösste Phase in Zollen =
$$6 \frac{u'_a - m}{u'_a - 0 \cdot 27365}$$
.

Ist $m > u'_a$, so findet keine Finsterniss für den gegebenen Ort statt. Die Bestimmung der Grösse der grössten Phase kann aber auch leicht mit der folgenden Tafel III mit binreichender Annäherung vorgenommen werden; das verticale Argument dieser Tafel ist m, das horizontale u'_a .

Die vorstehenden Formeln sind für die Rechnung wesentlich bequemer als die entsprechenden Hansen'schen, bei denen oft eine drei- bis viermalige Durchrechnung erforderlich ist, um den richtigen Werth von t zu finden. Es wird sich daher stets empfehlen, die vorstehend mitgetheilten Formeln zu benützen, bei denen die eingeführten Abkürzungen nirgends die zulässigen Greuzen überschreiten. Nichtsdestoweniger sollen nachfolgend auch die strengen Hansen'schen Formeln angeführt werden.

 t_0 sei ein Näherungswerth des Stundenwinkels der Sonne zur Zeit der grössten Phase, ausgedritekt in Graden und Decimaltheilen des Grades. Ist aber kein Näherungswerth bekannt, so setze man in erster Näherung: $t_0 = \lambda + \mu$ (hierbei wird das erste Glied in m cos M der Null gleich)

$$m \sin M = \gamma \qquad -\eta \cos y + \xi \sin y \sin (G+t)$$

$$m \cos M = (t_0 - \lambda - \mu) \frac{n}{15} - \eta \cos k + \xi \sin k \sin (K+t)$$

$$m' \sin M' = -\varkappa \xi \sin y \cos (G+t_0)$$

$$m' \cos M' = n - \varkappa \xi \sin k \sin (K+t_0)$$

$$t_1 = t_0 - 15 \frac{m}{m'} \cos (M+M')$$

$$\log \varkappa = 9 \cdot 4180$$

$$\log 15 = 1 \cdot 1761$$

$$\tau = t - \lambda$$

m und m' stets positiv zu wählen und der Bogen $t_0 - \lambda + \mu$ immer kleiner als $\pm 50^{\circ}$.

 t_0 ist der verbesserte Werth des angenommenen Stundenwinkels, der als Grundlage für eine weitere Annäherung dient, indem man den so gefundenen Werth von t_1 statt t_0 in die obigen Formeln einführt. Die Rechnung ist so lange zu wiederholen, bis der Anfangswerth t_0 mit dem Endwerthe t_1 gentigend übereinstimmt. Der Werth von m in der letzten Näherung dient nach der oben gegebenen Formel oder nach der folgenden Tafel III zur Bestimmung der Grösse der grössten Phase in Zollen.

Ist (M+M') im letzten Versuche nahe an 90°, so wird der nördliche Theil der Sonnenscheibe verfinstert sein.

Ist (M + M') im letzten Versuche nahe an 270°, so wird der stidliche Theil der Sonnenscheibe verfinstert sein.

Im ersten Falle liegt der vorgelegte Ort auf einer südlichen, im zweiten auf einer nördlichen Grenzeurve.

Denkschriften der mathem.-naturw. Cl. Lil. Bd.

Tafel III.

$a \stackrel{f_a}{\sim} a$	o:528	0.230	0.232	0.234	0.236	0'538	0'540	0.242	0'544	o · 546	0.548	0.320	0.22
	Photos - Comment States - 1 St.	Consequent Lawry consolidates as with					7010	12.1	12.1	12'0	12.0	x x · 0	11.
0.00	12.2	12'4	12'4	12.3	12.3	12.2	11,3	11,0	11.0	8.11	11.8	11.7	11.
10	12.5	15.5	12.1	12'1	12.0	11.8	11.2	11'7	11.6	11.6	11'5	11.8	11,
02	15.0	11,3	11,0	11.8	11.8		11'5	11.4	11'4	11'4	11.3	11.3	11.
03 04	11.2	11.2	11'7	11'6	11.3 11.0	11,2	11.3	11.5	11.5	11.1	11.1	11.1	11.
							11,0	11.0	11,0	10.0	10.0	10.0	111
0.02	11,3	11'2	11.5	11.5	10.0	10,8	10.8	10,8	10.7	10.2	10.3	10.6	XO.
o6	11 0	11.0	11.0	10.2	10.7	10.0	10.0	10.6	10,2	10.5	10.5	10.4	70.
07 08	10.6	10.2	10.2	10.2	10 4	10'4	10.4	10,3	10.3	10'3	10.8	10.3	10,
09	10.3	10.3	10,3	10.3	10.5	10'2	10.1	10.1	10.1	10.0	10.0	10.0	10
)· 15	10.1	10.1	10.0	10,0	10,0	9.9	9.0	9.9	9.9	9.8	9.8	0.8	9.
11	9.9	9.8	9.8	9.8	9.7	9'7	9.7	9.7	9.6	9.6	9.6	9.6	ή.
12	9.6	9.6	9.6	9.2	9.2	9.5	9.2	9.4	9.4	9.4	9'4	9.3	9.
13	9'4	9.4	9.3	9 3	9.3	9.3	9.2	9.2	9.2	9.5	9 · r	9.1	9.
14	9.5	9.1	ð.1	0.1	9.1	9'0	ō,0	9,0	ō.o	8.0	8.9	8.0	н.
. 15	8.0	8.0	g·8	8.8	8.8	8.8	8.8	8.8	8.7	817	8:7	8.7	н.
16	8.7	8.7	8.6	8.6	8.6	8.6	8.6	8 5	8.5	8.5	8.5	8.5	8.
17	8.4	8'4	8.4	8.4	8.4	8.4	8.3	8.3	8.3	8.3	8.3	8.3	н.
18	8.2	8 2	8.2	8.2	8.1	8.1	8.1	8.1	8.1	8.1	8 10	8 0	8.
19	8 0	8.0	7.9	7.9	7.9	7.9	7.9	7.9	7.0	7.8	7.8	y. H	ÿ.
.20	7.7	7.7	7.7	7.7	7.7	7.7	7.7	7.6	7'6	7.6	7.6	7.6	2.
21	7.5	7.5	7.5	7.5	7.5	7.4	7.4	7.4	7.4	7.4	7.4	7.4	
22	7:3	7'3	7.2	7.2	7.2	7.2	7.2	7.2	7 . 2	7.4	7 4	7.2	7
23	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7'0	7.0	7.0	6.9	6.
24	6.8	6.8	5.8	6.8	6.8	6.8	6.8	6.8	6.4	6.7	6.7	6.7	6.
25	6.6	6.6	6.5	6.5	6.2	6.5	6.2	6.5	6.0	<i>e</i>			
25	6.3	6.3	6.3	6.3	6.3	6.3	6.3	6.⁺3	6.3	6.2	6.5	6.8	11:
27	6.1	6.1	6.1	9,I	6.1	6. I	6.1	Q. I	9, I	6.3	6.3	0.3	0.
28	5 9	5.9	5.9	5.9	5.6	5'9	5'9	5'9	5'9			10. x	10.
29	5.6	5.6	5.6	5.6	5.6	5.6	5.6	5.6	5.0	5.0 5.0	5 ' 9 5 ' 6	5.6	5.
.30	5.4	5.4	5.4	5'4	5'4	5'4	5'4	E 1 4				1	
31	5.1	2.1	5 2	5 ' 2	5.5	5.5	5.3	5'4 5'2	5'4	5'4	5 4	5.4	- 5
32	4.9	4.0	4'9	4'9	4.0	4 9	5.0	5.0	5'2 5'2	5'2	5 2	5.2	5.
33	4.2	4.7	4.7	4'7	4.7	4.7	4 7	4.2	-	5.0	5.0	5.0	5
34	4 4	4.4	4.2	4.2	4'5	4.2	4.5	4.2	4 · 7 4 · 5	4'8 4'5	4 ' 8 4 ' 5	4.8	4
35	4.2	4 2	4'2	4.5	4'3	4.3	4'. 3	4'3				7	
36	4.0	4.0	4'0	4.0	4.0	4.0	4.1	4 3 4 1	4'3	4'3	4.3	4.3	4.
37	3.7	3.4	3.8	3.8	3.8	3.8	3.8	3.8	4'1	4'1	4, 1	4.1	4.
38	3.2	3.2	3.2	3.2	3.6	3.6	3.6	3.6	3'6 3'6	3.0	319	3.9	3.1
- 1	3.3	3.3	3.3	3'3	3.3	3'4	3.4	3'4	3'4	3'7 3'4	3.2 3.2	3.7	3.
40	3.0	3.0	3.1	3.1	3,1	3.1	3.2	3.5				3'5	3.
42	2.5	2.8	2.8	2.0	2'9	2.0	2.0	3.0	3.5	3.3	3,5	3.3	3,
43	2.3	2.3	2.6	2.6	2.7	2.7	2 7	2.7	3.0	3.0	3.0	3.0	3.
44	2.1	2.1	2'4	2'4	2'4	2.5	2.2	2.2	2.5	2.8	2.8	3.8	3.
- 1			1	2.5	2.5	2.5	2.3	2.3	2.3	2'6 2'3	2.6	2.6	2.
45	1.8	1.0	1,0	1.0	2.0	2.0	2.0	2.1			,	2.4	**
47	1.4	1.4	x . 7	1.7	1.4	1.8	1.8	1.8	2'1	2'1	2.1	2.3	3.
48	1.1	1.4	1'4	1.2	1.2	1.2	x.2	1.6	1.0	1.0	1,6	5.0	3,
49	0.0	0.0	1'0	1 2	1,3	1,3	1'4	1'4	1.4	1'7	1.7	1.7	ĭ.
50	1.	- 1		1.0	1,1	1.1	1.1	1'2	1.4	1,2	1.2	1.2	I.
51	0.4	0.7	0'7	0.8	0.8	0.0	c g	0.5		A is	1.3	1.3	1,
52	0 2	0.5	0.2	0.6	0.6	0.6	0.7	0.0 0.2	1,0	I,O	1.0	1.1	1.
53	0.0	0.0	0.0	0.3	0'4	0'4	0.2	0.2	0.8	0.8	0.8	0.8	o.
54			0.0	0.1	0,1	0.5	0'2	0.3	0.5	0.6	0.6	0.7	٥.
55			-	0.0	0.0	0.0	0.0	0.0	0.1	0'4	0.4	10.4	٥.
55								- 5	0.1	0,1	0.5	0.3	o,
57				. , .			ļ	*	0.0	0.0	0.0	0.0	0.
58										Ť	~ 0	0.0	
		. [1	ľ	1		J				ı			1

Bei Anwendung dieser Tafel hat man für u_a' jene Verticalcolumne zu benützen, welche dem vorgelegten

Hilfstafel III.

					1.	11118626	fel III.	pagasan di anggangan di mendapakan di	#10:542)==#44.0450pub###########		interestant bearing		
u'_{n}	0'552	0.554	0.226	0.228	0.260	0.262	0'564	0.266	0.568	0.570	0.24	0'574	0'576
03 03 01 0,00	11'9 11'5 11'3	11'9 11'6 11'4 11'0	11'8 11'6 11'4 11'2 11'0	11.8 11.4 11.4 11.6	11.2 11.3 11.4	11.1 11.2 11.2	11.7 11.4 11.2 11.0	11.6 11.4 11.8	11.6 11.4 11.5 11.0	10.4 10.8 11.1 11.2	10.2 10.3 11.1 11.2	10.2 11.1 11.3 11.2	11'4 11'2 11'0 10'8
04 0 05 06 07 08	11.0 10.8 10.6 10.4 10.2 10.0	10.8 10.4 10.4	10.8 10.2 10.8	10.2 10.3 10.4	10.1	10'7 10'4 10'2 10'0	10.6 10.4 10.2 10.0 9.8	10.0 10.4 10.4	10.6 10.4 10.4 9.9 9.7	10.2 10.3 10.1 9.9 9.7	10.2 10.3 10.1 9.9 9.7	10.2 10.3 10.1 9.9	10.4 10.2 10.0 9.8 9.6
09 0'10 11 12 13	9'7 9'5 9'3 9'1	9'7 9'5 9'3 9'1 8'9	9'7 9'5 9'3 9'1 8'8	9°7 9°5 9°2 9°0 8°8	9.6 9.4 9.2 9.3 8.8	9.4 9.2 9.0 8.8	9 6 9 4 9 2 9 0 8 8	9.6 9.4 9.2 8.9 8.7	9.5 9.3 9.1 8.9 8.7	8.7 9.3 9.3 9.3	9°5 9°3 9°1 8°9 8°7	9.5 9.3 9.1 8.9 8.7	9'4 9'2 9'0 8'9
0°15 16 17 18	8·7 8·4 8·2 8·0 7·8	8·6 8·4 8·2 8·0 7·8	8 · 6 8 · 4 8 · 2 8 · 0 7 · 8	8 · 6 8 · 4 8 · 2 8 · 0 7 · 8	8·6 8·4 8·2 8·0 7·8	8·6 8·4 8·2 7·9 7·7	8 · 6 8 · 3 8 · 1 7 · 9 7 · 7	8.5 8.3 8.1 7.9 7.7	8·5 8·3 8·1 7·9 7·7	8 5 8 3 8 1 7 9 7 7	8.3 8.x 7.9 7.7	8.5 8.3 8.1 7.9 7.7	8·5 8·3 8·1 7·9 7·7
0'20 21 22 23 24	7.6 7.4 7.2 6.9	7.6 7.4 7.1 6.9 6.7	7·6 7·4 7·1 6·9 6·7	7.6 7.3 7.1 6.9 6.7	7.5 7.3 7.1 6.9 6.7	7'5 7'3 7'1 6'9	7 · 5 7 · 3 7 · 1 6 · 9 6 · 7	7.5 7.3 7.1 6.9 6.7	7.5 7.3 7.1 6.9 6.7	7·5 7·3 7·x 6·9 6·7	7.5 7.3 7.1 6.9 6.7	7 5 7 3 7 1 6 9 6 7	7.5 7.3 7.1 6.9 6.7
0'25 26 27 28 29	6.2 6.3 6.1 5.9	6.5 6.3 6.1 5.9	6 · 5 6 · 3 6 · 1 5 · 9 5 · 7	6.5 6.3 6.1 5.9 5.7	6 · 5 6 · 3 6 · 1 5 · 9 5 · 7	6·5 6·3 6·1 5·9 5·7	6·5 6·3 6·1 5·9 5·7	6.5 6.3 6.x 5.9	6.5 6.3 6.1 5.9 5.7	6·5 6·3 6·1 5·9 5·7	6·5 6·3 6·1 5·9 5·7	6.5 6.3 6.1 5.9 5.7	6 · 5 6 · 3 6 · x 5 · 9 5 · 7
0.30 31 32 33	5'4 5'2 5'0 4'8	5 ' 4 5 ' 2 5 ' 0 4 ' 8 4 ' 6	5 · 4 5 · 2 5 · 0 4 · 8 4 · 6	5 ' 4 5 ' 2 5 ' 0 4 ' 8 4 ' 6	5 · 4 5 · 2 5 · 0 4 · 8 4 · 6	5 5 5 5 5 5 6 4 8 4 6	5 · 5 5 · 2 5 · 0 4 · 8 4 · 6	5.5 5.3 5.0 4.8 4.6	5 5 5 3 5 1 4 9 4 6	5.5 5.3 5.1 4.9 4.7	5 5 5 3 5 1 4 9 4 7	5 · 5 · 5 · 5 · 5 · 1 4 · 9 4 · 7	5.5 5.3 5.1 4.9 4.7
9:35 36 37 38 39	4 4 4 1 3 9 3 7	4'4 4'2 3'9 3'7	4'4 4'2 4'0 3'7	4'4 4'2 4'0 3'8	4'4 4'2 4'0 3'8 3'6	4 '4 4 '2 4 '0 3 '8 3 '6	4 · 2 4 · 0 3 · 8		4°2 4°0 3°8	3 8		4.5 4.3 4.1 3.9 3.7	3,8
0 · 40 41 42 43	3°3 3°1 2°8 2°6	3°3 3°1 2°9 2°7	3 3 3 2 9 2 7	3'3 3'1 2'9 2'7	2.2	3 · 4 3 · 2 3 · 0 2 · 7 2 · 5	3 4 3 2 3 0 2 8	3 2 3 0 2 8	3'2	3 · 2 3 · 0 2 · 8	3°3 3°1 2°9	3,1	3.3
45 46 47 48	2 · 2 2 · 0 1 · 8 1 · 6	2°2 2°0 1°8	2'3 2'0 1'8 1'6	2 3 2 1 1 9 1 6	2'3 2'1 1'9	1.4 1.4	2'I	2 · 2 2 · 6 1 · 8	2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	2 ' 2 2 ' 0 1 ' 8	2'3 2'1	2°3	2':
0°50 57 58	0,2	0.5	1 1 2 1 0 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1 2 1 2 0 8 0 6 0 6 6 0 6 6	0 0 6	0.0	0,7	7 0'5	1 1.5	1 1 2 1 5 6 8 6 8 6 8 6 8 6 8 6 8 6 8 6 8 6 8 6	1 2 1 0 8 0 8	2 0.0	0, r r,
0°5; 5; 5;	5 ° 0			1		1		r 0.	1 0.3	2 0.2	0.5	0.	i o.

Werth von u'_{α} zunächst liegt.

Will man die Grösse der Phase für einen vorher gegebenen Stundenwinkel 3 kennen, wie es z. B. bei der Frage nach der Grösse der Phase für Sonnenaufgang oder Sonnenuntergang der Fall ist, so berechnet man:

$$\begin{split} m \sin M &= \gamma - \eta \cos g + \xi \sin g \sin (G + \vartheta) \\ m \cos M &= (\vartheta - \lambda - \mu) \frac{n}{15} - \eta \cos k + \xi \sin k \cos (K + \vartheta). \end{split}$$

Hiebei hat man, wenn nöthig, durch Subtraction von 360° zu beachten, dass der Winkel $9-\lambda-\mu$ stets innerhalb der Grenzen -50° und +50° eingesehlossen ist, was immer erreicht werden kann, wenn die Finsterniss für den vorgelegten Ort möglich ist. Der stets positiv zu nehmende Werth von m gibt mit Hilfe der Tafel III oder mittelst des Ausdruckes:

$$6\frac{u_a'-m}{u_a'-0\cdot 27365}$$

die Grösse der Phase für den gegebenen Stundenwinkel in Zollen.

B) Anfang und Ende der Finsterniss.

Den Stundenwinkel der Sonne für Anfang und Ende der Finsterniss rechnet man am bequemsten nach der folgenden von Dr. Robert Schram herrübrenden Transformation der von Hansen biefür gegebenen Formeln.

Es sei \mathcal{S} ein beliebiger Nüherungswerth, am besten der Stundenwinkel für die Zeit der grössten Phase In diesem letzteren Falle ist schon durch die vorhergehenden Rechnungen m' eventuell auch m und M gegeben; ist aber keine Nüherung bekaunt, so setzt man $\mathcal{S} = \lambda + \mu$. Man hat dann:

$$G + \Im = G'' \qquad K + \Im = K''$$

$$m \sin M = \gamma - \eta \cos y + \xi \sin y \sin G''$$

$$m \cos M = (\Im - \lambda - \mu) \frac{n}{15} - \eta \cos k + \xi \sin k \cos K''$$

$$m \text{ stets positiv}$$

$$u_2 = u'_a - f_a \eta \sin \delta'.$$

Bezeichnet man mit d die Correction, die man an $\mathfrak I$ anzubringen hat, um den Stundenwinkel t der Sonne zur Zeit des Anfanges oder des Endes der Finsterniss zu erhalten, so wird man, falls $\mathfrak I$ mit dem Stundenwinkel der grössten Phase identisch und m' aus der diesbezüglichen Rechnung bekannt ist, in erster Näherung $d_a = -\frac{15}{m'}\sqrt{u_2^2 - m^2}$ und $d_c = +\frac{15}{m'}\sqrt{u_2^2 - m^2}$ setzen; ist aber kein genäherter Werth bekannt, so wird man in erster Näherung d = 0 annehmen. Man hat weiter:

Anfang

$$m'' \sin M''_a = +x'' \xi \sin g \cos \left(G'' + \frac{d_a}{2}\right)$$
 $m'' \cos M''_a = \frac{n}{15} + x'' \xi \sin k \sin \left(K'' + \frac{d_a}{2}\right)$
 $m'' \cot M''_a = \frac{n}{15} + x'' \xi \sin k \sin \left(K'' + \frac{d_a}{2}\right)$
 $m'' \cot M''_a = \frac{n}{15} + x'' \xi \sin k \sin \left(K'' + \frac{d_e}{2}\right)$
 $m'' \cot M''_a = \frac{n}{15} + x'' \xi \sin k \sin \left(K'' + \frac{d_e}{2}\right)$
 $m'' \cot M''_a = \frac{n}{15} + x'' \xi \sin k \sin \left(K'' + \frac{d_e}{2}\right)$
 $m'' \cot M''_a = \frac{n}{15} + x'' \xi \sin k \sin \left(K'' + \frac{d_e}{2}\right)$
 $m'' \cot M''_a = \frac{n}{15} + x'' \xi \sin k \sin \left(K'' + \frac{d_e}{2}\right)$
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Die Näherungen mitssen für Eintritt und Austritt gesondert berechnet werden. Wird sin χ' in der ersten und zweiten Näherung grösser als die Einheit, so setze man $\cos \chi' = 0$, bleibt aber $\sin \chi' > 1$ auch bei der letzten Annäherung, so findet keine Finsterniss für den gegebenen Ort statt.

d wird also ein Näherungswerth sein, der in die Formeln 2) eingesetzt, eine neue Annäherung ergibt; dieses Verfahren ist so lange fortzusetzen, bis der neue Werth von d mit dem früher erlangten genügend stimmt. Die Phase ist sichtbar, wenn

$$\sin \delta' \sin \varphi + \cos \delta' \cos \varphi \cos t$$

innerhalb der Grenzen -0.01 und +1.00 liegt. Der Positionswinkel des Eintrittes Θ_a und des Austrittes Θ_c für directes Bild (vom Nordpunkt des Sonnenrandes nach Ost gezählt) findet sich nach:

Hiebei ist M''_a , M''_c , χ'_a und χ'_c der letzten Annäherung zu entnehmen. Will man den Positionswinkel statt vom Nordpunkt der Sonne, von dem durch die Sonne gehenden Verticalkreise an, ebenfalls für directes Bild nach Ost gezählt erhalten, so rechnet man:

$$\operatorname{tg} K_{n} = \frac{\sin t_{n}}{\cos \delta' \operatorname{tg} \varphi - \sin \delta' \cos t_{n}}, \qquad \operatorname{tg} K_{e} = \frac{\sin t_{e}}{\cos \delta' \operatorname{tg} \varphi - \sin \delta' \cos t_{e}}$$

sin K mit sin t gleichbezeichnet,

dann ist der Positionswinkel für Anfang und Ende

$$\Theta_a' = \Theta_a - K_a, \qquad \Theta_e' = \Theta_e - K_e.$$

Zur Ermittlung der Hauptumstände der totalen und ringförmigen Finsterniss für einen gegebenen Ort kann man sich der vorangehenden Formeln bedienen, nur hat man überall statt u'_a und f_a die entsprechenden Werthe u'_i und f_i einzusetzen; in der ersten Näherung wird man für $\mathfrak I$ immer jenen Werth wählen, welcher nach A) p. XXIV und XXV für die Zeit der grössten Phase gilt; die Grössen u'_i und f_i bestimmt man nach:

$$u_i' = 0.5473 - u_a', \qquad \log f_i = 9_n 9978 + \log f_a.$$

Tafel IV.

<u>+</u> - d	$\log \varkappa''$	in d	log x"	1.0	log x"	<u>-1-</u> ; d	log x"	<u>-1-</u> d	log x"
0° 1 2 3 4 5 6 7 8 9 10	8n2419 8n2419 8n2419 8n2418 8n2418 8n2417 8n2417 8n2416 8n2415 8n2415 8n2415	10° 11 12 13 14 15 16 17 18 19 20	8n2413 8n2412 8n2411 8n2409 8n2408 8n2406 8n2405 8n2403 8n2401 8n2399 8n2397	20° 21 22 23 24 25 26 27 28 29 30	8n 2397 8n 2394 8n 2392 8n 2390 8n 2387 8n 2384 8n 2379 8n 2375 8n 2372 8n 2369	30° 31 32 33 34 35 36 37 38 39	8n 2369 8n 2366 8n 2362 8n 2359 8n 2355 8n 2351 8n 2347 8n 2349 8n 2339 8n 2335 8n 2330	40° 41 42 43 44 45 46 47 48 49	8n 2330 8n 2321 8n 2321 8n 2316 8n 2312 8n 2307 8n 2302 8n 2296 8n 2286 8n 2280

In sämmtlichen auf die Sonnenfinsternisse bezüglichen Formeln bezeichnet immer:

t den Stundenwinkel der wahren Sonne am bezuglichen Erdorte,

Fügt man zu diesen Grössen die im Canon unter den Elementen gegebene mit Z bezeichnete Zeitgleichung hinzu, so erhält man den entsprechenden Stundenwinkel der mittleren Sonne. Um Stundenwinkel in Zeit zu verwandeln kann man sich der folgenden Tafel V bedienen. Geht man in diese Tafel ein:

mit dem Stundenwinkel t erhält man wahre bürgerliche Ortszeit,

" "
$$t+Z$$
 " mittlere " "
" " wahre " Greenwicher Zeit,
" " $\tau+Z$ " mittlere " " also Weltzeit.

Tafel V. Verwandlung von Stundenwinkel in Zeit.

Stunden- winkel	1	ı, m	Stunden-	IQUII II	h.	m.	Stunden-	la la	. m.	Stunden- winkel	lı.	ın.	Stunden- winkel	h.	III.	Stunden- winkel	h.	lu.	Stunden- winkel	lı.	lil.	Stunden- winkel	lı.	m.	Stunden-	winkei	111.	Stunden- winkel	111.
180° 131 182 183 184	0	4. 8.	0 225 0 226 0 227 0 228 0 229	3 3	r	4 · 0 8 · 0 2 · 0	270 271 272 273 274	6 6 6	4'6 8'6	315° 316 317 318	9 9 9	0 ¹¹ 0 4 ¹ 0 8 ¹ 0 12 ¹ 0	1 2 3	12 12 13	0"0 4 0 8 0 12 0	46 47 48	15 15	0"0 4'0 8'0 12'0	91 92 93	18 18 18	4'0		21 21 21	4.0	o o	02 03	0,1 0,1 0,0	o'5; o'5;	
185	0 0 0	24' 28' 32'	0 230 0 231 0 232 0 233	3 3 3	2 2 3	o ' o 4 ' o 8 ' o 2 ' o	275 276 277 278 279	6 6 6	20 0 24 0 28 0 32 0	0 320 0 321 0 322 0 323	999	20.0 24.0 28.0 32.0 36.0	5 5 7 8	12 12 12	20'0 24'0 28'0 32'0 36'0	50 51 52 53	15 15 15	20'0 24'0 28'0 32'0 36'0	95 96 97 98	18 18 18 18	20 0 24 0 28 0 32 0 36 0	140 141 142 143	21 21 21 21	20'0 24'0 28'0 32'0 36'0	0.0	05 06 07 08	0 ° 2 0 ° 3 0 ° 3	0 ' 5 0 ' 5 0 ' 5	5 2 2 5 2 2 7 2 3 8 2 3
191 192 193	0 0 0	44 ° 48 ° 52 ° 6	235 236 237 238 239	3 3 3 3	4 4 5	0'0 4'0 8'0 2'0	280 281 282 283 284	ნ ნ ნ	40 ° 6 44 ° 6 48 ° 6 52 ° 6	325 326 327 328 329	9 9	40.0 44.0 48.0 52.0 56.0	10 11 12 13	12 12 12	40.0 44.0 48.0 52.0 56.0	55 56 57 58	15 15 15	40 0 44 0 48 0 52 0 55 0	100 101 102 103	18 18 18	40 0 44 0 48 0 52 0 56 0	145 146 147 148	21 21 21 21	40'0 44'0 48'0	00000	11 12 13 14	o 14 o 15 o 15 o 16	0 6 0 6 0 6 0 6	2 2 5 3 2 5 4 2 6
196 197 198	1	8 · 6	240 241 242 243 244	4 4	I	4°0 8°0 2'0	285 286 287 288 288	7 7 7 7	0.0 4.0	330 331 332 333	10	0'0 4'0 8'0 12'0	15 16 17 18	13	0'0 4'0 8'0 12'0	60 61 62 63	16 16 16	0,0	105 105 107 108	19	0'0 4'0	150 151 152 153	22 22 22 22	0'0 4'0 8'0	000	16 17 18 19	o 18 o 17 o 18	o'6 o'6	0 2 · 6 2 · 7 2 · 7 2 · 7 2 · 8 2 · 8
201 202 203	I I	24 ' 6 28 ' 6	245 246 247 248 249	4	2:	4 ° 0 2 ° 0	290 291 292 293 294	7 7 7	32'c	335 336 337 338 339	10	20'0 24'0 28'0 32'0 36'0	21 22 23	13 13	20 0 24 0 28 0 32 0 36 0	65 66 67 68	16 16 16	20'0 24'0 28'0 32'0 36'0	110 111 112	10 10 10	20'0 24'0 28'0 32'0 36'0	155 156 157 158	22 22 22 22	20 ° 0 24 ° 0 28 ° 0 32 ° 0	0 0 0 0	21 22 23 24 25	1,0 0,0 0,0	0 . 4 0 . 4 0 . 4 0 . 4	1 2 · 8 2 2 · 9 3 2 · 9 4 3 · 0
205 207 208	r r	44 ° 0 48 ° 0 52 ° 0	250 251 252 253 254	4 4 4	48	4'0 3'0	295 296 297 298 299	7 7 7	44 ° 0 48 ° 0 52 ° 0	340 341 342 343	10	40.0 44.0 48.0 52.0 56.0	25 26 27 28	13 13 13	40'0 44'0 48'0 52'0 56'0	70 71 72 73	16 16 16	40.0 44.0 48.0 52.0 56.0	115 116 117 118	19 19 19	40 ° 0 44 ° 0 48 ° 0 52 ° 0 56 ° 0	160 161 162 163	22 22 22 22	40.0 44.0 48.0 52.0	0. 0.	27 28 29 30	1.5	o · 7 o · 7 o · 8	7 3 1 8 3 1 9 3 2
210 211 212 213	2 2 2 2	0'0 4'0 8'0	255 256 257 258 259	5 5 5 5	12	1 ° 0	300 301 302 303 304	8 8 8	0.0	345 346 347 348	II II II	0'0 4'0 8'0 12'0	30 31 32 33	14 14 14	0.0 4.0 8.0 12.0	75 76 77 78	17 17 17	0:0 4:0 8:0	120 121 122 123	20 20 20 20	0'0 4'0 8 0	165 166 167 168	23 23 23 23	4 0 8 0 12 0	0. 0. 0.	32 33 34 35 36	1 3 1 3 1 4 1 4	o 18 o 18 o 18 o 18 o 18	2 3 3 3 3 3 4 3 4 5 3 4 6 3 4
215 216 217 218	2 2 2 2	20°0 24°0 28°0 32°0	250 251 252 253	5 5 5 5	26 28 34	3.0	305 306 307 308	8 8 8	20°0 24°0 28°0	350 351 352	11	20'0 24'0 28'0	35 36 37 38	14 14 14	20.0 24.0 28.0 32.0	80 8x 82 83	17	32.0	125 126 127 128	20 20 20 20	28 ° 0	170 171 172 173	23 23 23 23	32'0	0.	38 39 40 41	1.6 1.6	o 190 o 180 o 180	3.6
220 221 222 223	2 2 2 2	40 · 6 44 · 6 48 · 6 52 · 6	265 266 267 268	5 5 5 5	44 48 52	0.0	310 311 312 313	8 8 8	40 ° 0 44 ° 0 48 ° 0 52 ° 0	355 356 357 358	II II II	40.0 44.0 48.0 52.0	40 41 42 43	14 14 14 14	36.0 40.0 44.0 48.0 52.0	85 86 87 88	17 17	40'0	132	20 20 20		175 176 177	23 23 23	36 0 40 0 44 0 48 0 52 0	0	43 44 45 46	r . 8 r . 8 r . 8	9.96 9.96 9.96	3 3 7 4 3 8 5 3 8
		·	259 270				314 315					56°0			56.0			5 6.0	134	20	56 o	179		56.0	go ·	48	1.0		3 3.0

II.

Canon der Mondfinsternisse.

Erläuterung der im Canon der Mondfinsternisse angeführten Zahlen.

Der Canon der Mondfinsternisse enthält die Hauptumstände aller Mondfinsternisse, wel che sich zwischen dem Datum:

— 1206 April 21 (julianisch) und 2163 October 12 (gregorianisch) ereignen. Als Grundlage hiezu dienten die im XLVII. Bande der Denkschriften von mir publicirten Tafeln zur Berechnung der Mondesfinsternisse; die nach diesen Tafeln erhaltene wahre Greenwicher Conjunctionszeit wurde jedoch für den Canon durch Hinzufügung von zwölf Stunden und Anbringung der Zeitgleichung mittelst der folgenden Tafel VI in Weltzeit umgesetzt.

Tafel VI.

zur Reduction der Zeitaugaben der Tafeln zur Berechnung der Mondesfinsternisse auf mittlere Zeit.

r>				Management of the Adapt Surgement	Ju	liani	ischo	Jah	rhur	dert	е						egor. undert
Datum	-1200	-1000	800	600	400	-200	o	200	400	600	800	1000	1200	1400	1600		Datum
I 1 I 11 I 21	+24 +26	+-18" +-23 +-25 +-25	+17" +22 +24 25	+16" +20 +23 +24	+14" +19 +22 +23		+12 ^m +17 +20 +21	+12" +16 +19 +20	+11" +15 +18 +19	+10 ^m +15 17 18	- -10" - -14 - -17 - -18	+ 9" +13 +16 +17	+ 9" +13 +15 +16	+ 9" +13 +15 +16	+12 +14	+ 4" + 8 +12 +14	I 1 I 11 I 21 I 31
II 10 II 20		+23 +20	- -23 - -19	-†-22 - -19	-122	+21	- -20 - -17	- -17 - -17	⊹18 ⊹16	- -18 - -16	+17	+16 +15	16 14	+15	+14	+14 +14	II 10 II 20
III 2 III 12 III 22	+ 8	+15 + 8 + 1	+15 + 9 + 2	+ x5 + 9 + 3	+15 + 9 + 4	+14	+14 +10 + 5	+14 + 9 + 5	+13 + 9 + 5	+13 + 9 + 5	+12 + 9 + 5	+12 +8 +5	+11 + 8 + 4	+IX + 7 + 4	+ 7	+13 +10 + 7	III 2 III 12 III 22
lV 1 lV 11 lV 21	12	5 11 15	- 4 - 9 - 13	3 8 12	- 7	6 9	5 8	o 4 7	+ x - 3	3 6	+ 1 2 5	+ I - 2 - 4	+ I 2 4	+ I 2 4	- 2	1.	IV 1 IV 1 IV 2
V 12 V 22 V 33	I 15	17 16 14	15 15 13	14 14 13 9	13 13 12	12 12 11 8		ro ro g 7	- 8 - 9 - 8 - 6	- 8 - 8 - 7 - 6	7 7 6 5	6 6 6	5 - 5 - 5 - 3	5 4	- 4	4 4	1 37
VI 10 VI 20 VI 3	0 + 2	+ 2	r	5 0 1 5	5 o	- 5 o + 4	4 o + 3	- 4 o + 3	4 o +- 3	3 o + 3	- 2 0 + 3	1 '	· - 1	+ 2	H- 8		~~~
VII 2	o11 o13	+12		+ 10 + 10	+ 8 +10 +10		+ 8	+ 6 + 8 + 8	+ 6 + 7 + 7	7	+ 5 + 6 + 6	- - 6	+ 6	i -16	i + 6	i - - 6	VII 2
VIII 1	9 +10 9 + 6	5	i	-l- 6		+ 5	+ 4	+ 7 + 4 0	·f· 4	+ 3	+ 2	2	+ 4	1 4 :	1 +	ı 3	VIII
ΙX	8 — <u>8</u>	5 2	10	9	g	8		8	8	8 8	8	8	3	3	9	9 (i IX.
X X X	18 —2	5 -2	3 22	-21	21	20	, rg	x8	x 8	-17	x	5 -1	6 -1	б г	6 r	6 -1	5 X
XI XI XI	17 -1	7 -x	7 17	7 -16	j I	5 z ē	5 -15		-I	4	t I	3 -1	3 1	2 -1	2 -:	2 1	5 XI
XII XII XII XII	17 + 27 +1	б + т	7 + 1 5 + 1	5 + 1 4 + 1	3 - 5 + 2 +1	4 + 1	4 + 3	3 + 4	9 +	2 + :	2 +	2 + + 7 +	2 +	2 + 7 +	2 +		4 XII

Diese Tafel schliesst sich somit den Zahlen der Tafeln zur Berechnung der Mondesfinsternisse au.

Die auffällig grossen Werthe der Reduction für von der Gegenwart entfernte Epochen erklären sich aus dem Umstande, dass in den Tafeln zur Berechnung der Mondesfinsternisse die Zeitgleichung mit dem Argumente "mittlere Anomalie der Sonne" tabulirt wurde und der erstrebten Annäherung entsprechend, nur das von der ersten Potenz der Zeit abhängige Glied Berücksichtigung fand.

Es schien daher, um die hier gemachte Rückreduction möglichst richtig auszuführen, entsprechend, jene aus den Tafeln sich ergebenden Worthe zu benützen und in die vorstehende Tafel aufzunehmen.

Es scheint auch hier der Platz zu sein, aufmerksam zu machen, dass die auf p. [50] meiner Syzygientafeln angegebenen numerischen Werthe für σ_p und σ_i sieh auf die Annahme gründen, dass man bei Berechnung der Mondfinsternisse ohne Nachtheil, wie dies auch in der That der Fall ist, die Sonnenparallaxe gegen die Mondparallaxe vernachlässigen kann. Wollte man dieselbe mit in Rechnung ziehen, so hätte man anzuwenden:

$$\sigma_p = 1.5708 - u_a'$$
 $\sigma_t = 1.0235 - u_a'$

statt jener in den Syzygientafeln angeführten Werthe:

$$\sigma_{\nu} = 1.5682 - u_{\nu}'$$
 $\sigma_{\ell} = 1.0222 - v_{\nu}'$

welch' letztere Werthe bei den vorliegenden Rechnungen durchaus in Anwendung gekommen sind.

Infolge der Abzählung der Gattung der Finsternisse des Canons findet man, dass in einem julianischen Jahrhundert durchschnittlich 154·3 Mondfinsternisse stattfinden, von denen etwa 71·6 total, 82·7 partiell sind

Die Columnen des Canons sind:

- 1. Columne enthält unter der Überschrift Nr. die fortlaufende Nummer der Finsternisse.
- 2. Columne gibt das Datum der Finsterniss nach Weltzeit angesetzt und zwar bis zur Finsterniss Nr. 4307 inclusive nach dem julianischen Kalender, von da ab nach dem gregorianischen Kalender.
- 3. Columne gibt den zum Datum gehörigen Tag der julianischen Periode und wurde hauptsächlich desshalb angesetzt, um mittelst dieser Zahl auf etwaige andere Kalenderzählungen mit Hilfe der Schram'sehen Tafeln (Hilfstafeln für Chronologie im XLV. Bande der Denkschriften der math.-naturw. Classe der kais. Akademie der Wissenschaften in Wien) in bequemer Weise übergehen zu können. Ein weiterer, allerdings nicht wesentlicher Vortheil der Angabe der zum Datum gehörigen julianischen Tage besteht darin, dass man dadurch im Stande ist, den Wochentag des vorgesetzten Datums zu bestimmen. Dividirt man nämlich die dem Datum entsprechende Tageszahl der julianischen Periode durch sieben, so ist der Tag ein:

see pos	Montag,	wenn	der	Rest	0.
•	Dienstag,	"	1)	. ,,	1,
	Mittwoch,	17	• • •	"	2,
	Donnerstag,	"	"	"	3,
	Freitag,	2)	21	2)	4,
	Samstag, Sountag,	"	**	17	5,
	CONTRACTOR CONTRACTOR				ti int

Columne gibt die Weltzeit der grössten Phase der Finsterniss in Stunden und Minuten. Die Angaben sind, abgesehen von der beträchtlichen Unsicherheit, die den Mondtafeln für entfernte Epochen anhaftet, als bis auf wenige Minuten richtig auzusehen.

Columne enthält die Grösse der Finsterniss in Zollen und deren Decimaltheilen; alle Finsternisse, welche kleiner als 12 Zoll ausfallen, sind partiell, diejenigen, welche grösser werden, total. Bei Vergleichung dieser Angaben mit anderweitigen Rechnungsresultaten wäre zu beachten, dass der Vergrösserungsfactor des Erdschattens $\frac{1}{40}$ angenommen wurde.

- 3. Columne führt in zwei Subcolumnen die halbe Zeitdauer der Partialität und die halbe Zeitdauer der totalen Verfinsterung auf, wobei unter der halben Dauer der Partialität die halbe zwischen der ersten und letzten äusseren Berührung des Vollschattens mit der Mondscheibe verfliessende Zeit, unter der halben Dauer der Totalität dagegen die halbe zwischen der ersten und letzten inneren Berührung des Vollschattens versliessende Zeit zu verstehen ist. Da hiebei nur deren durchschnittliche Werthe angesetzt sind, so wird man in der halben Dauer bei partiellen Finsternissen in den extremsten Fällen um 6 Minuten, bei den totalen um 3 Minuten irren können.
- 7. Columne gibt in zwei Subcolumnen die Länge à (östlich von Greenwich positiv, westlich negativ gezählt) und die Breite \varphi jenes Erdortes, für welchen zur Zeit der wahren Conjunction das Centrum des Erdschattens im Zenith steht.

Mit Hilfe der letzteren Angaben und mit Benützung der folgenden Tafel VII wird es leicht sein, zu entscheiden, ob eine gegebene Mondfinsterniss für einen Ort, dessen geographische Breite durch Ф, dessen östliche Länge von Greenwich (westliche Längen negativ genommen) mit l bezeichnet werden möge, sichtbar ist oder nicht. Man bildet zu diesem Zwecke zunächst:

$$l - \lambda$$
 oder $\lambda - l$,

und benützt entweder die erste oder die zweite Form, um diesen Bogen stets positiv zu erhalten; liegt derselbe zwischen 180° und 360°, so bildet man überdiess seine Ergänzung zu 360°. Man erhält auf diese Weise einen stets positiven Bogen, der kleiner als 180° ist und mit h bezeichnet werden soll. Mit den Argumenten φ und Φ entlehnt man aus der Tafel VII, bei der man sich auf geographische Breiten bis $\pm 50^{\circ}$ beschränkt hat, und die nach der Formel;

$$\cos H = - \operatorname{tg} \varphi \operatorname{tg} \Phi$$

berechnet ist, den halben Tagbogen II. Es ist nun

die Phase der Finsterniss sichtbar, wenn
$$H > h$$
 ist,

"" " " " " " " " " $H < h$ ".

Sollte O negativ sein, so geht man in die Tafel ein, indem man das Vorzeichen von O positiv annimmt und jenes von φ verkehrt.

Die hier aufgestellte Regel wird auch für den Beginn oder das Ende der Finsterniss benützt werden können, wenn man im ersteren Falle à um eine entsprechende Correction vermehrt, im zweiten Falle um dieselbe Correction vermindert in Rechnung zieht. Diese Correction erhält man in Graden ausgedrückt, indem man die im Canon in Zeitminuten angegebene halbe Dauer der Verfinsterung durch 4 dividirt. Je nachdem man à für Anfang oder Ende der Partialität oder für Anfang oder Ende der Totalität bestimmen will, wird man die halbe Dauer der Partialität oder diejenige der Totalität durch 4 zu dividiren haben.

Dieser eben erläuterte Rechnungsmechanismus kann aber leicht durch die Benützung eines Globus ersetzt werden. Will man nämlich alle jene Orte kennen, welche die Mitte der Finsterniss wahrnehmen können, so bringe man den durch λ und φ bestimmten Ort der Erdoberfläche durch entsprechende Drehung des Globus nach dem Zenith; alle Orte, die über dem sogenannten Horizonte des Globus liegen, werden die Finsterniss sehen, diejenigen aber, welche unter demselben stehen, nicht. Will man ähnlich jene Orte bestimmen, die den Anfang oder das Ende der Finsterniss sehen, so stelle man statt der Länge λ im ersten Falle $\lambda + \frac{\text{Halbe Dauer}}{4}$, im zweiten Halbe Dauer ein und verfahre in ähnlicher Weise. Je nachdem man die halbe Dauer der Partialität oder Totalität einstellt, wird die betreffende Bestimmung für den Anfang und das Ende der Partialität oder Totalität gelten.

Th. v. Oppolzer

Tafel VII für den halben Tagbog en = H.

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24° 23 22	90	1 -	9	88	87	86° 87 87	86	85		83	82° 82 82	81° 81	80° 80 81	79° 79 80	77° 78 79	76° 77 78	75° 76	74° 75 75	72° 73 74	71° 72 73	70° 71 72	68° 69 70	66° 68 69	65° 66 67	бз [°] 64 65	бо° б2 б3	58° 60 61	-24° -23 -22
-21 -20 -19	90 90	8 0	9		88	87	86	85 86 86	85	84	83 83 84	82 82 83	81 82 82	80 81	79 80 80	78 79 79	77 78 79	76 77 78	75 76 77	74 75 76	73 73 74	71 72 73	70 71 72	68 69 71	б7 68 б9	65 66 68	63 64 66	-21 -20 -19
-18 -17 -16	90	0 8	9	89	88 88 88	88	87 87 87	86 86 87		85	84 84 35	83 84 84	82 83 83	82 82 83	81 31 82	80 81 81	79 80 81	78 79 80	77 78 79	76 77 78	75 76 77	74 75 76	73 74 75	72 73 74	70 71 73	69 70 71	67 69 70	18 17 16
-15 -14 -13		- 1	0	28	88	88		87	86	86	85 85 86	84 85 85	84 84 85	83 84 84	82 83 83	82 82 83	81 32 82	80 81 82	80 80 81	79 80 80	78 79 80	77 78 79	76 77 78	75 76 77	74 75 76	73 74 75	71 73 74	-15 -14 -13
-12 -11 -10	90	9	0	8g	89	88	88	87 88 88	87	87	86 86 86	86 86 36	85 85 86	85 85 85	84 85 85	84 84 85	83 84 84	82 83 84	82 82 83	81 82 83	80 81 82	80 81 81	79 80 81	78 79 80	77 78 79	76 78 79	75 77 78	12 11 10
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- 6 - 5 - 4	90	9	0	90	89	89	89	89 89 89	,,,	89	88 88 89	88 88 08	88 88 88	87 88 88	87 88 88	87 87 88	87 87 88	86 87 87	86 87 87	86 86 87	85 86 87	85 86 87	85 85 86	84 85 86	84 85 86	83 84 86	83 84 85	- 6 - 5 - 4
- 3 - 2 - 1	9¢	9 9	0	_	90	90 90	90	89 90 90	90	**	89 89 90	89 89 90	89 89 90	89 89 90	89 89 90	88 89 89	88 68 08	88 89 89	88 89 89	88 89 89	88 88 89	87 88 89	87 88 89	87 88 89	87 88 89	87 88 89	86 88 89	3 - 2 - 1
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+18 +19 +20	9	0 2	I	91	92 92 92	93 93 93	93 93 94	94 94 94	95 95 95	95 96 96	96 96 97	97 97 98	98 98 98	98 99 99	99 100	101	101	102 102 103	103	104 104 105	105 106 106	107	107 108 109	109	111	111 112 114	113 114 116	+18 +19 +20
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III.

Iconographie zum Canon der Sonnenfinsternisse.

Die Karten haben den Zweck, die Hauptpunkte der Centraleurve zur bildlichen Anschauung zu bringen und bei den so wichtigen Untersuchungen, ob und welche Finsternisse für einen gegebenen Ort bedeutend sein können, als Leitfaden zu dienen. Zunächst finden sich die drei Hauptpunkte der Centralität, nämlich Centralität bei Sonnenaufgang (△), Centralität im Mittag (○), Centralität bei Sonnenuntergang (▲) in der Karte eingetragen. Um die drei zusammengehörigen Punkte sofort zusammenfinden zu können, wurden dieselben durch einen Kreisbogen verbunden. Die Art der Zeiehnung des Kreisbogens weist auf die Gattung der Finsterniss hin; erscheint nämlich derselbe ganz ausgezogen, so ist die Finsterniss eine totale, erscheint er punktirt, so ist die Finsterniss eine ringförmige, wechseln Punkte mit kürzeren Linien ab, so ist die Finsterniss eine ringförmigtotale. Am Curvenbogen selbst ist an passender Stelle das Datum der Finsterniss in einer Weise ersichtlich gemacht, welche kaum einen Zweifel darüber bestehen lässt, zu welcher Curve das betreffende Datum gehört. Es ist klar, dass diese so ausgezogenen Kreisbogen in einer gewissen Annäherung sich dem Verlaufe der Curve der Centralität anschliessen und umsomehr der Wahrheit nahe kommen werden, je näher das betreffende Curvenstück einem der Hauptpunkte liegt; selbst aber von diesen Punkten entfernter liegende Curvenstücke werden sich in nicht allzu erheblicher Weise von der Wahrheit entfernen, so dass die Fehler bei dem kleinen Massstabe der Karte in nicht allzu bemerklicher Weise zum Ausdruck gelangen. Man kann daher, ohne irgend erheblichen Täuschungen unterworfen zu sein, die so ausgezogenen Kreisbogen mit der Curve der Centralität identificiren, und die Karten geben sonach vorzügliche Hilfsmittel ab, alle für eine bestimmte Localität bedeutenden Finsternisse mit Sicherheit beraussuchen zu können; doch darf man hiebei niemals vergessen, dass die von den Hauptpunkten entfernt liegenden Punkte oft wesentliehe Abweichungen zeigen können, und dass besonders für die älteren Zeiten die Rechnung selbst einigermassen unzuverlässig wird, in Folge der Unsicherheiten, die unseren gegenwärtigen Mondtheorien anhaften.

Es ereignete sich nicht selten, dass die den Kreisbogen bestimmenden Hauptpunkte insoferne ungunstig gelegen waren, als zwei derselben aneinander so nahe zu liegen kamen, dass dadurch eine sichere Bestimmung der Lage des Kreisbogens vereitelt wurde. Um hier der angestrebten Idee, die Kreisbogen als Ersatz für die Curve der Centralität gelten zu lassen, möglichst nahe zu kommen, wurde für einen entsprechend gewählten Stundenwinkel ein vierter, für die Bestimmung des Kreisbogens günstig gelegener Punkt ermittelt, der dann zur Bestimmung der Lage des Kreisbogens verwerthet wurde, wobei aber in Folge der überschüssigen Bedingung der Zug dieses letzteren nur so gewählt werden konnte, dass er sich den beiden naheliegenden Punkten möglichst anschmiegte. Um in diesem Falle aber nicht die Hauptpunkte ausserhalb der Curve setzen zu müssen, wurden dieselben, wenn auch nur durch eine Correction in den nüchstliegenden Theil der Curve verrückt. Dieser Vorgang wurde bei den folgenden Curven eingehalten:

Nr. 217, 261, 300, 304, 347, 390, 507, 709, 732, 879, 986, 1513, 1642, 1889, 2233, 2670, 2687, 2967, 3246, 3420, 3435, 3773, 3989, 4048, 4605, 4648, 4690, 4714, 4732, 4806, 4913, 4927, 5070, 5137, 5164, 5270 5839, 6101, 6169, 6565, 7885, 7666, 7691, 7810.

Die Berechnung dieser Curvenpunkte ist grösstentheils von den Herrn F. K. Ginzel und A. Stein maszler, ausgeführt worden und ebenso die weiter unten erwähnten Zusatzrechnungen bezüglich jener Finsternisse, für welche die Hauptpunkte der zwölfzölligen Curve zu ermitteln waren.

Für jene Curven, die statt des Mittagspunktes nur einen Mitternachtspunkt (•) besitzen, wurde derselbe Vorgang wie oben eingeschlagen, nur dass die so ermittelten Curven relativ häufig zwei naheliegende Punkte zeigten, für welche in ähnlicher Weise, wie dies oben auseinandergesetzt wurde, Abhilfe geschaffen wurde. Für jene Curven, für welche der Mittags- oder Mitternachtspunkt imaginär wurde, sind zur Bestimmung der Lage eines Kreisbogens zu wenig Bedingungen vorhanden. Um aber auch hier den zu zeichnenden Verbindungsbogen der Curve der Centralität möglichst nahe zu bringen, wurde für einen passend gewählten Stundenwinkel oder geographische Breite ein nahe in der Mitte gelegener dritter Punkt ermittelt, der zur Bestimmung des Kreisbogens diente; doch sind solche Punkte in der Karte nicht besonders markirt worden. Die bezüglichen Finsternisse hier hervorzuheben, erscheint unnöthig, da dieser Vorgang bei allen Finsternissen, deren Mittags- oder Mitternachtspunkt imaginär ist, und die auf der nördlichen Hemisphäre sich zeigen, befolgt wurde.

Ganz dasselbe Verfahren wurde für jene Curven eingehalten, für welche die Grenzeurve von 12 Zell (südlich) berechnet wurde, und die Finsternisse in der Karte nicht weiter von den übrigen unterschieden. Von den letztgenannten Finsternissen werden viele sehr klein; man hat bei diesen zu beachten, dass das Gebiet der Siehtbarkeit auf der Seite der Convexitit zu suchen ist.

Eine derartige bildliche Darstellung, welche die Kosten des vorliegenden Werkes wesentlich erhöhte, dient wohl nur zur Leitung bei historischen Untersuchungen, hat daher für Finsternisse, die sich auf der südlichen Halbkugel allein abspielen, keine wesentliche Bedeutung; ich habe mich daher entschlossen, nur jene Curven einzutragen, die nördlich über den — 30. Breitegräd ansteigen; es kommen daher auch Bruchstücke von Curven, soweit dieselben in das Bereich der Karten fallen, zur Darstellung. Manche der Curven erscheinen durch die Grenze der Karten in zwei Theile zerfällt; jeder dieser Theile erhielt die ihm zukommende Bezeichnung. Ausgeschlossen von der Darstellung wurden jene wenigen, kaum in Betracht kommenden Curven, die, ohne dass einer ihrer Hauptpunkte in der Karte liegt, mit einem geringen Theile ihres Zuges dennoch in das Gebiet der Karte gelangen.

Die Curven wurden mit grosser Sorgfalt von Herrn J. Strobl in Karten eingezeichnet. Die Übertragung dieser auf den Stein wurde zwar in ziemlich befriedigender Weise ausgeführt, doch ging ein Theil der Genauigkeit, welche das Original aufwies, verloren. Es würde die Kosten der Iconographie wesentlich erhöht haben, hätte man durchaus die in den Zeichnungen des Herrn Strobl erlangte Genauigkeit erreichen wollen. Da aber diese Karten nur den Zweck haben, einen Überblick zu gewähren, und der Verlauf der Curven, besonders in jenen Theilen, welche den berechnoten Hamptpunkten fern liegen, ohnedies häufig genug ziemlich von der Wahrheit entfernt ist, babe ich mich begnügt, in den Karten eine solche Annäherung als ausreichend zu betrachten, bei der keine Abweichung, im grössten Kreise gezählt, mehr als einen Grad beträgt.

I.

Canon der Sonnenfinsternisse.

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		A 37's Will flood scientists and addition comprohession of action floor promised and for floor action for		**************************************	Carre	martin - Babba, (Philips, Address of the control of	Company of the Compan	ng nga a agang sa ababasa at sa da da gang sa	of a transmission of the	***************************************	E discharge discharge a color		The second control of the second sec	(t r a	d [0		And a second second
ı	288°78	-0'0068	g·7418	225°49	86°58	9.5263	g·9884	9.9740	9,,3584	g,,3918	9 9864	103°6	+ 12 + 1	3 + 71	I5	+138	14	y.:#i
3	30'37	-0'3916 +0'7170	9.7151	212'18	87.06	0.2111	9.9830	9.9758	944315	912545	9'9928	105,8	82 + 6	7 99 0 24			8 + 29	2.4
4 5	310,38	-1.1100 -1.1100	9.7629 9.7629	353.00	87.36	9.2003	9.9818	9.9761	9'4535	0.1868	9.9990	73.3		, p. 11	g			$\begin{vmatrix} p \\ p \end{vmatrix}$
6	33'55	+1:4177	9.4018	198.38	88.11	9.2013	9.9795	9.9769	9:4764	9,,0185	9.9976	107.5	166 - - 3	7 104	,	28	6a	$P_{p^{\oplus}}$
7 8 9	157'24 279'92	0.8018	9.7263	148 12	92.94	9.5122	9.9833	9.9756	944341	9.2522	9,0929	TOD.O	+137 - 2	3 164	- 53	116	72	2.
10	314'55	0,1010	9.7529	135.58	93.41	9.5257	9.9881	9.9741	9,,3641	9.3858	0.8868	103.8	20 1	8 + 45	- 8	+104	- 19	₹:ii
11	189'43	0.7950 0.6059	9.7661	123'26	93.32	9:5432	9.9926	9.9718	9,,2623	9.4736	9.9799	101,0	- - 83 - - <i>i</i>	i3 + 14 i6 +174			38 + 25	, , t . I'
13 14	92'51 350'32	+1.4620	9,4039	269.29	89.89	9'5973	9.9929	9.9631	7n6521	9, 5973	0.02031	20.3	person bases	possible possible	***********	participation of the second	\$1000M	$\frac{p}{p}$
		1.2787												er arres				r
15 17 18	175'44	+1.3283 +0.7083 -0.5597	9.7366	257.20	87.87	9.6159	9.9985	9'9594	8,9225	g,, 6068	9.9612	95.2	+140 -	II.	1	124 24		
19	1'49	+0.5003 0.0038	9.7597	245 93	85.95	9'6327	919943	9'9557	9,2056) g,, 6000	9.9625	100.1	62 +	9 2 1 118	- 24	+ 67	x o	1:i1
21						1							j 41 :		ŀ	136		
22	130'89 249'41	+0'9022 +1'4377	9.7116	48.84	83.63	9.6837 9.6837	9.9825	9,9501	9'4449	9'5532	9.9920	72.6)	j 1		(+ 46)		1 1
24 25	91.22 91.22	-1.3804	9'748o	17.30	83'44	9.6852 9.6852	9'9799 9'9493	9'9490	9,4740 9,6593	9 9 . 2 1 o <u>c</u> 9 0 . 2 1 o <u>c</u>	9.9726	f 52.5	33)(-7		Efficient	16	- 44	i
26	319.55	+0.8005	9 ' 7092	192'07	86.34	9.6907	9'9441	9'9402	9,,6780	9,,0680	9 ' 99 70	118.7	7 + 7 +	79 + 54	+ 59	- ·IIo	+ 24	7.
28	300.00	0'1815 0'5576	9.7024	183 83	88 77	9.6941	9.9396	9.9392	9,6927	7 8 4 5 7 9 5	1919997	1110.6	24 ; 5 8 - - ; 6 - - 73 - -	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+ 6	+112	23	2:41
30	329.96	-0.2261	9.7198	175.79	9 x ' 34	9.6930	9 9400	9 9395	9,6912	8.6187	9.0996	rig.	36	6 - 21	39	- 92		
31	240'22 62'75	-1.3920 -1.3492	9.7242	333.60	96 · 36	9.6794	9'9587	9 9436	9.6192	9,13713 58,16794	9.9876	64.6	5		- Production of the Party of th	**************************************	\$-10.00M	$\frac{p}{p}$
33 34	303.09 98.52	+1'4207 -1'2430	9.7586	167.82	96 80 3 93 63	5 gʻ669∠ 3 gʻ688∶	9 · 9689	9 ' 946 <u>5</u> 9 ' 940 <u>9</u>	9,,5625 9,,675	5 9 · 4641 5 9 · 0683	(9.9807 9.9979	118.	1	II II		#1/rest		$\frac{p}{p}$
	282.34	0'7067	9 . 2046	324'90	96.98	9 6730	9 9 683	9 9456	9.5663	9n467	9 . 980	67.3	3 27	52 + 85				
37	277 73	4-0'0077	0 7072	315 32	2 96 7/	1g'6622	9'978	9486	5 9:487:	2 9 " 533"	7 9 ' 9 7 3 1	t 70'9	4 + 64 +	17 - 82	20	136	1-1- 18	1""
38 39	338 6x	o'7168	9.7304	1305'02	2 95 68	3 g · 648:	2 919874	19 952	1 9 3 7 3 1	8 912576:	2 g ' g668	75'	5 - 134 + 2 - 36 + 2 + 82 -	28 + IO	1- 20	y - 58	+ 54	1 141
										1								
42	146.76	-1.3265 +1.3655 +1.2657	9'7556	294'09	94.0	19.632	19 9943	3 9 ' 9 5 5 8	3 9 205	8 9 2 5 9 9 1	6 9 9 9 6 2 6	79'9	9	ma		- Second	2007.10.4	$\frac{p}{p}$
	223.80	-0'6770	9 762	250.83	3 87 . 5	79.564	9 997	9.9686	5 920529	99n543	x 9'97x8	3 96	I 1	33 + 134 18 - 84				1
46	59'25	-0.0048	9 ' 740!	238 ' 5	3 86 7	5 9 5 5 4 4	9 993	9 97 1	5 9,1241	4 9 2 4 8 3 :	2 9 9 7 8	3 100,	5 119 +	10 59	x		, 1	
47 48	209'63 154'91	+o'7170	9 7438 9 7×37	51 60 225 4	5 86 · 5	7 9 535 8 9 526	1 9 990′ 1 9 988	9 9 9 7 2 5	9 9 3 3 5 8 9 3 5 8 9 3 5 8 9 3 5 8 9 8 9 8 9 8 9 9 9 9 9 9 9 9 9 9 9 9	6 9 439 6 9 39 1	9 9 9 9 8 6 4	77	7 + 95 - 6 + 158 +	29 1-152	: 3.	3 147		
49 50	72.20	+1'4583 -1'0440	9.7667	39 5	5 86 · 6	9.21	9.985	9 9 9 9 7 4	9.498	9 9 340	49.889	75	2 -		-	_		$\frac{p}{p}$

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	Nr.	Julianischer Kalender	T $egin{array}{ c c c c c } Julian, & Wel \\ Tag & Zei \\ \end{array}$		Z	ε	P	Q	$\log p$	$\log \Delta L$	$\log q$	u_a'	$\log f_a$	log 7
	51 52 53 54 55	-1185 IX 19 -1185 IX 8	1288 311 14 23	'4 164 '718 '9 344 '230 '3 153 '944	-0.15 +3.08 -0.60	23.850 23.850 23.850	350.330	173.000	0'5999 0'7240 0'7226	9'7541 9'7257 9'7286	8.7501 8.7259 8.7274	0.2282	7.6655 7.6668	9.8837 9.9467 8.4111
	56 57 58 59 60	-1183 I 23 -1183 II 21 -1183 VII 19	1288 665 19 7 1288 842 8 58 1288 990 1 55 1289 019 19 14 1289 167 7 15 11	143.442 292.939 2 322.455 2 104.374	+3.67 +4.42 -0.53	23.851 23.851 23.851 23.851	164'154 195'418 344'741	6.667 162.489 194.604 347.160	0.7411 0.6896 0.7368 0.7433 0.7102	9'7055 9'7641 9'7103 9'7027	8.7093 8.7607 8.7134 8.7072	0.5671 0.5353 0.5678 0.5698	7.6681 7.6708 7.6735 7.6696 7.6655	9"8723 9"7547 0'1710 0"1659 0"1285
	62 63 64 65	-1181 I 1 -1181 VI 28	1289 197 1 6 1289 344 8 2 1289 521 23 56 1289 598 20 52 1289 876 2 6	2 271 077 0 83 198	-1.10 -1.88	23.852 23.852	353.219 180.035 1.268	355.210 178.568 1.572	0 7331 0 6938 0 7446	9.7163 9.7286	8 7 7 5 5 9 8 7 7 5 5 9	0.5535	7.6692 7.6748 7.6644 7.6758 7.6635	o'rree 9'8564 9"803r 7"4777 9'0873
	69 70	-1180 XII 11 -1179 V 7	1290 555 0 56	34.121	-1.88	23.853 23.853 23.853	163·937 195·867 348·300	166·374 198·145 346·087	0.7050	9 7306 9 7450 9 7487	8.7200	0'5611	7 · 6777	9n8285 9'9428 0'1596 0n1413
	72 73 74 75	-1177 IV 16 1 -1177 X 9	1290 732 17 6 1290 909 17 4 1291 086 16 24 1291 264 10 17 1291 440 18 9	207.977 24.051 196.502 13.998 185.174	-2.88 2 -1.05 2 -2.52 2 -0.04 2 -1.93 2	23.854 1 3.854 1 3.854 1 3.854 3	71'492 1 57'044 3 78'622 1 5'717 86'030 1	72.855 56.475 78.074 7.253 83.898	0 · 7391 0 · 6905 0 · 6960 9 · 6960 9 · 7287 9	77059 77639 77006 7581 7190	8 · 7 · 1 0 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.5725 0.5312 0.5751 0.5751	7 · 6773 7 · 6629 7 · 6766	9 '9070 9 '1222 9 '1223
7 7 8	77 78 79 -	-1175 IX 28 1 -1175 II 23 1	291 943 14 13.1	174·208 - 324·279 -	1 29 23 4 35 23	3 854 16 3 854 19 3 854 35	3.997 19 3.137 35	1.358 o 1.746 o 2.714 o	7287 9 7171 9 6953 9 7053 9	7209 8 7350 8 7576 8 7467 8	7206 0 7321 0 7540 0	5584 7 5484 7 5389 7 5474 7	*6680 c	1621 no869
8 8 8 8	4 -	-1173 IT T	292 120 8 37·8 292 297 14 16·1 292 475 0 6·0 292 651 18 58·2 292 829 10 13·3	123'996 +	0.40 23 4.52 23 0.31 23	3 · 853 17 3 · 852 35	1 · 164 17 9 · 688 35	1.441 0.	6900 g.	7635 8 7061 8	7595 o 7099 o 7445 o 7	5348 7 5685 7 5427 7 5556 7	6693 9 6709 8 6680 8	*8774 *8743 *4740 *5851 *8387
86 88 89 90	7	1173 XII 23 12 1172 I 22 12 1172 VI 17 12 1172 VII 17 12	292 976 19 47 7 293 006 6 42 3 293 153 21 27 9 293 183 13 20 8 293 331 11 37 1	261 · 721 + 291 · 472 + 74 · 255 -	0 · 24 23 3 · 53 23 2 · 37 23 0 · 63 23	·851 34. ·851 15. ·851 16.	4 205 343	3'319 o. 3'848 o.	6906 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	7621 8· 7548 8· 7021 8· 7032 8·	7594 o · 7517 o · 7056 o ·	F207 7.	6766 o, 6737 o 6629 o 6654 o,	1292 1302 1825
91 92 93 94 95	— : — :	1170 V 27 12	93 862 9 1 0 94 040 6 34 1		72 23 798 23 72 23	*850 173 *849 359 *849 182	3 996 172 3 965 2 3 634 180	316 0	7329 9.7 7136 9.7	7168 8· 7370 8· 7435 8·	7170 0. 7361 0. 7397 0.	5572 7. 5547 7. 5421 7. 5702 7.	6623 9. 6778 7n 6621 9n 6779 9.	7503 4975 3704 8561
96 97 98 99 100	-1 -1	1169 V 17 129 1169 XI 10 129 158 IV 6 129 168 IX 29 129 167 III 26 129	94 217 0 21.2	43 224 -2 317 295 -2 5 185 +0	'42 23' '96 23' '93 23'	848 191 848 14 848 170	'405 190 '747 14 '457 172	1390 016 1634 017	0924 9 7 7445 9 6 7013 9 7	525 8 9 994 8 9 528 8 9 269 8 9	7576 0.5 7063 0.5 7488 0.5	5316 7.6 5764 7.6 5383 7.6 587 7.6	5621 gn 5776 o 5644 gr	1482 9187 9543
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						y	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	003 9	005 70	SIII V	005 9		λΙφ	G r a	φλ	φ	
par insiste	e de contra de la compansión de la contra del la	Constitution of the Consti	V MELTING METER M	And the section of the party of the section of the sec	A publish remains Agent rise.	n tier i median i serve gree had elemente gree i del elemente gree green de elemente	To find the bound of the property of	CONTRACT DESCRIPTION (AND LABOR.)	A CONTRACTOR OF THE PERSON OF A	dry different States of will action with 198	gyana yanin muun ha, gye, ink di ndanas. Valdadiseen diinkki kudhuski asalimisch	A Company of the Comp					
52	214'80	+1.4107 +0.7620	9.7562	353'41	30.41	9,4961	9'9779	9.9776	9'4929	8n5781	9.9997	71.0	+ 73 +	32 139		6 8	$p_{t^{*}}$
53 54 55	277'73 32'95	- 018845 - 010258	9'7278 9'7307	340.03	01.02	0.2000 0.2010	0.0801 0.0200	9.9769	9:4756 9:4721	9°0276 920409	9 · 9975 9 · 9974	72.6	+ II - 97	44 + 74 - 16 - 33 - 8 - 79 +	62 + 129 5 + 27	- 78	y-tit
		0.7452													61 24	32	
57 58	312.81	+0'5685 +1'4827	9.4153	135.82	91.60	9:5257 9:5785	0.0000 0.0840	9'974¤ 9'9664	923683 8.8415	9:3818 9:5710	9.9676 9.9870	103 9 85 7	- 37 +	47 + 51 +	50 +121	- - 20 	
59 60		1'4653 1'3443													general general general	******	$\frac{p}{p}$
		-1.2882 -10.7185												42 + 60 +	23 +109	 + 4x	p_{p^*}
63 64	182.04 181.02	-0'6354 -0'0030	9.7607 9.7185	80°22	88.30 88.30	9.6112 9.6157	9.9982	9 9595 9 9595	8.8025 819184	9:6058 9:6067	9 9614 9 9613	95°2	+131 +166 +	39 +179 - 5 -132 -	16 130 24 66	32 5	r t#
65 66	0.31	_												30 12	67 + 89	45	
	229.66	0.8766 1.4420	9.7326	58 · 60 209 · 38	84·81 83·36	9·6433 9·6766	0.00x1	9'9534 9'9444	9 3252 9 6020	9.5862 9.4081	9'9651 9'9651	76.8	3r		87 - 99	- - 63 	.1.
ճց 70	198.65 232,16	1'0232 1'0232												gab tribut	pyronografia yroniary	Brighton)	1) 1)
71 72	81 · 87	+0.8072 -0.2516	9.766a	200'38	84 47	g·6859	9,9450 9,8450	9'9417	g,6499	912781	9.9920	62.4	-ro5 +	76 - 70 +			
73 74	333.12 60.00	0'1325	9.7028	10.08	86.39 86.39	9.6899 9.6916	9.9437	9'9399	9,6794 9,6810	920602 8 9904	9'997¤	Q1.3	- 125 + - 41 +	36 - 67 + 1 + 20 +	2 6	+ 58	t^{ii}
75	92.71	1'4450											159 -			0.3	'n
76 77 78	173.98	11'2912	9.7379	2.71	89 15	9.6894 9.6774	9.9408	9'9406	9'6887 9'6176	8.4236 9.3676	9.9878	3 50.8 3 115.2	2	agants pathosas		Annual	$\frac{p}{p}$
79 80	31'15 225'52	1.2215	9.7487	333'63	96.42	9.6908	9.9407	9'940	9,6210	923731	9.9875	64'	5 -151 -	69 21 -	70 + 45	- 23	$\frac{p}{r}$
81 82	20'50	0'0208	0 708	1 324 60	nla6 aa	a 6728	9085	19 945	9'5049) gn4095	10.0803	31 07.7	4 - 98 -	65 + 57 +	· 19 + 25	1- 20	7"
83	181'30	1000385	9.7502	136'64	96.79	9.6623	9'9773	9'948	3 924986 3 914843	9'5254	9 974	71.00	1 -159 +	23 -105 +	22 - 124	- - 10 - - 56	1:4
			1	1		1	1							30 + 23 -			p
86 87 88	273'64	1 · 3290 + 1 · 3465 + 1 · 3497	9.7568	3 304 87	95.64	9.5908	9 9999	9 9 9 5 2	1 8 . 3078	3 9 · 5 9 0 2	9,364	75 2 88	3	arrigar - garrinad	annumber Annue Ann	distributes biologicality	$\frac{p}{p}$
89 90	16'40	-1.223 -0.6781	0.7052	2 116 3	7 04 43	19 635	5 9 9 9 9 3 1	9.955	1 9 / 2 4 0 4	1 9 . 2000	0 9'9033	glioi.	6 - 86 -	37 + 2 ~	- 6 ₅ -l- 9 ₅	- 4x	$t \frac{p}{t}$
	182'12	+0.5627	9.718	75.2	88.02	9.5716	9.9988	9'967	8 9468 5 92042	9 5599 7 9n 544	9'969	84° 6 96°	6 +100 + 8 +111 +	27 +176 + 6 +171 -	- 56 9 <u>c</u>	+ 37	7""
92 93 94	317.34	0'2346	9'745	6 63 6	2 87 02	9 5539	9 ' 995	19 970 19 971	4 9 · 1766	5 g 2 4 8 3	9.975	0 100.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21 + 44 53 + 85	- 51 105	+ 33	
95	l	+1.2223					.] .	ĺ						74 180		50	\int_{-t}^{p}
96 97 98	275.46	+1.4067	9.701	5 225 0	1 86 ' 57 5 80 ' 31	9.526	9 9 9 9 8 8 2	2 9 ' 973 3 9 ' 977	9 9 n 3 0 2 i 5 1 9 1 4 9 3 i	8 9n 389 2 8 562	7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	7 71.	8 - 47 -	38 + 23 -	- 67 -131 - 63 +113		p_{p}
99 100	40.68	0'0002	0.7200	174.76	000156	5 a 496	19 977	7191977	5 9n494	4 8 477	0 9 9 9 9 9	gliog.	2 117	46 - 49 13 - 144	- 70 + 24 + 3 - 8:	4 - 82	

Nr.		T	L'	Z		Ъ			log				
	Julianischer Kalender	Julian. Welt- Tag Zeit	L	Zı	ε	P	Q	$\log p$	$\Delta ilde{L}$	$\log q$	u'u	$\log f_u$	log y
101 102 103 104 105	-1166 III 16 -1166 IX 8 -1165 II 3	1295 251 2 7.9 1295 427 17 20.4 1295 575 9 38.0	164°912 344°123 154°343 303°879 333°175	+3'10 -0'14 +4'32	23 847 23 847 23 847	187 · 187 6 · 346 163 · 851	356°321 188.194 6.441 162.098 193.944	0.7420 0.6894	9'7048 9'7641	8·7505 8·7084 8·7608 8·7143 8·7076	0.5429 0.5669 0.5360 0.5661 0.5683	7.6735 7.6668 7.6720 7.6721 7.6682	9,1906 9,8371 9,7308 0,1782
106 107 108 109 110	-1165 VIII 29 -1164 I 23 -1164 VII 19 -1163 I 12	1295 929 16 19.5 1296 284 5 34.1	143.840 292.928 104.428 282.180	+0'26 +3'65 -0'51	23.848 23.848 23.849	14.554 171.804 352.475	346 · 539 16 · 564 169 · 359 354 · 392 178 · 530	0.7136	9.7412 9.7532 9.7378 9.7148 9.7595	8 7381 8 7496 8 7360 8 7158 8 7567	0.5462 0.5414 0.5517 0.5603 0.5401	7.6668 7.6707 7.6735 7.6655 7.6748	0,1477 0.0983 9.8655 9,8492 7.9199
111 112 113 114 115	-1162 I 1 -1162 VI 27 -1162 XI 22 -1162 XII 22	1296 953 11 41·3	271,496 82,943 230,489 260,685	+1 ·42 -1 ·89 -2 ·59 +0 ·12	23.850 23.851 23.851	187.867 8.412 163.946 195.837	188.680 6.750 166.360 188.121	0.7365 0.7204 0.7078	9.7620 9.7117 9.7290 9.7434	8 . 7595	o'5674 o'5392 o'5608 o'5595 o'5503	7.6644 7.6758 7.6635 7.6779 7.6768	8.6271 9.8248 9.8996 0.1602 0.1419
117 118 119 120	-1161 VI 16 -1161 XI 12 -1160 V 7 -1160 X 31	1297 169 17 24·3 1297 318	72 502 219 170 34 494 207 664	-2:43 -2:90 -1:89 -2:88	23.851 23.851 23.852 23.851	16.916 171.452 356.186 178.546	345 · 287 14 · 480 172 · 715 355 · 778 177 · 885	0.4121 0.420 0.420 0.429	9.7378 9.7050 9.7643 9.7009	8.7100 8.7592 8.7071	0'5383 0'5458 0'5733 0'5307 0'5753	7.6621 7.6628 7.6777 7.6624 7.6773	0,0395 0,1769 9,2110 9,1421
122 123 124 125		1298 026 2 26.0 1298 174 18 47.8 1298 204 7 5.8 1298 351 0 28.7	196 302 345 829 14 257 155 698	-2.52 +2.95 -0.06 -0.21	23.821 23.821 23.821	343.646 13.626 162.534	6.544 183.744 345.732 16.030 161.104	0.7276 0.7299 0.7186 0.6944	9'7195 9'7385 9'7585	8 · 7216 8 · 7194 8 · 7306 8 · 7551	0.5584 0.5487 0.5393	7.6637 7.6724	9.6258 9.7396 0.1775 0.0887 0.1698
127 128 129 130	-1157 III 6 -1157 VIII 30 -1156 II 23 -1156 VIII 19	1298 528 21 19.4 1298 705 16 50.6 1298 882 21 37.4 7 57.1	334 990 145 214 323 988 134 744	+3.80 +0.21 +4.35 +0.40	23.851 23.851 23.850 23.850	351 · 570 170 · 725 359 · 220 179 · 051	352:037 171:457 357:789 181:345	0.7438 0.6901 0.7395 0.7060	9'7018 9'7630 9'7073 9'7465	8.7594 8.7105 8.7432	0:5692 0:5359 0:5669 0:5445	7.6709 7.6694 7.6693	0n0811 9n9077 9.8953 8n8713 8.9230
134 135		1299 414 17 30·3 1299 562 4 36·3 1299 591 15 6·2 1299 739 3 57·3	124 115 272 874 302 450 84 689	+0'31 +1'58 +4'24 -1'80	23.850 23.849 23.849 23.849	187 · 383 344 · 123 15 · 473 165 · 002	189°532 343°334 13°660 164°617	0.7296 0.6901 0.6969 0.7445	9'7199 9'7627 9'7560 9'7022	8.7201 8.7597 8.7526 8.7058	0.5587 0.5388 0.5407 0.5663	7.6680 7.6757 7.6724 7.6637	9#8364
137 138 139 140	-1154 XII 23 -1153 VI 18 -1153 XII 13 -1152 VI 6	1299 916 20 28 5 1300 093 6 36 1 1300 271 9 7 9 1300 447 16 11 4	262 · 141 74 · 053 251 · 230 63 · 721	+0'29 -2'38 -0'95 -2'70	23 · 849 23 · 848 23 · 848 23 · 846	352.030 173.128 359.968 181.771 7.611	353'429 171'088 2'386 179'436	0.6940 0.7316 0.7147 0.7087	9.7585 9.7183 9.7357 9.7449	8.7561 8.7182 8.7349 8.7411	0.5417 0.5558 0.5552 0.5413	7.6765 7.6629 7.6773 7.6623	9.8338 9.8074 7.4595 9.1966
142 143 144 145	-1151 V 27 -1151 XI 20 -1150 IV 17 -1150 X 10 -1149 IV 7	1300 802 7 47 6 1300 979 14 34 9 1301 127 17 23 1 1301 303 22 45 7	53 · 643 228 · 500 15 · 687 186 · 833	-2.71 -2.68 -0.21 -2.06	23 845 23 845 23 845 23 845	14.722 169.684 350.006	189.660 14.498 171.747 347.642	0.6919 0.7445 0.7024 0.7213	9.7630 9.6995 9.7516 9.7284	8.7580 8.7064 8.7475 8.7286	0'5313 0'5766 0'5384 0'5586	7.6621 7.6779 7.6636 7.6758	9 8509 9 9517 0 1474 9 9534 9 9586
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211 212 213 214 215	-1123 XI 10 -1122 V 7 -1122 X 1	1311 020 8 1311 196 19 1311 374 21 1311 521 17 1311 551 5	9'9 35'13 32'9 177'72	0 -2'94 5 -1'91 4 -1'50	23 · 840 23 · 840 23 · 840	185.863 11.937	183'582 14'309 160'836	0.7217	9.7231 9.7298 9.7598	8.7275	0.5357 0.5626 0.5500 0.5398 0.5468	7.6625	9'4389 9n7322 0'0353 0'1793 0n0749
216 217 218 219 220	-1121 IX 21 -1120 III 16 -1120 IX 10	1311 699 11 1311 876 9 1312 053 11 1312 231 0 1312 407 18	41.6 167.09 53.4 345.35 2.9 156.46	9 -0.85 5 +2.99 2 -0.24	23.84	6 358 03 6 358 03	2 171.062 8 356.423 4 180.637	o. 6909 o. 7377 o. 6909	9.7014 9.7622 9.7100 9.7433 9.7352	8 · 7587 8 · 7120 8 · 7405	0.5379 0.5638 0.5478	7.6667	9#9732 9'9245 9#2700 9'1877 9'7526
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226 227 228 229 230	-1116 I 2 -1116 VI 28 -1116 XII 23	1313 618 6	11.6 273.55 46.9 84.62 15.6 262.36	$\begin{vmatrix} 4 & +1.65 \\ 3 & -1.76 \\ 3 & +0.35 \end{vmatrix}$	23.84 23.84 23.84	4 359 85 3 180 10 3 7 52	8 177.883	0.7175	9.7071	8 7320 8 7441 8 7118		7.6758 7.6636 7.6767	
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24 24: 24: 24: 24:	2 -1110 II 2 3 -1110 VIII 2 4 -1109 II 1	4 1316 040 6	0 10'3 176'7; 5 25'8 325'5; 4 18'2 136'4; 5 56'4 315'0; 4 57'9 125'4	36 +4·3 09 +0·4 05 +4·5	3 23 84 0 23 84 3 23 84	1 170.74 1 350.65 1 179.06	.0 168 349 7 352 32 8 178 02	0.6018 0.4348 0.4008	3 9.7427 5 9.7103 8 9.7618	8.7400 8.7130 8.7584	0°5465 0°5654 0°5366	7.6746 7.6693 7.6696 7.6681	9'9144 9%9458 8'0900
24 24 24 24 25	7 -1108 VII 2 8 -1108 XII 2 9 -1107 I 2	3 1316 394 23 9 1316 571 6 4 1316 719 22 3 1316 749 13 9 1316 896 6	5 42 0 114 5 2 51 9 264 0 3 9 3 293 9	33 +0'0 89 +0'5 63 +3'7	5 23.84 2 23.84 3 23.84	2 163.89 2 195.43	4 · 250 5 · 166 · 200 2 · 197 · 810	5 0.7333 5 0.7243 5 0.7126	9 9 7 1 5 6 9 9 7 2 4 7 9 9 7 3 9 5	8.7167 8.7252 8.7376	0.2606 0.2611 0.2200	7.6666 7.6766 7.6736	9'7518 0'1554 0n1352

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	173.20	o · 6436	9.7166	90.97	184,08	9'5937	0.0000	0.0537	9//3155	9 3930	9.9649	103.0		37	173	- 63	- 88	36	r# P P
205	245.68	I .3773	9.7426	270'60	0 0 0 0	9'5955	0.0000	9 9034	λ 2000	9"3933	9 9034	l ag a					page -	pp. 4-4	2)
207	295 62	-1.2377 -1.3543 -10.8194	9 7439	80.1	7 88'38 6 82'#6	0.6823	0.0816	0.0408	0.451	925500	9.9706	107 6	114	1	82	J- 38	- 31		$\frac{p}{r^{*}}$
208		0'4737 0'1471												- 44 + 28		- 11	7 9	8 13	-1-
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214	256.88	3 1.188	9.752	0 200'2	4 84.5	5 9 084	9.952	19-942	3 9 10 40	3 9 1 2 7 3	9 99~	,		(4) p. 16-160		*	granes	,	$\begin{bmatrix} p \\ \vdots \end{bmatrix}$
216	328.3	-0'940 +0'840	4 9.764	3 170.7	3 33.9	2 6 . 000	0 9 942	79 940	4 97 002	5 9 9 3 3	5 5 5 5 5	61.	. 62	30	7	79 18	+ 95 + 110 + 64	41 28 18	7* 'r
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224	327.3 28.0	7 -0.203	9 759	298	30 94 7	2 9.638	5 9 9 9 9 9	9 9 9 9 5 4	9, 278	33 9 592	8 9 963			1		6g		30	1.1
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234 235	t go.s	47 -1-0 · 30:	24 9 ' 73	37 215. 44 32.	34 86 ·	08 0 . 2 r 84 0 . 2 r	03 9 . 98 03 9 . 98	44 9 9 97 37 9 97	52 9#41 50 9 '43	97 9#29	31 9 99	29 74	1 167	-+- 3	106	+ 29	- 34	1-3	3 114
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24	153.	14 1 . 54	73 9 73	78 140	57 93	33 9 . 52	21 9.98	558 9 97	44 9#3	9929 33	90 9 94	00 108	3					jeure e	$ p_{\perp}$
24 24 24	2 64'	96 +1.19 40.82 710.88	12 9 7	147 318	47 93	37 9 5	33 9 9	277 0 '0'	727 0 3	021 0'4	1510'98	24 102	1 + 5	5 4	9 - 70 7 + 108 7 + 80	3 4	8 14	5	071 "
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256 257 258 259 260	-1104 V 18 -1104 X 19 -1104 XI 10	B 1317 950 4	4 4 9 45° 2 17°1 188° 3 58°4 218°	398 —2·62 339 —2·45 331 —2·16 347 —2·95 714 —0·79	23 · 845 23 · 845 23 · 845	185.863 11.053 161.930 193.723 349.415	183.537 13.400 160.807 191.682 349.538	0'7240 0'7233 0'6919 0'7004 0'7447	9.7247 9.7281 9.7607 9.7512 9.7016	8·7254 8·7259 8·7577 8·7489	0'5619 0'5508 0'5402 0'5464 0'5672	7.6779 7.6621 7.6759 7.6776 7.6643	9,7310 0.0040 0.1816 0,0736 0,0067
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265 267 268 269 270		5 1319 347 15 9 1319 524 17 1 1319 672 22 9 1319 849 3	7 21'0 145' 2 29'0 295' 3 27'9 105'	+3.82 +0.21 +3.82 -0.43	23.844 23.843 23.843 23.843	343'464 14'171 193'618 351'598 170'766	343°031 12°663 193°877 353°265 168°544	o:6896 o:6944 o:7445 o:6966 o:7272	9.7639 9.7592 9.7007 9.7561 9.7229	8·7602 8·7549 8·7057 8·7530 8·7223	0.5361 0.5366 0.5716 0.5411 0.5558	7.6720 7.6681 7.6708 7.6734 7.6656	0,1419 0'0812 0,1143 9,8592 9'9305
271 272 273 274 275	-1098 VII 20 -1097 I 3 -1097 VI 20 -1097 XII 23	1320 735 14	4 12.8 95. 5 20.6 273. 6 21.2 84. 4 48.0 262.	28i — 1 '08	23.842 23.842 23.841	359'711 '79'337 '7'414 187'994 14'587	2°101 177°178 8°744 187°576 14°010		9.7494 9.7063 9.7641	8.7305 8.7455 8.7109 8.7594 8.7068	0'5562. 0'5401 0'5712 0'5314 0'5752	7.6746 7.6645 7.6758 7.6636 7.6767	8,4195 8,7654 9,8475 9,8315 0,1428
276 277 278 279 280		1320 883 15 1320 912 23 1321 050 0 1321 238 1 1321 414 12	3 29 0 74 0 19 6 220 0 1 34 8 36 0 2 22 2 209 0		23.840 23.840 23.840 23.839	167 158 196 651 349 904 175 842 357 802	169 426 198 300 347 475 177 976 356 207	0.6955	9.7473 9.7578 9.7329 9.7205 9.7568		0.5347 0.5570 0.5552 0.5429	7.6621 7.6628 7.6777 7.6624 7.6773	0.0517 0n1523 9n9590 9.5882 9n2772
283 284 285	-1093 IV 17 -1093 X 11 -1092 III 7	1321 946 5 1322 123 18 1322 271 0	5 35 5 15 42 9 187 187 187 187 187 187 187 187 187 187	21 -0 · 14 34 -2 · 12 26 +3 · 75	23 · 838 23 · 838 23 · 838	13.602	184.604 6.213 190.644 15.844 167.868	0.0897	9.7029 9.7630 9.7075 9.7475 9.7445	8.7064 8.7607 8.7100 8.7454 8.7414	0.5390 0.5632 0.5473	7.6628 7.6767 7.6636 7.6758 7.6679	9.75902 9.6818 0.0557 0.0739 9.9366
286 287 288 289 290	-rogo VIII 9	1322 625 15 1322 802 12 1322 980 7 1323 156 13	7 5 325 9 2 1 9 136 9 7 44 5 315 5 3 55 8 125 1	18 +4.31 30 +0.40 17 +4.52 89 +0.36	23.838 23.839 23.839 23.839	357°765 186°894 5°550	351.789 177.700 357.484 188.154 3.572	0.7383 0.6914 0.7445 0.6936 0.7319	9'7625 9'7010	8.7123 8.7588 8.7061 8.7565 8.7180	0.5354 0.5707 0.5378	7.6710 7.6693 7.6696 7.6708 7.6681	9n9667 9'0685 9n3334 9n7708 9'7152
295	-1089 II 3 -1089 VI 30 -1089 VII 29 -1089 XII 25	1323 659 9	38.8 86.2 550.3 114.6	24 +4·36 93 -1·63	23.840 23.840 23.840	195'154	166.069 197.556 342.252 11.590 172.116	0.7257 0.7134 0.6985 0.7089 0.7424	9.7555	8.7363 8.7511 8.7407	0'5362	7.6756 7.6723 7.6637 7.6666 7.6766	0'1694 0n1288 0n1363 0'0881 9'9211
297 298 299	-1088 VI 19 -1088 XII 13 -1087 VI 8 -1087 XII 2 -1086 V 29	1324 013 9 1324 190 23	0.6 252.4 11.6 66.1 18.0 241.1	702 50	23.841 23.841	1'413	3.478 183.201	0.411	9.7520 9.72 5 2	8·7090 8·7474	0.2608	7.6625 7.6776	9:7926 9:1875 9:0919 9:7300 9:9695

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256 257	237.81 240.96 220.12	0.5382 1.0052 1.1847 1.0155	9 · 7269 9 · 7301 9 · 7626	217 · 99 34 · 55 186 · 46	83'02 83'11 88'03	9.6694 9.6714 9.6876	9.9716 9.9680 9.9423	9.9466 9.9461 9.9412 9.9443	9#5442 9*5683 9#6841	9,,4902 9,4602 8,,7929 9,4041	9.9852 9.9813 9.9983	111.6 62.3 118.6	. . 52	10		53	148	50	r P P P P
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266 267 268 269 270	46.54 76.23	-1:3863 -1:2057 -1:3010 -0:7232 -0:8522	9.7612	341.6	3 95 · 00 2 96 · 27	9 · 6846	0 9502 0 9 9577	9'9420 9'9434	9,6550 9,6240	9,2335 9,3606 0,5623	9 · 9690 9 · 9883	115.6	5 98	56 60				28	ا ^{اد} ر (
271 272 273 274 275	34 ' 42 46 ' 45	0'0263 - -0'0583 - -0'7038 0'6784	9.7515 9.7662	287.4	5 92 · 9 9 92 · 9	9 · 6253 1 9 · 6223	2 0 · 996; 9 9 · 997 3 0 · 999;	9 9574 9 9579 9 960	9,, 1006 9 9 062 3 8,, 733	5 9 · 6049 5 9 · 6049	0 0 0 0 0 0 1 (0 0 0 0 0 1 (0 0 0 0 1 (97 9 82 8 93 4	3 98 1 + 32	+ 10 + 34 - 35	49	+ 27	+ 83 + 27 - 5 +133	+ 40	1 /di 5 /di
280	171'07 190'28 206'80 8'99	- -1 · 1265 1 · 1200 0 · 3875 0 · 1893	9'7597 9'7359 9'7227 9'7589	86.9 228.5 44.5 215.7	6 89 5. 3 86 6 9 86 8	1 9 59 x 9 3 9 5 5 2 4 7 9 5 5 1 4 9	9 9 19999 7 9 1988 7 9 1988	9 9 9 9 6 4 4 9 9 9 7 3 1 9 9 7 4 7 9 9 7 5	0 8 · 281 1 9 / 337 2 9 · 364 4 9 / 4 · 5	1 9 59 1. 9 9 4 1 8 6 9 5 3 8 3 1 9 2 9 7	1 9 9 9 4 1 9 9 8 4 2 9 9 8 6 7 9 9 9 1	2 105. 2 20. 3 103.	8 0 72 2 87 4 72	+ 4	10	23	133 61	+ 33	5 1 ⁻¹⁵ 6 1 ¹⁶
282 283 284 285	242.13 260.73 29.82	3 -0.3892 3 +0.4807 3 -1.1367 4 +1.1855 3 +0.8642	9 7 7 6 5 9 7 7 4 9 5 9 7 7 4 6 5	189.5 189.5 189.5	0 88 · 0 3 88 · 9 7 92 · 7	3 9 5 5 10 6 9 4 9 9 5 9 5 5 10	9 9 9 8 0 9 9 9 7 7 9 9 9 9 8 2	8 9 970 9 9 977 9 9 977 2 9 975	9 9,404 1 9.473 1 9,493 9 9.447	8 9 · 031 2 8 / 741 2 9 / 210	3 9 997 0 9 999 2 9 994	72. 73.	6 2 5 +111	+ 43	+171	-l· 5	5 - 139	7	3 P
287	42 86	3 -0.9262 5 +0.1171 2 -0.2155 2 -0.5899 1-0.5190	9.764	2 126 · 6	993'3	4 9 · 5 2 1 8 9 · 5 3 5	3 9 9 9 9 1 4 9 9 9 1	79'974 49'972 40'072	5 9 385 9 9 296 4 9 295	0 9	4 9 · 982 2 9 · 982	3 101.	9 62 1 17	1 45	- 2 + 73	5	4 + 53	2 5 - 2	3 /* 3 / 1 /*
292 293 294 295	132.44 29.71 159.31	5 +1 4770 4 -1 3453 1 -1 3687 1 +1 2250 20 8338	9 740 9 757 9 746 9 704	0 294 9 4 73 0 0 103 0 2 249 8	7 92 · 9 1 87 · 1 6 91 · 7 1 86 · 6	3 9 557 5 9 621 9 9 575 0 9 627	9 9 9 9 9 5 8 9 9 9 9 7 1 9 9 9 9 8 1 9 9 9 9 6	5 9 9 9 5 9 2 9 9 5 8 6 9 9 6 6 1 9 9 5 7	5 9 158 1 9 048 9 8 2897 0 9 226	1 91520 7 9*605 7 9*565 8 91604	4 9 9 9 7 4 7 9 9 6 1 3 9 9 6 8 2 9 9 6 1	7 81 4 83 5 94 7 98	9 3		II.				13 7#
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306 307 308 309 310	1084 1083 1083 1082 1082	III 27 IX 20 II 15	1325 1325 1325	578 755 903	9 3 23 5 14 4	19'2 52'2 45'2	355'94 167'46 316'86	7 -1.55 +1.95 8 -0.87 0 +4.51 +2.99	23.842 23.842 23.842	5'000 185'720 343'09	180°219 2°547 187°599 1 342°790 2 12°189	o'7135 o'7340 o'68g3	9.7389 9.7134 9.7642	8 7381 8 7355 8 7157 8 7601 8 7557	0.5511 0.5466 0.5658 0.5354 0.5353	7.6748 7.6654 7.6736 7.6707 7.6667	9.2951 9.6525 9.7305 0.1510 0.0624
311 312 313 314 315	-1081 -1081 -1080	II 5 VII 31 I 25	1326 1326 1326	258 434 612	10 18	52·7 42·1 44·6	306.38 116.12 305.65	3 -0.24 0 +4.38 7 +0.11 5 +3.83 7 -0.41	23.84 23.84 23.84	351'31 170'09 359'49	1 193 351 2 353 68 8 167 831 9 1 869 3 176 537	0.6978 0.7258 0.7204	9.7550 9.7246 9.7297		0'5411 0'5557 0'5562	7.6721 7.6668 7.6734	onioi3 9.8748 9.9591 8.6599 9.0813
315 317 318 319 320	-1078 -1078	VII g	1327 1327 1327	143 320 468	14 22 22	1'0 44'3 31'6	95°50 273°1′ 57°4	77 +1.6	23.83 23.83 23.83	9 187°21 8 14°46 8 166°28	8:46; 5:186:95; 66:13:77; 88:168:60; 197:59	0.6902 4 0.7434 9 0.7081	9.7643	8 7597 8 7070 8 7417	0.5318 0.5745 0.5411	7.6645 7.6758 7.6622	0.0810 0.1380
321 322 323 324 325	1078 1077 1076 1076	V 20 XI 12 V 2	1327 2 1327 8 1328	823 999 177	21 11	18.4 12.1	47'1 220'6 36'5	29 -2·5 13 -2·5 33 -2·9 -1·9 -2·9	0 23 83 4 23 83 9 23 83	7 174 95 7 357 80 6 183 14	3347.48 57 177.02 04 356.29 183.58 6.29	7 0.7313 3 0.6948 6 0.7445	9 7190 9 7577 5 9 7024	8.7188 8.7554 8.7060	0.5560 0.5655 0.5655	7.6624	9n276 1 9n48 1 3
326 327 328 329 330		X 2 III 1 IX 1	8 1328 1 1329	70g 856 033	3 7 3 19	21.0 53.8	198 9 346 9	84 —2 6 96 +2 8	8 23 83 6 23 83 4 23 83	6 13.5; 6 169.6; 6 349.8	189.69 32 15.81 33 167.31 36 351.32 09 177.31	4 0.705 9 0.707 1 0.739	3 9 ' 746 I 4 9 ' 746 I I 9 ' 707 I	8 7442 8 7426 8 711	0 · 5488 6 0 · 5437 4 0 · 5685	7 6767	0'0730 9'9605 9n9837
331 332 333 334 335	-1072 -1072 -1071	VIII 1	5 1329 9 1329	565 747	21	20.6	326'3 135'9	43 +4 2 20 +0 4 86 +3 0	23.8 24 23.8	35 186 4 36 5 0 36 163 6	62 187.82	18 0.130 19 0.130 56 0.094	5 9 759 9 9 718 0 9 721	8 755 1 8 719 9 8 722	8 0.2923	7 7 6694	9'6710 6 0'174 7
336 337 338 339 340	-1071 -1070	VIII VI 2	9 133	0 24	6 6 4 17	32'4 48'6	1 125 2 5 275 0	10 -0.6 180 +0.3 142 +1.8 103 -1.6 111 +0.4	39 23.8 31 23.8	37 13'3 37 171'1 37 351'8	56 341.59 30 11.02 51 171.88 71 352.26 19 177.13	16 0'707 36 0'742 55 0'690	6 9.745 9 9.701 2 9.764	3 8·742 6 8·707 4 8·759	5 0.231	4 7 · 6683 0 7 · 6757 3 7 · 6637	0.0583 7 9.9278 7 9.8385
34 ¹ 34 ² 34 ³ 34 ⁴	2 — 1069 3 — 1068 4 — 1068 5 — 1068	XII I XI XII	3 133 8 133 2 133 2 133	0 95 1 13 1 27 1 30	2 20 0 17 7 20 7 7	48 : 47 : 43 : 43 :	252.3 66.3 211.3 241.3	341 -2:5 35 -2:5 317 -1:5	36 23.8 57 23.8 97 23.8	39 185'8 39 9'2 39 161'8 39 193'7	53 183.45 79 11.55 17 160.86 46 191.83	54 0.720 27 0.698 27 0.698	4 9.727 2 9.724 8 9.761 4 9.753	7 8.727 7 8.723 7 8.759 5 8.751	9 0.559 2 0.553 1 0.540 2 0.545	8 7.6773 0 7.6622 3 7.6773	9,7277 9,9316 0,1831 0,00723
34 ¹ 34 ¹ 34 ¹ 35 ¹	7 — 1067 8 — 1066 9 — 1066	IV i	133 18 133 13 133	1 63 1 80 1 98	2 II 9 8 7 I	50°: 28°: 4°:	1 189 1	17 -2'	72 23 ' 8 28 23 ' 8 23 23 ' 8	40 169 6 40 355 7 40 177 6	97 347.58 75 170.98 62 353.99 56 180.09 178 1.88	0.434	3 9 700 5 9 714 2 9 738	6 8.737 4 8.714 0 8.727	2 0 540 9 0 559 0 0 552	7.6628 7.676 4 7.663 7 7.675 1 7.664	8 9'9436 6 9%60xx 8 9'32x8

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366 367 368 369 370	-1059 -1058 -1058 -1057 -1057	V 19 XI 12 V 8	1334 1335	752 939 116	17 30'9 21 56'4 18 43'3	46.914	-2.48 -2.93 -1.96	23.834 23.833 23.833	182°225 5'629	356.394 182.543 6.394 188.709 15.824	0'7448 0'6904 0'7385	9.7623	8.7564 8.7656 8.7601 8.7118 8.7430	0.5656 0.5400 0.5612	7.6778 7.6622 7.6777 7.6624 7.6773	9#27xG 9#33x7 9*6794 9#9864 0*0734
371 372 373 374 375		IX 22 III 18 IX 11	1335 1335 1335	619 796 973	2 56 c 7 8 3 2 42 3	169.049 347.348	-0'97 +2'83 -0'32	23.833 23.833 23.833	349.548 3 177.514 3 356.913	166.710 350.933 176.856 356.398 187.424	0'7399 0'6907	9'7064 9'7635	8.7106	0.5700 0.5333 0.5721	7.6654 7.6737 7.6666 7.6724 7.6680	9'985 6 9#996 4 9'325 8 9#473 2 9#708 9
376 377 378 379 380	-1053 -1053 -1053	VII 25	1336 1336 1336	475 505 652	23 24.6 13 14.2 4 52.3	146.726 297.292 326.619 107.379	+3.94 +4.29 -0.31	23.83	1 342 542	2 473 165 586 196 786 7 340 991	0'7284 0'7165 0'6963	9.7205	8.7214 8.7333 8.7536	0.2614	7.6733 7.6694 7.6657	
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396 397 398 399 400	-1046 -1046 -1045 -1045 -1044	X 1 II 26 VIII 22	1339 1339	280 428 605	23 12'5 1 41'5	178 · 215	-1.56 +4.22 +0.39	23.837 23.837 23.837	192.636 350.492 168.989	11'049 192'550 352'417 166'649	0.7443	9.7530 9.7275	8.7403	0.5744 0.5407 0.5555	7 6747	919159
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361 362 363 364 365	35.0 88.6	0 +1 . 26	840 9 745 945 9 757 944 9 737	9 298 · 13 9 8 79 · 60 8 1 109 · 30 9 9 254 · 12 8 6 68 · 48 8	8 · 53 9 · 579 3 · 24 9 · 625 7 · 89 9 · 579	9.999 9.996 9.998	1 9 · 966 5 9 · 957 0 9 · 967	3 8 · 803 5 9 · 106 7 8 · 977	1 9 573 0 9 604 5 9 555	2 9 · 9 6 · 7 2 9 · 9 6 · 7 2 9 · 9 6 · 7	86 · · · · · · · · · · · · · · · · · · ·	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
366 367 368 369 370	84'5 150'8 100'0	570 · 2 32 + 0 · 4 500 · 9 55 1 · 1	146 9 . 704 786 9 . 764 702 9 . 712 840 9 . 746	4229 48 8 1 43 92 8 7 216 34 8	6.70 9.54 6.56 9.53 6.61 9.52 6.79 9.51	97 9 992 20 9 989 42 9 987 90 9 984	6 9 · 972 9 9 · 973 8 9 · 974 7 9 · 974	2 9 · 368 2 9 · 368 9 9 · 415	5 9 470 8 9 423 9 9 378 9 9 307	0 9 · 980 8 9 · 984 3 9 · 987 7 9 · 990	2 75° 1 102° 2 76°	
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39 39 39 39	2 327 3 178 4 57 5 285	· 62 -1 ·	2170 9 73 3114 9 74 5035 9 77 4970 9 76	390 194 96 144 12 23 129 186 84 565 344 20	85.63 9.6 86.32 9.6 87.80 9.6 94.47 9.6	886 9 · 92 896 9 · 92 920 9 · 92 842 9 · 92	166 9 9 9 4 145 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	108 9266 106 9 67 398 9268	591 9215 766 9 ° 07 379 8282 527 9217	15 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	955 118 970 61 990 119 952 62	1 1 - 24 + 40 + 36 + 6 + 98 - 15 ril 1 4 + 118 - 10 + 177 + 28 - 107 + 46 ril 2 2 3 - 1 - 66 - 39 + 14 - 59 ril 2 2 3 - 2 2 3 - 2 2 3 - 2 2 3 2 2 3 3 - 2 2 3 3 3 3
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111.	Julianischer Kalender		Welt- Zeit	IJ	<i>L</i>	ε	P	Q	$\log p$. $\Delta \widetilde{L}$	$\log q$	u'_{a}	$\log f_u$	log y
401 402 403 404 405	-1044 VIII 10 -1043 II 4 -1043 VII 31 -1042 I 24 -1042 VI 21	1340 137 14 1340 314 5 1340 491 14	4 39 7 5 36 7 4 18 0	306.487 116.703 205.248	+4'37 +0'13 +3'78	23'835 23'834 23'834	6.674 185.836	185.868 2.606	0'7414	9'7043 9'7645 9'7026	8.7495 8.7086 8.7601 8.7075 8.7384	0.2430 0.2430 0.2403	7.6721	9:3570 9:8045 9:6048 0:1257 0:1330
406 407 408 409 410	-1042 VII 20 -1042 XII 15 -1041 VI 10 -1041 XII 4 -1040 V 29	1340 816 2	2 16·4 1 40·8 5 10·2	254'034 67'906 243'110	-0.71 -2.25 -1.70	23.833 23.833	349'933 173'174 357'839	347.485	0.4133	9'7160 9'7592	8.4163	0'5579	7.6655 7.6772 7.6625 7.6776 7.6622	0.092 ± 9.053 % 9 : 8066 9 .267 % 9.099 6
411 412 413 414 415	-1039 V 19 -1039 XI 12 -1038 IV 8 -1038 X 3	1341 702 1 1341 879 20 1342 026 22 1342 204 10	1 17.2 0 48.8 2 57.4 0 45.1	8'147 180'071	-2.47 -2.95 +0.66 -1.69	23.831 23.831 23.831 23.831	189'359 13'515 158'250 349'328	187.718 15.852 166.044 350.618	0'7376 0'7045 0'7404	9'7114 9'7433 9'7493 9'7053	8.7596 8.7127 8.7419 8.7453 8.7101	0'5604 0'5509 0'5401	7.6778 7.6622 7.6777 7.6642 7.6749	9.6816 9.9467 0.0114 0.005H
416 417 418 419 420	-1037 IA 22 -1036 III 18 -1036 IX 10 -1035 II 6	1343 061 7	0 18'3 7 49'3 2 42'2 7 17'3	168.746 347.767 157.610 308.225	-0.95 +2.80 -0.30 +4.43	23.830 23.830 23.830	356.604 185.351 4.219 163.108	355.981 186.934 2.056 165.224	0.7435 0.6965 0.7282 0.7297	9'7016 9'7574 9'7207 9'7192	8.7072 8.7217 8.7217 8.7203	0.2012 0.2008 0.2012	7.6654 7.6737 7.6666 7.6724 7.6718	9:4287 9:513() 9:664 x 9:5927 0:190()
421 422 423 424 425	-1034 VII 22 -1033 I 15	1343 266 22 1343 415 9 1343 592 5 1343 769 9	2 26'4 3 19'4 5 33'8 9 1'2	146.849 297.091 107.800	+0'16 +3'92 -0'27	23.831 23.831 23.831	12.395 170.385	196.258 10.211 171.222 351.076 176.636	0.7048	9.7479 9.7637	8.7320 8.7451 8.7066 8.7592 8.7108	0'5445 0'5729 0'5328	7.6680 7.6709 7.6733 7.6657 7.6745	0.095 % 0.034 4 9.949 4 9.9114 9.275 %
425 427 428 429 430	-1032 VI 30 -1032 XI 24 -1032 XII 24	1344 123 13 1344 301 7 1344 448 13 1344 478	3 41 4 7 30 9 3 58 8 25 0	274.639 87.212 233.665 263.729	+1 · 76 -1 · 55 -2 · 47 +0 · 45	23.833 23.833 23.833 23.833	7.578 161.820 193.698	183°281 9°757 161°111 191°928	0.7293 0.6965	9.7309 9.7626 9.7556	8 · 7304 8 · 7204 8 · 7600 8 · 7528	0.5570 0.5556 0.5400 0.5433	7.6646 7.6757 7.6637 7.67.8 7.6766	9.7156 9.8474 0.182 x 0.0680
431 432 433 434 435	-1031 VI 19 -1031 XI 14 -1030 V 9 -1030 XI 3	1344 803 5 1344 979 21 1345 157 18	39 0 53 6	76 595 222 846 37 784	-2.16 -2.01 -2.04	23.834 23.834 23.833	15.758 169.638 354.025	16 402 171 108 352 014	0.7437 0.6938 0.7322	9.7583 9.7583	8.7557 8.7557	0.5655 0.5423 0.5569	7.6622 7.6629 7.6777 7.6624 7.6774	0°175€5 9°946€5
436 437 438 439 440	-1029 X 23 -1028 IV 17 -1028 X 11 -1027 III 9	1345 511 23 1345 688 22 1345 865 23 1346 014 7	3 54'I 33'3 3 44'9 8 8'8	17'314 189'280 338'809	-2.75 -0.29 -2.21 +3.56	23.834 23.834 23.834 23.834	185.228 11.398 192.451 349.961	186.865 10.407 192.249 351.968	0.441 0.441 0.4015	9.7093 9.7625 9.6998 9.7519	8 · 7576 8 · 7059 8 · 7480	0'5701 0'5322 0'5752	7.6628 7.6768 7.6636 7.6758 7.6679	9"693G 9"9854
44 ¹ 442 443 444 445	-1026 VIII 21 -1025 II 15 -1025 VIII 11	1346 368 18 1346 544 21 1346 722 22 1346 899 13	19.0 18.1 4.8 35.9	328·262 137·751 317·344 127·395	+4.21 +0.38 +4.51 +0.40	23.834 23.833 23.833 23.833	358.368 176.880 6.269 185.247	0'652 175'039 7'181 185'425	o'7243 o'6988 o'7419 o'6895	9'7255 9'7543 9'7037	8 · 7249 8 · 7506 8 · 7078	0.2264	7.6697	0.0167 9#1766 9.4325 9.7779 9#6486
445 447 448 449 450	-1024 II 4 -1024 VII 1 -1024 VII 31 -1024 XII 25 -1023 VI 21	1347 224 20 1347 254 5 1347 401 10	9'3 46'2 1 51'9 2	88 746	+0.12 +0.12 +0.61	23.832	163'776 193'693 349'895	166·206 195·731 347·455	0.2155 0.2010 0.2152	9 7404 9 7525 9 7390	8.7485	0'5447 0'5397 0'5528	7 6637	0'1152 0'1569 0n0733 9n9543 9'8598
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402	33 '53 262 '79	+0.6376 -0.4952	9 · 7065 9 · 7666	130,00	96 ° 90	9.6659 9.6541	9.832	9'9476 9'9506	9.5188 9.4319	9,5118	9.9697	100.0	- 94 + 34	+ 18	41 + 93	24 10	+ 4	+ 55 - 43	t
404 405	26.82 19.41	+1.3222 +1.3322	9 · 7047 9 · 7443	308.62	30,12	9.6525 9.5975	0,0000 0,0842	0,0031 0,0211	9.4170 7"7916	9,5629 9'5974	0.0631 0.0680	73.7 90.4	garten dell	gal-Manage Bro-Majorey		To and	Magazina Magazina		$\stackrel{p}{r}$
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407 408 409	149 '54	-0.8990 +0.6406 -0.1850	9.7181	80.10	88.00	9.5789	9.9992	9 9664	8.7816	9'5733	9.8623	86.3	+127		151	+ 62	62 +- 21	+ 40	y its t
410	180.40	0.1228	9.7042	68.39	87.38	9.5592	9.9966	9.9694	9.0986	9.23×2	9'9733	82.3		I4	180	- - 13	120	O	7.131
411 412	199'2	1 +0 · 4804	9.7135	56.04	86.67	9'5409	9.9923	9.9720	9 2684	9.4681	9 9804	78.8	+129	+ 36 66	+ 77 - -166	47	+136 143	18 48	r
	166.3	1 +1.0266	9.7513	9.92	88.93	9'4993	9'9780	9.9772	9:4921	8.7578	9,3663	21.0			40 MT 41	W 1 MA 100	21-20-4	6. 1 miles	$\frac{p}{p}$
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410	9.7	4 十0・39 x 5 9 十 x · 5 5 2 0	9 7229	152'53	92.61	9.2020	9.9822	9.9765	9 4478	9,1872	9 9948	100.2	81	39	6	+ 33	+ 55	- - 6	$p^{\#}$
421	126.8	6 1 · 244;	9'7358	332'61	92.67	9,2102	9.0818	9.9760	9 ' 4535	9,,1919	9 9947	73.3		province.	GAME TAXAB	Marrie 4	totoresi		27
423 423	318.2	2 +1.082 9 +0.890 7 -0.815	9 ' 7033	3 285 40	92'04	9.5697	9 9982	9.0678	8.9637	9 4 5 5 5 9	9.0200	84.3	- 6	+ 52	+ 39	+ 42	11 .	51	r
424	312.8	4-0.188	9.7087	272'82	90.42	9.2901	9.9999	9 9643	8 2464	9,5897	9 9644					12	+104	+ 11	y str
426 427	140'7	3 -0.089 4 -0.519	9 7496	84.22 261.00	89.07	9 · 6044	919997	g · g6a;	8,5603	9 · 6026	9,9625		+150 100			1	78 + 60	32	1.
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43 ⁴	179'8	3 0 · 494 9 + 0 · 967	9'7118	194'9	3 85 · 63 2 86 · 23	3 9 . <u>688</u> 3	9 945	9.940	9,669 0,9669	5 9 1 5 4 5 6 5 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6	7 9 ' 9953 1 9 ' 9968	2 QI.(I	172	42	102	57	T_{-}
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44	324.6	6 -0.120 +1.030	29.730	156.6	4 95 ' 94	9.0813	9 9554	9'943	g ₂ 634	1 9 ' 325;	9 9 9 9 9 9	116'		34	8n	2	- 33	+ r	$\frac{p}{r}$
44	139.8	б +0.270 2-10.20	7 9 . 756. 6 0 . 7050	148'3	1 96 · 82	2 9 · 6752	9 9646	9 9449	9 9 1 5 8 8 1 3 9 1 5 8 7 1	5 9 434 6 9 437	1 9 . 583 1 8 6 . 6 8	1 23.8	+143 +152	+ 38 + 13	-137 -153	+ 33	-77 -104	+ 52	7 2 1 2
44	22'4	5 -0.445	9.766	4 139 5	9 96 . 89	9 6657	9 9744	9 947	5 92 523	7 9.506	4 9.976	4 110.0	88	5	27	10	25	44	
44 44	7 127.5	3 +1 ·303	0 9 742	4 102 0	9 92 0	0 9.614	998	9 959	7 8 8 8 9 7	0 9 606	3 g ' g6 r	3 94	9	an rum			principality	#*************************************	$\frac{p}{p}$
44	344'7	1 -1'183 4 -0'900 3 +0'724	29'741	278.5	0 91.3	ე ე∙ნი8ყ	9 999	3 9 960	8 8 740	4 9n 604	0,061	6 86.	6 — 107 6 — 17		11			- 5	
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451 452 453 454 455	-1022 X	/I 10 II 4 V 30	1347 1347 1348 1348 1348	933 110	5 7	53.4 50.3	243'529	-1·75	23.829	5.659	186.423	0.7450	9.7017	8.7576 8.7054 8.7592 8.7136 8.7405	0.5660 0.5405 0.5596	7.6772 7.6625 7.6776 7.6622 7.6778	9,12681 8,15702 9.6830 9,19018 0.0766
456 457 458 459 460	-1020 -1020 -1019 I	V 18 X 13 V 8	1348 1348 1348 1348 1349	641 789 966	15 18	39'7	191'150	-2 40 -2 34 -0 62	23.828	349'174	165.337 194.559 350.359 175.748 355.636	0.411	9.7044	8.7467 8.7352 8.7096 8.7598 8.7076	0.5726	7.6635 7.6622 7.6759 7.6643 7.6748	0.0376 0.1789 0.0126 9.5187 9.5417
461 462 463 464 465	-1017 I	II 19 X 11	1349	676 852	4 6	25.8 20.5	348.017	+2 77	23.828	3'939	195.651	0.7269 0.7196	9'7564 9'7221 9'7320 9'7493 9'7009	8.7525 8.7231 8.7305 8.7467 8.7063	0'5511 0'5446	7.6654 7.6737 7.6666 7.6724 7.6720	9,6081 9,5616 0,0779 0,0209 9,9654
466 467 468 469 470	-1014 -1014 V.	I 25 II 22 I 14 II 11	1350 1350 1350	532 708 886	4 22 14	47 7 47 4 0 0 26 6	290.703	-0.24 +2.97 -0.86	23.831 23.830 23.830	177.779 358.271 185.575 6.789	8.909 8.909	0.7388 0.7074 0.7179 0.7306	9'7460	8.7589 8.7115 8.7423 8.7317 8.7193	0.2427	7.6669 7.6734 7.6656 7.6746 7.6645	9n9396 9'3249 9n1849 9n7032 9'8011
47x 472 473 474 475		7Î 1	1351	211	10 1	9 4 40'9	58.755	-2.64 -2.64	23.831	193.615 344.924	161.221 191.924 344.466 15.423 171.201	0.6959 0.7442	9.7567	8.7604 8.7539 8.7057 8.7058 8.7550	0.5397 0.5423 0.5654 0.5663 0.5428	7.6776 7.6758 7.6622 7.6637 7.6778	0'1818 0n0657 0n1573 0'1521 9'9472
476 477 478 479 480	-1010 I. -1011 X -1011 X	U 14 V 9 U 39 V 29	1351 1351 1351 1352 1352	743 919 097 274	14 8 5	5°0 5°0	37 875 211 864 27 786	-1.56 -3.00 -1.56	23.832 23.832 23.832	177'541 1'809 185'165 10'567		0.2161 0.2324 0.2324 0.6913	9.7338 9.7456 9.7083 9.7632	8.7413 8.7122 8.7580	0'5564 0'5410 0'5712 0'5316	7.6624 7.6528	9n6895 919526
483 484 485	-1008 II -1008 II	X 12 II 9 X 1	1352 1352 1353	775 954 130	17 1 5	23 · 7 49 · 4	338 984	-0.42 -3.55	23.832	168'201	192.009 351.437 165.816 0.068 174.704	0 7020	9.7500	8.7061 8.7467 8.7293 8.7234 8.7519	0.5406 0.5554 0.5565	7.6766 7.6665 7.6679 7.6679	9n967x 9n3033
486: 487: 488: 489: 490:	-1007 VII -1006 VI -1006 VI	II 21 II 15 II 13 II 11	1353 1353 1353 1353	484 662 810 839	5 3 13	42 · 5 17 · 4 26 · 4 33 · 7	138'160 317'041 99'259	+0.38 +4.50 -0.77 +0.42	23.831 23.831 23.831 23.831	103.110 103.010	185.047 12.193 165.458 195.219	0.2073	9.7641 9.7388 9.7511	8.7602	0.5347 0.5695 0.5462	7.6693 7.6696 7.6708 7.6646 7.6681	9n 6040
	-1005 XI -1004 V -1004 XI	I 26 I 20 I 15	1354 1354 1354	341 518 696	8 12 3	58·3 50·0	265 521 78 082 254 754	+0.64 -1.44	23.830	357 791	356.633	0.7360	0,4 <u>0</u> 04	8.7140 8.7581	0'5605 0'5402 0'5662	7.6637 7.6765 7.6629	9n9567 9'9053 9n2757 8'6949 9'6832
496 497 498 499 500	-1003 XI -1002 IV -1002 V	V 30 V 29	1354 1355 1355 1355 1355	050 197 226	14 1 13 4 22 3	8 · 8 ; 14 · 7 39 · 5	243 852 29 112 57 064	-1.75 -1.39 -2.65	23.827	13.552 166.650	185.742 15.928 164.596 193.704 350.150	0.4100	9 7405 9 7523 9 7404	8 · 7392 8 · 7477 8 · 7366	0.2376	7 · 6776 7 · 6628 7 · 6622	9n8522 0.0784 0.0635 0n1553 0n0172

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4	15 I	182°67	0'1854	9.7621	267°09	8ე°5ნ	9.5904	9.9999	9.9642	8,, 2508	9#5900	9'9643		+109	- 1			-	. 1	474
4	153	58.88	-0'0372 -0'7976	9.7636	255'10	88.01	9.5712	9.9983	9.9676	8,,9508	9#5583	9.9696	95'5	+ 26 112 21	+ 32	+ 84 - 58 + 65	- - 8	0	+ 22 + 22 - 42	<i>t</i> #
	155 155	263.12 263.12	+1.1830	9 7 7 4 3 9	242 ' 38	86.91	9.2231	9.9946	9.9704	9 1955	915065	9.9764	99'5							p
,	156 157	278·84 52·04	+1.0002	9·7528	22.60 55.58	87.70	9'5064	9.9804	9'9753 9'9717	9 · 4680	9'1112 9'4581	9 • 9 9 6 3 9 • 9 8 0 4	72 · 8	1		beninda Soloma		#	\$100000 \$100000	$\frac{p}{p}$:
4	158	160,32 160,31	-1.03303	9.7663 9.7663	10.47	88.57	9,4963 9,4963	9.9789 9.9784	9 9775 9 9775	9 1 4823 9 1 4882	8,8928 8,7773	9'9992 9'9987	72.0	+134	+ r	 163	+ 24	- 92	37	t II
1	160		0'3481								!			ļ	- 2	97	- 21	31	38	
1	161 162	129'51	-0.4026 +0.3644	9'7243	165.01	91'46	9.4960	9.9790	9'9775	944813	8,0036	9.9986	107.7	+163	42 39	47 126	- 25 + 27	66	6 + 4	$\frac{t}{t^{\oplus p}}$
4	163 164 165	277 37	-1'1965 -1'0492 -0'9234	9'7514	152.89	92.62	9'5074	9,9818	9.9763	9#4518	9.1842	9 9949	100.6		AP VI	promote	- - 51	46	- - 67	p_{\perp}
	166		0'8702											- 74		- 26			59	t
4	167	68 · 66	+0'2113 -0'1531	9'7099	284 · 98	90'83 91'99	9.2401	9.9983	9.962r	8 · 9524 8 · 5438	9.5570	9'9698 9'9654	84.5 92.2	- 128 + 47	6	6g 107	9 -⊢ 14	- 14 + 167	+ тб то	l"#
1	169 170	145.65 35.73	-0'5049 +0'6326	9.7347 9.7216	84.30 84.30	90 44 89 10	9'5904 9'6043	3,3338 3,3333	9.9618 9.9618	8 2604	9,5899 9,6025	9 9643	88.0	120	+ 33			67 - - 52	- 27 + 37	1
•	17 I	169.70	+1.5200	9 7648	231.93	84.02	9'6500	9'9852	9.9516	914088	925633	9'9688	106.0			anama .			prosecus prosecus	$\begin{bmatrix} p \\ p \end{bmatrix}$
4		212'01	-1'1632 -1'4363 -1'4193	9'7047	46'01	83 43	9'6585	0.0800	9'9495	9.4726	9'5384	9'9724	71.6	l		_		\$****** \$*******	2000	$\frac{p}{p}$
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	476 477	225.76	-0'6404 -0'2220	9.7360	212.33	83, 13	9.6751	9'9653	9 9449	9 2 5 8 4 6	914411	9,8822	113.6	i + 83	+ 35	+114 +137		160		2,18
١,	478 479	302.82	+0'1603	9.7105	203 36	83.08	9.6834	9 9550	9 9425	9, 6362	923290	2686,6	1116.3	8 8	3	+ 50	1	+ 35 + 139 (- 99)	54	7
		ŀ	+0.8966							1					30			99,		$\binom{1}{p}$
1	481 482 483	43'61	+1.0677 -0.0376	9.7527	352 44	1 92 * 35	9.6903	9'9419	919403	9 685	8,868	ເ ໘ ′ ໘໘88	8 60.6	(- - 87	(-82)	*****		+ 40	39	
1	484	204 38	-0.3000	9.7263	344 8	94 43	9 6886	9 9468	9 9400	9 6686	9,1510	9'9954	61.0	+ 86	39 43	+150 +101	21 32			j j.
	486	254'29	+o·5535	9.7054	336.6	4 96 02	9.6834	9.9550	9 9425	5 g · 636:	91329	x 9 · 9899	63.4	7 + 41	+ 7	g8	- 26	+151	+ 58	3 7:11
-	488	251'16	0'4018 1'2645	9 . 706	327.7	196.84	9.674	9 9554	9 945	9 584	4 92439	9 9 9 9 8 2 9	66 4	5		149 	IC		*****	p
	489 490		+1.2022														-			$\frac{p}{p}$
			-0.3028 +0.8046											+117 - 95						
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	495	191,8	+0.482	2 9 7 63	267.4	7 89 6	29.291	19.999	9 9 9 64	181199	5 91 590	8 9 964	3 31,	o +rra	- - 27	7 - ÷168	+ (-136	+ 2	5 t**
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Nr.	Julianischer J. Kalender	Julian. Wolt- Tag Zoit	<i>II</i>	<i>Z</i>	E	P		$\log p$	ΔL	$\log q$	u_u	$\log f_a$	log γ
501 502 503 504 505	1000 IV 8 13	355 729 I 54.8 355 906 23 II.5	8 933 179 592	-2'34 -1'67	23 ' 826 23 ' 826 23 ' 826		355'361 185'760	0.7425 0.6988 0.7256	9.7645 9.7622 9.7552 9.7234 9.7304	8.7599 8.7082 8.7512 8.7245 8.7288	0.5312 0.5739 0.5368 0.5607 0.5513	7.6635 7.6759 7.6643 7.6748 7.6654	9:5982 9:5604 9:5366 9:5375 0:0573
505 507 508 509 510	998 11 17 13 998 11 12 13 997 11 6 13	356 437 15 0 3 356 586 0 x1 8 356 762 2x 23 8 356 940 0 27 1 357 117 12 22 5	318.864 129.134 307.724	+4'49 +0'43 +4'40	23 827 23 827	169·958 349·160	9'718 170'238 350'128 175'887 0'003	0.6014	9.7505 9.7608 9.7625 9.7088 9.7443	8.7479 8.7060 8.7586 8.7123 8.7411	0.5446 0.5714 0.5349 0.5675 0.5443	7.6736 7.6706 7.6683 7.6720 7.6669	0'0103 9'9839 9"9636 9'3822 9"3238
511 512 513 514 515	996 VII 21 13 996 XII 16 13 995 I 14 13 995 VI 11	357 471 21 27 2 357 619 7 53 8 357 648 18 48 1 357 796 8 4 8	108 245 256 120 285 972 69 143	0'22 0'48 2'98	23.827 23.828 23.828	6.056 161.808 193.472	161.308	o'7317 o'6894 o'6950	9'7343 9'7178 9'7633 9'7576 9'7030	8.7329 8.7181 8.7607 8.7547 8.7062	0'5537 0'5587 0'5393 0'5411 0'5654	7.6734 7.6656 7.677x 7.6746 7.6625	9,46854 9,7528 0,1819 0,0603 0,1822
516 517 518 519 520	995 XII 5 13 994 V 31 13 994 XI 25 13 993 V 20	357 825 23 47 9 357 973 23 30 6 358 150 11 20 0 358 328 11 27 3 358 504 21 38 3	245'315 58'573 234'349 48'291	1.60 -2.63 -2.44 -2.49	23.829 23.829 23.829	169.652 352.230 177.550 0.936	14.490 171.287 350.095 179.984 358.668	0.7064	9.7021 9.7567 9.7208 9.7324 9.7473	8.7541 8.7201 8.7319 8.7430	0'5671 0'5432 0'5550 0'5573 0'5401	7.6622 7.6778 7.6622	0°1281 9°9477 9″8584 9°3461 8°9174
521 522 523 524 525	992 V 9 x 992 Xl 2 x 991 ili 30 x 991 lX 23 x	358 682 16 18 9 358 859 13 35 3 359 036 15 44 1 359 184 22 32 9 359 361 1 30 4	38.231 211.564 0.070 170.222	-2.02 -3.01 +1.26 -1.06	23.830 23.830 23.830 23.830	9'705 192'245 348'676 167'936	191.819 350.825 165.230	o 6908 o 7436 o 7039 o 7183		8.7114 8.7585 8.7063 8.7452 8.7307	0'5311 0'5759 0'5407 0'5555		9,6874 9,9155 0,0680 9,9950 0,0367
525 527 528 529 530	980 IX 12 1 989 III 9 1 989 IX 2 1 988 II 26	1360 247 12 35.	7 159'495 2 338'828 4 149'000 1 327'827	-0'42 +3'56 +0'09 +4'22	23.83 23.82 23.82 23.82	5 176 108 5 202 9 184 303 8 12 84	184 744	0.6964 0.7431 0.6895 0.7410	9.7563 9.7637 9.7053	8 7068 8 7601 8 7091	0.5405 0.5686 0.5357 0.5680	7 · 6725 7 · 6679 7 · 6693	9n4139 9.5260 9.6985 9n5626 0.0858
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544 545	16.38	-0'2774 -0'3315	9.756	193.1	88.6	9 · 5 · 3 9 · 495	9 9 9 8 1 4 9 9 9 8 1	9'976	7 9 461 6 92482	2 9 128 6 8n874	4 9 · 996 2 9 · 998	73.	7 - 77	+ 32	- 13	+ r	9 + 145 6 + 47		2 1 1
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566 567 568 569 570	-973 X 4 -972 III 30 -972 IX 22 -971 III 19 -971 IX 12	1366 124 16 1 1366 300 22 1 1366 478 19 2	2'0 170'47	+1.56 8 -1.10 2 +2.64	23 827 23 827 23 827	356'506 175'842 4'548	165.327 358.657 174.273 5.133	0.7287 0.6952 0.7436	9 7332 9 7211 9 7571 9 7023 9 7634	8 · 7206 8 · 7540 8 · 7063	0.2408	7.6653 7.6665	0:0422 9#5114 9:5535 9:6406 9#5257
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804 805	- 866 VII 24 - 865 I 18	1404 956 18 36.	4 III.556 4 289.658	-0.01	23.809	184'351	185'091	0.7431	9.7022	8 7074 8 7598 8 7093	0'5721 0'5325 0'5716	7.6731 7.6658	9,6209
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816 817 818 819 820	- 861 V 1 - 861 IX 26 - 860 III 22 - 860 IX 14	1406 698 20 48. 1406 846 20 30. 1407 024 3 57. 1407 200 20 5.	3 31 200 6 174 486 0 352 831 0 163 218	+2'35	23.813 23.813 23.813 23.813	16'165 166'996 355'001 174'343	13.729 157.996	0.7008 0.7122 0.7419 0.6806	9.7528 9.7408 9.7032 9.7645	8.7483 8.7369 8.7080 8.7599 8.7080	0.5386 0.5440 0.5721 0.5328	7.6739 7.6664	0,1549 0,0920 9,6277
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836 837 838	- 852 IV 21 - 852 X 16 - 851 IV 11	1409 976 19 45 7 1410 154 9 43 3 1410 331 11 30 1	22°399 195°038	-3.01 -0.41	23'807 23'806	172'312 355'215 180'960 2'828	357 · 648	0.7060	9.7216 9.7308 9.7478 9.7064	8.7209	0.5550	7.6627 7.6768 7.6634	9.8535 9n6383 8n9280
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856 857 858 859 860	- 843 X - 842 IV - 842 IX - 841 III	12 1413 28 7 1413 43 2 1413 60 26 1413 78 23 1413 96	2 4 18'2 9 11 44'6 6 3 45'2 4 14'6	185 '516	+1.26	23.810 23.810	166°775 354°307 174°045	12.899 167.671 354.278 173.005 4.777	0.7107 0.7423 0.6896 0.7410 0.7001	9'7025 9'7646 9'7038	8 · 7385 8 · 7075 8 · 7598 8 · 7086 8 · 7492	0.5732 0.5320 0.5716	7.6624 7.6751 7.6652 7.6739 7.6664	0'0995 926840 9'7548
861 862 863 864 865	840 IX 839 I 839 VII	11 1414 31 3 1414 49 30 1414 64 26 1414 82	8 16 0.2 4 18 46.2 3 2 31.5 5 2 21.3	163.088 342.781 152.379 302.499 113.298	+3'28 -0'07 +4'17	23.810 23.809	11'362 190'005 348'139	179'434 13'684 188'058 348'199 169'061	0.7228 0.7229 0.7000 0.7445 0.6924	9'7275 9'7529 9'7002		0'5543	7.6726 7.6678 7.6712 7.6750 7.6659	949378
866 867 868 869 870	- 838 VII - 837 I - 837 VII	19 1414 997 15 1415 177 8 1415 351 5 1415 529	7 2 50·8 1 17 8·4 1 9 10·8 1 42·8	141'937 291'239 103'039 280'170 92'582	+3'40 -0'46 +2'29	23.807 23.807	355.534 176.526 3.364	198.301 353.791 178.928 0.895 186.950	0.6894 0.7361 0.7139 0.7337	9'7645 9'7108 9'7421 9'7370 9'7156	8.7604 8.7139 8.7383 8.7357 8.7161	0'5678	7.6697 7.6743 7.6648 7.6755 7.6638	0n 1840 9n6252 9'4913 9'4803 9n6747
871 872 873 874 875	- 836 XI 1 - 835 V 1 - 835 XI	3 1415 883 18 1416 031 3 1416 207 7 1416 385	3 46.4 2 23.7 16 10.0 13 39.9	269 322 81 909 228 455 43 135 217 455	-1'77 -2'84 -2'19	23.805 23.805	347'309	9'946 193'301 349'131 169'205 357'601	0.6976	9.7590 9.7018 9.7546 9.7232 9.7293	8·7565 8·7055 8·7525 8·7223 8·7294	0.5664	7.6764 7.6631 7.6777 7.6623 7.6774	9.9855 000980 000373 9.8985 906414
876 877 878 879 880	- 834 X 2 - 833 IV 2 - 833 X 1 - 832 III 1	3 1416 562 7 1416 739 2 1416 916 6 1417 093 3 1417 242	17 46 0 19 16 5 17 6 0 3 16 1	206 · 172 22 · 766 194 · 728 344 · 273	-3'02 0'74 -2'58 +3'16	23'804 23'804 23'804 23'804	2'734 188'837 9'877 167'449	188.328 9.361 169.401	0 · 7435 0 · 7064	9.7010	8 7451 8 7104 8 7595 8 7072 8 7436	0.5725 0.5313 0.5744 0.5433	7.6628 7.6768 7.6634 7.6760 7.6676	8,0812 9,4165 9,8750 9,9756 0,0413
883 884 885	- 831 VIII 2 - 830 II 1	9 1417 950	12 55 0 17 51 4 15 21 2	333'675	+0.29	23 ' 804 23 ' 803	175 797 354 382	010 -74	0.7296	9 7577 9 7350 9 7198 9 7582 9 7016	8 · 7203 8 · 7549	0.5522	7.6643 7.6714 7.6689 7.6699 7.6705	0110959
887 888 889 890	— 829 VIII — 829 XII 3 — 828 VI 2	8 1418 304 5 1418 482 0 1418 629 4 1418 806	15 20.7 1 54.9 6 48.1 22 3.9	311.572 122.562 270.752 83.648	+4.47 +0.38 +1.20 -1.65	23 805	J1 149 167 446	3'390 189'689 13'429 165'128 351'145	0.7398	9 · 7635 9 · 7066 9 · 7475 9 · 7448 9 · 7099	8:7596 8:7105 8:7438 8:7427 8:7114	0.5343 0.5687 0.5426 0.5494 0.5617	7.6684 7.6718 7.6670 7.6763 7.6632	0,0210 9'9903 0'0420
893 894 895	— 827 XII 8 — 826 VI 3 — 826 XI 28	3 1419 100 3 1419 338 3 1419 515 3 1419 693	23 11 6 12 46 1 1 44 7	72 967	-2 17 -1 32 -2 49	23 806 23 807 23 807	357 605 183 230 5 770	174°594 357°276 184°627 3°757 193°561	0.7322	9'7021 9'7586 9'7175	8:7175	0.5396 0.5658 0.5420 0.5568 0.5552	7'6770 7'6626 7'6776 7'6623 7'6778	9'5938 9'3632 9'4423 9'7323 9'9980
897 898 - 899 -	– 825 V 23 – 825 X 18 – 824 IV 12	1419 840 1419 869 1420 017 1420 194 1420 371	II 7.6	52'045 196'603	-2'45 -2'67 -0'14	23.808 23.808 23.808	14.429 166.613 353.553	343 '052 12 '065 167 '400 353 '679 172 '675	0.5987 0.7092 0.7427 0.5898 0.7403	9 7443 9 7015	8:7400 8:7072 8:7595	0'5361 0'5418 0'5743 0'5316	7.6633 7.6622 7.6761 7.6642 7.6751	0n1125 0'1037 0'1052 9n7380 9'7700

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Nr.	μ	γ	$\log n$	G	K	$\frac{\log}{\sin g}$	$\log \sin k$	$\log \cos g$	$\log \cos k$	log sin ðʻ	log cos ở	N'	bei ⊙A gang	H	im Mi	ttag	bei Unter	⊙ gang	$ _{F} $
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851 852	75°27 238'91	-0'1424 -0'2763	9'7615 9'7615	49°11 225 °03	83°65 83°34	9.6559 9.6603	g'9827 g'9789	9.9502 9.9490	9'4420 9n4825	9°5543 9°5340	9'9702 9'9730	72°8	-126 - + 57 +	24	- 74 -+110	+ 12 - 37	II I60	+ 8 - 33	2·# t
853 854	71,40	-0.8812	9'7182 9'7395	39.79 215.73	83.ro 83.o8	9.6667 9.6667	9 9736 9 9694	9°9473 9°9464	9'5292 9"5593	9'5024 9:4699	9 ' 9769 9 ' 9769	112,3 60,1	+179 + +175 -	17	-114	-⊦ 6x	11 (+147)	+.55	2.38 2.
		-1.2322						9'9414						-					v
857	250.30	+1.3500 +1.2577 -0.4831	9'7046	183.95	88.75	9'6914	9'9404	9 9453 9 9400 9 9400	gatgor	825889	9'9997	119'4		 					2) 2) t
859	239.33	+0.5686 +0.2489	9'7060	175.85	91.35	9.6920	9'9401	9.9396	916911	8.6123	9,9996	119'4	+- 50 +-	64	1.130	+ 43	- 71 - 173 - 179	_	9.18
861	293.1 <u>e</u>	0.1635	9'7289	167.84	93.66	ე : 68ეე	9'9444	9 ' 9405	9n 6770	9.0698	9:9970	118.6	+ 2 +	19	- - 64	4	+124	38	r
862 863	39,35	-0.8666	9'7550	159'80	95'44	9'6841	9'9520	9'9422	9:16487	9'2723	9'9922	117.0	r 6g	32	-111	6 6	97	79	$\begin{bmatrix} P \\ t \end{bmatrix}$
865	217'82	- -1'0257 - -1'1357	9.7638	126.60	95.85	9 . 649 o	9'9863	9'9490	9 4 2 5 9 9 3 3	9'5592	9 9733	105'4				******		0.0004	2)
866 867	337°17 220'53	1'5277 0'4219	9'7664 9'7130	151'39 305'08	96.48 95.68	9'6747 9'6479	9 '9617 9 '9874	9 · 9450 9 · 9522	9n6043	9:3960 9:5755	9 . 986 r	114'5 75'2	58	 36	143	48	153	11-11-11 (C)	p
868 869	78.40 314.29	十0,3033 十0,3000	9'7442 9'7391	117.03	94.21 94.62	9 ' 6362 9 ' 6362	9'9927 9'9943	9°9549 9°9559	9:2573 9:2086	9°5946 9°5991	9 • 9635 9 • 9627	79'9 79'3	155 + 16 +	27 7	- 77 + 44	-†- 42 6	II 98	- - 6	2***
		-0.4728															-157		
872	234.41	+0:9672 -1:2530 -1:0897	9'7039	95,13	90182	g'6030	9'9997	9,3250	825167	9,0010	ე , ენ23	92'1	y	heing	151	52	133	64	$p \\ p$
874 875	66.88	+0'7916 -0'4379	9'7253	51'81	86.57	9'5356	9'9968	9.9728	9'3094	9.4409	9 9828	77.8	153				+ 36 + 47		2**
876	227.82	0'0121	9'7515	39 ' 88	86 ' 72	9.2189	9 ' 9862	919748	9'3932	9 ' 3404	9,9893	75.3	+ 72	15	132	+ 12	161	14	Zili:
877 878	88.76 107.97	-⊦o∙26og o∙7498	9'7074 9'7663	27.23	87 · 11	9.2081 9.2081	9 ' 9838 9 ' 9838	9.9762 9.9762	914290 9'4491	9,2505	9 ' 9930 9 ' 9946	73'5	144 + 162	64	- 87 102	42	41	32	$t_{}$
879 880	228.74	+0'9454 1'0997	9'7488	340.18	91'97	9 4974 9 5012	9 '9799 9 '9799	9 9774	9:4730	9n0112 9n0390	9 9977 9 9974	72.6	82		- 67	1- 70	4	+ 53	p
881 882	1 '42 254 '67	1 · 4853 1 · 2470	9'7596	15 29 148 42	88.36	9'5044 0'5137	g ' 9786 o ' 0831	9'9767 9'9755	9'4870 0#4371	8'9472	0,0030 0,0083	72'I	prins/1990 m. 1999 Mail		property brokenski		,		$\frac{p}{v}$
883 884	88.20 xx.10	+0'3912 -0'4831	9.7220	327.78 335.59	92'91	9.2092 9.2092	9 ' 9838 9 ' 9880	91976x 919742	9'4295 9n3660	9n2529	gʻgg2g gʻg870	74'I	- 74 + -152 -	15	- 92	тб		41	t
885		0'3450			.	.							1						
887	42.65	+0.2303 -1.0495 +0.9780	9 ' 7087	301'88	93'25	9'5435	9'9932	9.9717	9'2455	9114800	9'9792	79'4		******				*****	p_{\perp}
889	283.67	-0.0834	9 ' 7468	257 38	87.8x	9'6148	9 9985	919596	829155	926060	9'9514	95'2	_			_ 6o		_	p
891	136.10	+0.3922	9.7644	245 92	85 96	g · 6320	9'9944	9 9560	92053	92 5992	9'9527	100,1	+172 +	- 30	134	0	75	+ 12	t ^{ri} !
892 893	12.13	-0.2308 -0.2308	9 · 7607 9 · 7607	58 · 89 235 · 37	84 86 84 39	g'6424 g'646g	9 9902 9 9878	9 9535 9 9524	9'3207 923681	9 · 5865 9 · 5765	9.9667 9.9667	76'9	+139 - - 78 -	· 24 · 1	16g 14	- 39	+ 65	28	t
894 895	200 86	+0'5399 0'9954	9 7197	49 01 225'49	83'40	9 · 6588	9 9 9 7 9 5	9 9503 9 9494	9 4427 924773	9 5534 9n 5353	9 9703	108.6	+ 34	59		55	(+ II)		
		-1.2957 +1.2597															_	_	$\left egin{array}{c} p \\ p \end{array} ight $
898 899	9'22	+1'2740 -0'5470	9·7668 9·7668	10.00 101.00	86 40 86 93	9 6892 9 6893	9'9445 9'9433	9 9407 9 9406	9n6768 9:6805	920620 8.0830	9'9971 9'9979	p1.3		- 61		 _ 33			$\frac{p}{t}$
goo	357 12	+0.5889	9 7068	183.41	48 · 82	9.6925	9.9400	9.9396	926913	8n 5637	919997	119.4	59 -	- 65	+ 13	+ 40	+ 6g	+ 7	1#
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Nr.	Julianischer	T Julian.	Welt-	L'	Z	ε	P	Q_{\perp}	$\log p$	$rac{\log}{\Delta L}$	$\log q$	u_a'	$\log f_a$	logγ
	Kalender	Tag	Zeit								7			
901 902 903 904 905	- 823 IX 25 - 822 III 22 - 822 IX 15	1420 549 1420 725 1420 903 1421 080 1421 228	15 36'0 23 22'7 3 3'3	174'062	-1.36 -1.36 -0.66	23.808 23.808	181 511 10 736 189 665	13.023	0'7014 0'7213 0'7244 0'6986	9.7521 9.7260 9.7260 9.7540 9.7004	8.7478 8.7277 8.7249 8.7508 8.7054	0'5390 0'5576 0'5544 0'5420 0'5723	7 · 6652 7 · 6739 7 · 6664 7 · 6726 7 · 6716	9°2779 9n1402 9°9925 9n9215 on0682
906 907 908 909 910	— 820 I 30 820 VII 26	1421 405 1421 434 1421 582 1421 760 1421 936	18 59'9 10 40'4 0 33'8	152.782 302.228 113.609	-0'09 -4'16 -40'08	23.807 23.806	197.856 355.278 175.823	168.549 198.008 353.452 178.250 0.742	0 6929 0 6893 0 7350 0 7124 0 7126	9'7609 9'7121 9'7402 9'7387	8.7564 8.7605 8.7148 8.7370 8.7367	0'5352 0'5355 0'5661 0'5461 0'5518	7.6672 7.6711 7.6730 7.6659 7.6743	0'0336 0"1740 9"6483 9'5727 9'4581
911 912 913 914 915	- 818 VII 4 - 818 XI 29	1422 114 1422 291 1422 468 1422 616 1422 792	6 54'4 10 14'7 11 17'2	239 692	-1'12 -2'18	23'805 23'804 23'804	11'261 192'231 347'324	192 324	0.6926 0.7450 0.6984	9.7600 9.7017 9.7536	8.7151 8.7572 8.7053 8.7514 8.7236	0'5401 0'5668 0'5451	7.6648 7.6755 7.6638 7.6777 7.6622	9n6024 9°9811 0n0690 0n0376 9°9391
916 917 918 919 920	- 816 V 13 - 816 XI 7 - 815 V 3	1422 970 1423 147 1423 325 1423 502 1423 679	10 22'5 1 53'5 2 49'3	228 · 669 43 · 294 217 · 347 33 · 234 205 · 861	1.01 3,15	23.803	179°285 2'679 188'007	187.654	0.400	9'7277 9'7509 9'7644 9'7014	8.7281 8.7465 8.7099 8.7597 8.7075	0'5600 0'5382 0'5735 0'5308 0'5748	7.6777 7.6623 7.6774 7.6628 7.6768	9,6430 8
921 922 923 924 925	- 814 IV 22 - 814 IX 16 - 813 III 13	1423 827 1423 856 1424 003 1424 181 1424 358	19 53 5 12 49 0 20 18 0	23 178 164 755 344 377	0'75 0'75	23.802	196'673 345'754	169 · 133 198 · 370 343 · 353 177 · 294 352 · 624	0.4148	9'7454 9'7566 9'7364 9'7185 9'7590	8 · 7422 8 · 7522 8 · 7352 8 · 7191 8 · 7559	0'5434 0'5354 0'5522 0'5595 0'5385	7.6662 7.6634 7.6728 7.6676 7.6714	0.0633 0.1535 0.1039 9.6478 9.7130
926 927 928 929 930	— 811 VIII 15	1424 712	18 34 8 22 48 1 9 39 3	143 687 322 420 133 261	+0'28 +4'42 -10'48	23.802	2'214 190'66d	189 183	0'5910 0'7390	9.7629 9.7078 9.7459	8.7112 8.7426	0'5355 0'5673 0'5442	7.6689 7.6699 7.6705 7.6684 7.6752	9,4721 9,2759 0,0040 9,9691 0,0445
931 932 933 934 935	ور XII و 80 – ا	1425 569	5 52'5 5 37'6 21 39'6	83'379	+1'23 1'66	23 803	356.216 1 356.216	350'212 5 174'641 2 356'266 5 184'693 2 2'803	0'6898 0'7443 0'6945	9'7628 9'7024 9'7579	8.76ox 8.76ox 8.7556	0'5390 0'5659 0'5422	7.6632	9.5988 9.5006
936 937 938 939 940	- 807 VI 2 - 807 X 28	1426 278 1426 425 1426 454 1426 502 1426 780	10 0'3 18 18'4 20 10'5	34 528 62 461 207 738	-1.67 -2.47 -3.05	23.80	5 344 06: 5 13 55: 5 166 50:	193 561 2 342 321 2 11 235 3 167 181 5 353 033	0.6976	9.7567 9.7458 9.7009	8 · 75 16 8 · 74 15 8 · 7069	0.2409	7.6768	0n1344 0'0757 0'1093
941 942 943 944 945	- 805 IV 13 - 805 X 6 - 804 IV 2	1426 956 1427 134 1427 310 1427 489 1427 665	19 25 0 23 49 5 6 36 3	14'365 185'105	+0'11 -2'05 +1'20	23.80	5 1.42 5 181.31 5 10.03	2 172 416 4 3 50 7 178 922 9 12 28 5 187 6 1	0 7028 2 0 7201 8 0 7258	9.7508 9.7295 9.7245	8 · 7465 8 · 7290 8 · 7235	0'5574 0'5546	7.6642 7.6751 7.6652	9.0960 9n0793 9.9650
946 947 948 949 950	- 803 II 20 - 803 VIII 16 - 803 IX 15 - 802 II 2 - 802 VIII 6	1427 990 1428 020 1428 167	18 8 ° 0	134'658	+0.46 -0.66	23.80 23.80 23.80	5 166 71 5 197 51 4 354 94	5 347 172 9 168 093 3 197 78 3 353 04 7 177 63	9 0.6935 8 0.6893 3 9.7349	9'7601 9'7641 9'7136	8.7559 8.7604 8.7157	0'5363 0'5364 0'5647	7 6726	0'0527 0n1658 9n6770

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Nr.	μ	γ	$\log n$	G	K	$rac{\log}{\sin g}$	$\log \sin k$	$\log \cos g$	$\log \cos k$	log sin ð'	log cosoʻ	N'	bei ⊙ gan		im M	ittag	bei U nt ei	i ⊙ rgang	F
								0					λ	φ G	λ	φ ι (l	λ	Ιφ	
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902	54'97	+0.1381	9,4305	175'76	91.32	9.6923	9 9 9 4 0 2	9'9397	926907	8.6208	9 9996	119.4	118	18 21	- 57	- 7	+ 5	+ 40 - 37	r
904	224 33	+0.9828 0.8346 1.1700	9'7561	167.95	93.Qx	9.0888	9.9447	9'9409	926762	9 '0645	9'9971	118.2	+ 64	+- 50 28		- 65		(十71) 82 	N . II
роб	335 24	- -r · 0805	9.7629	136'40	96'72	g · 6610	9 ' 9777	g•g48g	9114950	9.5249	9'9742	109.4	<u></u>	parading		_			$\left \begin{array}{c} 1 \\ p \end{array} \right $
908	337.55	1 · 4927 0 · 4449 0 · 3738	9'7143	315'15	96.69	g'6608	9'9788	9'9489	9'4845	9≈5334	9'9731	21.1	50		+ 27	- 48			$\frac{p}{r}$
910	79.13	0.3871	9.7408	302,01	95.66	9 6476	9 9875	9 9523	9'3732	9 25755	9.0669	75.5	142	+ 35	十173 81	+ 45 - 5		6 29	
912	278.85	-0.4003 -0.9574	9'7621	294'32	94'07	9'6322	9 19942	9'9559	9,5002	9115987	9'9628	79'8	+ 37	· 55	+ 50 + 77	r + 53		32 -i- 66	ß II
914	354 30	1.1722 1.0905 1.8692	9'7557	250 . 67	87.56	9'5642	9'9972	9'9687	9110559	915422	9'9719	97'0	u .	48	173	- - 81	- 53	1 62	P P P
916	157 . 18	···· 0 1 4 3 9 5	9 7299	238 47	86.77	9'5435	9.9933	9.9717	9,2411	9,4816	9'9791	100'5	- - 133	I5	159	44	80	35	
917	337.28	+0.0627 +0.2560 -0.6797	9 ' 7530 9 ' 7064	52'11 225'45	86 59 86 62	9'535I 9'5237	9 .9 909	9.9728	9'3060 9#3563	9.4422	g ' 9827 g ' 9866	77.8	39 95	- 8 + 27	+ 22 +151	- · I	I50	- - I	7. ^{cl} ;
920	196.46	+0.9348	9 7036	211.66	87.12	9 5201	9 9835	9 9747	9,4317	9 3447	9.9933	105'9	+148	+ 79	十142 十171	32 - - 66	158 130	+ 52	juli
922	112,63	1 · 1570	9.7585	27.89	87.27	9'5123	0. 0 818	9 9758	9'4531	9'2009	9'9945	73 3	P-12-14	-	BANGET B		*******	1000 cod	p
923 924 925	122.61	-1.2703 -0.4444 -0.5164	9'7207	340'77	91'94	9'4984	2086.6	9'9773	9'4708	920361	9'9974	72'7	+174	9 15	-127	+ 21		1 43	
	153.33	012965	9 ' 7036	327 ' 46	92'91	9'5085	g • 9840	9.9762	9'4271	912557	ე . ეე28	74'2	4-138	- 32	151	28	gr		,.
927	97 95 154 68	1'0092 1'0092	9'7650 9'7650	136'02 314'49	93 39 93 40	9'5238 9'5254	9 9879 9 9884	9'9743 9'9740	9 3573	9,3783	9 · 9872 9 · 9864	76.4	(十 g)	+ 24 (75)	97	25	34 38	- 3 - 64	(1)
930	50.95	- -i-1080	9 7479	269 24	89 88	9 5422	0.0000	9.0633	7n 6822	925965	9 9632	80.3			-1- 43			1 54	P
932	267.91	— I Об5о +о 3970	9.7649	257'37	87.01	9'6148	9 9985	9.9596	8,9157	9116059	9,3614	95'2	-i- 38				- -x5x		$p_{t^{\#}}$
934	144.78	-0'3166 -0'2758 +0'4556	9.7600	246.33	86.03	9'6315	9'9945	9'9561	9n x 977	9115998	9 9626	99.9	+148	- 6	146	40	68	24	1
		o gg86									į			٠			L.	(-67)	
937 938	335'II 93'98	-1'3627 -1'1905	9 · 7586 9 · 7478	25°77 49°36	83.23 83.81	9'6772 9'6540	919585 919830	9 9444 9 9507	9.4381 9.4381	9.3594	9'9884 9'9703	72'9			_				$\left egin{array}{c} p \\ p \end{array} ight $
940	129 45 228 45	+1'2860 -0'6151	9.7665	17'82	85'03	9 6854 9 6854	9 9520	9 9422 9 9418	9,6488	9,2233	9,5938	62'5	+ 82	- 64	+140	34	16o	- 10	$\begin{bmatrix} \mathcal{I}^j \\ t \end{bmatrix}$
942	110,80	+0.6034 +0.1247	9.7529	10.33	86'85	9 6896	9'9435	9 9406	9 6803	9.0006	9 9978	6r'2	172	21	-113	+ 14	51 43	+ 8 + 36	
943 944	179 ° 09 275 ° 34	-0'1200 -0'9226 -0'8102	9 7317 9 7266	183.64 2.87	88 84 89 09	9 6922 9 6904	9 9401 9 9406	9 9397 9 9403	9:6897 9:6897	8 4500	9 ' 9997 9 ' 9998	119'4	+119	+ 23 + 38	+179 —	— ro	—115 (— 30 + б4	36 (83)	ρ. γ.:‡:
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957 958 959 960	— 799 XI 29 — 798 V 24 — 798 XI 18 — 797 V 14	1429 556 6 45 4 1429 732 17 39 4 1429 910 10 3 6	53'715 228'545 43'678	-2'18 -2'48 -2'86 -2'17	23'801 23'801	355°198 178°419 2°646	167:352 357:549 176:370 3:730 186:949	0'7228 0'7020 0'7413	9.7266 9.7263 9.7523 9.7034 9.7645	8 · 7250 8 · 7270 8 · 7479 8 · 7092 8 · 7598	0.5518 0.5608 0.5373 0.5740 0.5306	7.6778 7.6622 7.6777	916434
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967 968 969 970	- 795 IX 16 - 794 III 13 - 794 IX 6 - 793 III 2	1430 943 10 26.3 1431 121 5 33.1 1431 298 2 50.6 1431 475 6 6.6	355.008 165.048 344.166 154.543 333.192	-0'77 +3'18 -0'16 +3'97	23.799 23.799 23.799	174.605 353.655 182.490 1.803 190.169	352·397 182·776 2·743	0.7323 0.6935 0.7446 0.6912 0.7384	9'7171 9'7596 9'7012 9'7623 9'7091	8.7178 8.7567 8.7060 8.7590 8.7122	0.5596 0.5388 0.5693 0.5366 0.5656	7.6663 7.6727 7.6677 7.6713 7.6691	9'7933 9#7349 9#3803 9'1869 9#9832
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977 978 979 980	790 VI 24 790 XII 19 789 V 15 789 VI 14	1432 685 15 16·3 1432 863 18 39·3 1433 010 17 24·6 1433 040 1 32·3	260 603 - 44 966 - 72 885 -	-0'07 -2'23 -2'18	23 801 23 802 23 802	4'016 191'110 343'198 12'686	1.878 193.532 341.575 10.425	0.4169	9 7207 9 7330 9 7579 9 7474	8 · 7202 8 · 7324 8 · 7527 8 · 7430		7.6763 7.6631 7.6770 7.6623 7.6625	9:4337 9:5727 9:9998 0:1556 0:0460
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960	335'4	18	0.607	6 9.766	52.4	86,28	9'5426 9'5360	9'9934 9'9910	9'9726 9'9719	9,3032	9,4807 9'4451	9.9792 9.9824	77'9	- 25 - 27 -	24 + 28 47 + 28	- 3	+ 87 + 87	- 4 - 24	t:
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1017	-773 I 26 -773 VII 16 -772 I 16 -772 VII 2 -772 XII 36	1438 916 18 44 1439 094 15 12 1439 270 22 11 1439 449 3 10	6 104 320 2 282 653 0 93 659 5 271 768	-0.34 +2.56 -1.00 +1.29	23 798 23 798 23 799 23 799	183'053 3'196 191'056	354.381 184.705 1.004 193.464	0'7436 0'6962 0'7281 0'7183	9.7635 9.7029 9.7563 9.7223 9.7315	8.7606 8.7068 8.7536 8.7215 8.7312	0'5667 0'5422 0'5551	7.6742 7.6649 7.6753 7.6639 7.6763	9.6236 9.6772 9.4205 9.4721 9.9991
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1037 1038 1039 1040	-764 VIII 5 -764 VIII 5 -764 XII 31 -763 VI 25	1442 047 8 32 1442 224 6 19 1442 372 13 42 1442 548 19 42	2 313 512 6 123 97 5 273 29 5 84 78	1 +4·46 7 +0·41 5 +1·47 7 -1·55	23'800 23'800 23'799 23'799	189.97 9 347.25 9 167.96	9 562 189 713 349 323 165 574	0'7378 0'6911 3'0'7444 5'0'7017 4'0'7218	9.7621 9.7012 9.7503 9.7302	8 · 7585 8 · 7055 8 · 7479 8 · 7280	0.5369 0.5691 0.5461 0.5504	7.6762 7.6633	9.9521 9.9809 0.0432
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1011	348 ' 64	+o'126	9.7639	162'15	91'82	9 4982	9.9798	9 ' 9774	9»4746	9.0052	9,0048	107.4	- 56	+ 25	· - 12	J. T2	+ 75	- 10	t ^{i‡}
1013	200'63	+o'859	9'7446	140'40	92.85	0.2106	0.0830	0,0440	04204	910490	9 9973	72'7 106'2	132 50	- 80	6 66	78	+ 71	- 47 + 42	かれ
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		10 01/0	g yaga	208 00	03.38	9.0783	grgarr	9 9439	926073	914010	9'9857	114.2	42	+ 59			+ 62	+ гз	grills
1025	72'73	0.100d	9'7501 9'7346 9'7234	26 · 12	83.67	6799	9'9584	9'9435	g • 620g	9'3678	9 9878	64'6	31	26	+ 25	- - ï2	+ 95	+ 24	Į#i
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1033	318.43	-0.5579	9 7033	34 X . 64	22,10	6858	9.0400	9.0410	920805	8,6000	9.9996	110,1		6o	+ 50	 49	+100	6	
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1036	263.81	-0'2140	9'7x18	(46,10	06.08	6733	0.0677		5770								+146	2 <i>4</i>	y.
1038	271'66	0'9570	9 7033	36.67	6'77 0	6624	9009	9403	9 5030	9114004	9.0800	07.5		+ 39 49	+ 49	+ 59	+ 60 (+ 72)	+ 73	S. It
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1050	83.50	-0'6466 -0'6466	9.2162	19.798	88.01 g	4988	9803	9773	9 4 6 9 6	0484	9 9973	72.7	-154	+ 23	- 89	+ 49	- 5	+ 57	7:4
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1051 1052 1053 1054 1055	-758 -758 -757	X 8 IV 3 IX 27 III 23 IX 17	1444 1444 1444	468 645	19	9'0 43'8 21'8	187 ⁹ 118 5'345 176'473 354'526 165'794	+1.08 +1.08	23'795 23'795	181'099 1'232	187 217	0'7450 0'6922 0'7366	9.7609 9.7013 9.7120 9.7120	8.7139	0'5394 0'5677 0'5388 0'5624 0'5494	7.6752 7.6651 7.6740 7.6663 7.6727	9n7608 9n0256 90225 9n9271 9'9207
1056 1057 1058 1059 1060		I 31 II 27	1445 1445 1445 1445	000 148 325 502	3 1 7 1	32.5 10.3 54.5 28.6	314.890 343.882 125.756 304.329 114.867	+3.21 +0.45 +4.25 +0.16	23'795 23'796 23'796 23'795	197 245 346 574 174 811	164.510 194.781 347.720 174.473 353.523	0'7146 0'7417 0'6895	9'7505 9'7378 9'7051 9'7639 9'7034	8 · 7474 8 · 7354 8 · 7087 8 · 7607 8 · 7074	0.5435 0.5483 0.5670 0.5366 0.5670	7.6716 7.6677 7.6673 7.6729 7.6660	0.0642 0n1846 0n1054 9.6438 9n7371
1061 1062 1063 1064 1065	-753 V -753 V -753 3	I to II 5 KI 30	1445 1446 1446 1446	856 034 210 358	5 11 16 20	12.0 34.4 13.6 25.9	241.305	-0.34 +2.57 -0.98 -2.07	23.797 23.797 23.797	2'421 190'948 11'037	193'340	0'7268 0'7198 0'7035	9.7553 9.7238 9.7301 9.7503 9.6997	8 7526 8 7230 8 7297 8 7461 8 7062	0.5422 0.5547 0.5572 0.5393 0.5763	7.6742 7.6649 7.6753 7.6639 7.6777	9#3973 9*3504 9#9964 9*9834 0*1148
1000 1067 1068 1069 1070	-752 X -751 -751 X -750	Y 5 V 5	1446 1446 1447 1447	712 890 057 245	19 17 1	25 · 2 14 · 0 26 · 1	229.801 45.738 218.549 35.432	-2'80 -2'23 -3'13 -1'70	23,798	173'460 358'928	178'645	0'7375 0'7071	9.7635 9.7080 9.7464 9.7339 9.7197	8.7583 8.7122 8.7423 8.7331 8.7190	0'5312 0'5715 0'5405 0'5562 0'5558	7.6622 7.6777 7.6623 7.6775 7.6628	9n9214 9'7918 8n9770 8n9895 9'8500
1072 1073 1074 1075	-749 II -749 II -749 II -749	V 24 X 18 X 18	1447 1447 1447 1447	569 599 746 776	6 2 18 2	19.0 24.0 42.1 19.1	167.236 196.870	+2'04 -0'86 -0'93 -2'72	23.799 23.799 23.799 23.799	345'526 15'782 165'502	187 · 487 345 · 022 16 · 267 167 · 193 197 · 549	0'7441 0'7439 0'6058	9.7575 9.7021 9.7026 9.7570 9.7630	8 · 7549 8 · 7059 8 · 7059 8 · 7535 8 · 7600	0.5423 0.5660 0.5404 0.5388	7.6768 7.6662 7.6634 7.6728 7.6761	9n8877 on1398 or1764 or0923 on1516
1077 1078 1079 1080	-748 11 -747 II -747 VII -746 I	I 3 I 27 I 20	1448 1448 1448 1448	101 278 455 632	7 1 1 5 12 5 16 4	18.2 22.3 18.2	345 456 156 562 334 838 145 675 324 389	-0'28 -3'85 -0'21 -4'35	23.798 23.798 23.798 23.797	173'729 1'811 181'736 10'172	l	0'7176 0'7072 0'7385 0'6907	9'7186 9'7332 9'7451 9'7083 9'7628	8.7589	0'5594 0'5532 0'5450 0'5667 0'5357	7.6689 7.6700 7.6704	9'2048 9n2177 9'9356
1082 1083 1084 1085	-745 VI -744 V	I. 7 I. 1 I. 25	1449 1449 1449	134 312 488	2 4 8 15 4	5 ' 4 5 ' 1	95°262 273°452 85°020	-0.00 +1.47 -1.53	23.796 23.796 23.796	167'155 355'102	188 · 987 349 · 267 164 · 749 357 · 326 174 · 097	0'7201	9.7015 9.7492 9.7317 9.7220 9.7560	8.7400	0.5698 0.5462 0.5498 0.5624 0.5356	7.6752 7.6640 7.6763	0n0481 0'0551 9n6555
1087 1088 1089	-743 XI -742 V -742 V	I 9 6 1 5 1 5	1449 1450 1450 1450	020 168 198	8 4 9 3 16 1 1 1	7 6 7 0 9 1 9 8	74 972 250 626 36 965 64 925	-2'05 -1'81 -2'40	23'795 23'794 23'794 23'794	9.618 163.782 193.267	184'812 8'456 166'206 195'343	0.400 0.400 0.400	9'7015 9'7644 9'7038 9'7393 9'7516	8 7076 8 7597 8 7095 8 7358 8 7470	0'5748 0'5307 0'5737 0'5449	7.6770 7.6626 7.6775 7.6627 7.6623	9'9616 0'1583
1095	-741 IV -741 X -740 IV	26 1 19 1 14 1	450 450 450	523 599 877	0 1 12 2 I 4	x · 8	209.080 239.295 26.551 198.241 15.847	-1 · 04 -2 · 78 -0 · 02	23 794 23 793 23 793 23 793	172'307 353'127 180'305	14.696 174.057	0 7221	9'7273 9'7131 9'7615	8 · 7402 8 · 7276 8 · 7143 8 · 7591 8 · 7055	0.5513 0.5604 0.5599 0.5396 0.5671	7.6769 7.6778 7.6633 7.6761 7.6642	0.1881
1097 1098 1099	/30 11	27 I	451 4 451 4	108 108	3 19 17 5: 0 9/	9 9 1 1 4 2	187 540 5 097 176 783 325 751 354 537	+1'11 -1'54	23 792	188'260 9'124 166'252	186 432	0'7122 0'7016	9.7135 9.7393 9.7517		0.5398 0.5609 0.5512 0.5418 0.5468	7.6751 7.6652 7.6739 7.6701 7.6664	928907 9.9103
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1054	120.82	-0 .8454	0.7141	353'25	00'72	9 4900	9 9/00	9 9779	924919	0.3948	9.9999	108.1	+178	rr 24	-116	+ 8	- 45 - 53	+ 12 12	$t^{i i}$
1055	322.08	0'8332	9'7430	162.64	91.80	9'5002	9:9794	9.9771	914779	8.9957	9 9997	107.6	- 57	一 7 ⁰ 十 73	+ 44	- 65 + 67	- 44 +117	- 40 + 39	r-t#
1056	65 ' 38	r · 1592	9 ' 7525	306.51	03'42	0,8400	0.0015	010000						_					
1058	200.82	x · 2747	9 7390	115'38	02'01	9.2032	9'9798	9'9768	9 4746	9n 0493	9'9973	72'5		Persona			_		p p
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K				1	1								+102	26	+ 155	12	-154	- 35	2'
		0'2496 0'2241 0'9917											+115	- 1 7	- x73	- 36	105	g	
1063 1064	348'34 61'88	-0.9917	9'7321	270'16 80'36	90'25	9'5947	0,0000	9 9635	7 0116	9 3924	9 9635	89'9	-147	- 66	(168)	十 36 (一74)	+170	- 66	
1065	132,38	+1.3027	9.7018	228.14	83.60	9.6561	0.0810	9.820r	9n 45 13	910048 915489	9,8408 9,8419	86'I		+ 6 o	(+116)	(+82)	+ 83	+ 64	p
1066	208 ' 44	o * 8354	9.7656	43'31	83'26	0.6614	0.0223	0:0486	7:40										
1067	123'95 83'77	0.8354 -+0.6191 0.0948	9.7102	217.91	83'04	9.6689	9 97/3	9'9467	9 4977	9°5234 9°14889	9 9743	70.2	163	- 55 + 55	+159 117	- 43 + 24	- 147 - 62	- 35 + 16	t
1069	201.36	0'0976	0'7361	208 63	83,30	0.6081	0'06'7	9 9409	9 5000	9 4009	9.9811	07:21	138	- 27	- 83	-+- XI	15	十 17	t^{ii}
1.070	A31 A4	+0.7080	9.7218	20'25	83.66	9.6795	9.9586	9 9436	o.ex50	9.3692	9,3822	64.6	+ 54	- 1g	+119	- - 65	128	+ 66	galli
1071	24'16 26'68	0'7722	9.7596	200.19	84 56	9 6842	9 . 9 5 2 0	9 ' 9422	9n 6488	912721	9.9922	117.0	102	23	- 34	71	- - 8g	74	$_{t}$
1073	272.79	-1.2010	9 7045	18.14	84'00	0'6842	9'9405	9'9404	9.6898	814181	9 9999	60'7	protecting	_		******	Processes.		$p \\ p$
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1077	291'46	0°609x 0°5674 0°1602	9.7353	349 54 9 163 00 9	34.85	9 6896 9 6868	9'9436 9'9486	9 9407	9 16801 9 16618	92058 912055	9'9978	61'2	16	65 61	- 59	50	— I	- 9 - 7	7' 2****
1079	13'60	o·1651	9.7105	154'74	6 25	0.6812	0.0643	9 9417	9.0509	912345	9 9935	02.0	- - 89	18	+x54	x	-148	-⊹ 36	t^{i}
1080	65.66		9.7649	333.28	6.34	9.6788	9.9589	9 9438	9. gr 82	923709	9.9876	64.7	-134	+ 33	- 76	+ 59	+ 38 58	- 34 + 75	t#
1801	16'62	o·8978	9.7037	45'83	16.03	0 * 6727	0:0677	0.045	a ## *#					11		ll ll			18
1082	226.04	-1.1140	9 ' 75 x 3 2	298 22 2	94.68	0.6376	9.9922	9 9547	9 2763	925919	9 9640	78:2						73	\mathcal{P}
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	7 34	-1.1397 -1.1290	9 /4+3	44 44 6	50 50 6	1 52701	0.087016	102201	2 2 5 7 5 10	1 2840	********	. HE . Y	_			_			p p
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1094	9 45	-0.2821	9 7 5 3 6 2	32'40 8	7'07 9	5022	9 9838 9	9760	4286	3. 22 Q X	9928	74 2	R + l_	- 70	🕶 🗸 📗			+ 61 - 52	riti t
1095	200'43	-0.0292	9.7038	19:56	8 '04 5	4973	9.0803	9773	4688	) · 042Ĭ	9973	72 8	+ 95	- 19	+×54	+ 5	-144		21.11
1096	47'23	+0.0000	9 7624	89.29	9 '02	9'494I	9.9785	9778	214878	317238	9994	(07:9	50 -	- 23	+114	+ 2	十178	- x3	t#
1098	87'22	+0.8134	9.7414 I	76.06 0	0'43	4930	9.9782	9.9779	9'4901 8	5544	9997	72'0	- 6 <i>H</i> l.	Foll	+141 80	- 53	-156	- 33	7.14
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1107 1108 1109	- 735 VII 15 - 735 XII 11	1453 121 0 2'0	293'950 104'335 252'499 66'235 241'010	-2.35 -1.03 -2.35	23 · 795 23 · 795 23 · 795	190 · 777 10 · 277 166 · 305 349 · 280 173 · 436	8'234 166'531 350'187	0'7021 0'7442 0'6g18	9'7517 9'6995 9'7629	8 7475 8 7062 8 7579	0'5575 0'5391 0'5763 0'5314 0'5708	7.6743 7.6648 7.6775 7.6623 7.6777	9n9908 9'9514 0'1164 9n9593 9'7926
1112 1113 1114	- 733 XI 19 - 732 V 15 - 732 XI 7 - 731 IV 4	1453 830 10 10 4 1454 006 22 25 0 1454 154 21 1 2	45.841 218.822 6.829	-2.81 -2.22 -3.14 +0.65	23'795 23'796 23'796	358 '055 181 '075 6 '722 188 '984 344 '777	8'753 187'543	0.7314 0.7314 0.6037	9 7448 9 7354 9 7182 9 7582 9 7028	8.7406 8.7345 8.7178 8.7559 8.7062	0'5414 0'5556 0'5565 0'5422 0'5671	7.6622 7.6777 7.6623 7.6774 7.6650	9n 2374 8n 9859 9'7977 9n 8851 on 1609
1117 1118 1119 1120	- 731 IX 29 - 731 X 28 - 730 III 24 - 730 IX 18	1454 184 12 50 8 1454 332 3 15 4 1454 361 14 10 2 1454 508 23 52 5 1454 686 15 17 4	178.239 208.038 355.087 167.482	-1'64 -3'09 -2'07 -0'94	23.796 23.796 23.796	14.893 165.255 196.845 352.816 173.399	167 034 197 584 350 653	o · 6898 o · 6898	9'7024 9'7559 9'7627 9'7202 9'7313	8 7056 8 7527 8 7596 8 7200 8 7302	0.5658 0.5418 0.5394 0.5576 0.5550	7.6628 7.6741 7.6768 7.6662 7.6728	0'1523 0'1002 0n1499 9n8244 9'7774
1122 1123 1124 1125	- 729 IX 7 - 728 III 3 - 728 VIII 26 - 727 I 22		156.499 335.190 145.387 295.481	-0'28 +3'83 +0'22 +3'70	23.796 23.796 23.795	1 261 181 295 9 696 188 820 346 974	182 698 8 946 188 331	0'7393 0'6904	9 7467 9 7070 9 7632 9 7015 9 7480	8.7106 8.7590 8.7061	0.5433 0.5683 0.5348 0.5706 0.5463	7 · 6676 7 · 6714 7 · 6689 7 · 6699 7 · 6741	9.0465 9.0912 9.9147 9.9274 0.0550
1127 1128 1129 1130	- 727 VIII 17 - 727 VIII 15 - 726 I 11 - 726 VII 6		105'781 134'442 284'557 95'509	-0.25 +0.46 +2.72 -0.85	23.795 23.795 23.794 23.793	18.000 166.396 196.630 354.979 175.056	163 978 194 522 357 151	0.7187 0.7300 0.7187	9 7587 9 7334 9 7193 9 7206 9 7571	8.7550 8.7309 8.7196 8.7218 8.7527	0.5382 0.5495 0.5595 0.5627 0.5355	7.6704 7.6650 7.6684 7.6752 7.6640	0.1826 0.0881 0.1846 9.6675 9.6302
1133	- 725 VI 20 - 725 XII 20 - 724 V 16 - 724 VI 15	1456 251 18 27.6 1456 428 16 20.2 1456 605 17 44.3 1456 753 23 24.6 1456 783 8 37.8	85 432 261 807 47 386 75 353	-1'49 -0'04 -2'28 -2'04	23'792 23'791 23'791	2'433 183'700 g'56g 162'924 192'40g	8 300 165 358	0.6905 0.7404 0.7156	9.7011 9.7643 9.7376 9.7376 9.7500	8 · 7594 8 · 7102	0.5746 0.5311 0.5729 0.5457 0.5387		
1137 1138 1139 1140	- 724 XII 8 - 723 V 6 - 723 X 29 - 722 IV 25	1456 930 7 14 0 1456 959 21 39 9 1457 108 6 50 3 1457 284 21 12 5 1457 462 8 15 8	250 511 - 36 976 - 209 415 - 26 301 -	-1.00 -3.15	23.791 23.791 23.790	345 . x63 17 . 089 17 . 444 353 . 066 179 . 463	14'668 173'104 352'221	0 · 7082 0 · 7209 0 · 7372 0 · 6909 0 · 7450	9 7433 9 7288 9 7117 9 7620 9 7015	8 7596	0.5508 0.5593 0.5603 0.5665	7·6775 7·6776 7·6627 7·6769 7·6633	0n1146 0'1870 9'9076 9n7706 8'7146
1142 1143 1144 1145	- 721 IV 14 1	1458 170 18 32·0	15.607 187.838 336.538 5.126	+0'02 -2'25 +3'75 +1'12	23'790 23'790 23'790	0'947 187'493 8'950 165'779 195'958	185 583 11 400 163 785	0.7135	9'7595 9'7151 9'7377 9'7533 9'7415	8.7571 8.7159 8.7364 8.7496 8.7381	0.5408 0.5594 0.5527 0.5403 0.5451	7.676x 7.6642 7.675x 7.6687 7.6652	8.9092 9.8476 9.9033 0.0887 0.1489
1148	- 719 VIII 17 1 - 718 II 11	1458 318 15 25 5 1458 496 0 38 2 1458 672 15 26 1 1458 850 16 37 1 1459 026 19 41 4	326 · 140 -	-4'30 -0'45	23.790 23.790	345 471 174 099 353 038 182 344 1 069	174'015 352'036	0.6897	9 7031 9 7643 9 7046 9 7532 9 7268	8 7078 8 7607 8 7086 8 7503 8 7259	0.5697 0.5349 0.5681 0.5418	7 6701 7 6701 7 6687 7 6716 7 6672	0n1402 9.6997 9n8231 9n3093 8.9925
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Nr.	μ	γ	$\log n$	G	K	$\frac{\log}{\sin g}$	$\log \sin k$	$\log \cos g$	log	log	log	N'	bei ⊙Auf- gang	im Mittag	bei ⊙ Untergang	$ig _{I^{r}}$
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***	2020				_		•									<del> </del>
1102	6x 6	-1.332 -0.467 -0.609	0 9 ' 7062 3 9 ' 7663	306.23	93°41	9.5356 9.5379	o.oore	9.9727	913039	9'4440	9 9825	10201				p
1103	307 ° 21 299 ° 72	-0.609 -0.230	6 9 · 7051	204'12	92.86	9:5537	9.9956	9.9703	92500	9:4532	9'9817	78 · 2	- 124 + 15 - 4 - 27	- 64 + 12 + 50 - 19	8 + 38 +100 43	t*
1105	4.83	-0.1220 0.1220	6 9.7277	102.28	91.24	9 5555	3.3382 3.3328	9.0075 9.0200	9'1415 8"8868	9:5205	9.9747	81. g	- 12 - 20	+ 61 - 33 - 4 + 31	+126 - E	t
птоб		1		I							l	1 1				2.5
1107	173.79	+0.894	29'7538	91 62	90.25	9 5754	0,0000	9'9669 9'9640	8,8713 8,0066	9n5667	9.0649	85'4	93 67	( 71)(79) 174 86	- 25 - 63	
IIIOG	320.36	~~0'0ID	ממפלי מום	62.80	Rairoi		D	2000	34 3430	9113434	9 9052	103.5	·		-	p
1110	247.09	0'620	3 9 . 7 1 1 1	227'75	83,22	9 6570	0.0810	9'9499	9 39 59 9 9 45 57	9"5476	9'9082	74'4	+ 28 - 57 + 73 + 51	+ 46 - 49 + 119 + 20	+ 95 - 45 172 19	
1111	192'06	-0.172	7460	43.40	80.00				;		,					ĺ.
1113	333 05	0.6276	ובסבלים	24.66	82:00		5 5 5 5 5 5	3 3400	943443	944000	9 9784	TII.O	28   I5	+ 28 - 24	-125 + 9 + 101 - 26	-1.
1114	157'41	-0.767	9 . 7603	208 92	83'40	9 . 6772	0.0616	0,0443	0.5040	9 4070	3 3010	07.3	- 46 + 15	+ 28 - 24 + 19 + 60 -167 - 72	+123 + 57	2,145
5	~JO:53	1 4488	9 . 7048	4.9x	88.46	9.6897	9.0413	9 9406	9 6876	8.6810	9.2995	60.8	25	72	- 41 - 69	p
1116	10.31	-  1'4200 -  1'2595	9.7044	26.16	83 70	9.6787	9 9 9 5 8 6	9 ' 9439	g· <b>6</b> rg6	0.3670	0.0820	54.6				
2218	32'18	-1.4125	0.7646	200 68	84 - 55	0.60.0	9 9403	9 9405	9110090	8.0934	0.0000	119.3		MALIANA BORNIA	-	$\begin{vmatrix} p \\ p \end{vmatrix}$
1119	177'93 51'05	0 6674	9'7223	357'20	00.80	9.6912	9 9 9 9 9 9 9 9 9	9 9400	9,6905	9n2779 8n4398	0,0608 0,0630	60.6	-109 - 71	-167 - 52	-109 - 12	p
					"	9 4907	9 9424	y gaoz	9110830	8.0412	9.9983	119.0	r3r  - - 65		+- I7 -I- 8	1.4
1121	321,30	-0'1113	9'7488	349'62	93.16	6897	9435	9 9 9 4 0 6	g·68o3	920027	9 9978	. 6r·2	27 22	+ 37 + 2	-l- 08 l-l- 9#	· t·
1123	188'72	-0'8217	0.7653	347'DY	25:00/	16850			3	5 2000	3 3349	117 0	-1-130 Lt. 30	127   1	7I 34	<i>"</i> .
1125	781,88 733,81	1'1350	9.7501	54 49 9 308 78	96.98	6518	9575	9,9432	926247	9'36or	9 9883	115'7	-1170 - 3x	136 57	-106 - 78 -113 - 75	1 1 1
					1	, , l,	, ,,,,	5 50-0	3 4.77	9"5014	9.9091	73 7	Managery Montaine			p
1127	75'18	1.5227 1.5227 1.5297	9.7606	333.67	6 23 g	6762	9593	9446	9'6165	9::3664	9'9879	64 8	`  ·	Perfeta	Married Married	<i>p</i>
1128	55.85	1'5297	9'7213	45 44	6 87 2	6707	3.896.6	9344	9n 2928	9'4595	9 9812	112.2	Winds months	trove person	Manage Bases	p
1130	70.75	-0'4650 0'4268	9.7592	00.38	3,4 20 5	, 6348 (	9.9918 9.9964	9544	9°2835	915916 916038	9'954x	78 o	-146 - 36 108 30	- 51 - 51 -169 + 49	8 14	1'
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1132	65.74	-l-0'2338 0'3149	9'7664	98'94 9	1.46 g	.6088	0 997 x   9	9.008	9 0609 9 8 2622	926051	0.0612	82.8	-153 + 6	- 96 - 10 - 66 + 5	- 42 - 19	grife Elle
1134 1	77'40	r - r 18a	0.7306	55.44 8	6.600		3397 8	, 9020	3317	Super 3 G	3.8053	87.0	-123 - 55	84 + 42	- 9 - 20 - 50 + 58	7:4
1135 3	08.75	-1'0822	9'7520	87.72	9 65 9	5915	9.9999	9640	3 · 1548	9.2013	9.0041	80.1 28.0	Smartes Livering		before brown	p = p
1136 2	94'97	1'3020	0'7453	28.16	6. 57 0					_						_
1138 2	86.60	+0.8084	0.2138	44 84 8	5 5 T 5	2032	999019	9050	30015	345800	) '966 r	92'8		**************************************		p
1139 1	42.75	-0'5806	0.7641 2	15'76 8	6.88 0	5742	900319	9743	30126	3 3850 0	9868	76.3	- II - - 39		+177 + 64	2 rote
11403	02.11	+0.0218	9,7037	32.28 8	7,108	5079 9	9839 9	9762	4279	3,3235	9929	74 2	- 3 - 13	-147 - 49 + 54 + 13	-119 - 18	214
1141	18'80	+0'0811	9.7616 2	02 90 8	7'74 9	5014 9	. 6086.	9750	n4620	MIIon	0063	.07.0	- 80 th av	- 18 - 3		t*
1143 2	12'08	+0.8004	017308 r	80 160 8	8.080	140500	1 a u B a l	9773	4/10	0322	9974	72 7	- 29 - 61	+ 30 - 41	+ 96 - 27	2.
1144 3	07'89	-1 2267	9 7553 3	31'66 9	2 74 9	5109 9	.0820 0	97759	4498 g	n 7404 g	9993	73.4	+ 83 <del> </del> 71	+154 + 54		1 · · · · · · · · · · · · · · · · · · ·
			7455	, 20,0	פובני פ	49729	9777 9	9774	4943	3 5568 9	9997	7x.8				2)
1146	55 '22 - 86 '51	-1'3810	9'7052 I	40'26 9	3 29 9	51929	9862 9	9749	n 3945 9	3394 9	9894	04.7				p
1148	53 03 -	-0 6654	9.7068 1	27 00 0	3 38 0	53500	90000	9740 9	38000	n35179	9887	75 5 -	+109 + 15 -112 - 28	+170 + 18 - 57 - 27		$t^*$
														- 63 - 28	0 0	$t_{ii}$
					3	9	22000	9/02/9	ma 504 g	51729	975 I	98'0 -	-178 13	-II4 + 25	- 53 - 3	7-11:
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1153	- 717 XII 22 - 716 VI 16	1459 205 3 57 1459 381 7 20 1459 529 12 33 1459 706 16 30 1459 735 23 46	263'670	+0'26	23.791	9'577 166'238	7.616 166.352	0'7008	9'7529	8 · 7490 8 · 7060 8 · 7573	0.2331 0.2360	7'6626	9.9198 0.1187 9.9198
1156 1157 1158 1159 1160	- 716 XII 10 - 715 VI 6 - 715 XI 29 - 714 V 26 - 714 XI 19	1459 883 12 28 1460 061 7 46 1460 237 18 31 1460 415 16 52 1460 592 7 19	7 252·211 6 66·570 7 240·990 56·237 1 230·046	-1'07 -2'34 -2'11 -2'44 -2'82	23.792 23.792 23.793 23.793 23.793	173 408 357 178 181 079	171'710 359'560 178'641	0'7359 0'7100		8 · 7 1 4 1 8 · 7 3 9 3 8 · 7 3 5 7 8 · 7 1 6 7	0.5699 0.5424 0.5548	7.6648 7.6775 7.6623 7.6777 7.6622 7.6777	9.7936
1162 1163 1164 1165	- 713 X 10 - 713 XI 8 - 712 IV 4	1460 740 3 39' 1460 769 19 15' 1460 917 11 49' 1461 946 23 4' 1461 271 23 24'	2 45 637 1 189 311 3 219 242 3 6 653	-2:33 -3:13 +0:95	23 794 23 794 23 794 23 794	152'103 155'080 195'811 352'103	166'937 197'649 349'889	0.7445 0.6974 0.6902 0.7281	9'7033 9'7021 9'7549 9'7621 9'7221	8 · 7053 8 · 7518 8 · 7595	0'5662 0'5658 0'5430 0'5401 0'5559	7.6623 7.6752 7.6774	0n 1824 0 · 1255 0 · 1062 0n 1495 9n 8640
1168 1169 1170	- 711 IX 18 - 710 III 14 - 710 IX 7	1461 448 17 18. 1461 626 3 55. 1461 803 8 59. 1461 980 3 45.	356 207 1 167 399 3 345 917 1 156 206	+2'06 -0'95 -3'03 -0'27	23 794 23 793 23 793 23 793	9 142 188 368	8*523 187*770	0.7048 0.2300 0.2300 0.2436	9.7636	8.7443 8.7099 8.7593 8.7065	0.2318	7.6662 7.6728 7.6676	9.7948 8.7466 8.9494 9.8890 9.29043
1174 1175 1176	- 709 VII 28 - 709 VIII 27 - 708 I 23 - 708 VII 17	1462 158 1 39 1 1462 1462 1462 1462 1462 1462 1462 14	335.610 116.357 145.197 295.606	+3.80 2 +0.23 2 +0.23 2 +3.71 2	23 · 792 23 · 792 23 · 792 23 · 792	17.531 165.697 196.121 354.790	163'274	o · 6956 o · 7170 o · 7287 o · 7289	9.7349	: .	0.5378 0.5492 0.5597 0.5628	7.6728 7.6689 7.6661 7.6699 7.6741	0n0642 0'1725 0'1078 0n1702 9n6848
1178 - 1179 - 1180 -	- 707 VII 6 1	1463 013 23 56 4 1463 191 1 48 3 1463 368 15 56 4	284 359 95 926 272 955 85 804	-2.69 -0.84 -1.41 -1.47 -2.76 2	3'791 3'790 3'790	2°282 182°894 9°480 191°573	2:813 183:477 8:109 193:795	0.7437 0.6905 0.7397 0.7055	9'7008 9'7639 9'7060 9'7486	8.7538 8.7067 8.7592 8.7106 8.7444	0'5742 0'5318 0'5719 0'5398	7.6640 7.6763 7.6632	9.6907 9.3416 9.3916 9.9542 0.0059
	705 XI 10 1 704 V 5 1 704 X 29 1 703 IV 24 1	1463 870 6 7.9 1464 047 14 40:4 1464 224 21 54:0 1464 401 16 58:8	47 379 220 626 36 720 209 835	-2 · 27   2 -3 · 13   2 -1 · 76   2	3.789 1 3.788 3 3.787 1	70 ' 553 3 553 ' 045 3 78 ' 580 3	72'120 352'305 78'276	0.7381 0.6903 0.7449	9'7106 9'7624 9'7020	8 7562	0 5582 0 5608 0 5399 0 5658	7.6623 7.6627 7.6627	0.1129 0.1851 9.9512 9.7713 9.1368
1190 — 1191 — 1192 — 1193 —	702 III 15 702 IV 14 702 IX 8 702 X 8 701 III 5	464 726 16 26 7 464 756 1 54 3 464 993 22 45 3 464 993 16 37 9	198.951 — 347.253 + 15.664 + 158.038 — 187.826 —	2.84 2 2.91 2 0.03 2 0.36 2 2.25 2	3 787 I 3 787 I 3 787 I 3 787 3	55 231 1 95 223 1 45 037 3	11.290 6 63.317 6 92.820 6 45.860 6	0.7148 0.6993 0.7104	9 ' 7361 9 ' 7546 9 ' 7431 9 ' 7023	8.7073	0'5542 0'5388 0'5436	7.6761 7.6672 7.6642	9n 7955 9 * 8994 0 * 1038 0n 1276 0n 1532 0 * 1907
1196 1197 1198 1190	700 VIII 17 14 699 VIII 6 14 608 I 14	465 436 0 48 0 465 612 3 10 9 465 790 11 53 7 465 966 15 5 2	140.909 + 325.537 + 136.048 + 315.867 + 125.556 +	0'17   23 4'27   23 0'46   23 4'48   23 0'45   23	3 787 I	52°522 3 81°954 1	73 675 6 51 412 6 83 934 6 58 149 6 92 527 6	0'7411 0'7011 0'7223	9 7644 9 7051 9 7521 9 7284 9 7260	8 · 7605 8 · 7093 8 · 7491 8 · 7275 8 · 7258	0.5342 0.5686 0.5417 9.5544	7.6687 7.6701 7.6686 7.6786	9 7332 9n8533 9n2317 8 6618 9n9708
1200 -	698 VI 28 14	465 114 20 30 9 465 292 0 1 9	274'806 + 87'133 -	1'62 23	789 1	56 · 129 1	56 · 128   c	7446	9 7539   8 9 6996   8	8·7502 8·7060 8·7567	0 5754	7 6762	9.8892 0.1222 0n0238

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1151	232°45	o · 9607	9.7293	294°58	92°86	9 ' 5558	9'9956	9'9700	9'1498	925194	0.0240	8104	23	~ Go	( 48)	(84)		f0	,.
1152	382.23	+0.8314 +1.3143	9.7550	103'21	91,80	9'5733	9 9986	9'9672	8, goir	0 5 6 3 3	0.0088	04.0	37	+ 55	+ 74	+ 78	+172	59 + 47	1
1154	72.12	o'9847	9.7644	62.01	85'49	9.6358	9.9927	9 9551	9 2578	9 ' 5939	0.0637	78.6	( 64)	(67)			32	59	t
1155	173.22	- -I:518o	9.7666	92,62	90.40	9.5917	9,9999	9 ' 9640	8,, 2154	9,29x3	9.9641	ðī,o	*****	Manual 4					$\mathcal{P}$
1156	10.03	+0.6217	9.7125	238.26	84.78	9.6430	9.9899	9'9534	9"3293	9 1 5 8 4 5	9.9653	103'4	51	+ 47	6	+ 17	+ 47	23	7.St
1157	399.05	0.2513 0.0969	9 7452	52'97	84'10	9'6500	9.0860	9'9517	9:3977	9 5 5 6 8 4	9'0580	74.4	· l· o	- 28	-l- 62	+ 7 - 25	+125	+ 1	/il:
1159	73.93	-0.5459	9.7189	43.56	83'25	9.0018	9 9775	9.9486	9 4960	9 5256	9'074X	70'6	145	I3	70	+ 55	+ 16	22 + 48	7:11
1,00	290 01	o·7662	9 7012	210 22	03 07	9.0078	9-9721	9 9471	9#5412	9#4904	9.9782	111.4	13	27	52	- 73	175	64	t
1161	239:34	-1'5220	9.7053	12.26	86:29	9 6869	9 9455	9'9414	9.6732	9 '0797	g ' gg 68	61.7		\$4+174** <b>4</b>			****		2)
1103	2.33	+1 3350	9.7569	186.20	87.92	g: 68g2	9'9419	9'9407	9116853	8,8148	o coor	IIO.O	*	arrivos.		Faceret	*****		$\frac{p}{p}$
1165	285.26 285.66	1'4110 0'7312	9.7640	4.77	83 · 44 88 · 50	9.6742	9.9627 9.9627	9'9451	9" 5991 9 6887	9#4069 8:6697	9'9853	60.7	 -+· 14	76	- - 86	- 54	+144	18	p
						!												1.5	
1166	77'38	+0'0558	9.7319 9.7503	178 gi	90.35	g.6g2o	0.0401	9'9398	a.6000	8 0323	0,0000	119.2	141	+ 68	165	+ 45	15	+ 9 + 33	ante l
1108	239.55	0.0800	0.4080	171,00	92'80	916916	9'942r	9'9399	946845	8'0445	0.0083	ira.o	. ⊢ 57	24	-I-IIO	I	4-178	34	,
1170	234 27	+0'7745 0'8022	9 7037	162.22	94 88	9'6872	9 9435	9'9408	9,6614	9,511 <u>0</u>	9'9979 9'9942	117.7	+ 58	25	+113	+ 56 56	96   152	1 78 77	
							' I			ĺ									
1172	197:34	1'1592 1'4877	9 ' 7598	342'06	94.90	9 6820	9'9506	9'9429	9 6543	9,2217	0.0030	62.8	Anny Park			Property as	B-1100M	m	$\begin{bmatrix} p \\ p \end{bmatrix}$
1173	83.22	1'4797	9 ' 7369	129'36	96,12	9.5515	9'9842	9'9513	9#4233	0'5581	ი ინინ	106.5	Marian and	\$1000 mm	AND ALES	******	Mark to M	Berthard	$\frac{p}{p}$
1175	184,11	0'4840	9.7215	309.16	96.12	9 653 r	9.9842	9.0200	9.4227	9 2 5 6 0 9	9.0602	73.5	4- gr		180	- 52	114	12	
1176	284'14	+0'4906	9.7603	110.88	94.93	9 • 6398	a, aort	010542	0113010	0.2884	o ' oб <i>a'</i> 7	102.6	11	1. 28	1- 70	-l- E2	- <u>⊬150</u>	-i- 15	£:#1
1177	211.21	0.5100	9,4030	298 ' 58!	94'76	9.6387	9,3919	9'9544	9 2826	9#5919	თ. ინ4ი	78.0	+ 88	-j- r	1-147	IO	I 6 I	+ 23	2.114
1179	203 02	0'2464 0'9000	9.7082	286.99	92.84	9.6212	9.9972	9 ' 9582	9.0483	0,6051	9'9615	83.0	- -118 - -112		180 	+ 41		21 60	
1180	57.98	-1,0134	9.7506	99,00	01.47	ე•60ეი	9,9993	9.9607	8,, 7651	9'6045	0.0010	93.6		portrang		Nov **	44	Print to 1	p
1181	65.08	_I '2970	9 ' 7466	241.02	86.84	9 . 5507	9'9942	9.9707	9,12128	914992	9'9772	99.8	8419214	gerenna.		******	p.o		p
1183	208.02	+1.2313	9 7325	274 72	90.75	9.6024	9,9998	ე ენ21	8 4799	9,6011	0.0623	88'1			3 r	8a	+ 97	67	$\frac{p}{r^{\rm diff}}$
1184	276'61	-0.1320 +0.1320	9 ' 7645 :	228'99	86.57	9.5306	9.9898	919735	943322	0#4103	0.0845	102.0	- - 8	22	+ 80	- 53	+169	- 47	t
1103	4~ ~/	70 1370	9 /042	44 07	30 03	9 5220	9 9003	9 9745	9.3017	9.3823	9.9870	76.3	102	6	- 43	- 22	+ 24	21	7
1186	151'43	+0.0762	9.7606	216:36	86.87	9'5140	9 ' 9850	9 9754	914110	9113025	9,9910	105.3	+149	+ 19	-151	- 7	- 85	II	
1188	340'19	-0.6259	9 7 3 8 2 3	203,13	87.70	9'5034	9'9809	9 9 9 7 6 7	914632	QUITT2	0.0062	107'0	34	+ 68	- 69 + 26	+ 49	+ 88	22	
11881	66.93	1.3415	9'7565	344 ' 54	91.64	9 5023	9 9788	9.9769	9 4846	820404	0'0083	72'2	Proposed		pm;	50000	p	P10-7-10	$\boldsymbol{p}$
-					1											,			p
1191	67.41	-1.4230 +1.2213	7044	153'20	92.28 88.07	9.506r 9.4087	g'g818	9.9764	9114517	9'1786 8"7208	9,0000	106.6		La comp	A	*****			2
1193	309 . 69	+0.24 role	9 * 7665   3	331,83	92.67	9 5068	gʻg824	0.0764	9 4465	021088	9 9945	73.6	15	+ r6	+ 46	1 -		+ 48	N .
1195	187.27	-0.1202 6	9 7542	310,39	93.30	9.2181	9 ' 9865 9 ' 9865	9 · 9750	9"3897 9"3884	9:3429 9:3472	9,8800 9,8805	75.5	++ 136   - - 103	- 30	157   174	- 35 23	113 124	- 58 + 5	
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1197	351.38	-0.0459 c	9.7281 S	307 '08	93 41	9 5370	9'9912	9:9726	0.2005	024485	0'0822	78.0	+ 67 133		+133 + 14	1 -	-168 -112	_	
1198	43.84	+0.7748 c	9.7560)	115'15	92.80	9 5542	0'0055	0'0701	0.1578	0'5161	0.0752	0818	146			+ 71			t ^{**}
1200	184 48	-I.0262	7636	73.50	87 25	9 6204	9 9974	9.9584	0,0321	9.6052	9.9612	93'5 83'2						March 1	$\frac{p}{p}$
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1202 1203 1204	698 VI 698 XI 697 V 697 XI 696 V	I 21 I 17 I 11	1466 1466 1466	468 646 823	20 4 14 5 3 1	6 · I	263.39 263.39	20'23 41'94 31'07	23.780 23.789 23.789	173°350 356°315 181°076	358 733 178 547	0.4173	9'7118 9'7413 9'7382	8.7600 8.7149 8.7377 8.7371 8.7155		7.6659 7.6769 7.6626 7.6775 7.6623	o'1643 9'7959 9"5177 8"9837 9'6651
1207 1208 1209	- 695 - 695 - 695 X	V 26 X 20 II 19	1467 1467 1467	355 502 532	1 3 20 2 8	35 · 6 19 · 6	56 or 200 43 230 46	5 -2'11 -2'42 6 -2'89 6 -2'81 7 -0'12	23.791 23.791	164 966 196 800	13,180	0'7447 0'6984 0'6907	9.7020 9.7537 9.7617	8.7573 8.7052 8.7509 8.7590 8.7225	0.5415 0.5658 0.5442 0.5405 0.5544	7.6777 7.6622 7.6762 7.6777 7.6641	9n8836 0.0963 0.1104 0n1497 9n9029
1212 1213 1214	- 693 I - 693 I - 692 II	V 5 X 29 H 24	1468 1468 1468	034 211 388	0 5 11 3 16 5	36 · 4 36 · 8	6.79 178.36 356.57	3 -2 35 1 -0 96 9 -1 06 6 +2 00 7 -0 92	23.791	172 '963 359 '940 180 '645 8 '510 187 '99	357'750 181'857 8'036	0.7036 0.7405 0.6899	9'7499 9'7049 9'7640	8·7596		7.6650	9*8076 7#7216 8#7898 9*8580 9#8837
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122 <u>7</u> 1228 1229	- 687	ll 30 V 27 (l 20	1470 1470 1470	130 278 455	14 19 15	39'7 55'9 5'2	272 87 57 76 231 8	4 -2'00 4 +1'37 9 -2'46 7 -2'75 8 -2'26	23.78 23.78 23.78	345 17 7 17 01 7 169 64 6 353 04 6 177 67	5 14 55 8 171 11 4 352 40	2 0.238 2 0.239 1 0.239	9 7 7 3 2 0 1 9 7 7 0 9 4 3 9 7 7 6 2 7	8 7312 8 7112 8 7604		7.6763 7.6622 7.6777	9.9915
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1237 1238 1239	- 684 I - 684 - 683 I - 683 I - 682 I	X 19 H 15 X 8	1471 1471 1471	519 666 843	0 16 6	39°5 48°7 4°3	198.9 157.7	17 -2.8 56 +2.8 10 -0.3	1 23 78 8 23 78 4 23 78	5 16'4	57 18°04 58 173°25 53 350°88	6 0'737 6 0'690 32 0'740	5 9.708 0 9.764 5 9.706	9 8 712 3 8 750 9 8 710		7.671	9.7696 9.7696
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1257 1258 1259	- 675 IV 15 - 675 X 9 - 674 IV 5	1474 442 1474 619 1474 796 1474 974 1475 150	8 22.0 19 25.0 0 41.5	17:328 189:404 7:174	-0'11 -2'35 +0'94	23.788 23.788 23.788	172.845 359.187 180.428 7.813 187.695	357.074 181.542 7.489	0'7226 0'7023 0'7410 0'6897 0'7424	9.7264 9.7513 9.7039 9.7644 9.7024	8.7264 8.7468 8.7088 8.7596 8.7075	0.5598 0.5387 0.5723 0.5321 0.5724	7.6752 7.6651	9.8159 8,8521 8,6121 9.8209 9,8670
1262 1263 1264	- 673 III 25 - 673 VIII 19 - 673 IX 17	1475 328	17 26.4 8 31.9 21 46.4	137'704 166'929	+0'44 0'99	23 '788 23 '788 23 '788	345'996 16'358 164'513 195'350 354'180	18'078 162'100 193'082	0.7258	9 7558 9 7380 9 7234	8.7412 8.7515 8.7354 8.7234 8.7181	0'5376 0'5490 0'5596	7.6700 7.6663 7.6688 7.6727 7.6715	0,0899 0'1456 0'1384 0,1466 9,7352
1267 1268 1269	- 671 VII 28	1476 007 1 1476 184 1 1476 361	17 44.2 15 22.3	306.367 117.058	+4'29 +0'28	23.787 23.787 23.786	181 '441	171'674 2'083 182'305 7'584 192'354	0'6938 0'7442 0'6912 0'7379 0'7080	9'7599 9'7005 9'7629 9'7082 9'7453	8.7557 8.7559 8.7584 8.7119 8.7416	0.5358 0.5729 0.5335 0.5693 0.5426		9 17791 9 2337 9 0896 9 19369 9 9468
1272 1273 1274	- 669 VI 8	1476 715 1476 864 1477 041	23 3'4 2 27'2 0 4'5	253*957 283*995 68*157 243*095 57*500	1.38 1.38	23.786 23.785 23.785	345'183 16'911 168'740 353'955 176'751	342'949 14'433 170'110 352'517 176'217	0'7044 0'7170 0'7399 0'6895 0'7443	9'7472 9'7337 9'7082 9'7630 9'7026	8.7452 8.7325 8.7101 8.7608 8.7061	0'5553 0'5621 0'5397	7.6753 7.6623 7.6777	0,1102 0'1787 0'0284 9,7699 9'4955
1277 1278 1279 1280	- 667 V 16 - 667 XI 10 - 666 IV 6 - 666 V 5	1477 750 1477 897 1477 926	6 28.7 3 42.9 7 52.6 16 28.1	46.924 221.304 8.489 36.611	-2'22 -3'15 +0'78 -1'74	23'783 23'782 23'782 23'782	184 956 8 764 163 917 193 611	11'195 162'195 191'296	0'7306 0'7173 0'6973	9'7199 9'7329 9'7572 9'7465	8.7326 8.7527 8.7423	0'5555 0'5568 0'5360 0'5409	7.6624 7.6774 7.6649 7.6628	8.8753 9.6648 9.8981 0.1379 0.0772
1283 1284 1285	- 665 IX 19 - 664 III 15	1478 252 1478 428 1478 606	0 43'3 13 38'6 16 39'5	358 · 313 168 · 645 348 · 038	+1'84 -1'01 +2'87	23.487 23.487 23.487	10 309 172 446 351 744 180 937	17.864 172.774 350.429 183.056	o'6903 o'7397 o'7035	9.7011 9.7078 9.7642 9.7066 9.7497	8.2108 8.2000	0'5712 0'5328 0'5694	7.6768 7.6661 7.6729	9#8947
1288 1289 1290	- 602 VII 19	1479 137 1479 285 1479 462	15 13 1 7 2 6 9 15 13 1	337'486 147'050 296'924 108'178	+3.43 +3.80 +3.80	23'783 23'783 23'783	359'516 189'334 7'908 165'750 346'031	357.221 191.561 6.218 165.522 347.481	0'7268 0'6974 0'7445		8.7232 8.7526 8.7061	0'5575 0'5394 0'5737	7.6689 7.6700	8,15435 9,19348 9.8339 0.1336 010751
1293 1294 1295	- 660 VI 27	1479 639 1 1479 817 1479 993 2 1480 171 1	5 19·5 20 25·9 12 49·2	285 638 97 929 274 573 87 464	+2.83 -0.67 +1.58 -1.32	23.784 23.784 23.784 23.784	15 230 173 143 354 682 180 994 3 162	16.622 171.209 357.143 178.592 4.888	0.2100	9.7642 9.7378 9.7443 9.7413 9.7123	8.7168 8.7348 8.7396	0'5662	7.6752 7.6641 7.6762	9.8081 9.6797 8.9472
1298	- 660 XII 21 - 659 VI 16 - 659 XI 11 - 659 XII 11 - 658 V 7	1480 525 1	4 19 0 4 2 4 :	76.794 222.816 252.037	-1,00 -3,11 -1,61	23.785 23.785 23.785	188 949 11 199 164 881 196 795 349 667	11.113	0.7448 0.7004 0.6919	9.7017 9.7514 9.7606	8.7052 8.7490 8.7580	0.5403 0.5660 0.5462 0.5410 0.5515	7 6627 7 6774 7 6774	0.0310
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252	297'81 265'24	-0'7637 +1'1607 +1'2977 -1'4137 -0'8714	9.7038 9.7545	52.87 203.34	84 09	9 6498 9 6806 0 6533	9.9859 9.9827	9'9517 9'9508	9.3987 9.6336	9 · 5078 9 · 3251 9 · 5504	9.9901	116'1		9 -125 - 6		$\begin{bmatrix} p \\ p \\ p \end{bmatrix}$
:256 :257 :258	63.54 305.80	+0.6545 -0.0400	9.7285 9.7534 9.7061	194.91	85.66 86.27 87.88	9.6880 9.6886 9.6922	9.9467 9.9449 9.9410	9.9410 9.9408 9.9398	9,6686 9,6756 9,6883	9,1528 9,0797 8,8190	9'9955 9'9968 9'9991	00.8 01.2	112 6 5 3 172 2 170 1	7 - 54 + 4 2 + 55 + 7 - 114 2 + 163 + 5	0 + 3 + 13 2 +121 + 22 6 - 51 - 32 - 109 + 70 7 - 36 - 70	). [*
1262	76.17	-1'2300 +1'3983 +1'3753 -1'4017 -0'5435	9'7577	357.82	3 96 · 72 3 96 · 72	9.6877 9.6717	9'9413	9 9 9 4 1 2 1 9 1 9 4 5 9	9 9 687; 9 9 683 9 9 681	8 · 9 6 0 :	r   0 , 0 0 8 3 4   0 , 0 8 3 4 9   0 , 6 6 6 6	113.5	special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and special parameters and	II I .		
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1272	159'17	7 1 · 2887 1 · 2097 1 · 5097 0 · 5887 0 · 5887	9.7352	297.6 80.3	8 94 59 0 88 6 2 87 9	9   9 * 636, 8   9 * 578; 6   9 * 569;	1 9 , 9 8 1 9 , 8 8 1 8 , 8 8 1 8 , 8 8	4 9 ' 954 2 9 ' 966 2 9 ' 967	9 9 207 4 8 772 9 8, 963	3 9 . 573 1 9 . 555	9 9 . 940 9 9 . 964	3 86·	4 — — — — — — — — — — — — — — — — — — —	28 1174	57 - 98 - 3	$\begin{bmatrix} p \\ p \\ t \end{bmatrix}$
1275	278 °0; 3236 °7; 300 °7;	3 +0.0756 7 -0.4623 4 +0.7908 5 +1.373	9 · 722 9 · 735 7 9 · 759	1 56.4 0 229.7 1 10.2	4 86 . 7 o 86 . 5 8 88 . 8	1 0 540	2 9 . 992 9 9 . 977	5 9 9 9 7 2 0 9 9 9 7 7 9 9 9 7 7	29,320	0 9 40 9 7 9 42 5 8 7 7 4	1 9 984 7 9 999	3 78° 0 102° 2 71°	9 + 30 7 + 80 + 8	61 128	11 -142 1	38 r ⁴
128	3 130.Q 5 310.1		29.766	3 357 9	3 90'2	29.517	0 9 977	8 9 975	78 9 49: 78 9 49:	37 8 207	45 0 000	36 107	8 + 99 +		42 - 121 - 51 - 32 - 10 - 4 -	
128	7 222 7 8 283 7	1 -0'035 9 -0'860 2 +0'682 0 +1'360 5 -1'188	6 9 · 725 2 9 · 758 2 9 · 702	3 332 5 1 140 0	55 93 ° 2 16 92 ° 0	3 9 5 0 6 3 9 5 1 8 5 9 5 5 6	0 9 986 7 9 986	31 9 97 32 9 97 32 9 96	79 8 9 44 79 8 96	94 9" 16 26 9 34 56 9" 55	58 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	93 104 00 84	7 - 14 +	73 + 144 - 56 + 81 +	58 +154 +	18 1 th 42 1' 28 1 th - 1' 2'
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120	7 33 5 8 37 6	8 -0.760 -1.074 -5 +1.302 -1.415 -0.946	0 9 703 3 9 753	38 62° 34 212° 25 230°	82 85 1 29 83 1 55 85 1	47 9 63 22 9 67 01 9 63	519.99 289.96 979.99	27 9 95 56 9 94 97 9 95	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	95 9 59 329 9#43 96 9#58	379 9 96 361 9 96	31 113 51 102	1.4			51 t p p p p p p p p p p p p p p p p p p

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1302 1303 1304	- 657 IV 26 - 657 X 21 - 656 IV 15	1481 204 15 4 1481 382 3 2 1481 559 8 2	18"7 211°791 47'2 27'820 21'0 200'497 22'3 17'719 39'4 189'093	-1.07 -2.88 -0.12	23'786 23'786 23'786	358·385 180·276 7·057	181,582	0'7238 0'7010 0'7417 0'6898	9'7527	8 · 7253 8 · 7481 8 · 7082 8 · 7596 8 · 7079	0'5612 0'5376 0'5734 0'5314	7.6633 7.6762 7.6641	9.8214 9.1489 8.4223 9.7771 9.8538
1307 1308 1309	- 655 IV 5 - 655 VIII 29 - 655 IX 28	1481 884 15 2 1481 914 1 1482 060 16 2 1482 090 5 4	6.8 7.582 21.4 148.485 17.6 177.908	+0.88 +0.12 -1.64	23'786 23'786 23'786	15'666 164'032 195'084	347.856 17.482 161.637 192.776 355.677	0.6990	9 7548 9 7394	8 · 7396 8 · 7504 8 · 7368 8 · 7248 8 · 7168	0.5462 0.5374 0.5490 0.5595 0.5626		0,1050 0'1285 0'1499 0,1376 9,7658
1312 1313 1314	653 VIII 8	1482 593 1 1 1482 769 23 1 1482 947 1 2	13'9 127'712 27'0 306'078	+4'47 +0'49	23.785 23.784 23.784	1 · 407 180 · 809 8 · 875	181.802	0'6929 0'7444 0'6915 0'7373	9.7006 9.7623 9.7093	8 · 7566 8 · 7058 8 · 7580 8 · 7126 8 · 7401	0'5363 0'5721 0'5344 0'5678 0'5442	7.6715	9.8112 9.1324 8.8392 9.9234 9.9234
1317 1318 1319	- 651 VI 18 - 651 XII 12	1483 301 7 2 1483 449 8 5 1483 626 9	81'6 295'059	+3.65 1.82 0.87	23.783 23.783	16'741 167'844 353'049	342.965 14.259 169.115 352.610 175.184	0'7158 0'7406 0'6894	9.7486 9.7351 9.7071 9.7633 9.7030	8.7463 8.7337 8.7094 8.7608 8.7064	o'5538 o'5631 o'5393		0,1096 0,132 0,0619 0,7702 0,6031
1322 1323 1324	- 649 XI 21 - 648 IV 16	1483 981 0 3 1484 157 13 1 1484 335 12 1 1484 482 15 2 1484 511 23 4	(3'2 57'323 (8'4 232'521 27'4 10'023	2'41 2'74	23, 280 33, 281	184.064 8.461 163.164	2.563 181.879 11.179 161.552 190.479	0.6963 0.7291 0.6963 0.6960	9'7314 9'7583	8.7537 8.7209 8.7312 8.7536 8.7439	0'5546 0'5579 0'5350	7.6640 7.6640	8.8805 9.5777 9.8992 0.1562 0.0480
1327 1328 1329	- 648 XI 9 - 647 IV 6 - 647 IX 29	1485 013 21 2	30'0 221'239 8'00'5	-3'14 +0'75	23.780 23.780 23.779	16.315 171.748 351.475	344.687 17.711 172.223 350.059 182.501	0.7390 0.7390	9 · 7066 9 · 7640 9 · 7075	8.7114 8.7597 8.7114	0.2602	7.6741	9.8455 9.8455 9.9076
1333 1334	- 045 IX 8	1485 722 15 1	5'6 157'911	-0.33	23.779 23.779	7.512	190.940	0.7283	9.7568 9.7006	8.7216 8.7538 8.7063	0.5575 0.5396 0.5729	7.6675 7.6715 7.6728	8,8055 9,9092 9,8107 0,1423 0,,0963
1337	043 VII 19	1486 224 20 5 1486 402 12 3 1486 570 4 5	67'7 296'680 6'0 108'458	+3.77	23.780 23.780	172,949 353,933 180,882	16.272 170.945 356.400 178.504 3.967	0.7322 0.7163 0.7088	9.7159	8.7180 8.7335 8.7409	0.5478	7.6740 7.6651	9117383
1342 1343 1344	- 641 I 1 - 641 VI 27 - 641 XI 22 - 641 XII 22 - 640 V 17	1487 288  IO =	13'7 87'209 52'9 234'042	-1.32 -2.65 +0.29	23 782 23 782 23 782	10,305 164,881 196,766	187.913 10.100 166.995 198.001	0'7449 0'7015 0'6026		817055	0.5472	7.6769 7.6769	0'1158 0'1507
1347 1348 1349	- 639 V 6 - 639 X 31 - 638 IV 26	1487 613 8 4 1487 789 23 1487 967 11 2 1488 144 15 5 1488 321 10 3	9'9 38'272 31'6 211'637	-3'17 -3'17	23 782 23 783 23 783	357°543 180°171 6°246	175°037 355°607 181°075 6°228 186°280	0.7000 0.7422 0.6898	9'7541 9'7023 9'7647	8.7493 8.7078 8.7597	0.5364 0.5744 0.5310	7.6627 7.6769 7.6633	9,3301 8,2149 9,7243

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1301	189°71	o · 6628	9.7270	203°33	84°02	9.6825	9 ' 9552	9.9428	926355	9n 3274	g, ggoo	116°2	-+129 -+ 6	5 +179 + 3	i -124 -+ 1	5 24
1302	58.25	o'140g	9.7548	20.33	84.24	9.6840	9 9 5 2 2	9'9424	9 6483	9'2747	9'9922	63.1	-115 - 3	1 — 56 H	2 + 0 + 1	8 t
1304	304'21	- -o*5986	9.7667	12.80	86.50	9.6879	9 9 4 5 4	9.8411	9'6737	1080°C	9.9967	61,6	15 - -	3 + 47 + 5 5 + 128 - 5	+140 + 6	64 t*
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1306 1307	49'97 192'49	-1 ·2763	9'7448 9'7567	344°76	94'37 88'31	9 6860 9 6875	9'9476 9'9420	9'9417 9'9412	g•6658 g•6849	9n 1595 8 · 7261	9'9954 9'9994	61.0				$\begin{bmatrix} p \\ p \end{bmatrix}$
1308	68.85	1.3727	9'7413	156.60	95'87	9'6789	9'9560	9 '9438	9,6317	9.3240	0,0001	116.0				
1310	173.60	0.5845	9.7178	336'78	95 97	9 ' 6827	9.9550	9 9426	9.6360	9n3259	9,8800	63.4	- <del> </del> - 98 6	-165 - 5	-105 -	9 1.
1311	277.22	10.6474	9.7626	148.45	96.77	9.6741	9 ' 9 <b>6</b> 46	9'9452	925883	9.4312	9.9836	113.4	- 17 - 6	+ 90 + 6		6 th
1312	167.81	-0'1356 -0'0691	9 · 7028	328.08	96·85	9 6556 9 6556	9'9648	9 · 9448 9 · 9476	9.5875	9:4372	9.9831	66.3	+102 - 1 +122 + 1	5 165 5 168 1	7 142 3	30 2 4
1314	195'02 30'34	+0.8383 0.8272	9.7115	318.22	96.86 96.25	9'6646 9'6535	9 9754	9.9479	9.5150 9.4363	9,5131	9.9756	107.0	+105 + 3 - 89 - 3	4 -1-156 -1- 4 5 37 3	1 1 .	- 1
1317	282.80	1 4900	9'7371	308.30	96.03	9'6506	9850	9'9515	9.4116	9115627	ე . ენ8ე	73 9	********		\$0-0000 Build	- 2
1319	317.23	0 · 5891	9'7654	267 02	89.55	9,2896	9,8888	9 9644	82704	925891	9'9645	91.5		2 -1- 42 5	9 +128 - ;	34 t
1320	330.22	+0.4010	9.7052	80123	88.62	9.5780	9.9992	9 9665	8.7752	9.5725	9.9674	86.3	4I - - I	8 + 29 - 4	6 103 :	25 1.4
1321	190.01	+0.0750	9'7579	255 21	88.03	9.2201	9'9983	9'9677	8,,9467	925574	9.9697	95'4		9 +170 1	· II	1 Z ^{1 1}
1323	5'20	0.3783	9 7335	242 '62	86,06	9.2200	9'9947	919706	gu xgoc	9 . 5052	9'9765	99'4	47 5	7 2 3		40 7"
		-1.116							9'4684				. 1	annesse grand		- P
1326	151'5)	1.502	0.7026	193'43	88150	0.4076	0.0788	9.9776	024842	8,,8848	0.0087	107.8	3	proceeding (processor)		p
1327	72.32	+x'533	9'7086	229 ' 41	86'53	9'5332	9.9898	9'9731	913306	9,4246	9'9841	102.8	3		1 -130	- P
1329	144.83	3 0 18 084	9.7096	179 53	3 90.05	9'4923	9'9780	9.9780	924923	7'4249	0,0000	108.1	( 143 3		8 73	72 1
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1333	47'55		9.7589	153'00	92.28	9 5052	9.0820	9'976	92450	9.1802	9'9950	106.6	5] x 3 x   £	6 - 43 + 5	1 + 26 +	23 tili - 1)
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1336	290.28	3 +1 323	0 9 ° 76 5 8	140.0	1 93 ' 31	9'5215	9'9857	9'974	5 924009	9.3362	9.989	104 '	,			_
1338	10.26	5 0 ' 547	19.7383	95'94	1 90 87	9 5847	9 9998	9 965	3 8 1 5 6 4 9	9.5827	9 9656	92.	8 65 2	3 -134 + 3 8 - 11 - 1	1 + 41	32 1-6
1339	251'12	4 0 . 078	19'7449	272 86	5 90'43	9 589	9 9999	9'964	18.252	925891	9 9645	88 9	9 + 44 -	5 +109 - 2 0 -113 + 3	7 +173 -	3 2-14
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1342	129.3	4 +0'989	9 . 2040	73.28	87.21	9 620	9 9978	9 958	4 9 041	2 9 605	9.9616	83	r + 89 + 6	1 -102 - 7 2 (+ 47) (+7	1) + 43 +	47 t 66 r
1344	338 7	3 - -1 ' 305 4 1 ' 414	79.7619	250 76	5 85 78	9 624	9 996	9'957	792103	926033	3 9 9 6 1 9	981	o	- projection (0.000)	anning to	$- \mid p \mid$
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1346	316.0	Ho · 667	9.7256	212 2	3 83 · x 6	9 674	9 965	9 945	92584	924393	9.9829	113	6 + 6 +	51 + 52 +	+ 108 +	18 1-4
1348	353'5	10.019	4 9 7045	203'I	2 84 0	2 g ' 683	5 9 954	8 9 942	5 92637	3 923253	3 9 ' 990	1 116	3 48 :	36 - x67 + 35 + 6 -	3 + 73 -	27 1
1349	59 5 339 3	2 +0'530 2 -0'697	9 7668 7 9 7056	20.6	5 84 49 3 85 7	9 9 688 9 9 688	4 9 952 8 9 946	9 942 2 9 940	4 9 · 646 8 9 <i>n</i> 670	5 9 · 280: 4 9 · 143	9.991	8 118.	2 - 129 +	5 66 6 10	7 + 26 + 50 +113 -	57 to
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1352 1353 1354		1488 499 1488 646 1488 675	8 40'7 o 21'9 13 57'9	349°721 18'117 159'341 188'951 339'076	-0.17 -0.43 -2.35	23 · 783 23 · 783 23 · 783	14.909 163.636 194.888	347°316 16.825 161.264 192.544 355.091	0'723I 0'7108 0'7003	9.7535 9.7410 9.7261	8 · 7381 8 · 7490 8 · 7384 8 · 7261 8 · 7156	0.5463 0.5376 0.5490 0.5596 0.5625	7.6641 7.6716 7.6752	0,1239 0,1089 0,1268 0,1309 9,8022
1357 1358 1359	636 VIII 29 635 II 23 635 VIII 19 634 II 12 634 VIII 8	1489 178 1489 355 1489 532	8 30 0 7 13 9 9 4 5	328 087 138 435 316 986	+4'22 +0'43 +4'47	23.783 23.782 23.782	0'957 180'251 8'525	181.372	o'7446 o'6919 o'7364	9.7610 9.7006 9.7006 9.7109 9.7419	8 · 7055 8 · 7575	0.5366 0.5712 0.5357 0.5661 0.5459	7.6687 7.6400	9'8371 8'9652 8n3314 9'9051 9n8885
1362 1363 1364	— 633 II г — 633 VI 29 — 633 XII 23	1489 857 1489 886 1490 034 1490 211 1490 388	15 33'6 15 30'0 17 57'3	306.055 88.985 265.532	+4'27 -1'21 +0'45	23 781 23 781 23 781	16'503 166'967 353'020	342.052 14.012 168.132 352.691 174.162	0'7144 0'7412 0'5891	9.7500 9.7365 9.7060 9.7635 9.7037	8.7350 8.7610	0'5463 0'5519 0'5640 0'5390 0'5649	7.6769	0"1103 0'1658 0'0923 9"7717 9'6881
1367 1368 1369	- 632 XII 12 - 631 VI 6 - 631 XII 1 - 630 IV 27 - 630 V 27	1490 742	19 59'8 20 54'1 22 58'4	67.723 243.743 29.514	1'20	23'779 23'779 23'779	183 · 180	180'940 11'166 160'869	o.6972 o.7277 o.7198 o.6955 o.7046	9'7549 9'7231 9'7299 9'7594 9'7496	8.7528 8.7222 8.7300 8.7545 8.7452	o'5440 o'5537 o'5588 o'5340 o'5389	7.6623	8.8829 9.4696 9.9009 0.1749 0.0165
1372 1373 1374	- 630 Xl 21 - 629 IV 17 - 629 X 11	1491 599	1 5 17'1 5 10'7 5 17'1	202 060 232 437 19 441 190 566 9 267	2'74 0'31 2'43	23.778 23.778 23.777	170'995 351'277	171.284	0'7444 0'7398 0'6911 0'7378 0'7065	9.7002 9.7057 9.7636 9.7085 9.7470	8.7106	0'5753 0'5730 0'5320 0'5698 0'5418	7.6763 7.6777 7.6641 7.6752 7.6650	9"9166
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1383 1384	- 625 II 3 - 625 VII 30	1492 002	15 52'3 4 50'3 19 56'6	307.659 119.042	-0.38 -4.33 -4.0.35	23.777 23.778 23.778	15 343 172 686 353 245	346.408 15.998 170.615 355.714 178.362	0.4148	9.7634 9.7342	8.7601 8.7190 8.7320	0.2361	7.6714	9.8337 9.7862
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1454	120'9	7 1 30	87 9 7	545	311,50	95 79	0.0234	9 9 9 7 2 9 9 5 4 4 9 9 8 2 5 9 9 5 6 2	9'9429	0,6385	0,3100	0.0002	116'4	84 	- r	26				
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1461	327 · 43	0'13	199.7	287	102:39	92'04	0,0140	9.9986	g <b>'</b> <u>95</u> <u>9</u> 8	8.19072	9 6054	9'9615		- 29		  -  - 32	ł		12	y:#1
1464	150.87	.1.53	7 9 7	016:	233, 53	86.60	9.5905	9'9992 0'0000 9'9914	9.0632	7#9014	9.5964	9.9632		75 1176	·l· 44	28 143	+ 29 39	+ 15 -102		1
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1473	327 21	1.401	0 9 7	239	11,53	92 37 9 88 81 8	3 5048	9 ' 9 7 8 9 9 9 ' 9 8 1 0 9 9 ' 9 7 8 5	9.9700	0.4824	9 1 3 2 4	9 9960	73.0	Brook Street	+ 53	67	+ 33	- 5		p
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1476	121 . 26	+0.748	2 9 7 7 2	229 3	322.82	93.18	5155	9,9853	9753	9.4076	913122	9 . 9907	74'9	+175	+ 32	127	-1- 39	73	- <del> </del> - бі	2.26
1479	61'45	-0'010	1 9 . 70	092 r	10.42	03.11	5456	9'9893 9'9901 9'9941	9733	9.3238	914252	9.9840	77.4	47 + 30 126	32 13	+ 9 + 97	33 16	+ 62 + 157	56 11	); );
7400	/ 4/	, 0 ,0,	× 9 70	2522	198 02	93.00	5494	9 9945	9, 9200	9.1983	9#5013	9 9770	80.4	+137	···· 51	124	б4	- 43	- 33	t
1481	66'04 201'41	+0.759	3 9 7 7 6 5 9 7 7 4	744 x 185 2	07'16	92.21 g 87.35 g	. 5057	9 9977	9.9684	gn <b>oo6</b> 6 gn <b>o19</b> 3	9 · 5485 9 » 605 1	9'9616 9'9710	96·2	-164	- <b>-</b> 51	64	+ 70	+ 23	+ 40	γ.#  }
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Nr.	Julianischer Kalender	T' Julian. Welt-Tag Zeit	L'	Z	ε	P	Q	$\log p$	$rac{\log}{\Delta L}$	$\log q$	$u_a'$	log/"	logy
1502 1503 1504	— 579 III 5 — 579 VII 31 — 579 VIII 30	1509 613 4 29 7 1509 642 15 24 9 1509 790 11 32 8 1509 820 3 46 1 1509 967 20 13 8	120'516 149'532	+3'61 +0'41 +0'06	23'776 23'775 23'775	15'312 164'612 195'332		o.6989 o.7104 o.7366 o.6890	9'7538 9'7419 9'7034 9'7111	8.7504 8.7387 8.7071 8.7134 8.7610	0'5422 0'5467 0'5675 0'5652	7.6727 7.6688 7.6663 7.6701 7.6740	0.1230 0.1301 0.1649 0.1569 9.7946
1507 1508 1509	- 577 I 14 - 577 VII 9 - 576 I 3	1510 144 11 58.3 1510 322 11 42.1 1510 498 16 48.3 1510 676 22 20.8 1510 853 4 55.6	288.221 99.055	+3.03 +3.03	23'774 23'773 23'773	0.676 180.650 8.658	171'321 2'634 178'296 10'975 187'383	0'7414 0'7003 0'7233 0'7234 0'7007	9.7055 9.7520 9.7280 9.7256 9.7535	8 · 7085 8 · 7493 8 · 7263 8 · 7261 8 · 7492	0.5652 0.5445 0.5519 0.5603 0.5370	7.6641	g·8599 8·7700 8//7826 g·8994 g//9088
1512 1513 1514	- 575 VI 17	1511 031 1 35.2 1511 178 14 44.3 1511 41.0	235.575 266.015 50.832 78.710 224.098	+0.48 -2.28 -1.78	23'771 23'771 23'771	16.173 168.492 198.024	343 887 17 166 169 546 198 000 349 254	0.7445 0.7416 0.6928 0.6901 0.7351	9.6994 9.7620 9.7648 9.7116	8.7062 8.7088 8.7571 8.7598 8.7151		7.6778 7.6769 7.6623 7.6627 7.6774	0.1863 0.1845 9.9908 0.1788 9.9263
1517 1518 1519	- 574 XI I - 573 IV 28 - 573 X 22	1511 533 5 54 1 1511 709 12 15 7 1511 887 14 44 6 1512 064 1 29 0 1512 241 16 51 9	30'350	-3.54 -1.54 -3.00	23'771 23'771 23'771	358 730 185 833 6 682	179 · 622 356 · 314 187 · 742 5 · 467 194 · 062		9'7425 9'7385 9'7159 9'7600 9'7016		0'5430 0'5534 0'5584 0'5405 0'5670	7'6627 7'6769 7'6633 7'6762 7'6641	9:3902 9:0561 9:7387 9:7565 O::1230
1522 1523 1524 1525	- 572 X 10 - 571 III 7 - 571 VIII 31 - 570 II 24	1512 389 6 57 9 1512 418 17 27 7 1512 566 3 42 6 1512 743 18 37 4 1512 920 13 55 1	191'344 340'160 151'183 329'528	-2.50 +3.53 0.00 +4.16	23'770	14.605 171,433 351.612	345 · 298 15 · 598 169 · 193 354 · 032 177 · 535	0.7276		8.7590 8.7225 8.7280	0'5390 0'5578 0'5549	7.6717 7.6752 7.6685 7.6702 7.6700	0,1541 0,0908 9,8985 9,8839 8,3436
1527 1528 1529 1530	- 569   1 14 - 569   VIII 9 - 568   1 5 - 568   II 3	1513 097 23 14.5 1513 275 5 19.0 1513 451 23 26.7 1513 600 9 54.0 1513 629 21 30.0	319.038 129.329 278.848 308.518	+4'44 +0'53 +2'04 +4'34	23.771 23.771 23.771	7 239 154 787	187.502	o · 6898	9.7058 9.7637 9.7026 9.7454 9.7567	8.7603 8.7069 8.7433	0'5575 0'5360 0'5584 0'5490 0'5406	7.6688 7.6715 7.6675 7.6761 7.6729	8,, 5966 9,, 8321 9, 8417 0, 1235 0,, 1392
1532 1533 1534 1535	- 568 VII 29 - 568 XII 24 - 567 VI 19 - 567 XII 13	1514 308 19 45.3	118.539 267.794 79.995 256.396	+0.36 +0.40 -1.40 -0.68	23.772 23.772 23.773 23.773	15 235 172 651 354 066	342'918 13'042 174'739 352'578 180'437	0'7280 0'7300 0'6956	9.7221 9.7178 9.7588	8.7217	0.5654	7.2 <b>6</b> 61	0,1180 0'1456 9'8347 9,7080 7'5515
1537 1538 1539 1540	- 566 XII 2 - 565 V 29 - 565 X 23 - 565 XI 21	1514 485 21 58 6 1514 662 19 7 1 1514 840 14 2 0 1514 987 9 55 6 1515 016 23 48 2	244.896 59.911 203.477 233.610	-1.87 -2.33 -3.03 -2.71	23 774 23 774 23 775 23 775	187 '071 11 '528 162 '809	3'385 185'646 13'762 160'572 192'200	0.7058	9'7067 9'7462	8.7588 8.7113 8.7436 8.7438 8.7312	0'5723 0'5397 0'5485	7.6624 7.6776 7.6623 7.6763 7.6776	9:3727 9:8267 0:0045 0:1742 0:1185
1542 1543 1544 1545	- 564 X 12 - 563 IV 7 - 563 X 1 - 562 III 27	1515 165 11 7.9 1515 342 0 28.4 1515 519 12 7.2 1515 696 16 27.6 1515 873 14 17.5	192'706 10'658 182'048 359'892	-2'57 +0'60 -1'94 +1'72	23'775 23'774 23'774 23'774	170 798 358 364 178 807 6 352		0 6898 0 7444 0 6944 0 7321	9.7630 9.7580	8.7114 8.7599 8.7056 8.7549 8.7175	0'5384 0'5674 0'5406	7.6753	9.8916 9.1978 9.0108
1548 1549	- 561 III 16 - 561 VIII 11	1516 051 5 14 1 1516 198 12 46 1 1516 227 23 7 3 1516 375 18 26 2 1516 405 11 14 6	349 329	+4'41	23.774	14'753	342°324 12°348	0 6979	9.7436 9.7026	8.7514 8.7401 8.7065	0'5407 0'5449 0'5686	7.6674	9n7964 on1311 o'1130 o'1831 on1456

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Nr.	μ	γ	$\log n$	G	K	$\sin y$	sin <i>k</i>	cos y	cosk	sin oʻ	cosô'	<i>N</i> ′	gang \(\lambda\)	φ	λ   r a	φ	Unterg $\frac{\lambda}{\lambda}$	φ — φ	F
1502 1503 1504	44.09 357.01 232.45	-1.3273 +1.3493 +1.4620 -1.4350 -0.6231	9'7439 9'7055 9'7131	344'45 133'41 157'51	94 ' 44 96 ' 51 95 ' 77	9.6854 9.6572 9.6807	9'9479 9'9805 9'9548	9 9419 9 9498 9 9433	9 · 6645 9 · 4664 9 · 6370	9,1672 9,5407 9,3106	9'9953 9'9721 9'9953	62'2 108'2 116'3		- 51	-116		_ _ _ _ _ 44		p p p p
1507 1508 1509	352°36 72°46 151°16	+0'7243 +0'0589 -0'0606 +0'7932 -0'8106	9'754I 9'730I 9'7277	201.30 113.13 305.11	93·87 93·55	9.6372 9.6301 9.6431	9°9896 9°9948 9°9957	9'9533 9'9563 9'9571	9:3341 9:1477	9,5832 9,5999 9,6019	9.9622 9.9622 9.9622	99.7 81.2	60 137 +157	· 9 - 6 - 39	+ 7 - 73 - 155	19 + 20 + 30	+ <b>6</b> 5 16	+ 16 12	t::: 1:::: 1::::
1512 1513 1514	198·95 45·82 143·40		9.7653 9.7667 9.7667	91,15 90,20 91,15	91.25 80.85 90.18	9.6091 9.5482 9.5970	9'9993 9'9941 o'0000	9.9632 9.9711 9.9632	8.7800 9.2170 7.8515	9,6043 9,4949 9,5969	9.9632 9.9632 9.9632	86.5 80.0	- 169		*******	 (+78)  76		 72 64	р Р Г* Р
1517 1518 1519	7:46 40:83 203:78	0.2456 0.1138 0.5479 0.5709 1.3273	0,400 0,4180	220'04 36'95 206'98	86 · 73 86 · 84 87 · 42	9'5177 9'5145 9'5047	g · g853 g · g853 g · g864	9 · 9750 9 · 9754 9 · 9766	9,,3910 9,4079 9,4497	9#3405 9*3089	9.9920 9.9998 9.9893	74'9 106'6	69  + 94  - + 98  +	47	8 37	19 23	+ 60 + 21	- 21 - 18	t# r# r t# 1'
1522 1523 1524	81'39 234'33 101'48	-1,4260 +1,2322 -0,7624 +0,0221	9 ' 7639 9 ' 7246 9 ' 7309	193'80 335'75 144'87	88 · 53 92 · 38 93 · 07	9.2122 9.2034 9.2001	9'9846 9'9812 9'9846	9.9756 9.9767 9.9771	9,4860 9,4592 9,4167	8,8992 9,1361 9,2884	9.9916 9.9929 9.9986	73.1	- 59 - 166	34	-107	- + 48 - 41 - 10		+ 68 - 63 + 16	1.
1527 1528 1529	329.92 169.09 329.92	-0.0395 -0.6793 +0.6945 -1.3780	g·7658 g·7048 g·7474	310'64 119'17 265'83	93'43 93'11 89'34	9'5310 9'5463 9'6012	9'9899 9'9941 9'9998	9 9734 9 9713 9 9623	9 · 3290 9 · 2119 8 · 4257	9,4220 9,4939 9,6002	9 ' 9843 9 ' 9778 9 ' 9625	91.4 99.8	+ 14 -	- 53	+110	- 59	112 174 88	- 15 - 29 + 32	t
1532 1533 1534	214.78 97.23 253.13	-1'3122 -1'3983 -0'5105 -0'5105	9 7241 9 7200 0 7600	253'78 65'10	92 · 25 87 · 30 86 · 00	9'5668 9'6197	9 9977 9 9975 9 9945	g 9583 g 9586 g 9561	9n0129 9n0274 9'2014	9.5491 9.6051 9.5988	9.0027 9.0020 9.000	96 3 96 7 80 0		~ 37	-+ x o g	8	+100	- 19	t
1537 1538 1539	335.68 30.23	+0'2359 -0'6710 +1'0104 +1'4933 -1'3137	9 7089 9 7501 9 7481	231'25 47'13 197'25	83 · 89 83 · 56 85 · 25	9'6525 9'6560 9'6824	9.9846 9.9811 9.9500	9'9511	9,4180 9,4606 9,6568	9, 5624 9, 5426 9, 2058	9'9690 9'9719 9'9944	72.1	+ 175   - -	- 1 - 24 	-153 -112 -	+ 36 66 	75 8   	+ 26 - 53 	t** r p p
1542 1543 1544	191.62 1.67	-0.9042 +0.7792 -0.1577 +0.1025 +0.5940	9.7651 9.7601	181,46 181,46	87 · 20 87 · 62 89 · 53	9.6889 9.6917	9'9430 9'9415 9'9400	9'9408 9'9399 9'9400	926817 9.6867 926914	8.9478 8.8725 8.1586	0.0000 0.0038 0.0033	119'4	59 -	- 79 - 38 - 35	<del></del> 68	+ 6	- 5	+ 22 + 20 - 24	t# 2. t#
1547 1548 1549	10.46 160.68	-0.6257 -1.3523 +1.2972 +1.5243 -1.3983	9 7570 9 7456 9 7046	330'17 352'31 142'69	96 · 57 92 · 36 96 · 90	9.6735 9.6887 9.6679	9.9632 9.9424 9.9712	9 9 4 5 4 9 9 4 0 8 9 9 4 7 9	9.5969 9.6836 9.5474	9n4099 8n8730 9'4824	9.9851	01.1			+ 92	- 42	+162	- 68 - - -	r p p p
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		misch Jende		Julia Tag		We Ze				a contract of the second									35. (1.12)//12 (1.1)		the training of the second
1552 1553 1554	- 55	IV c	I 30 l 24 I 19	1516 1516	729 907 083	18 A 20 1 23 5	7'5 4'1 57'5	120'2 299'2 109'5	30 - 77 -	+4°37 +0'40 +3'90 +0'02 +3'02	23	773 773 772	352°375 171'682 0'497 179'905 8'542	170.485 2.520 177.513	0.74	07 014 116	9·7640 9·7662 9·7509 9·7298 9·7242	8.7606 8.7093 8.7483 8.7278 8.7248		7.6727 7.6663 7.6740 7.6651 7.6752	9,8099 9,8989 8,6376 7,9391 9,8944
1557 1558 1559	- 55	8 X.I 7 7 \	I 4 I 3 7 30	1517 1517 1517	586 616 763	9 .	44'7 36'0 10'6	246 7 277 1 61 2	772	0'54 1'69 +1'82 2'32 1'16	23.	771 771 771	188'544 343'824 16'072 167'617 197'189	343.72 15.95 168.81	0.24	145 121 134	9°7548 9°6996 9°7027 9°7614 9°7649	8.7061 8.7082 8.7564	0'5736 0'5324	7.6776 7.6762 7.6623	9n8690 0n1874 0'1823 0'0227 0n1589
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1612 1613	- 536 XI 1 - 536 XI 1 - 535 III 28	1525 412 5 47 1525 559 23 42 1525 589 11 2 1525 736 18 22 1525 914 10 21	4 183.810 3 213.647	-2'05 -3'25	23.766 23.766 23.766	192'155 342'836 14'438 170'219 350'917	15.623 167.890	0'7010 0'6923 0'7250	9'7016 9'7516 9'7605 9'7261 9'7255		0.5660 0.5442 0.5408 0.5542 0.5586	7.6627 7.6742 7.6769 7.6659 7.6731	0,1690 0,0871 9,9531
1616 1617 1618 1619 1620	- 534 IX II - 533 III 7 - 533 VIII 31 - 532 I 27	1526 268 13 52° 1526 445 21 43° 1526 622 13 41° 1526 771 2 51°	8 150.773 8 120.773	-0'59 +3'48 +0'02 +4'01	23'765 23'765 23'765	178 714 358 658 187 126 6 131 164 480	359.709 186.875 5.247	0.7421	9'75'7 9'7037 9'7642 9'7034 9'7427	8.7481 8.7084 8.7605 8.7079 8.7406	0.2341	7.6672 7.6717 7.6635 7.6702 7.6738	9,7691 9,7691
1621 - 1622 - 1623 - 1624 - 1625 -	- 532 VIII 19 - 531 I 15	1526 800 14 1' 1526 947 5 19' 1526 976 17 19' 1527 125 10 46' 1527 301 19 42'	1 111'198	+0'11	23'766 23'766 23'766	195.452 343.796 14.030 172.419 352.438	341.406 11.749	0.7133	9'7549 9'7393 9'7251 9'7153 9'7605	8.7516 8.7364 8.7245 8.7176 8.7560		7.6700 7.6652 7.6688 7.6751 7.6642	
1628 1629 1630	- 530 VI 30 - 530 XII 24 - 529 VI 20 - 529 XI 14		5 90.881 2 257.266 3 80.763 3 225.855	-1 04 +0 61 -1 53 -3 09	23.768 23.768 23.768 23.769	9'795	1'985 185'369 12'137 160'579	0'7441 0'5917 0'7372 0'7086 0'7029	9.7088 9.7448 9.7487	8.7581 8.7127 8.7406 8.7464	0.5319 0.5705 0.5418 0.5477	7.6760 7.6634 7.6768 7.6628 7.6775	9,8193 9,9374 0,1736
1631 - 1632 - 1633 - 1634 - 1635 -	- 528 XI 2 1 - 527 IV 29 1		215'017	-1,30 -3,50	23.759	194.629 348.707 170.620 356.692 178.518	170 · 252	0.0803	0.4654	8.7608 8.7059	0.2020	7.6632 7.6632	9.8993 9.5029
1636 — 1637 1638 — 1639 — 1640 —	526 X 12 I 525 III 9 I 525 IV 7 I	529 221 21 41 6 529 369 4 55 8 529 398 14 14 4	20.959 193.371 342.024 10.554 182.248	-2.63 +3.38 +0.63	23'769 23'769	4.846 186.529 343.275 13.421 194.273	188 963 341 586	0 7297 0 7183 0 6961 0 7065 0 7387	9.7468	8 7308 8 7531 8 7428	0.5563 0.5564 0.5379 0.5417 0.5699	7.6753 7.6684	9.6542 9.7719 0.1532 0.0702 0.1286
1644 — 1645 —	523 II 15 1 523 VIII 10 1 522 II 4 1	529 723 21 26 4 529 900 8 56 5 530 078 12 51 3 530 254 14 42 1 530 432 22 45 8	321 189 - 130 799 - 310 418 -	+0 30 +4 39 +0 54 +4 37	23 769	170'441 359'909 178'581	2.053	0.7388	9 7485 9 7327	8·7107 8·7455 8·7309	0.5351 0.5663 0.5445 0.5512 0.5607	7.6689	9n8516 9'9570 7n9027 9'1101 9'8731
1648 —	521 I 25 15 521 VI 21 15	530 609 3 40 3 530 757 5 50 6 530 787 1 17 0 530 934 13 3 1 530 963 20 31 5	269 127 - 299 269 -	+0.84   : +3.88   : -1.55   :	23 767 23 767	187 · 107 343 · 699 15 · 696 165 · 891 195 · 639	343 374 16 360 167 347	0.7442	9.7018	8 7050 8 7070 8 7547	0.2332	7·6768 7·6740	9n7871 on1904 o'1734 o'0800 on1188

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1606 1607 1608 1609	159'37 125'79 267'33 242'57	-0.8428 +0.4024 -0.1144 -0.3862 +0.5625	9.7161 9.7412 9.7433 9.7152	258 · 48 73 · 01 246 · 03 61 · 34	88'40 87'80 87'20 86'91	9*5754 9*5664 9*5549 9*5473	9 9990 9 9978 9 9958 9 9943	9,8415 9,828 9,868 9,869	8n8439 9.0029 9.1383 9.2058	9,,5678 9,5495 9,5204 9,4969	9'9681 9'9708 9'9747 9'9775	94'3 83'8 98'4 80'3	+100 +163 + 30 + 65 -162	+ 16 + 2 - 31	-127 + 92 +119	+ 45 26 5	+151 +177	14 12	/* /* 2'
1612 1613 1614	345.48 342.41	1 · 1652 1 · 4757 +- 1 · 2220 0 · 8976 0 · 8332	9 · 7536 9 · 7625 9 · 7282	184.65 220.48 1.80	89 · 49 86 · 56 89 · 80	9 · 4969 9 · 5222 9 · 4946	9'9776 9'9863 9'9777	9'9774 9'9745 9'9777	924953 923922 94944	8,4278 9,3489 8,0147	o,oooo 889 9,889 9,9998	108'2	175			 71 58	15 +- 86	+ 82 - 74	19
1617 1618 1619	28.98 140.93 23.68	+0.1124 -0.1287 -0.6042 +0.5876 +1.3630	9 : 7059 9 : 7663 9 : 7056	157.67 336.38 144.24	93.08 93.18 93.18	9 4983 9 5026 9 5115	9,0840 9,0811 9,0810	9:9773 9:9768 9:9757	914610 914607 914122	9'0973 9"1247 9'2940	9'9966 9'9961 9'9914	73'1 73'1	91 139 104	53	30 136	47	ნე	20	2 ¹⁴³
1622 1623 1624	253:35 75:87 340:53	1 '3247 1 '4357 1 '2815 0 '6473	9 · 7412 9 · 7272 9 · 7175	99.69 131.68 277.52	91°38 93°44 91°08	9.2803 9.2803	9 ' 9992 9 ' 9895 9 ' 9996	9 · 9661 9 · 9659	8,,7732 91:3377 8:6648	9'5749 9'4146 9%5782	9'9670 9'9848 9'9664	93'7 93'7 87'1	- 3x	39 37		+ 23 - x7		43	
1627 1628 -1629	15.71 350.01 246.45	+0.0218 +0.0910 -0.6597 +0.8658 +1.4913	9.7648 9.7110 9.7468	77'13 253'18 67'03	87 19 87 19 87 88	9.6145 9.6207 9.6296	9'9985 9'9973 9'9949	9'9597 9'9584 9'9565	8 * 9237 920438 9 * 1835	9 · 6053 9 · 6049 9 · 5998	9.9616 9.9616 9.9616	84'7 95'9 80'4	53 80 73 + 11	31	+ 8	+ 29 65	十 53 十102	+ 10 - 43 + 59	t#
1632 1633 1634	200.01 200.01	- 1'3047 1'0707 0'3184 0'1278	9.7098 9.7655	31.71 205.94	83'21 83'72	9:6743 9:6789 n:6830	9 · 9548 9 · 9583 9 · 9549	9'9451 9'9438 9'9426	9.5875 9.6209 9.6367	9 ' 4333 9#3642 9 '3247	9.9834 9.9881	66.3 115.4 63.7	-124 +109	44	104	9	137	- 8	1.
1637 1638 1639	146.27 254.05 29.90	+0.4510 0.5914 1.4230 +1.1755 1.3447	9 · 7339 9 · 7593 9 · 7488	189.62 346.88 7.60	87 06 93 80 87 66	g·68gx g·6845 g·688g	9'9432 9'9465 9'9423	9'9407 9'9421 9'9407	9»6811 9:6696 9:6839	8,,9695 9,20948 8 : 8682	9.9988 9.9981	61,0 61,0		I	+110 -155 -	-1 39 - 48			
1642 1643 1644	316.40 8.45	-0'7105 -0'9058 -0'0080 +0'1288 -0'7467	9.7101 9.7506	151'38 142'56	95'57 95'60 95'93	9.6771 9.6771 9.6686	9'9616 9'9616	9'9443 9'9443 0'0468	9,6064 9,6051 9,5472	9:3990 9:4025 9:4845	9.9859 9.9856	111.7 65.4	122 79 113	+ 75 - 24 + 28	( 124) 8 39	(+80) - 15 + 26	+ 133 + 48 + 18	+ 39 + 23 - 14	14 1-t4
1647 1648 1649	20.33 101.00 521.31	-0.6124 -1.5503 +1.4907 +1.2022 -1.3147	9.7020 9.7038 9.7616	282'54 312'23 95'14	92°09 96°40 90°82	9'6141 9'6554 9'6026	9.9997 9.9816 9.9982	9'9597 9'9503 9'9620	8.9159 9.4542 8n5176	925460 925460 9.6012	9.9615 9.9623	72°3 92°1	garantee garantee	18	+122	- 20	-1-16g	51	t p p p

<b>3.</b> T.,		$T^{i}$	7,			72			log				
Nr.	Julianischer Kalender	Julian. Welt- Tag Zeit	L'	Z	ε	P	Q	$\log p$	$\Delta  ilde{L}$	$\log q$	$u'_u$	log/"	logy
1652 1653 1654	- 520 VI 10 - 520 XII 3 - 519 V 30	1531 111 6 41 6 1531 289 3 14 0 1531 465 14 21 1 1531 643 10 41 5 1531 820 4 9 3	71.978 246.565 61.576	-2'03	23.766	174'651 358'726 183'185	177.083 356.354 184.851	0.4122 0.4084 0.4122	9.7374	8.7131 8.7411 8.7340	0.5671 0.5457 0.5514 0.5600 0.5404	7:6773 7:6624 7:6623 7:6623 7:6776	9"9257 9'6829 9"0536 9"4796 9'7495
1657 1658 1659	518 X 14 518 XI 12 517 IV 9	1532 174 19 55'1	194 · 889 224 · 857 12 · 035	-2'71 -3'14 +0'46	23.763 23.763 23.763	342'681 14'417 169'512	191'075 344'817 15'692 167'147 352'998	0.232 0.232	9.7504	8.7480	0.5658 0.5456 0.5414 0.5525 0.5602	7.6624 7.6754 7.6774 7.6648 7.6742	0,1737 0.0870 0.0818
1662 1663 1664 1665	- 516 IX 21 - 515 III 18 - 515 IX 10 - 514 II 6	1532 676 13 22 9 1532 853 21 23 0 1533 031 5 44 4 1533 207 21 4 3 1533 356 11 7 2	172.825 351.405 161.609 311.982	x · 33 2 · 58 0 · 58 4 · 42	23.763 23.763 23.763 23.763	186.564 5.702 164.222	359'254 186'450 4'709 166'609	0.7426 0.6899 0.7420 0.7107	9.7532 9.7029 9.7644 9.7039 9.7414	8.7081 8.7604 8.7086 8.7393	0.5389 0.5716 0.5332 0.5703 0.5493	7.6660 7.6730 7.6673 7.6716 7.6726	9 / 2091 9 / 7459
1668 1669	- 514 VIII 31 - 513   26 - 513 VII 22	1533 385 22 4'1 1533 532 12 47.2 1533 562 0 56.2 1533 710 18 45.8 1533 887 3 23.2	121.208 111.208	+0.40	23'754	13,248	340'752	0.7334 0.7334	9.7408	8.7380 8.7259 8.7165	0'5400 0'5461 0'5564 0'5658 0'5338	7.6687 7.6664 7.6701 7.6738 7.6652	
1672 1673 1674 1675	512 VII 10 511 I 3 511 VI 30 511 XI 24	1534 064 19 35.0 1534 241 20 34.9 1534 418 19 36.8 1534 596 11 42.4 1534 743 12 12.0	101.386 278.404 01.518	-1.01 +1.02	23'764 23'765 23'765	0'271	185 185	0.6922 0.7363 0.7102	9.6999 9.7621 9.7101 9.7430 9.7498	8·7574 8·7137 8·7393	0'5746 0'5329 0'5693 0'5430	7.675x 7.6642 7.6760 7.6633 7.6777	1 1
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1682 1683 1684 1685	- 507 III 19 - 507 IV 17 - 507 X 12	1535 629 II 8.7 1535 807 6 2.7 1535 954 12 50.1 1535 983 21 40.5 1536 161 10 26.8	352 726 21 081	-3'10 +2'43 -0'40	23.767 23.767 23.767	186.414	188.828 341.112 10.406	0.7195	0.2300	8.7296 8.7540 8.7440	0.5548 0.5577 0.5364 0.5404 0.5712	7.6762	9'5720 9"7655 0"1666 0'0437
1687 1688 1689 1690	- 506 IX 1 - 505 II 26 - 505 VIII 21 - 504 II 16	1536 485 16 15 5 1536 663 20 55 8 1536 839 22 19 9 1537 018 6 34 3	152.321 332.031 141.510 321.321	-0'07 +4'02 +0'37 +4'38	23.767 23.766 23.766 23.765	7 733	168'448 1'696 175'600 9'855	0.7379 0.7052 0.7169	9'7636 9'7090 9'7473 9'7344 9'7201	8.7117 8.7441 8.7323	0'5344 0'5666 0'5443 0'5511 0'5608	7.6684 7.6704 7.6699 7.6689 7.6714	9n8771 9'9781 8n6491 9'2511 9'8554
1693 1694 1695	- 503 II 4 - 503 VII r - 503 VII 3r	1537 519 20 31 8 1537 549 4 18 9	280°250 310°230 92°597 120°816	+2'16 +4'36 -0'92 +0'43	23.765 23.765 23.764 23.764	15.397 165.062 194.944	343'137 15'952 166'638 195'520	0.7439 0.7436 0.6958 0.6904	9 7579 9 7004 9 7014 9 7585 9 7639	8 · 7067 8 · 7537 8 · 7594	0.5370 0.5749 0.5723 0.5344 0.5330	7.6676 7.6759 7.6728 7.6634 7.6662	9n7462 0n1933 0'1657 0'1051 0n0998
1697 1698 1699 1700	- 502 XII 14 - 501 VI 10	1537 696 14 58 4 1537 874 10 17 9 1538 050 23 5 1 1538 228 17 14 4 1538 405 13 7 7	257.780	-0.57	23.763	350.917 173.793 358.723 182.284 6.610	356 380 183 855	0.7309 0.7073 0.7073 0.6904	9 7356 9 7439	8 7326 8 7423 8 7121	0.5658 0.5470 0.5504 0.5609 0.5401	7 6773	9n927i 9'7487 9n9533 9n3364 9'7494

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1655	243'51	0.3014	9.7636	246'35	87.22	0.2222	9.9929	9.9699	9"1333	9°5495 9″5221	9'9708		- 35 + 65		+119			- 11 + 24	
1656	1'71	r · 0787	9 ' 7037	60'98	86.89	9:5473	9.9942	9.9712	9.2107	9'4954	9.9776		l .				and the same		p
1658	118.80	+1.3217	9'7617	233'54	86:58	9 ' 5389	9'9914	919723	9#2945	914537	0'0817	101.0							$\left  egin{array}{c} p \\ p \\ \end{array} \right $
1050	100.32	+0'9590 -0'8564	0.25go	184.30	89 48	9'4985	9.978r 9.9790	9 9773	9:4825	8.9244	9,9998	108.0	+ 66 177	+ 55 41		66	— 18 — 18	(+85) - 77	7. j
1661	19.60	+0'1672	9'7553	2'04	89:78	9'4927	9'9780	9'9780	9'4924	8.0662	0,0000		84	8	1		+ 45	- - 28	
1663	263,13	-0'5570	9.7665	349'44	91 11	9'4950	9'9786	9 9 9 7 7 7	9 4868	817798	9 9 9 9 9 2	72.1	+156 + 25	- 52	+102	7 39	+168	- 27 - 16	1
1004	346.01	+0.2424 -1.3003	9 7 7 4 3 4	302.60	93.30	9 5435	9.9928	9.9773	9.2556	9 1043 9 4765	9,9400	79°I	+151	i 49	130	+ 42	68		2)
1666 1667	144.35	-1.4882 -1.5882	9.7557	337,11	92.31	9.2002	g ' g8o5	9.9764	9 4 6 6 8	9,,1159	9.9963	72.8						jour distribution (	p
	130.03	+1.5342	9.7285	144 35	93,11	9.5143	9 9847	9'9754	9"4154	9 2957	0,0013				102	i- 27	##	40	$\frac{p}{p}$
	232.46	0.2001	9.7633	99.20	01,32	9.5791	9.9992	9.9662	8,7640	9.5740	9.9671	03.6	+ 74	- 37 - 38	+126	23	+176	+ 49 - 44	
1671	110,25	-0.0333 -0.0380	9.7021	277'04	91'02	9'5817	ე ' <u>ეეე</u> ნ	9.9658	8.0364	9, 5789	9.0663	87:3	171 166		111	20		+ 4 + 2	9*#: !#
1673	110,35	-0.6401 -0.7024	9.2123	264 86	80,18	9.6020	9:9997	9'9621	8,5163	ე" წიინ	9'9624	92'1	+164 92	35	111	64	22	38	,
1675	9.22	1.4883	9'7517	224.78	83.42	9 6576	9.9790	9 9390	9#4823	9.5293	9.9736	108.8					- -112	,,,,,,,	p
1676	200'09	1.1582	9.7385	253.54	87 26	0.6200	9 . 9975	9 ' 9586	920338	ე"ნo48	9.0616	96·8		Port 1	12800 <b>4</b>		V-211-2114		p
1678	231,03	+0.4042	9.7657	215'04	83,11	ე : ნ704	9.9686	9.9463	9#5643	944639	9.0808	112'5	4-102	-⊦ <b>6</b> 8	+137	1		1- 29	
1680	101.83	+0.1333	9 7571	200.12	83.66	9.6797	9 9 9 5 8 4	9.9435	9,6205	g 4309 g _n 3685	9.9878	115.4	157	+ 32	100	1	-	17	1
1681	347.42	+0.3732	9.7243	23.03	84.07	9'6824	9.9548	9 9427	9.6365	9.3224	9.9902	63.7	50	- 4	+ 7	-l- 37	- <del>-</del> 90	47 62	
1083	13.08	0.5827	9.7004	354'73	01,05	g : 6866	9.9422	9'9414	9'6842	817077	9.9994	91.1	MARKET		79	5.	1,173		p
1685	335 ' 52	1.3580 1.1022	9 7504	189.28	87 '09	9.6883	9 9470	9.9410	9,6803	8 g 667	9 9954	118.8			#17114	£	ARTH-RANK	8+2-0753	$\frac{p}{p}$
1686	261.97	-o.7535	9.7657	347'31	93.76	9 6877	9 * 9453	9.0412	9 6737	9"0849	9 9968	61.6	3			1	1	1 .	ata I
1688	130.06	+0.0208	9.7494	339'58	95 '48	0'6840	9 9522	0'0423	0'6479	0//2765	0.0021	63,1	-1-161	29	129	14	72	+ 44	1:4:
1690	272.18	0.1168 0.1283	9.7302	331,10	96.28	9'6768 9'6768	0.0010 0.0013	9'9443	9.6052	9.3993 9.4011	9.9857	65.4	+ 132	+ 20	+ 78	+ 37	- 96 +123	+ 66	
1691	350.66	-0'5574	9.7600	142'73	96 ' 92	9 6684	9,9711	9'9468	925481	9 4827	9.9789	111'8		12	+ 4	- rg	l- 54		. ;
1693	304.83	-1.2607 +1.4647	9'7034	321,85	96.89	g'666g	9.9720	9'9473	9'5413	944881	9.9784	68 6			potential.	Manager 1	Andriag		$\begin{bmatrix} p \\ p \end{bmatrix}$
1695	241.51	-1.5223 -1.5283	9.7659 9.7665	133'46	95 '48	9'6561 9'6194	9 19806	9.8201 9.8284	9n 0240 9n 4659	9.5392	9'9010	108.5			_				$\left  egin{array}{c} \mathcal{P} \\ \mathcal{P} \end{array} \right $
1696	46.19	-0.8454	9.2189	282 59	92 ' 08	9'6141	9.9986	9 . 9 5 9 8	8.0x30	926052	9.9615	84'9	159	- 55	- 44	- 82	- <del> </del> - 56	47	7
1698	167.12	-0.1130	9'7460	270'90	90,14	9'5955	0.0000	9.9634	7.7543	9#5954	9.9634	89.6	- 61 +127	6	-167	30	-101	E	5 r-t*
1699 1700	17.22	-0.2169 +0.2616	9.4242	84.69 258.93	88 '46	9.24gr 9.282o	9.999x	9.0668	8.5160	9 5834 9 5690	9.9679	94'	— 136 — 70	+ 35	16	- - 12 - - 10	22 39	+ 28	2 til
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1707 1708 1709 1710	- 497 - 496	III 29 IX 22 II 17	1539 1539 1539 1539 1539	439 616 793 941	5 4 13 35 4 38 19 12	9 2 2 172 ·	810 055 518 887	-2.0 +1.3 -1.3	7 2 2 2 2 8 2	3'760 3'760	1 177 '38 358 '02 185 '93 5 '35 163 '88	7 35 30 18	58.883 35.957	0 7430 0 6900	9.7020 9.7644 9.7045	8.7076 8.7602 8.7092	0.5728 0.5327 0.5707	7.6742 7.6660 7.6730	9n2733 9n7021 9'7094
1712 1713 1714 1715	- 496 V - 496 - 495 - 495 V	II 6	1540 2 1540 2 1540 2	1 1 7 2 1 4 7 2 9 6 1 7 2 1	20 24 9 8 44 9 2 35 9	7 312· 5 122·	450 490 016 114	+°°5, °°5; '4°4; '°4(	1 2; 7 2; 5 2;	3.4gr 3.4gc 3.4gc	194.41 342.51 13.14 171.92 351.01	4 34 9 1 6 17 6 35	0'797 3'739 0'041	0.7106 0.7227 0.7345 0.6924	9'7423 9'7278 9'7130	8.7492 8.7395 8.7273 8.7156 8.7577	0'5459 0'5565		0,1865 0,0776 9,8798
1717 1718 1719 1720	- 494 - 493 - 493 - 493	VII 22   15   VII 11   XII 5	1540 8 1541 0 1541 1 1541 3	81 1 28 2	4 14. 3 39. 8 59.	7 248	933 195 708 309	+0.16 +3.12 -0.36	23	3 · 763 3 · 763 3 · 763	162.23 8.19 162.23	б 1 18 1 16	0.720 4.957 0.586 0.686	0.4000 0.4322 0.4322 0.6038	9.4012	, ,	0.2338	7.6738 7.6652 7.6751 7.6642 7.6776	8n6084 9n8023 9'8621
1722 1723 1724	- 492 - 492 - 492 - 491	VI 30 XI 24 V 20	1541 5 1541 6 1541 8	36 83 r 60 r	3 25° 2 1° 4 4°	9 91'2	75 -	1'00 2'49 2'23	23 23 23	763 764 764	170 58 354 88	9 34 6 1 3 17 1 35	7.998 8.589 0.429 4.059	0.7416	9'7379 9'7059 9'7152 9'7637 9'7039	8.7365 8.7082 8.7156 8.7611 8.7068	0'5634 0'5588 0'5394	7.6760 7.6623 7.6633 7.6777 7.6624	0,1904 9'9005
1727 1728 1729 1730	490 - 490 - 489 - 489	XI 3 : II 30 : IV 29 :	1542 39 1542 53 1542 56	92 12 39 20 59 5	\$ 29°3 36°2 3°3	31.5	49 62 67	-3 · 28 -1 · 37 -1 · 28	23 23 23	764 764 764	186.346 342.046 11.85	1 188 5 346 6 9	0'901 8'740 9'577 9'667	0'6979 0'7269 0'7207 0'6944 0'7037	9'7539 9'7237 9'7285 9'7596 9'7500	8 · 7224 8 · 7285 8 · 7547 8 · 7454	0'5591 0'5353 0'5392	7.6775 7.6627 7.6770 7.6658 7.6632	9'1332 9'4662 9'7621 0'1814
1732 - 1733 - 1734 - 1735 -	- 488 I - 488 I - 487 I - 487 I	X I	543 07 543 24 543 42	9 4	49 '9 7 '2	163'1 342'79 152'29	68 99 -+ 98	0.69 3.30 0.05	23 23 23	764 764 764	169 · 5 1 g 358 · 996 177 · 556	162	7'939	0.7402 0.6906 0.7369 0.7066 0.7153	9.7051 9.7633 9.7098 9.7459 9.7359	8.7097 8.7589 8.7126 8.7427 8.7338	0.2333 0.2220	7.6670 7.6718 7.6684	0n1192 9n9048 9'9946 8n9481 9'3430
1737 - 1738 - 1739 -	- 486 VI - 485 - 485 VI - 485 VII	I II I	543 95 544 10 544 13	7 16 5 4 4 12	3,3	131,48	25 + 25 + 25 - 30 +	0'35 4'39 0'28 0'53	23	763 763 763	7'302 185'936 15'024 164'273 194'318	15	6'461	0.7300 0.6947 0.7438 0.6968 0.6906	9'7188 9'7588 9'7013 9'7574 9'7635	8.7525 8.7525	0.5606 0.5374 0.5717 0.5356 0.5340	7'6689 7'6714 7'6643	9'8320 9n7072 0'1554 0'1278 0n0818
1742 1743 1744 1745	484 VI 484 XI 483 V 483 XI	I 20 15 I 14 15	544 636 544 813 544 990	5 7 23 22	23.4 47.1 47.5 4.9	92'86 268'97 82'37 258'12	о — б + 7 — 9 —	0.89 0.79 1.53 0.54	23.	761 761 760	350'825 172'961 358'695 181'392 6'604	175 356 182	398 378 865	o.7184 o.2060	9 7092	8.7435	0'5483 0'5493 0'5610	7.6628	9n9301 9.8046 9n0614 9n1222 9.7486
747 -	482 XI 482 XI 481 IV	1 5 15 1 4 15 7 30 15	345 316 345 345	13	34 8 47 I		1 - 3	70	23':	759 3 759 .	189 · 399 142 · 542 14 · 425 167 · 938 150 · 410	344 15	774	0'7043 0'6944	9'7478 9'7582 9'7315	8 · 7457 8 · 7559 8 · 7292	0'5481 0'5423 0'5496	7.6776	929556 021794 0.0888 0.0388 929475
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1903	335'16	+0.7263	9.7574	59'47 235'40	84 · 98	g ' 6403 g ' 6456	g · g880	9 9541	0,3661	9.5804	ე . ენნე ე . ენნე	104.5	62	- 31	21	7.1	+130	53	$\left  egin{array}{c} t^{\$} \\ p \\ p \end{array} \right $
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1956 1957 1958 1959 1960	-394 II 28 -394 VIII 25 -393 II 18 -393 VIII 14 -392 II 7	1577 563 I 1577 740 9	49.6 334.833 50.2 145.852 58.9 324.183 31.1 134.999 43.0 313.662	+0.24	23.752	357.694	171'897 355'634 178'510	0.7251	9 · 7265 9 · 7248 9 · 7522 9 · 7038 9 · 7641	8 7487	0.5559 0.5568 0.5422 0.5679 0.5363	7.6697 7.6692 7.6711 7.6678 7.6726	9,19867 9,19804 9,13030 9,13716 9,6985
1961 1962 1963 1964 1965	-392 VIII 2 -392 XII 28 -391 I 27 -391 VI 23 -391 VII 22	1578 242 21 1578 272 9 1578 419 2 1578 448 14	46'5 124'076 14'1 273'259 30'5 303'072 57'4 85'136 0'7 113'379	+1.37 +4.07 -1.30 +0.25	23'749 23'749 23'749 23'749	14.000	184.292 344.868 15.850 161.221 191.074	0.2101	9'7044 9'7412 9'7538 9'7403 9'7263	- 1	0.5668 0.5516 0.5428 0.5444 0.5536	7.6664 7.6767 7.6738 7.6629 7.6652	9"7026 0"1865 0'0807 0'1610 0"0876
1966 1967 1968 1969 1970	-391 XII 18 -390 VI 12 -390 XII 7 -389 VI 2 -389 XI 26	1578 773 17 1578 951 4 1579 128 11 1579 305 4	29.6 262.122 40.7 75.006 59.8 250.676 6.4 64.995 47.4 239.182	-1'82 -1'38 -2'16 -2'44	23'748 23'748 23'747 23'747	172.383 357.473 181.082 4.604	357.628 182.005 2.929	0.6937 0.7444 0.6920 0.7364	9.7137 9.7609 9.6994 9.7626 9.7098	8.7561	0.5678 0.5326 0.5764 0.5315 0.5706	7.6773 7.6625 7.6776 7.6623 7.6777	9"9594 9'8140 9"3866 8"9660 9'6388
1971 1972 1973 1974 1975	-388 V 22 -388 XI 14 -387 IV 11 -387 X 5 -386 III 31	1579 659 10 1579 807 21 1579 984 12 1580 161 22	40'8 227'952 52'7 16'263 38'6 187'215 27'4 5'444	+1.10 -5.31 +0.10	23'746 23'746 23'746 23'746	12.250 168.554 348.519 176.380	169·809 348·293 175·715	0'7440 0'7440 0'7440	9'7443 9'7363 9'7070 9'7638 9'7026	8.7354 8.7099 8.7610	0'5643 0'5375	7.6624 7.6775 7.6647 7.6744 7.6658	9,9405 0'0390 0'0361 9,9865 9'5421
1976 1977 1978 1979 1980	-386 IX 25 -385 III 21 -385 IX 14 -384 III 9 -384 III 9	1580 693 16 1580 841 0 1580 870 11	31'0 176'592 21'2 354'652 29'7 165'877 55'3 315'010 11'5 344'079	+2·30 +4·42 +3·22	23 745 23 745 23 745 23 745 23 745	184.366 4.756 162.011 192.743	182 178 7 192 160 402 190 459	0.4028 0.4028 0.4028	9'7553 9'7208 9'7307 9'7578 9'7473	8.7208 8.7299 8.7546 8.7441		7.6732 7.6670 7.6718 7.6724 7.6684	9n4718 9n6085 9.6366 0.1834 0n0473
1981 1982 1983 1984 1985	-383 VII 24 -382 I 18 -382 VII 13	1581 726 11	24'3 115'013 55'1 293'762 44'9 104'442	+0'31 +3'46 -0'15	23'746 23'746 23'748	349 675	348 233	0.2388	9 7033	8.420 8.420	0.5372	7.6736	0.0790 9.9230 9.9901 9.2060 9.2554
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2007 2008 2009	- 3 - 3 - 3	73 V 73 - 72	III XII 2: VI 2:	2 I 9 I 3 I	585 585 585	033 182 359	21 12 1	15'1 43'8 9'4	123 ' 273 ' 85 '	959 291 450	+1 28 -1 27	23'7 23'7	48 48 48	192'710 350'196 171'528	160'425 190'345 352'010 170'437 357'455	0'7232 0'7342 0'6929	9.7126	8.7381 8.7264 8.7156 8.7569 8.7061	0.2324	7.6664 7.6767 7.6629	0.1802 0.0635 9.0632 9.8591 9.3961
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2017 2018 2019	- 3 - 3 - 3 - 3	68 68 67	IV r	1 1 5 1 1 1	586 586 587	747 924 101	5 12 8	9'0 59'5 32'6	187 187	981 518 268	+o'13	23 7 23 7 23 7	44	175.628 356.355 183.709	348 · 258 174 · 844 358 · 253 181 · 469 6 · 868	0.7436 0.6984 0.7280	9'7542	8 · 7070 8 · 7516 8 · 7222	0'5664	7'6744 7'6658	9,9920 9,6235 9,4996 9,5366 9,6094
2022 2023 2024	— 3 — 3	66 65 65 V	IX 1 III IIII	9 2	1587 1587 1587	633 781 957	4 1 12	53'6 33'6	165 315 125	785 425 590	-0.85 +4.41 +0.57	23 7	744 744 745	12.260 169.830 348.966	189 949 13 531 170 464 347 439 180 242	0.7405 0.6906	9.7057 9.7631 9.7057	8.7099 8.7600 8.7124	o'5693 o'5636	7.6665	0,0266 0'0654 9'9354 0,0175 9'2511
2027 2028 2029	— 3 — 3	63 63 " 62	I I VII I I	8 : 3 :	1588 1588 1588	490 666 844	8 2	16.6 43.9 57.3	293 104 282	876 714 582	+2.37	23'7	745 745 746	185 979 5 916	354 862 188 086 4 429 193 902 346 572	0'7295 0'6957 2'0'7436	9:7185	8.7201 8.7540 8.7067	0.5638	7.6643	9n7452 9'7067 On 1068
2032 2033 2034		362 361 361	V 2	27 24 5	1589 1589 1589	168 346 522	8 8 16	20.1	240 55 229	· 800 · 533 · 683	-3.0	23 7	746 747 747	353'74	1 356 18 1 356 18 1 173 98	9   0.7296 7   0.7174	5   9 · 7 18 0 1   9 · 7 35 2 9   9 · 7 45 2	8.7199 8.7320 8.7434	0.5316 0.5658 0.5469 4.0.5497 0.5613	7.6777	9.7526
2037 2038 2039		359 359 358	X 2 III 2	1 25 22	1590 1590 1590	054 231 379	16 22 5	18.3 56.5	35 208 356	'422 '068 '255	-3.5	6 23. 6 23. 6 23.	748 748 748	10.26 192.06 348.28	183.49 9.90 2 193.55 3 345.86 4 170.95	3 0.7445 4 0.6946 8 0.721	9 701 9 758 9 730	9 8 · 705.	4 0'5417 2 0'552	7 7 6763	9'9931 0n0121 0n0266
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2052 2053 2054	- 352 VI 12 - 352 XII 6 - 351 V 3	1592 978 11	52'2 75'745 1'2 250'398 5'6 37'193	-1.42	23'743 23'743 23'743	188 109 12 256 166 895	9'823 167'934	0'7344 0'7125 0'7118 0'7421	9'7122 9'7408 9'7393 9'7055 9'7149	8'7157 8'7373 8'7380 8'7082 8'7152	0.5686 0.5438 0.5533 0.5642 0.5585	7.6773 7.6625 7.6776 7.6630 7.6623	9.6318 9.8598 0.0366 0.0956 0.1913
2057 2058 2059	- 350 IV 22 - 350 X 16 - 349 IV 11	1593 332 11 4 1593 509 21 ; 1593 686 15 ;	34.7 198.707	-2.03 -0.81	23.41 23.41	348 · 271 174 · 816 356 · 207 182 · 991 4 · 228	173'920 358'174	o'6892 o'7430 o'6992 o'7267 o'7226	9.7639 9.7639 9.7530 9.7242 9.7274	8.7074 8.7507 8.7235	o'5384 o'5655 o'5442 o'5544 o'5583	7.6764 7.6638 7.6755 7.6647 7.6743	9"9953 9'6968 9"5176 9"4420 9'5881
2061 2062 2063 2064 2065	- 348 IX 24 - 347 II 19 - 347 VIII 14	1594 218 12 : 1594 366 9 : 1594 542 19 :	36.8 5.413 27.5 176.705 55.7 326.335 24.8 136.237 38.9 315.777	+4'26	23.741 23.741	169.482	13'093 170'237 346'708	0.4413 0.4413 0.4413 0.4413	9.7503 9.7046 9.7626 9.7113 9.7446	8.7093 8.7593 8.7135	0'5403 0'5706 0'5362 0'5637 0'5472	7.6659 7.6731 7.6710 7.6679 7.6724	0n0026 0'0544 9'9502 0n0403 9'3067
2067 2068 2069	- 345 I 29 - 345 VII 24 - 344 I 18	1595 075 9 1595 251 16 2 1595 429 10 4	26'9 125'582 17'6 304'90' 23'1 115'26' 46'8 293'65' 59'2 77'11'	+4'15	23.742	185'765 5'182 193'231	354'194 187'802 3'813 193'610 345'820	0'7150 0'7308 0'5947 0'7441 0'6973	9.7372 9.7171 9.7594 9.7004 9.7570	8.7063	0'5481 0'5638 0'5351 0'5742 0'5348	7.6737	9n4854 9n7306 9.6484 on1016 on1332
2071 2072 2073 2074 2075	- 344 XII 7 - 343 VI 3 - 343 XI 27	1595 606 9 1 1595 753 16 1 1595 931 15 1 1596 108 1 1 1596 285 21 1	19'9 66'94: 37'8 240'90	-1.27 -2.06	23'744	168,448 352,863 176,260	166.293 355.303 174.024	0.7180	9'7635 9'7194 9'7334 9'7465 9'7090	8.7211 8.7304 8.7446	0.2480	7.6776 7.6623 7.6777	0.0651 0.0280 9%8112 9.5170 9.1049
2077 2078 2079	- 341 V 12 - 341 XI 6 - 340 IV 1	1596 964 13	12'7 45'83 14'7 219'24	+1.00 2 -3.30 2 -1.00	23'745 23'745 23'745	9'358 192'000 347'620	183'575 8'886 193'576 345'187 170'589	0.6947	9'7574 9'7319	8 7055 8 7547 8 7295	0'5657 0'5425 0'5507	7.6626 7.6770 7.6657	9,5464 9,9533 0,0106 0,0488 0,0296
	- 338 III 11 - 338 IX 4	1597 319 1 1 1597 496 7 1597 673 18 1 1597 850 7 1598 028 10	7'4 346'19 8'5 156'18	+3.06	23.745	4.602	4.822	0.7435	9.7064	8.4002 8.4000	0'5718 0'5341 0'5681	7.6719	9'5804 9'5919 9n5271
2086 2087 2088 2089 2090	- 336 I 20 - 336 VII 14 - 335 I 8 - 335 VII 4	1598 353 4 1 1598 529 16 1598 707 4 1 1598 884 9 3	2 9 205 400	0 + 3.56 $0 + 2.51$	23'744 23'744 23'743	349 916 169 914 357 208	351.267 169.104 357.017	0.7361	9.7104 9.7629 9.6997	8.7137 8.7582 8.7059	o'5683 o'5752	7.669r 7.6748 7.6644 7.6758 7.6636	0n0191 9n9772 9'9328 9n4298 9'1004
2091 2092 2093 2094 2095	- 334 VI 23 - 334 XII 17 - 333 V 14	1599 061 5 1599 238 23 1599 415 12 1599 563 17 1599 593 7 1	11.6 261.61	-1.20 -0.20	23.741 23.741 23.740	187.258 12.250 166.004	189.677	0.7139	9'7391 9'7406 9'7047	8.7357 8.7392	0.5522	7.6629 7.6773 7.6626	
2096 2097 2098 2099 2100	- 332 V 2 - 332 X 27 - 331 IV 21	1599 740 15 1599 917 18 1 1600 095 6 1 1600 271 22 2 1600 449 16 4	7'6 36'912 4'1 209'845	-1.56 -3.29	23 740 23 739 23 730	173.953 182.220	179.889	0.7426	9.7048 9.7518 9.7260	8 · 7497 8 · 7249	0.5646 0.5452 0.5530	7'6638	925294

2052 2053 2054 2055 2055 2056 2057 3	72 · 9 38 · 8 5 · 5 96 · 9 378 · 2 358 · 2	6 +	1.08	284 <u>c</u> 242 <u>c</u> 380 c	1.76	144	G		K	$\log \sin g$	log sin <i>k</i>	$   \frac{\log}{\cos g} $	$\log \cos k$	log	log	N'	bei ⊙. gan		im Mit	ag	bei ( Unterga	o mg	$I^{p}$
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2102 2103 2104	— 330 — 329 — 329 VI	X 5 III 2 III 26	1600 1600 1601	803 951 128	20 10.6 18 8.1 2 41.4	337'173 146'955	-2.35 +3.74 +0.21	23.739 23.739 23.739	11.666 169.051	188°744 12'733 169'925 346'072 179'703	0.417 0.6917 0.7357	9'7037 9'7624 9'7123	8.7478 8.7088 8.7587 8.7146 8.7410	0.5720 0.5357 0.5640	7.6693 7.6696	9"9743 0'0454 9'9682 0"0592 9'3692
2107 2108 2109	- 328 V - 327 - 327 V - 326 - 326	II 8 III 4 I 28	1601 1601 1602	660 837 014	0 8.4 18 30.7	315.856 125.878 304.672	+4'41 +0'58 +4'13	23.739 23.739 23.740	185.477 4.504 192.993	187.447	0.7320 0.6940 0.7443	9.7386 9.7160 9.7603 9.7560	8.7062	0.5637 0.5352 0.5736	7.6724 7.6665	9n5551 9n7097 9'5869 0n0941 0n1562
2112 2113 2114	— 326 V — 326 X — 325 X — 324	(II 19 VI 14 (II 8	1602 1602 1602	339 516 693	1 10'8 22 18'3 10 24'7	263 · 208 77 · 356 252 · 131	+0.01 -1.64 -1.54	23.74 I 23.74 I 23.74 I	168.418 351.985 176.259	354'415 174'053	0.7273 0.7205 0.7035	9.7210 9.7316 9.7478	8·7291 8·7457	0.5636 0.5490 0.5483	7.6625	0'0419 0'0280 9#8628 9'5159 8'6009
2117 2118 2119	- 323 - 323 - 322	V 23 XI 16 IV 12	1603 1603 1603	225 402 549	5 5'I	230'457	-2'17	23 742 23 743 23 743	8 435 191 972 346 893	183.675 7.850 193.631 344.451 14.494	0'7439 0'6955 0'7181	9.7028 9.7564 9.7339	8.7311 8.7538	0'5396 0'5651 0'5433 0'5490 0'5555	7.6623 7.6775 7.6646	9'9081 0"0104
2122 2123 2124	- 321 - 321 - 320	IV 2 IX 26 III 22	1603 1604 1604	904 081 259	9 39'0 14 41'1 2 26'6	189.468 7.115 178.251 356.897 167.036	+1'05 -1'72 +2'09	23'742 23'742 23'742	355'514 175'693 4'014		0'6899	9'7572 9'7008 9'7639	8.7526 8.7062 8.7596	0.2364	7.6657 7.6733 7.6670	0.0395 9.5875 9.6172 9.5329 9.4712
2127 2128 2129	- 319 - 318 - 318 - 317	IX 3 I 30 II 26	1604 1604 1605	789 938 115	19 58'4 12 44'5 0 0'6	346.575 156.118 306.503 117.001 295.207	-0'26 +4'19 +0'40	23 74 2 23 74 2 23 74 2	191'072 1 349'678 1 169'182	188 645 351 241 168 516	0.7037 0.7185 0.7372 0.6909 0.7442	9'7323 9'7095 9'7634	8.7307 8.7127 8.7587	0.5425 0.5532 0.5683 0.5330 0.5742	7.6705 7.6735 7.6655	9n9884 9'9623
2132 2133 2134	— 316 X	7II 4 XII 27	1605 1605 1606	646 824 000	7 9.3	283 · 887 95 · 640 272 · 798	+2.47 -0.58	23.746	9 12.315 0 186.434 9 12.315	2.397 188.86g	0.7323 0.7152 0.7093	9.7148 9.7373 9.7421	8.2123	0.2663 0.2511	7.6758 7.6636 7.6767	9.6140 9.7625 0.0327
2137 2138 2139	- 315 - 314	XI 17 V 14 XI 7	1606 1606	325 503 680	0 45 9 14 44 4	231'855 47'326 221'026	-3.31 -5.01	23'73 23'73 23'73	8 348 202 8 173 075 7 356 069	196.588 348.417 171.962 358.153 179.03	0.0890 0.7418	9.7636 9.7636 9.7508	8.7130 8.7613 8.7085 8.7486 8.7261	0'5392 0'5637 0'5463	7.6775 7.6626 3.7.677x	918210
2142 2143 2144	- 311	IV 21 X 16 III 13	1607 1607 1607	389 537	3 59 8 2 13 1	210 019 26 517 198 749 347 937 157 745	-0'80 -2'96	23.73 23.73 23.73	6 190.08 6 11.47 6 168.54	188.06	6 0.7010 1 0.7423 4 0.6924	9 7532 9 7027 9 7618	8.7489	0.5376 0.5733 0.5353		929420 0'0388 9'9884
2147 2148 2149	— зор V	III 25 II 20 III 15	1608	067 246 422	17 45 3 0 50 4 8 2 1	337'506 146'986 326'742 136'553	+0'22 +4'24 +0'52	23.73 23.73 23.73	6 355 47 6 185 10 7 3 90	7 187.00	4 0.712 9 0.733	9'7401 2 9'7148 9 9'7611	8 · 737	9 0.548 9 0.563 2 0.535	7 · 6692 4 7 · 6716 4 7 · 6679	9n 607) 9n 6800 9'523
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2102 2103	90.62	0'9425 1'1102 0'9294 1'1460 0'2340	9.7058	332'18	92.65	9 4939	0.0863	9 9779	9.4470	911937	9.9946	73'5	-160 +	51 - 9	8 + 67	+103 - - 70 + - 109 +	80 # P	
2106 2107 2108	330.85 71.56	-0:3590 -0:5125 -0:3863 -1:2420 -1:4330	9'7407 9'7181 9'7624	127 '29 306 '74 115 '39	93.38 93.36	9:5346 9:5347 9:5526	9 · 99 1 3 9 · 99 5 3	9 · 9 7 3 9 1 9 · 9 7 2 9 3 9 · 9 7 0 1	912994 912938 911604 911398	9'4447 9"4478 9"5±35	9'9825 9'9822 9'9756	78.2 98.8 81.6	-151 -102 +	41 - 6	18 4		p	įs
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212 212 212 212	2 324'7 3 43'2 4 213'6 5 39'1	4 +0 · 4 · 4 · 4 · 4 · 4 · 4 · 4 · 4 · 4 ·	8 9 759 2 9 703 1 9 766 9 9 709	0 178 · 7 0 357 · 7 5 170 · 7	6 90 · 4 8 90 · 7 3 92 · 8	0 9 · 692 0 9 · 690 6 9 · 690	49'939 69'940 69'940	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	7 9,692 2 9,690 2 9,683	3 8 · 089 2 8 · 338 3 1 8 · 955	93 9 . 998 93 9 . 999 98 9 . 999	0 119 9 60 2 119	5 - 107 + 6 + 80 0 - 102 +	- 12	41 -	_	46	) ::: (::: )
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21 21 21 21	42 83. 43 239. 44 212. 45 335.	54 -0.87 79 +0.97 59 -1.18	35 9 75 36 9 76 60 9 71	48 203 · 39 345 · 55 152 ·	90 92 ·	74 9 50 54 9 49 60 9 50	9, 9, 9, 9, 9, 9, 9, 9, 9, 9, 9, 9, 9, 9	310 9 97 791 9 97 819 9 97	770 9n46 774 9 '48 764 9n45	510 9#11 315 8#9: 505 9 18	119 9 99 249 9 99 831 9 99	063 107 085 73 049 100	7'0	+ 59	70	- (+ 98) - 8 - ro	(+83) + 32	t* 1) t*
27	47 87. 48 186	45 -0'40	93 9 71	69 319	51 93	27 9 5	749'9	866 9 9	750 9 3	875 9n3	439 9 9 422 9 9	891 7 827 10	5 · 5 + 97 2 · 1 - 14	42	十ェククリー	- 12 - 32 - 42 - 119 - 36 + 129	14	r th p

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Nr.	Julianischer Kalender	Julian. Welt- Tag Zeit	L'	Z	ε	P	Q	$\log p$	$rac{\log}{\Delta L}$	$\log q$	$u_{\alpha}'$	$\log f_a$	logγ
2151	- 308 VII 5	1608 747 161 481	7 98°039	0°47	230737	3420426	344°359	0.0002	9.7547	8'7501	0.5367	7 6637	0,,1774
2152 2153 2154	- 308 VIII 4 - 308 XII 29 - 307 VI 25	1608 777 0 58° 1608 924 9 32°	5 126.305 3 274.381 7 87.786	-1.08 +1.38 +0.00	23.737 23.738 23.738	12.331 168.364 351.125 176.247	13'386 166'113 353'536 174'098	0.425	9 7 7 6 2 2 9 7 7 2 9 7 9 7 7 4 9 1	8 · 7579 8 · 7234 8 · 7274 8 · 7471	0'5342 0'5624 0'5503 0'5473	7.6665 7.6767 7.6629 7.6773	0.0196 0.0290 0.0290 0.9084 0.5165
2157 2158 2159	- 305 XII 8 - 305 VI 3 - 305 XI 28	1609 456 10 38 1609 633 9 59 1609 810 11 28 1609 988 1 29 1610 135 3 37	6 252 505 5 66 614 4 241 683		23 738 23 739 23 739	359.507 184.128 7.510 191.965 346.113	0'738 183'770 6'813 193'700 343'673	o'740g o'688g o'7435 o'6965 o'7167	9.7067 9.7633 9.7032 9.7555 9.7356	8.7091 8.7610 8.7664 8.7530 8.7326	o'5630 o'5394 o'5649 o'5440 o'5475	7.6625 7.6776 7.6623 7.6777 7.6638	8,6734 9,5441 9.8576 0,0112 0,0949
2162 2163 2164	- 304 X 17 - 303 IV 12 - 303 X 6	1610 164 15 0 1610 312 21 5 1610 489 17 16 1610 666 22 22 1610 844 10 16	0 200°534 8 17°682 1 189°244	4-0.01	23 740 23 740 23 740	15 764 168 003 354 791 175 427 3 352	13'557 170'062 353'204 175'849 3'859	o'7283 o'7308 o'6955 o'7439 o'6904	9'7223 9'7166 9'7583 9'7637	8.7210 8.7184 8.7537 8.7060 8.7591	0.5652 0.5353	7.6623 7.6756 7.6647 7.6744 7.6658	0'1603 0'0465 9"6514 9'6433 9'4553
2167 2168 2169	— 301 III 23 — 301 IX 15 — 300 II 10	1611 020 22 16 1611 199 1 58 1611 375 3 53 1611 523 20 27 1611 700 7 49	9 357 268 3 166 983 5 317 445	+2.06 0.96 +4.40	23'740 23'740 23'740	182'777 11'891 190'684 349'366	181'302 14'078 188'249 350'842 167'977	0,4380 0,4141 0,4020	9.708x 9.7478 9.7336 9.7085 9.7637	8.7441 8.7321 8.7116	0.5424 0.5533 0.5680	7.6671 7.6719 7.6723	9,4212 0,0170 9,9831 0,0020 9,9879
2172 2173 2174	299 VII 26 298 I 18 298 VII 15	1611 877 20 29 1612 055 0 43 1612 231 21 48 1612 409 14 21 1612 586 5 54	9 117 424	+0.03 +0.03 +0.03	23.737 23.737 23.737	356.770 177.013 4.237 185.648 12.139	356'355 178'587 2'178 188'086 9'757	0.2122 0.2312 0.2122	9'7004 9'7583 9'7163 9'7356	8.7539 8.7182 8.7328	0'5356 0'5650 0'5478	7.6655 7.6749 7.6643	9"4927 9'4104 9'5978 9"7076 0'0287
2177 2178 2179	- 297 VII 4 - 297 XI 29 - 296 V 24	1612 734 6 24 1612 763 21 10 1612 911 8 56 1613 088 7 14 1613 265 23 45	5 96 63: 5 243 086	3 -2·17 3 -2·17	23.736	164.176 194.066 348.198 172.171 356.054	195 644 348 514	0.7379 0.6891	9,4028 6,4022	8.7122 8.7612 8.7092	0.5616 0.5395 0.5630	7.6635 7.6777 7.6623	0'1774 0"1216 9"9978 9'8732 9"5381
2182 2183 2184	- 295 X1 7 - 294 V 3 - 294 X 27	1613 442 12 36 1613 620 9 27 1613 797 1 6 1613 974 11 55 1614 122 10 9	4 221 18 0 35 99 5 209 85	3 -3.32 5 -3.30	23.73	3 909 1 189 274 1 11 336	6'175	0.7261	9.7225	8.7238 8.7503 8.7080	0.5625 0.5365 0.5742	7.6771 7.6632 7.6763	9.5575 9.9049 0.0342
2187 2188 2189	- 293 IX 16 - 292 III 13 - 292 IX 5	1614 653 1 40	7 26 91 0 168 610 8 348 25 8 157 78 0 337 55	3 -0.34 -0.34	23.73 23.73 23.73	4 346 · 928 3 176 · 435 3 355 · 027	345 049 178 827 352 671	0'7105	9.7146 9.7403 9.7416	8.7168	0.5473	7'6720 7'6682 7'6706	0n0858 9'5037 9n6464
2192 2193 2194	— 290 II 19 — 290 VIII 15 — 289 I 9	1615 007 16 4 1615 185 9 27 1615 362 8 52 1615 509 17 49 1615 687 12 16	5 326 49 1 136 97 9 285 51	+4.25	23 73 23 73 23 73	4 102 285	192 323 12 903 165 973	0'7447 0'6926 0'7252	9 7003 9 7614 9 724	8 · 7058 8 · 7573 8 · 7248	0'5360 0'5719 0'5351 0'5610 2'0'5518	7'6711 7'6678	010705 9'9985 0'0314
2197 2198 2199	- 288 XII 18 - 287 VI 13	1615 864 3 56 1616 041 17 7 1616 218 18 56 1616 395 17 52 1616 573 10 22	6 263 72 1 77 00	-1.02 +0.02	23 73 23 73 23 73	6 358 607 6 184 105 6 6 587	183 85	7 0 7416 3 0 6896 8 0 743	9 705 9 763 9 703	8.7611 8.7061	0'5630	7.6629 7.6773 7.6625	9n1252 9n5417 9.8005

Nr.	μ.	γ	$\log n$	G	.К.	$\log \sin g$	log sin <i>k</i>	log cos <i>g</i>	$\log \cos k$	log sin δ'	log cos စိ′	N'	bei ⊙Δ gun λ	Λuf- g	ntrali m Mittag \lambda   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \varphi   \var	Β Unto	i ⊙ rgang ∣ φ	$I^r$
2152	324'62 362'42	1'5047 1'0462 1'0690 0'8098 0'3285	9 · 7642   1 9 · 7244   2 0 · 7318	73.01 201.01	92.97 88.54 87.33	9'5530 9'6080	9,9951 9,9951	9.9587 9.9510	9,1740 9,0232	9.5111 9.6035 9.6045	3.3010 3.3010 3.3228	99'1 93'6 83'4		- 53		31 +14		
2156 2157 2158	341°33 330°26 352°04	0'0471 0'3500 1'0262 1'2442	9.7089 9.7654 9.7054	63.09 238.58 52.91 228.60	85.53 84.86 84.10	9.6352 9.6415 9.6495 9.6536	9'9928 9'9901 9'9860	9 · 955 ¹ 9 · 953 ⁸ 9 · 951 ⁸	9 · 2546 9 · 3240 9 · 3980	9.5949 9.5842 9.5677	9'9636 9'9654 9'9681	78.7 103.2 74.4	- 74	- 13 - 7	+ 19 +	20 - - 8 44 - -11 70 - -11	3 + 8	3 7:4: 1 t
2163 2163 2164 2164	142.44 80.34 159.25 332.4	2 1 · 4463 4 1 · 1130 4 0 · 4481 5 0 · 4398 7 0 · 2853	9.7187 9.7604 9.7658 9.7658	194.86 12.77 186.59 5.39	85 70 86 22 87 93 88 31	9.6868 9.6874 9.6917	9 9 9 4 7 9 9 9 9 4 1 2 7 9 9 9 4 1 2 9 9 9 4 1 2	9,841	9 · 6732 9 · 6879 4 9 · 6879	5 8 · 722; 0 8 · 8 · 8 · 8 · 8 · 8 · 8 · 8 · 8 · 8	9 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 999 · 99 · 99 · 99 · 99 · 99 · 99 · 99 · 99 · 99 · 99 · 99 · 99 · 99	61.7	7 137 2 143 3 37	+ 55 - 13	152 + 23 +	24 — 1 27 — 9 22 + 9	6 3	3 1 ⁿ
216 216 216 217	7 205 ° 0 8 236 ° 6 9 125 ° 3 0 299 ° 2	5 0 · 2637 1 · 1 · 0400 6 · 0 · 9618 8 · 1 · 0046 1 · 0 · 9725	9.7498 9.7357 9.7106 9.7657	358.03 170.64 328.09 139.62	96.85 96.46 96.86	9.688 9.688 9.688	7 9 941 9 9 943 9 9 965 6 9 974	9 9 9 40 1 9 9 45 5 9 9 48	3 9 588 3 9 586 3 9 586	3 8 · 957 1 9 · 435 1 9 · 503	6 9 · 998: 0 9 · 998: 1 9 · 999:	2 110.	8 + 46 4 (+ 19) 6 (-135)	— 45 (69) (+70)	granden gabriere gabriere		17) (-7) 19   - 5	5) r 3 (r) 2 t
217 217 217 217	2 191'2 3 142'4 4 33'8 5 263'3	4 -0.310g 4-0.3961 4-0.5106 7-1.0682	9.7604 9.7185 9.7377 9.7455	130°7 308°6 120°98 297°8	1 96 · 27 1 96 · 03 8 95 · 03 94 · 6	7 9 653 7 9 651 8 9 640 9 636	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	7 9 ' 95 ° 7 9 ' 95 ° 4 9 ' 95 ° 3 9 ' 95 °	9 9 4 1 5 9 9 3 1 7 9 9 2 6 9	8 9 5 5 5 3 9 n 5 9 1	2 9 · 969 2 9 · 964 8 9 · 964	0 73	8 +156 0 93 3	+ 7 - 16	-145	- 3	יין -ע	"
217 217 217 218	7 134 4 8 318 8 9 292 9 0 180 2	9 1 · 5047 7 1 · 3230 22 0 · 9950 22 0 · 7468 31 0 · 3453	9 · 7656 9 · 7689 2 9 · 7515	110°3; 254°4 68°7; 242°5	3 93 3 9 87 9 4 87 4 4 86 9	9 9 ' 0 2 5 5 9 ' 5 6 9 2 9 ' 5 5 8 9 9 ' 5 4 8	1 9 99 6 1 9 99 6 17 9 99 6	12 9 · 958 16 9 · 968 17 9 · 979	75 9n 128 30 8n 968 95 9	5 9n555 4 9 53 9n50	31 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	x 95 3 82 68 99	4	38 10		- 39 - 1	05 -	69 t 51 r# 28 t
218 218 218 218	3 195 9 4 359 9 5 332 9	00 -0'0510 (4 +0'3610 05 -0'803 -1'0820 09 +1'024	9 · 7633	44.7 216.3 358.3	4 86 · 6 9 86 · 8	1 9 524 8 9 513 8 9 494	12 9 '98! 12 9 '98! 12 9 '97!	32 9 97 31 9 97 78 9 97	9,35 43 9 36 56 9,44 78 9 49	25 9 38 25 9 38 21 9 30 40 7 198	37 0 . 000	9 76 11 105 00 71	3 +120		1			8 r ⁴ 38 t p p - p
218 218 218 219	37 90'; 38 186'; 39 206'; 90 300';	37 —1 · 501 73 — 1 · 218 17 · +0 · 318 72 — 0 · 443 27 — 0 · 438	5 9 · 7 1 66 9 9 · 7 4 2 4 0 9 · 7 4 3 2 3 9 · 7 1 5 9	5 166 · o 4 345 · 5 7 152 · 8 9 332 · 4	91 4 3 91 4 3 92 5 5 92 5	6 9 49 1 9 9 49 4 8 9 50 4 9 9 50 50	75 9 9 7 18 9 9 7 15 9 9 8 35 9 9 8	39 9 97 93 9 97 21 9 97 24 9 97	74   92 47 77   9 47 66   92 44 68   9 44	93 8291 86 9 18 60 92 18	03 9 * 99 34 9 * 99 23 9 * 99 66 9 * 99	85 72 49 106 48 73	'4 110 '5 + 89 '6 - 1	2 - 42	2 + 63	- 19 - - 36 +		9 r
21 21 21 21	92 314 93 310 94 87 95 6	30 +0.288 17 -1.176 00 +0.996 79 +1.075 93 -0.887	2 9 7 7 0 2 6 9 7 7 3 0 6 9 7 7 3 0	4 319'3 4 128'4 0 272' <u>9</u> 0 84' <u>9</u>	30 93 °4 15 93 °4 97 90 °4	13 9 . 53 15 9 . 58 19 9 . 60	84 9 9 9 49 9 9 9 92 9 9 9 17 9 9	97 9 9 96 97 9 9 96	49 9 30 29 9 31 45 8 26 22 8 51	71 9234 15 9 43 90 9258 26 9 60	88 9 98 87 9 96	30 102 46 88 25 88	·3 (-15 ·8 ·0 4	4) (+72	-	— 3,9 +	180 +	53 r
21	97 78' 98 103'	48 +0.331 36 -0.133 21 -0.348 82 +0.631 13 -1.027	49 707 319 765	9 73 3 6 249 7	57 87 · 70 86 · 85 85 ·	27 9 61 61 9 62 49 9 61	95 9 99 53 9 99 56 9 99	75 9 '95 61 9 '95 27 9 '9!	87 9 ° 03 574 9 ° 12	28 9 00 276 9, 60 85 9 59	044 9 96 022 9 96 035 9 96	17 83 21 98 37 78	1'2 —13 1'4 —17 3'6 —16	3 - 1	3 - 78 1 -105	+ 15 - - 44 -	25 -	1 7 26 t 45 7

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Nr.		T		L'	Z	٤	$P_{\perp}$	Q	$\log p$	$egin{array}{c} \log \ \Delta L \end{array}$	$\log q$	$u_a'$	$\log f_a$	$\log \gamma$
	Julianischer Kalender	Julian. Tag	Welt- Zeit											
2201 2202 2203 2204 2205	- 286 VI 2 - 286 X 29 - 285 IV 24	1616 720 1616 749 1616 898 1617 075 1617 252	5 15.1 0 51.3	66 · 457 211 · 655 28 · 203	-2.05 -3.33 -0.90	23'737 23'737 23'738	14'871 167'883 354'013	342°854 12'612 169'879 352'545 175'530		9'7374 9'7239 9'7152 9'7595 9'6999	8 · 7224 8 · 7175 8 · 7545	0.5461 0.5533 0.5667 0.5341 0.5748	7.6630 7.6623 7.6764 7.6638 7.6756	0,1181 0'1345 0'0520 9,7109 9'6625
2207 2208 2209	- 284 X 6 - 283 IV 2 - 283 IX 25		6 4.6 9 37.2 11 58.6	7,850	-2.44 +1.00 -1.45	23.737 23.737 23.737	182.214 11.232 190.377	3.278 180.949 13.478 187.936 350.348		9'7633 9'7091 9'7464 9'7351	8.7126 8.7427 8.7336		7.6744	9:3501 9:3769 9:9941 9:9692 0:0185
2212 2213 2214	- 281 VIII 6	1618 463 1618 640 1618 817	4 2'1 8 28'3 5 46'9	317.155 128.036 305.891	+4.40	23.737 23.736 23.736	356.444 176.342 4.014	167.513 355.915 178.025 1.891 187.347	o.6899 o.7439 o.6965 o.7304 o.7183	9'7009 9'7573	8.7062 8.7529	0.5339 0.5723 0.5369 0.5632 0.5494	7.6723 7.6666 7.6736	o'0093 9"5342 9'4993 9'5733 9"6490
2217 2218	- 279 VII 15 - 279 XII 9 - 278 VI 4	1619 496 1619 673	3 52'4 17 54'7 13 42'2	107.106	+0.04 -1.00	23.735 23.735 23.734	193°247 348°193 171°256	9.654 194.731 348.614 169.936 358.238	0.7387 0.6892 0.7403	9.7633	8.7099 8.7608 8.7099	o:5395 o:5623	7.6643	0'0228 0"0968 9"9981 9'9201 9"5389
2221 2222 2223 2224 2225	- 277 XI 18 - 276 V 13 - 276 XI 6	1620 027 1620 205 1620 382 1620 559 1620 707	17 52'2 8 28'9 19 57'2	232°379 47°452 221°004	-2'94 -1'99	23'731 23'731 23'732	3.883 188.435 11.248	177.265 6.101 186.610 11.991 168.549	0'7273 0'6987	9.7015 9.7558 9.7015	8.7226 8.7512 8.7076	0'5490 0'5537 0'5356 0'5749 0'5346	7.6771 7.6626 7.6771	8:4589 9:5558 9:8630 0:0312 0:0340
2227 2228 2229 2230	- 275 IX 27 - 274 III 24 - 274 IX 16 - 273 III 13	1620 737 1620 884 1621 062 1621 238 1621 416	8 11.2 9 44.8 15 41.0	179 550 358 937 168 668 348 285	+1'89 -1'06 +2'90	23 '731 23 '731 23 '731 23 '731	346.619 175.856 354.661 184.126	197°292 344°672 178°261 352°333 185°867	0 7323 0 7135 0 7092	9 7 7 5 7 9 7 7 3 9 0 9 7 7 4 2 9	8.7178 8.7365 8.7407	0.5310 0.5645 0.5473 0.5480 0.5632	7.6734 7.6669 7.6720	0#0947 9:5709 9#6758
2231 2232 2233 2234 2235	- 271 I 20 - 271 VII 16	1621 770 1621 947 1622 095 1622 272	16 43'4 16 52'0 2 2'5 19 18'8	337.299 147.724 296.596 108.741	+3.73 +0.18 +3.62 +0.12	23'731 23'732 23'732 23'732	198.118 11.101	2 · 039 3 · 191 · 744 1 · 12 · 489 3 · 165 · 786 1 · 351 · 858	0.7449 0.6932 0.7240	9'7007 9'7604 9'7256	8.7059	0.5365 0.5365	7.6697 7.6747	9.9792
2237 2238 2239 2240	- 270 VII 5 - 270 XII 30 - 269 VI 25 - 269 XII 19	1622 804 1622 981 1623 158	23 40'3 3 49'5 0 20'2 19 12'1	98.129 274.919 87.412 264.129	-0'45 -1'09 -0'09	23'733 23'733 23'733 23'733	357 743 184 053 5 683 191 94	4.772	0 · 7422 4 0 · 6890 2 0 · 7427 4 0 · 698	9 7047 9 7637 9 7045	8.7611	0.5649 0.5385 0.5646	7.6629 7.6629	9"3353 9"5366 9'7364
2242 2243 2244 2245	- 268 VI 13 - 268 XI 8 - 267 V 4 - 267 X 28	1623 305 1623 335 1623 483 1623 660 1623 837	4 38 2 13 29 9 8 21 1 14 3 7	76.867 222.826 38.687 211.406	7 -1.66 -3.30 -1.60 -3.34	23.734 23.734 23.734 23.735	13.98 167.81 353.19 175.07	351.849 5 175.27	4 0.725 8 0.733 9 0.694 8 0.744	9 7255 9 7135 9 7602 2 9 6999	8 · 7239 8 · 7259 8 · 7554 8 · 7058	0.5449 0.5526 0.5677 4 0.5333 0.5752	7.6525 7.6772 7.67630 7.6764	0'1067 0'0554 9"7658 9'6758
2247 2248 2249	- 266 X 17 - 265 IV 13 - 265 X 6	1624 015 1624 191 1624 369 1624 545 1624 694	14 1'2 17 7'2 20 13'2	18.453 188.936	$\begin{array}{c c} -3.02 \\ -0.05 \\ -2.44 \end{array}$	23.73 23.73 23.73	5 182°32 5 10°51 5 190°14	5 180.67	2 0.736 2 0.708 9 0.714	9 710 9 744 2 9 736	8 8 7 5 8 9 8 7 1 3 9 8 7 3 4 8 8 7 3 4	0.569: 0.5428 0.5529	7.6756	9°9672 9°9580
L														

Nr.	μ	·y	logn	G	K	log sing	log sin k	$\log \cos g$	$egin{array}{c} \log \ \cos k \end{array}$	log sin ô'	log cos ð'	N'	bei⊙⊿ gan λ	Auf- g φ	entralitin Mitta	g Unto	oi ⊙ ergang   φ	F
2202 2203	145°33 265°31	-1'3125 -1'3630 -1'1'1272 -0'5139 -1-0'4597	9.7259 9.7259	203.50 23.02	84.12	0.6813	9 9553	9.9521	9 3933	9,3248	0,0030	116 2 63 2	+114	- 56 - 55	+172 + 91 +	24 -12 23 +14		p p p t
2206 2207 2208	89 · 85 272 · 89 320 · 74		9.7654 9.7113 9.7484	13.06 186.39 5.68	86:14 87:99 88:24	9 · 6877 9 · 6914 9 · 6883	9'9456 9'9418 9'9418	9'9412 9'9400 9'9400	9.6729 9.6878 9.6855	9 * 0972 8 n 7969 8 * 7424 8 * 1646	0.0000 0.0000 0.0001 0.0001	61.4 61.4	153 26 50 78	15	- 93 + + 83 -	22 — 1 19 +15 — (- 6	9 47	) t*
2213	237 · 15 307 · 30 1261 · 48 5 · 142 · 54	+1.0216 5-0.3422 5-0.3744 3-0.4457	9 7031 9 7594 9 7201 7 9 7359	130'93	96.83 96.84 96.29	9 66539 9 6540	9 973 9 975 9 982	9 9473 9 9473 5 9 9483 8 9 9500	9 5337 9 527 9 5141 5 9 4407	9.552	9.9770	107	3 - 27 3 - 36	+ 37 + 2		38 11	17 :	1
221 221 221 221	7 234 5 8 92 2 9 29 9 9 311 6	7 +1.0540 2 -1.2493 3 -0.9950 7 +0.8320 0 -0.3450	0 0 . 4200 0 0 . 4200 0 0 . 4200 0 0 . 4220	255 '23 255 '23	89:53 88:63 88:04	9.5888 9.5777 9.5690	0.008 0.008 0.008	3 9 · 967 2 9 · 966 3 9 · 967	6 8, 288 5 8 772 9 8, 945	9,588 9,572 6,9,556	3 9 · 964 3 9 · 967 4 9 · 969	9 95° 1 86° 2 91°	9 — 2 + 107 3 — 130 4 — 22	+ 48 14	(+ 87) (- - 32 + + 48 -	78 + 4x +1	77 + 5	3 1 1 1 4 7 - t
222 222 222 222	2 89.9 3 307.3 4 119.4 5 91.0	0 + 0 · 0288 8 + 0 · 3599 3 - 0 · 729 7 + 1 · 074 8 + 1 · 081	6 9 ' 723: 5 9 ' 757: 5 9 ' 703: 5 9 ' 762:	2 242.79 5 229.5 5 11.3	3 86 · 72 3 86 · 72 3 88 · 80	9 5489 9 5410 9 529 9 496	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	7 9 9 9 7 7 9 9 9 9 7 7 6 9 9 9 7 7	0 9 258 5 9 326 6 9 487	9'472 1 9"421 0 8'811	0 9 · 9 8 0 6 9 · 9 8 4 1 9 · 9 9 9	7 99° 3 102° 1 72°	1	29 54 	56	31 +1	30 1	4 1 1 1
222 222 222 223	7 208 5 8 301 9 9 328 5 0 51 2	4 1 · 436 1 · 243 2 · 372 0 · 474 0 · 389	7 9 7 7 4 5 9 9 7 7 4 5 9 9 7 7 4 5	7 358 · 6 0 166 · 0 7 345 · 5	9 90 · 14 8 91 · 44 4 91 · 48	9 494 9 495 9 494	2 9 · 978 5 9 · 978 2 9 · 979	9 9 9 7 8 9 9 9 7 7 9 9 9 7 7	9'491 5 9:481 77 9'478	2 7 1 8 7 3 2 8 1 8 9 8 7 8 1 9 1 2	3 9 '998 3 9 '998	0 71° 6 107° 5 72°	9 - 7 7 - 34 4 - 119	40	- 48	- 29	13	- p
223 223 223 223	35 112 '2 34 209 '0 37 112 '2	37 +0'249 -1'132 44 +0'953 +1'085 -0'961	12 9 762 12 9 762 18 9 728	4 141.0 6 285.2 1 96.2	1 93 26	5 9 · 5 1 8 2 9 · 5 6 9 2 9 · 5 8 3	6 9 ' 98 5 9 ' 99 2 9 ' 99	9 9 974 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	19 9 39 8 78 8 95 8 55 8 1 588	37 9 55 37 9 58	22 g · g8g	7 104 19 84 19 92	'9 130 '4 140	+ 77 61	(+110)(	- 52	88 -	64 p
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2372 2373 2374 2375	- 210 V 4 - 210 IX 29 - 210 X 28 - 209 III 25	1644 656 II 18 6 1644 804 8 43 7	39'487 181'760 211'455 0'187	-1'51 -2'00 -3'36 +1'79	23.728 23.728 23.728 23.728	16'638 166'251 197'769 354'347	353'384	0.7349 0.6890 0.6915 0.7424	9 7047 9 7142 9 7640 9 7611 9 7040	8.7078 8.7145 8.7606 8.7581 8.7075	0'5593 0'5369 0'5401	7.6655 7.6631 7.6735 7.6764 7.6668	0'1898 0'0630 0"1741
2377 2378 2379 2380	- 208 IX 7 - 208 IX 7 - 207 III 2 - 207 VIII 27		5 349°383 7 160°484 5 338°798 9 149°565	+2.79 -0.52 +3.62 +0.09	23'727 23'727 23'727 23'726	2'370 182'639 10'742 190'554	191.641	0.7254 0.7234 0.7021 0.7415	9.7247 9.7265 9.7508 9.7046	8.7489 8.7239 8.7258 8.7472 8.7085	0'5562 0'5565 0'5421 0'5684	7.6693	9'3397 9"3844 9'9704 0"0022
2382 2383 2384 2385	- 205   I II - 205   VII   6 - 204   I I	1645 838 5 13 9 1646 014 16 11 9 1646 368 1646 547 1646 723 14 5 6	288·222 99·374 277·160	+2.87 -0.35 +1.65	23 · 726 23 · 725 23 · 725	355.907 176.263 3.765	358 234 173 832 5 738	0.7316	9.7431	8'7130	0'5612 0'5499 0'5460	7.6646	0'0593 9"5597 9'5265
2387 2388 2389 2390	- 204 XII 20 - 203 V 17 - 203 VI 15 - 203 XI 9	1646 901 4 16.9 1647 049 0 6 8 1647 078 7 25.5 1647 225 10 11.6	265.759 51.269 79.165 223.924	+0'25 -2'05 -1'50 -3'30	23.724 23.723 23.723 23.723	11.048 164.143 193.662 346.065	183 628 11 338 165 866 194 448 343 867	0'7441 0'6978 0'6916 0'7275	9.7599 9.6999 9.7567 9.7633 9.7210	8.7064 8.7520 8.7584 8.7224	0'5350 0'5314 0'5638	7.6772 7.6625 7.6625	9n6316 0'0245 0'1323 0n0629 0n1072
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2412 2413 2414	192 IV 192 V	19 1650 887 15 1651 035 15 1651 065 9 1651 212 7 1651 241	5 15 6'5 5 47'5 9 28'8	21.584 49.909	-0.30 -2.00 -2.70	23.725 23.725 23.725		346:669 17:474 166:283	0'7090 0'7425 0'7360 0'6890 0'6909	9.7417 9.7042 9.7128 9.7638	8.7071 8.7136 8.7608	0.5517 0.5659 0.5596 0.5376 0.5401	7.6646 7.6626 7.6746	9"9375 0"1303 0'1678 0'0697 0"1719
2417 2418 2419	- 191 IX - 190 III - 190 IX	4 1551 389 29 1651 567 24 1651 743 18 1651 921 14 1652 098	0 51'0 10 50'4 10 51'0	182'148	+1.82	23.725	174.100 1.763 182.262	184 576	0.2341	9.7264	8.7481 8.7251 8.7245	0.5441 0.5584 0.5584	7.6669 7.6721	9#7844 9*7105 9*2100 9#3189 9*9481
2422 2423 2424	- 188 VII	7 1652 275 2 1652 423 27 1652 599 22 1652 778 17 1652 954	3 51.4 3 51.4 3 51.4	310,000	+4.27 +0.56 +3.78	23.726 23.725 23.724	347.647	165.320 328.113	0.6916 0.7349 0.7096	9.7616 9.7416	8 · 7582 8 · 7147 8 · 7398	0.5381	7.6734 7.6656 7.6746	9,,9823 0,,0199 0,0835 9,5763 9,6070
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	– 184 XI – 183 V	9 1654 16	4 14.7 3 1 58.7	224 067	-3.30	23.721	353.894	351.764 181.686	0.7026	9.7492	8.7285 8.7473 8.7098	0.5495	7.6625	9.8610 9.7273 8.6035
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2572 2573 2574	- 126 - 125 - 125 - 124 - 124	LH	1675 1675 1675	486 663 841	23 8:	2'3 23'4 2'5	2' 172' 352'	378 469 033	+1.59 -1.35 +2.58	23.212	181'409 0'478 180'886	353'161 182'252 358'775 192'207 6'103	0.2080 0.2322 0.6018	9'7000 9'7626 9'7114 9'7439 9'7381		0.5340 0.5662 0.5452	7.6658 7.6722 7.6681	9n0805 8.6548 9n9416
2577 2578 2579	123 122	VII 29 VIII 28 I 23	1676	342 372 520	20 ; 5 6	37·8 2·4 0·3	151.	479 075 622	+0.61 +0.05 +3.84	23.713	346.543 16.851	168 · 244 346 · 372 15 · 577 173 · 622 356 · 935	0.6900 0.6938	9'7057 9'7643 9'7600 9'7015 9'7558	8 7 7 1 0 2 8 7 5 0 1 8 7 5 6 4 8 7 0 7 0 8 7 5 1 5	0'5326 0'5369 0'5734	7.6657 7.6693 7.6745	9'7374
2582 2583 2584	- 121 - 121 - 120 - 120 - 120	VII o	1677	052 228 406	2 : 17 : 8	12.8 12.8	278. 278.	035 348 514	-0.13 -0.14	23.713	3.767 189.708	179'601 6'192 187'467 13'490 166'393	0.7203	9.7314 9.7472	8.7292 8.7451 8.7099	0.5498	7.6637 7.6630	9.5358 919292 0.0608
2587 2588 2589	120 119 119 118 118	V X 3:	1677 1677 1678 1678	730 908 085 262	18 11 0 2 19 4	3'9 7'7 28'5 45'7	52° 226° 42° 215°	633 601 165 530	-2.00 -3.25 -1.68 -3.44	23.715 23.715 23.716	350.282 173.597 358.737 181.453	197.068 348.818 175.892 356.300 183.579	0.7389 0.7056	9.7458	8.7109 8.7438 8.7309	0.5618 0.5492 0.5482	7.6771 7.6626 7.6771 7.6630 7.6765	0n 1685 9n 9642 9 '7509 9n 0596 9n 1312
2592 2593 2594	- 117 - 117 - 116 - 116 - 116	X 20 III 10 IV 15	1678 1678 1678	616 764 794	21 : 22 : 6 :	21 · 3 42 · 8 50 · 4	204' 353' 21'	198 425 842	-3.22 +2.46 -0.30	23.716	188 850 345 976 16 084	5.757 189.406 347.389 16.430 162.672	0.7435 0.6946 0.6902	9 7006 9 7592 9 7641	8.7065 8.7548	0'5366 0'5320	7.6756 7.6679	9n9284 0n0770 0'1309
	- 114	VIII 29	1679 1679 1679	295 473	13 : 18 :	13 4 29 9 45 6	342° 152° 332°	968 474 158	+3 · 33 -0 · 04 +3 · 99	23.716 23.716 23.715	354 411 172 983 2 517	194.744 356.828 170.706 4.103 180.693	0.7152 0.7067 0.7367	9'7363 9'7456	8.7425 8.7128	0'5503 0'5450 0'5661	7.6693 7.6696 7.6708	9,7016 9,7016 9,3771

Nr.	μ.	<b>y</b>	$\log n$	G	K	$\log \sin g$	log sin k	$\log \cos g$	$\log \cos k$	log sin ð'	log cosð′	N'	bei ⊙Δ gan λ	Auf- g φ	entrali im Mitta \(\lambda\)   6	ug U	bei ⊙ nterga λ	ng p	F
2552 2553 2554	135 ° 02 15 ° 13 242 ° 88	+1'4097 -1'5407 -0'4602 -1'5759	9'7192 9'7399	159.70 181.32	95°37 89°59 95°44	9'6811 9'6894 9'6835	9'9527 9'9407 9'9523	9'9431 9'9407 9'9425	9n6456 9n6893 9.6479	9°2707 8n 1106 9n2737	9'9923 0'0000 9'9922	63.1 110.3 119.4	— + 37	_ _ _ _ 53 + 57		- 42 54 +	   165 +		p p p r-t t*
2557 2558 2559	129'68 347'50 23'05	+0.2756 -0.1696 -0.9950 -0.8944 -1.2720	9.7648 9.7622 9.7624	143'04 321'99 133'93	96.91 96.91	9.6683 9.6675 9.6567	9.9802 9.9719 9.9708	9'9469 9'9471 9'9500	9n5501 9'5424 9n4705	9.4797 9.4882 9.5368	9 ' 9793 9 ' 9784 9 ' 9726	108.3 68.2	+162 - 44 - 82	+ 58	-131 +	_7	- 76  - - 33)(-	30 -66)	r* t* t* t* t
2562 2563 2564 2565	282·51 143·00 150·08 152·41	+0'9730 -0'5310 +0'2199 +0'1464 0'5459	9'7547 9'7069 9'7658 9'7071	270.69 85.06 259.03 73.19	90°10 89°27 88°48 87°84	9'5944 9'5845 9'5750 9'5649	9.3931 9.3931 9.3931	9.9636 9.9636 9.9685	5 7 · 6368 8 · 4854 8 · 8226 8 · 9972	9n5944 9 5831 9n5681 9 5485	9.9636 9.9681 9.9681	89'7 88'1 94'1 83'9	- 4 +152 +150 +158	- 29 + 10 + 12 - 36	-143 -150 -151	55 H 35 H 13 H	- 159 - 76 - 87 - 97	- 29 - 13 - 4 - 25	t t* r
2567 2568 2569 2570	58.62 217.51 295.42 271.27	+0.8285 +1.3920 -1.2800 -1.3390 +0.6053	9.7416 9.7282 9.7150 9.7627	27.55 60.89 198.34 15.43	87 33 86 89 88 14 88 41	9.5096 9.5471 9.4977 9.4967	9.9819 9.9941 9.9799 9.9794	9 9 9 7 6 6 9 9 9 7 7 5 9 9 9 7 7 5	9 45 19 9 2 1 19 9 2 47 27 9 47 99	9:1933 9:4950 7:920160 8:9424	9.9940 9.9777 9.9976 9.9983	73.3	+ 18	_ _ + 20	+ 84 +	- 44	 -155	 _ - 55	p p t**
2572 2573 2574 2575	163.66 307.08 25.77 48.06	0.6702 0.1204 0.8742 0.8742 +-0.7618	9.7647 9.7136 9.7459 9.7402	2'93 170'67 350'24 157'41	89.69 91.03 92.22	9'4915 9'4955 9'4998	9.978	9 977	g, 490 1 g, 484 6 g, 488 2 g, 461	8 7219 4 8 7462 5 9 1036	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	72.	B — 9 D — 119 D — 137	+ 20	+ 53 +	- 6 - 79 -	113	- 15 - 43	$t^*$
2578 2578 2579 2589	131.66 252.02 267.86 21.99	+1.2305 -1.1345 +1.4257 +0.5462 0.4242	9.7663	145.02	92.93	9.2261	9,984	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	4 9n 104, 4 9n 420, 2 9 049 7 8n 791	9 9 5 5 7 0 7 9 5 5 7 0	9 973	5 105 83 7 93	6 — 1 + 37 8 — 80		+ 62	- 32	+ 33	27 7	i.
258: 258: 258: 258:	2 212 42 3 75 19 4 297 47 5 138 01	+0.3434 -0.8496 +1.1502 +1.2033	9.764	88.94 265.02 77.92 7.224.8	4 89 · 82 2 89 · 2 2 88 · 02 7 83 · 4	9.6579	9 999	7 9 9 9 6 2 7 9 9 9 6 9	3 8n 502 3 8n 502 1 8 8 9 4 17 9n 481	6 9 5 5 9 9 6 9 6 0 4 9 9 2 5 3 0	8 g · g62 2 g · g61 2 g · g73	6 92. 7 85. 5 108.	0 +178 1 — 8 —	- 50 -	- 76 - - -	- 82	+ 35	- <u>5</u> 3	$\begin{bmatrix} p \\ p \end{bmatrix}$
258 258 258 259	7 95 61 8 35 1 68 9 189 12 0 119 47	-0'920 -0'563 -0'114 -0'135	8 9 747 5 9 747 7 9 735 3 9 720	7 215 2 7 31 6 6 206 2	5 83 1 6 83 2 0 83 2 2 83 6	6 9 670 4 9 673 7 9 679	19.968 89.964 49.958	7 9 9 9 4 6 7 9 9 9 4 5 5 9 9 4 5	3 9 5 5 8 7 3 6 9 n 6 2 0	7 9 465 7 9 43 1 90 9 1 3 68	8 9 98 9 4 9 98 3 8 9 98 7	6 112 6 66 8 115	5 - 36 3 +117 4 -177	- 29 + 17 + 17	+172 $-121$ $+173$	+ 8 - 22	122 49	— 32	r-t*   r-t*   r-t*   r-t*
259 259 259 259	2 141 03 3 161 24 4 279 60 5 249 21	+1.406 +1.321 +1.164	0 9 · 76 x 7 9 · 76 x 7 9 · 720	8 197 5 2 355 2 0 15 9 4 167 8	7 91 4 7 85 5 0 93 5	7 9 · 688 3 9 · 683 8 9 · 685	3 9 '941 0 9 '948 4 9 '945	5 9 94 5 9 94 6 9 94	13 0 68	53 8n 663 10 9 175 25 9 065	33 9 · 999 51 9 · 995 57 9 · 995	5 60 1 62 0 118	9 — 3 — 3 — 8 —		8 + 6				
259 259	7 1'39 8 24'13	0 -1 · 5 · 3 0 -0 · 5 · 3 0 +0 · 6 · 18 2 +0 · 2 · 38 8 -0 · 1 · 18	0 9 738 7 9 747	7 159 8	6 95 3	8 9 682	7 9 95	23 9 94	28 9n 64	779.26	93 9 99	24 116 22 63	0 -11	1 - 1	3 — 16 3 —100	+ 55	+ 47	+ 1	1 t#

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2602 2603 2604	1	113 112 112	VIII I VI :	8 3 28	1680 1680 1680	004 152 329	2 I 4 23	29'4 26'0 52'9	279 93	807 902 174	+1 +0	66 93 64	23.7 23.7	14	189.817 345.926 168.542	9°762 191°259 343°527 170°805 351°954	0'6945	9.7595 9.7281 9.7240	8.7059 8.7550 8.7281 8.7226 8.7512	o 5357 o 5589 o 5537	7.6722 7;6667 7.6764 7.6631 7.6770	9n9242 0n1053
2607 2608 2609		111 110	VI XII VI XII XII IV	7	1681 1681	861 038 215	6 4 21	48 · 4 50 · 8 34 · 5 54 · 1 54 · 5	258 · 71 · 247 ·	930	-1 -1	71 75 89	23'7 23'7	11	1.717 184.782 9.560	177.636 1.827 183.685 11.591 161.119	o'68go o'741g	9.7636 9.7637	8.7613 8.7613 8.7493	0.2636		0,0103
2611 2612 2613 2614 2615	_ _ _	109 108 108 107	X : IV : X : IV	22 16 10 6	1682	540 717 894 072	15 13 15 6	40'8 34'6 50'0	206 23 194 13	142 685 001	-3 -0 -2 +0	30 42 81 53	23.7 23.7 23.7 23.7	10	345.487 172.200 352.788	190'764 347'276 171'005 352'800	0'7353 0'6932 0'7447	9.4114 9.4114 9.6994	8.7260 8.7150 8.7568 8.7062 8.7578	0.5683 0.5334 0.5743	7.6747	
2617 2618 2619	-	106 106 105	IX : III : IX : VIII :	26 18 14	1682 1682 1682	426 602 751	21 23 14	42·8 19·7 0·5	172	712 484 850	+1 -1 +4	55 35	23.7 23.7	709 709	189·297 8·154 166·681	358·388 191·651 5·756 167·816	0'7104	9.7425 9.7394 9.7050	8.7153 8.7397 8.7376 8.7094 8.7603	0.5452 0.5501 0.5699	7.6668 7.6722 7.6719	8.2126 9n9168 9.8619 0.1015 0n0750
2622 2623 2624	1 1	104 104 103	VII :	3 29 22	1683 1683 1683	105 282 459	13 21 16	42'0 0'6 14'6	311	618 884 435	+4 +0 +3	· 30 · 64 · 82	23.7	710 710 710	354:384	173°254 356°309 179°387	0.7430 0.6993 0.7270	9.7022 9.7546 9.7218	8 7574 8 7073 8 7504 8 7229 8 7280	0.5723 0.5615	7.6657	9.7562 9n6878
2626 2627 2628 2629 2630	_	102 102 101	VII XII I	8 3 1	1684	991 139 168	14 5 16	34'5 46'6	248 278	960 692 717	+1 -1 -0	· 12 · 74 · 81	23.7 23.7 23.7	712 712 712	11.28 165.69 197.57	187 420 12 528 166 488 197 123 347 812	0.7408 0.6902 0.6893	9.7068 9.7622 9.7635	8.7464 8.7092 8.7599 8.7608 8.7119	o 5639 o 5388	7.6637 7.6777 7.6765	0'0301 0'0812 0%1672
2631 2632 2633 2634 2635		101 100 100 99 99	XI :	17 11 6	1684 1684 1684 1685 1685	670 848 024	7 4 21	2.2 31.5 18.1	52 225 42	604 696 428	x x	·99 ·26 ·67	23 7	712 712 713	357.88 181.38 6.63	355 449	0.7170	9 7354 9 7170 9 7584	8.7323 8.7533	o:5469	7.6626 7.6771 7.6630	9.7565
2636 2637 2638 2639 2640		98 98 97	IV : IX : X : III :	26 20 20 17	1685 1685 1685	379 526 556 704	14 12 4 19	3'0 51'3 54'2	32 174 203 353	366 070 897 703	-1 -1 -3 +2	· 11 · 47 · 20 · 43	23 . 7	713 713 713 713	15 29 164 36 195 91 353 87	346.894 15.79% 162.233 194.458 356.296	0.6904 0.7286 0.7382 0.7167	9.7639 9.7199 9.7075 9.7347	8.7206	0.5316 0.5614 0.5707	7.6637 7.6723 7.6756	0'1097
2641 2642 2643 2644 2645		96 96 95	IX III VIII : VIII :	6 29 23	1686 1686 1686	059 235 413	2 12 2	30 2 8 4 43 8 32 6 22 0	342 152 331	948 837 883	+3 -0 +4	.32 .00	23'	713 713 713	2 03 180 86 9 62	180.30	0 0 7377 0 0 6902 0 0 7443	9.7092 9.7008	8.7440 8.7119 8.7594 8.7058 8.7544	0.5657 0.5351	7.6693 7.6695 7.6708	9'2848 8n8670 9'9651
2646 2647 2648 2649 2650		94 93 93	VII VII VI 2 XII 2	3	1686 1687 1687	915 092 269	6 0 10	47'1 16'3 15'2	103° 280°	638 121 020	-o +r -o	'04 '95 '65	23 7	712 711 710	167.71 353.80 175.90	343'39! 169'92! 351'96! 176'62;	0.7284 0.6073	9.7223 9.7549 9.7033	8.7213 8.7521 8.7064		7.6764 7.6631	0'0542 9n7284 9'5956
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Nr.	μ.	γ	$\log n$	G	K	log sin g	$\log \sin k$	$\log \cos g$	log cos k	log sin δ΄	log cos &	$N^{'}$	bei ⊙Aufgang λ   φ	λ   σ	g bei ① Untergang γ λ φ d e	$F_{-}$
2602 2603	247 97	+0.9625 -0.8398 -1.2743 +1.0546	9.7301	293 55	03.81	9.6293	9.9946	9 · 9565	9.1938	9×5979	9.9629 9.9629	80°2		-148 -	$ \begin{array}{c cccc}  & & & & & & & & & & & & & & & & & & &$	$\left egin{array}{c} t \ p \ p \end{array} ight $
2607 2608 2609	283 ° 05 249 ° 02 148 ° 29	+0.307 +0.145 2 -0.457 +0.830 1 +1.453	7 9 7057 8 9 7079 4 9 7533	84'72 259'18	2 89 23	9 595	9 9997	9 9654	8 5135	9.5825 9.5694	9.9657	89°5 88°0 94°1	+ 16 + + 59 - 2 +169 + 5	7 + 77 -	41 -171 + 1 15 +138 + 5 +165 - 2 35 - 98 + 4	3 r* 7 t* 7
2612 2613 2614 2615	56.3 27.3 58.5 281.8	1 —1:197 7 —1:355 0 —0:666 0 —0:663	7 9 · 7 6 3 5 9 9 · 7 6 3 5 8 9 · 7 6 4 5	28.3 198.1	2 87 33 7 88 19 0 88 3	9 506 9 506 9 4945 9 495	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	9 · 976 2 9 · 977 5 9 · 977	9 445 7 92470 5 9 476	5 9 · 198 0 92 0 0 8 5 8 · 95 6	9 9945 4 9 9977 5 9 9985	73.6	-102 + 2 -130 - 2 + 16 - 2	7 - 65 -	53 + 58 + 5	4 t*
2617 2618 2619 2620	7 141'9 3 169'3 29'4 249'3	7 -0.825 1 -0.727 9 -1.188	7 9 744 7 9 741 3 9 707 5 9 766	170'7 1315'0 124'0	3 90.3	7 9 '492' 8 9 '523' 3 9 '540	5 9 · 9 7 8 5 9 · 9 8 8 9 9 · 9 9 2	7 9 · 9 7 8 3 9 · 9 7 4 3 9 · 9 7 2	0 92486 3 9 359 1 92269	28.721 89n385 69.467	0 9 999 4 9 986 7 9 980	2 76.	3	54 -103	- 59 - 68 - 3 - 53 - 96 - 3	38 t
2623 2623 2623 2623	2 22.8 3 135.7 4 59.4 5 318.8	5 +1 · 387 9 +0 · 570 7 -0 · 487 0 -0 · 151 +0 · 278	9 756 2 9 724 3 9 73 1	8 100,3 0 588.0 4 301.0	9 92 6	4 9 557 7 9 561 5 9 576	4 9 · 9 9 6 3 9 · 9 9 7 1 9 · 9 9 9	5 9 969 3 9 969 1 9 966	7 9n 104 1 9 * 046 8 8n 799	4 9 528 7 9 549 6 9 569	6 9 973 9 9 967	7 97 2 83 8 93	8 +165 - 2 -127 - 9 - 30 +	20 -138 -	- 18 + 25 + - 10 - 83 - - 29 + 3 - + 38 + 109 +	43 7 t 43 7 t 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
262 262 262 263	7 35 6 8 271 4 9 66 6 0 193 8	7 -0 · 839 7 -1 · 209 6 -1 · 469 81 -1 · 604	17 9 7 7 6 4 97 9 7 7 6 5 1,0 9 7 7 6 5	2 235 2 4 265 9 8 49 7	84.4 489.3 7883.8	3 9 · 645 6 9 · 660 6 9 · 652	0 9 987 3 9 999 4 9 983	8 9 · 952 8 9 · 962 4 9 · 951	9 9n 368 4 8n 413 (1 9 ' 432	35 9n 573 31 9n 599 27 9 ' 554	9'967 94 9'962 14 9'979	5 89° 2 104° 6 91° 2 73°	6	67)		P P P P P P P P P P P P P P P P P P P
263 263 263 263	2 295 3 3 243 5 4 139 5 5 259 8	30 —0.13 75 +0.24 86 —0.83	9 9 7 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	2 215 2 5 31 8 3 206 0	26 83 ° 6 36 83 ° 2 34 83 ° 6	9 9 · 67 9 4 9 · 67 9 5 9 9 · 67 9	6 9 96 30 9 96 95 9 95	38 9 945 31 9 945 33 9 945	52 9 2 56 55 9 58 36 9 2 62	32 91146 55 9 43 09 91136	54 9 986 35 9 98 63 9 98	6 112 34 66 79 115	15 + 59 + 14 + 149 + 14 + 19 -	11 -145	+ 54 - 47 +	20 /
263 263 263 264	37 35 38 6 39 251		73 9 705 50 9 72 30 9 70 9 73	9 24 9 175 6 197 58 355	72 91 . 40 85 . 50 91 .	32 9 · 68 16 9 · 68 41 9 · 69	74 9 94 41 9 94 03 9 94	97 9 94 97 9 94 99 9 94	12 9n 68 23 9n 65 04 9 68	58 8 · 61 80 9n21 86 8n64	86 9 99 19 9 99 45 9 99	96 119 42 117 96 60	· 5	63 -109	- 42 - 51 - + 55 - 74 -	
264 264 264 264	12 208 · 13 10 · 14 211 · 15 258 ·	23 +0.19 81 -0.07 41 +0.92 -0.79	26 9 71 36 9 76 28 9 76 00 9 76	14 347 30 339 1 35 152 1	02 0g. 20 02. 18 02.	34 9 · 68 49 9 · 68 44 9 · 67	35 9 95 37 9 95 61 9 96	18 9 94 24 9 94 08 9 94	24 9n64 25 9 64 47 9n66	95 9 26 74 9 <i>n</i> 27 88 9 38	388 9 99 776 9 99 888 9 98	25 117 21 63 66 112	- 80 + 79 + 35 -	· 22 - 12 · 40 -	+ 55 - 74 + + 6 - 152 + + 6 + 47 - - (+115)(- - 46 + 129 -	31 7 -78) 1
26. 26.	47 284 48 183		30 9 72 50 9 75	44 117° 70 294°	55 94 °	50 9 03 01 9 63 85 0 62	04 9 99	44 9 9 5	553 9 20 563 9 20	040 9n 5	976 9 9 038 9 9	30 8 518 9			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	- 20 - 15

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2652 2653 2654	- 92 XII 12 - 91 V 8 - 91 VI 6	1687 623 11 ^h 2 ^m 687 801 6 43 6 1687 948 6 8 2 1687 977 16 22 2 6	258 514 43 804 71 835	-0.68 -1.74 -1.75	23'709 23'708	9.267 162.210	11.645 160.331	0.7411 0.7018 0.7104 0.7224 0.7362	9.7065 9.7499 9.7431 9.7298 9.7103	8·7481 8·7391 8·7275	0:5469	7.6626 7.6775 7.6630 7.6623 7.6766	9n5684 9'9203 0'1816 0n0472 0n1362
2657 2658 2659	- 90 X 21 - 89 IV 17 - 89 X 11 - 88 IV 6	1688 302 21 16 6 1688 479 23 22 6 1688 657 14 32 2 1688 834 0 3 6 1689 012 5 14 2	205'753 23'567 194'429 13'323	-3:30 -0:44 -2:80 +0:51	23.707 23.707 23.707 23.707	352.603 180.020 359.944 188.635	170.364 352.497 181.128 358.080 191.018	o.6925 o.7446 o.6933 o.7337 o.7118	9.7137	8·7575 8·7052 8·7569 8·7164 8·7381	0.5751 0.5336 0.5664	7.6646	9.8641 9n8521 7n2341 7n7216 9n8861
2662 2663 2664 2665	- 87 II 24 - 87 VIII 20 - 87 IX 18 - 86 II 13	1689 188 7 31 6 1689 336 21 26 2 1689 513 12 27 3 1689 542 21 30 7 1689 690 21 13 7	333'703 143'819 172'802 322'546	+3.92 +0.38 -1.37 +4.32	23 · 707 23 · 707 23 · 707 23 · 707	166.267 345.306 16.043 173.716	345'416 14'990 172'812	0.7110 0.7418 0.6898 0.6923 0.7427	9.7408 9.7045 9.7644 9.7613 9.7029	8.7390 8.7086 8.7605 8.7579 8.7078		7.6735 7.6707 7.6682 7.6721 7.6720	0'1152 010920
2667 2668 2669 2670	- 85 VII 30 - 84 I 23 - 84 VII 18	1690 045 0 16 4 1690 222 16 30 7 1690 399 10 26 3 1690 576 21 14 3	300 582	+4.28 +0.63 +3.83 +0.38	23 707 23 707 23 708 23 708	181 407 2 261 189 467 10 466	355 · 748 179 · 117 4 · 642 187 · 322 11 · 614	0.7260 0.7233 0.7023	9.7532 9.7236 9.7279 9.7499 9.7057	8·7494 8·7240 8·7264 8·7474 8·7087	0.2239	7.6668 7.6734 7.6656 7.6746 7.6647	9n7362 9n1140 9'3173 9n9163 9'9986
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	,	Julia Kal	nisch ender		Juli Ta			Velt- Zeit					1	Q	$\log p$	$egin{array}{c} \log \ \Delta L \end{array}$	$\log q$	u'a	$\log f_a$	logγ
2751 2752 2753 2754 2755	_	51 51 51 50	IX X	11	1702	684	4	46.8	165	433 812	-0.82	23 702	344 373	166° o11 197' 253 344' 742 14' 714 171' 701	0.2367	9.7121	8 7136 8 7607	0.2612	7.6746	0'1482 0n1638 0n1180 0'1172 9'8366
2756 2757 2758 2759 2760		49 49 48	VIII VIII VIII	24 21 14 9	1703 1703 1703 1703	215 393 579 747	7 3 10	59°0 9°8 10°2 49°0	333° 144° 133°	270 382 574 569	-0'17 +3'95 +0'36 +4'32 +0'64	23.405 23.405 23.405 23.405	180,730 1,007 188,963 9,004	9 943	0'7235 0'7261 0'7002 0'7427	9 7269 9 7244 9 7525 9 7038	8 · 7473 8 · 7264 8 · 7240 8 · 7495 8 · 7077	0.5563	7.6707	9n8074 8n8265 8 9688 9n8906 9 9351
276x 2762 2763 2764 2765 2765		40	VI	29 24 19	1704 1704 1704	924 071 249 426	20 21 4	25 6 58 6 44 3	94° 271° 83°	257 454 862	-0.55 +0.88 -1.16	23.403 23.403 23.404	197'098 346'693 173'537 355'256		0.4893 0.4120 0.4120	9.7640 9.7444 9.7403 9.7406	8'7584 8'7609 8'7151 8'7389 8'7371		7.6734	o.0859 on1557 on0950 9.7599 gn6281
2767 2768 2769 2770		45 45 44 44	VI XII IV V	8 3 29 28	1704 1704 1704 1705 1705	780 958 106 135	19 5 5 12	23.6 26.3 59.9	248 35 63	744 834 773 734	-1.31 -1.4	23.705 23.706 23.706 23.706	4'028 188'486 343'154 12'732	188'599 345'003 13'683	o'6933 o'7443 o'6990 o'6920	9'7130 9'7612 9'6994 9'7551 9'7626	8 · 7561 8 · 7565	0.5685 0.5324 0.5764 0.5365 0.5318	7'6623	9n0813 9'5378 9n9111 0n1591 0'0332
2772 2773 2774 2775 2776		44 44 43 43 42	IV X IV	18 11 7	1705 1705 1705 1705	312 460 636 814	5 17 22 23	16.4 27.4 16.4	237 25 196 14	352 499 207 886	-0.24 -2.30 -10.39	23.706 23.706 23.706	195'638 351'831 171'690 0'104		0.7358 0.7213 0.7014 0.7405	9.7105	8 · 7244 8 · 7140 8 · 7279 8 · 7479 8 · 7092	0.5700 0.5511 0.5452	7.6775 7.6644 7.6748	0 1715 0n1643 9n8718 9 8592 7 9972
2777 2778 2779 2780 2780	Marina Marina Marina Marina	41 41 40 40	IX	27 21 15 16	1706 1706 1706 1706	168 346 493 523	23 5 13 2	44 · 6 43 · 4 15 · 2 39 · 4	324 °C 353 °C	022 086 052 192	1.55 +4.27 +2.47	23'706 23'706 23'706 23'706	7.897 187.892 345.110 15.856	, · · · · ·	0'7435 0'5975 0'7161 0'7284	9.7026 9.7550 9.7349 9.7213	8.7606 8.7065 8.7517 8.7329 8.7209	0.5679 0.5412 0.5526 0.5580	7.6680	8.3001 9.8792 9.8331 0.1240 0.1629
2782 2783 2784 2785		39 39 38	VII	4 31 24	1706 1707	848 025 202	6 18	4 · 1 8 · 9	313.3	184 7 <b>5</b> 9	+4.29 +0.65 +3.92	23.706 23.705 23.705	353 310 173 450 1 365		o 6948 o 7445 o 6899	9.7579 9.7630 9.7630	8.7290	0.5545 0.5400 0.5680	7.6708 7.6733 7.6658	0.1278 011625 917590 9.7995 9.0648
2787 2788 2789 2790	Prince Prince Prince	37 37	VII XII V	9 4 29	1707 1707 1707 1708	557 733 881 058	13 23 19	26 · 8 58 · 3 45 · 6	250.7 65.0	535	-0.04 -1.28 -1.31	23.704 23.703 23.703 23.703	9'401 189'712 345'235 168'874	187 · 267 346 · 674 168 · 249	0.7052 0.7177 0.7386 0.6910	9.7465 9.7346 9.7071	8.7115 8.7444 8.7320 8.7115 8.7589	0.2420 0.2480 0.2721	7.6648 7.6756 7.6638 7.6776 7.6624	9'9162 9n9427 0n1428
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2816 2817 2818 2819 2820	- 2 - 2 - 2	6 VI 6 XI 6 XII 5 IV 5 X	2 30	1711 1711 1711 1712 1712	867 897 046	20 13 1	35'2	218 248 35	166 268 555 989 307	-1 -1	.46 .81	23'	703 703 703	351.033	12'946 161'284 193'816 353'399 169'552	0.7238 0.7348 0.7230	9'7253 9'7116 9'7285	8.7568 8.7256 8.7150 8.7265 8.7490	0'5321 0'5609 0'5694 0'5514 0'5452	7.6624 7.6766 7.6776 7.6636 7.6758	0'0032 0'1730 0n1624 9n9136 9'8657
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2872   73 ' 77   + 1 ' 3297   7268   10 ' 43   86 ' 87   56872   9 ' 9441   9 ' 9413   9 ' 6778   9 ' 1041   5   9788   61 ' 4	2867 2868 2869 2870	159.70 17.12 290.29	-0'1446 -0'6127 -0'6409	9'7072 9'7659 9'7547	26.47 200.22 18.23 192.38	83 · 64 84 · 58 84 · 94 86 · 37	9'6793 9'6853 9'6853 9'6869	9.9588 9.9522 9.9500 9.9453	9'9437 9'9426 9'9419 9'9414	9.6188 9.6480 9.6565 9.6738	9°3722 9°2322 9°2322 9°0701	9'9876 9'9923 9'9936 9'9970	64.7 116.9 62.6 118.4	63 +- 12 85 +-129	- 33 29 10	- 9 -+ 70 26	+ 4 - 7 + 53	+ 54 + 139 + 70	+ 17 - 24 + 63	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
2877 342 91 +0 0703 9 7644 333 95 96 28 9 6787 9 9585 9 9489 9 6202 9 33655 9 9880 64 6 - 52 - 21 + 16 - 9 + 74 + 29 # 2878 130 77 +0 0113 9 7739 146 02 96 88 9 6719 9 9673 9 9488 9 87572 9 74550 9 9816 112 9 +161 + 23 - 131 + 17 - 76 - 21 # 17 - 76 - 21 # 17 - 76 - 21 # 17 - 76 - 21 # 17 - 76 - 21 # 17 - 76 - 21 # 18	2872 2873 2874 2875	73.17 101.56 321.38 98.14	+1'3297 +1'4517 -1'4030 -0'6310	9.7268 9.7162 9.7620	10.43 163.05 184.45 341.93	86 · 87 94 · 73 88 · 63 94 · 98	9 6872 9 6842 9 6870 9 6837	9'9441 9'9493 9'9419 9'9502	9'9413 9'9423 9'9414 9'9423	9.6778 9.6594 9.6853 9.6555	9'0014 9'2010 8n6348 9n2267	9'9978 9'9945 9'9996 9'9937	61°4 117°5 119°0 62°7	+171	65			i	12	$egin{pmatrix} p \\ p \\ p \\ t \end{bmatrix}$
2882 344 34 + 1 · 0870 9 · 7665 99 · 16 9 · 48 9 · 6078 9 · 9992 9 · 9610 8 · 7716 9 · 6031 9 · 9619 93 · 7  2883 87 · 38 - 1 · 4263 9 · 7619 127 · 14 95 · 84 9 · 6473 9 · 9861 9 · 9524 9 · 3968 9 · 5651 9 · 9686 105 · 5  2884 55 · 88 - 0 · 7443 9 · 7031 275 · 17 90 · 82 9 · 6010 9 · 9997 9 · 9623 8 · 5183 9 · 5952 9 · 9626 87 · 9 - 152 - 45 - 55 - 72 + 37 - 41 17 2885 240 · 14 + 0 · 3607 9 · 7589 88 · 79 89 · 82 9 · 5909 0 · 0000 9 · 9642 7 · 8791 9 · 5968 9 · 9642 89 · 5 + 46 + 19 + 120 + 44 - 166 + 20 t	2877 2878 2879 2880	342'91 130'77 199'06 237'45	+0.0403 +0.0113 -0.40113	9.7644 9.7139 9.7461 9.7398	333°95 146°02 325°24 136°84	96 28 96 88 96 84 96 72	9.6787 9.6719 9.6695 9.6608	9'9585 9'9673 9'9685 9'9773	9'9439 9'9458 9'9466 9'9489	9'6202 3 9n5722 5 9'5653 9n4984	9n3655 9'4556 9n4601 9'5216	9.9886 9.9816 9.9812	64 · 6 112 · 9 67 · 4 109 · 5	52 +161 97 61	- 21 + 23 + 29	+ 16 131 +152	+ 17 + 43	+ 74 - 76 - 173	+ 29 - 21 + 68	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
2887 77 31 -0 4181 9 7350 77 54 88 30 9 5728 9 9988 9 9673 8 8756 9 5638 9 9687 85 4 -131 - 27 - 76 - 3 - 20 - 19 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2882 2883 2884 2885	344'34 87'38 55'88 240'14	+1.0870 -1.4263 -0.7443 -0.3607	9.7665 9.7619 9.7589	99'16 127'14 275'17 88'79	91'48 95'84 90'82 89'82	9.6078 9.6473 9.6010	9'9992 9'9861 9'9997	9'9616 9'9524 9'9623 9'9642	8n7716 9n3968 8.5185 7.879	5 9 · 5031 3 9 · 5651 3 9 · 5995 1 9 · 5908	9.9619 9.9686 9.9646	93 7 5 105 5 87 9 89 5		45 -+ 1g	120	72 + 44	166	+ 20	o l#
2892 315 14 +0 8634 9 7103 19 80 88 02 9 4977 9 9804 9 9774 9 4685 9 0475 9 9973 72 8 - 36 + 42 + 37 + 71 + 146 + 75 7 2893 138 27 -0 7368 9 7480 189 50 89 01 9 4925 9 9787 9 9780 9 4859 8 7313 9 9994 107 9 + 148 - 30 - 145 - 54 - 60 - 65 7 2894 38 65 +0 0783 9 7344 6 75 89 29 9 4911 9 9784 9 9781 9 4878 8 5830 9 9997 72 1 + 101 - 13 - 39 + 7 + 25 + 22 7 -	2887 2888 2889 2890	77'31 216'69 168'07 280'45	-0.4181 -0.6471 -1.3803	9'7359 9'7493 9'7106 9'7649	77'54 250'30 65'67 202'35	88.30 87.18 87.18	9 5728 9 5605 9 5543 9 5034	9.9988 9.9971 9.9957 9.9806	9.9673 9.9768 9.9768	3 8 8 8 7 5 6 2 9 n o 6 o 6 3 9 1 4 4 1 3 9 n 4 6 5 9	5 9 5 6 3 8 5 9 n 5 3 7 6 1 9 5 1 8 7 9 9 n 1 0 3 2	3 9 · 968; 5 9 · 972; 7 9 · 974; 2 9 · 996;	85'x 97'0 81'5 107'1	+ 94 5 —	+ 44	76	3	20	то	5
	2892 2893 2894 2895	315°14 138°27 38°65 271°70	+0.8634 -0.0296 +0.0296	9 7 7 1 0 3 9 7 7 4 8 0 9 7 7 3 4 4 9 7 7 2 1 4	19.86 189.56 6.75 176.08	88.02 89.02 89.29 90.4	9 4977 9 4925 9 4917 9 4895	9 9 9 8 0 4 9 9 9 7 8 7 9 9 7 8 4 9 9 7 8 4	9'9776 9'978 9'978 9'978	4 9 468 9 485 1 9 487 3 9 488	9 0473 9 8n731 8 8 5830 4 8 3460	9 9973 9 9994 9 9993 9 9999	72.8	36 36 3 +148 4 101 5 + 26	- 15 15	- 145 3 - 39 5 + 88	+ 5	1 — 60 7 — 25 7 — 149	- 65 + 25 - 26	5 t 2 r-t ¹⁴ 9 r ³¹
2897 300·77 +0·7053 9·7055 162·39 9·7060 34943 9·980 1 9·9778 9·4748 8·9952 9·9979 107·3 — 20 + 62 + 66 + 53 + 131 + 27 1 2898 334·57 +1·2677 9·766 341·40 91·92 9·5015 9·9796 9·9769 9·4757 9·0257 9·9975 72·5 — — — — — — — — — — — — — — — — — — —	2897 2898 2899	300'77 334'57 111'53	+0'7053 +1'2677 -1'3420	9.766	306'7'	91'7' 93'3! 91'9:	9 494; 9 9 536; 2 9 501	9 9 9 8 0 1 3 9 9 9 1 4 5 9 9 7 9 6	9'977 9'972 9'976	8 9n 471 7 9 295 9 9 475	4 8 · 995 6 9n449 7 9n025	9 9 9 7 9 4 9 9 8 2 3 7 9 9 9 7 3	78.	3 — 20 1 — 5 —		11 :		11 .	١.	474

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2906 2907 2908 2909 2910	10	VI XI XII V	4 30 24 24 21	1724 1724 1725 1725 1725	891 038 068	11 13 6	20.2 30.2 6.3	95° 240° 270°	062 646 943	+2:16 -0:45 -2:52 +0:78 -1:96	23.698 23.698 23.698	188.255 10.130 163.507 195.521 349.322	11,497 161,139 193,586	0'7444 0'5943 0'7213 0'7328 0'7259	9.6997 9.7603 9.7281 9.7141 9.7251	8.7060 8.7554 8.7283 8.7168 8.7236	o·5756 o·5333 o·5598 o·5675 o·5528	7.6764 7.6631 7.6775 7.6770 7.6626	9n8993 9'9375 0'1725 0n1582 9n9916
2911 2912 2913 2914 2915	11 12 12 13	XI V XI IV X	14 9 2 28 23	1725 1725 1725 1725 1726	570 747 924	19 15	9'6 56'0 49'4	46°	319 859 602	-1'27	23.699 23.699	171.406 357.614 179.297 5.562 187.245	358.510 179.463 4.518	0.6983 0.7427 0.6888 0.7418	9.7536 9.7044 9.7637 9.7049 9.7514	8.7513 8.7073 8.7609 8.7078 8.7488	0.5446 0.5647 0.5386 0.5648 0.5452	7.6630 7.6766 7.6636	9.8706 9.3599 8.7756 9.7260 9.7990
2916 2917 2918 2919 2920	14 14 14 15	III IX X III	19 18 13 12	1726 1726 1726 1726 1726	279 427 456	0 1 17	37.0	24' 167'	995 542 183	+2:20 -0:50 -1:01 -2:97 +3:10	23.699 23.699	163.937 195.254	11'454 165'752	0'7122 0'7246 0'7351 0'7240 0'6927	9.7401 9.7264 9.7126 9.7253 9.7606	8.7370 8.7248 8.7145 8.7252 8.7566	0.5472 0.5531 0.5649 0.5597 0.5365	7.6645	0n1582 0'1002 0'1751 0n1421 9n8261
2921 2922 2923 2924 2925	17	IX II VIII II VIII	2 26 21 15 10	1726 1726 1727 1727 1727	958 135 313	19 3 9	27°4 55°3 54°1	335° 145° 325°	631 489 087	-0'26 +3'80 +0'31 +4'24 +0'63	23.699 23.699	0°437	177'492	0.7445 0.6914 0.7352 0.7092 0.7129	9.7007 9.7619 9.7128 9.7427 9.7393	8.7055 8.7581 8.7144 8.7401 8.7365		7.6705 7.6683 7.6719	9'9092 8'5717 8'8424 9'8875 9n8296
2926 2927 2928 2929 2930	81 81 81 81 81	II VII VII XII	6 4 1 31 25	1727 1727 1727 1727 1727	667 814 844	18 18 1	1.6 14.3 46.7	314° 96° 124°	208 364 520		23.697 23.697	345°029 16°769 166°281 196°110 352°163	166.112	0.7322 0.6901 0.6935	9'7045 9'7154 9'7646 9'7607 9'7016	8.7095 8.7173 8.7596 8.7561 8.7075		7.6733 7.6632 7.6657	0n 1507 0'1903 0'0632 0n 1348 9n 8754
2931 2932 2933 2934 2935	19 19 20 20 21	VI VI XII XII V	15	1728 1728	346 524 700	n i O I	46·3 3·7	261°. 76° 250°.	402 112 324	-0'99 -0'41 -1'52 -1'66 -1'87	23.695 23.695 23.694	359°545 183°721 7°380	176.793 357.301 186.116 5.191 193.420	0.7210	9'7556 9'7212 9'7311 9'7483 9'7077	8 · 7227 8 · 7287		7.6774 7.6624 7.6776	8n6247 9n5311
2936 2937 2938 2939 2940	21 21 22 22 22	X XI IV X IV	23	1729 1729 1729 1729 1729	055 202 380	1 15 5	10.0 30.0 21.0	239° 26° 198°	473 638 743	-2.63 -0.64 -3.06	23'694 23'693 23'693	15 240 170 135 351 429	168.617	0.6905 0.6894 0.7387 0.7072 0.7182	9'7624 9'7635 9'7095 9'7447 9'7341	8.7598 8.7610 8.7117 8.7427 8.7318	0'5393 0'5628 0'5485	7.6644 7.6748	0'1071 9'9704 9n8784
2941 2942 2943 2944 2945	23 24 24 25 25	X III IX III III	21 16	1729 1730	911 088 236	11 15 18	12'3 33'0 45'2	5° 176° 326°	711 625 501	+1'30 -1'65 +4'18	23.693 23.693 23.693	6.953	185 352 7 451 166 269	0.7309 0.6965 0.7442 0.6953 0.6904	9.7176 9.7575 9.7688 9.7582 9.7639	8 · 7193 8 · 7534 8 · 7065 8 · 7550 8 · 7600	0.5368 0.5725 0.5392	7.6667 7.6724 7.6718	9n7820 9'8250
2946 2947 2948 2949 2950	25 26	VIII IX II VIII I		1730 1730	442 591 767	15 7 10	36'4 39'2 3'9	165' 315' 125'	462 830 876	-0.85 +4.31 +0.71	23 693 23 693 23 694	14'413 172'976 352'126	341 ' 583 13 ' 005 175 ' 413 349 ' 885 182 ' 369	0.7390 0.7164 0.7066	9'7079 9'7348 9'7466	8'7201 8'7114 8'7336 8'7432 8'7127	0.5533	7.6710 7.6732 7.6658	9n8412
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2002	160'14	+1.4040	9.7383	294'09	92.79	9'5533	9'9958	9.8463	9.1392	925184	9'9750	81.6	+133 + 23	7 -172 + 19 2 +139 - 18		
2004	250 138	-0.0399 -0.0399	9.7119	281'46	91.57	9 5733	9,9990	9.9673	8 . 8400	925657	9.9682	85.4	+ 36 - 9	+101 - 27 3 - 91 + 30	+162 - I	7***
2007	348'42	0'7930 -+0'8660	9.7623	81'77	88.67	9'6063	9'9994	9'9614	8 17244	9'6025	9,0621	86.7		+102 - 76 + 10 + 82		sate II
2908 2000	29°13	+1 4877 -1 4393 -0 9808	9.7300	227 93	83'68	g'6532 g'6131	9'9819	9'9599	9n4509 8n9166	9n 5445	0.0g14	95.5	(- 21) (-6g		+ 6 - 54	$\left[egin{array}{c} p \\ p \\ r \end{array} ight]$
2011	****	LO!7429	0.7557	27710/	83.13	0.6663	0'0710	9.0474	025418	024862	9.9786	xxx.5	+134 + 6	3 + ±75 + 3	5 -129 + 25	l ^{:‡:}
2913	62.62	+0.0206	9.7658	208'9	83'43	9.6762	9.0586	9 9440	0,0041 50 610	1914017 50 3602	9.9857	64 6	+176 + 2	71 124 5	32 + 55	t::
		6 0 · 6296								1	1		1	2 + 63 - 5	5 163 64	$\left  \begin{array}{c} \iota \\ v \end{array} \right $
2917	180'94	+1.4967 -1.3870	9.7285	18'23	85.00	9 6835 2 9 6876	9 ' 95°! 9 ' 9434	9 9424	19.6547 3.92680	7 9 · 2300 5 8 · 938	9 9930	118.8	3	50.100 AMOUNT		$\left  egin{array}{c} p \ p \ p \end{array} \right $
2920	220.86	-0.6200	9.7627	349'9	2 93 '04	9 6876	9 9439	99.941	9.678	7 81987	2 9 9979	01.3	53 - 7			3 t
2922	107'95		9 7640	342'2	9 94 9	3 9 6848	9 949	7 9 942	5 02624	19'357	4 0 : 0884	1115	6 + 53 + 2	9 +122 + 1	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	r it
0004	000100	*   .   .   .   M M Y S	2 0 17118	Y' KCC S	2 05 2	20'077	310'058	510 044	110'020	1192301	0,9 9002	4 04	29 1 2	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	S     SS     /	
2027	81.8	-1.4142 -1.5500	9'7174	4 325 'X	2 96 7	g 668	o g*g68	8 9 946	9 9 5 5 3	2   9n 459	0,0,091	4 07	5		AMERICAN PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE PARTICIPATION OF THE	$\begin{bmatrix} p \\ p \\ p \end{bmatrix}$
2020	1202 6	+1.1567 -1.3640 -0.7500	0'762'	7 136.8	1 06 6	5 0 650:	2 9 9 9 7 7	4 9 949	3.92490	719 520	0 9 9 7 4	3 109	4			p
2931	350.3:	+0'436	9.7577	7 99'9	4 91 6	2 9 · 608	б 9 ' 9 9 9 5 0 ' 9 0 0	1 9 960 7 9 962	8 8 8 8 9 7 4 8 9 4 9 9	9 9 603 2 9 599	29.961	94'	o 70 + 4 o + 8g	4 + 10 + 5 4 + 153 2	50 + 85 + 2 66 - 145	o t ⁱⁱ
2933	181'5	1	7 9 7 7 3 3	2 8g o	6 89 8 8 88 0	6 9 59 I	30.000	o g 'g64 6 g 'g66	x 7 7 7 6 8 o 8 n 6 4 6	3 9 59 1 4 9 1 5 7 8	o 9 966	5 92	7 - 38 + 3	, , ,	3 -125 - 1 18 + 66 + 3	
2036	87.8	-1.302	2 0 . 764	4 215 6	2 86 . 8	7 9 ' 5 1 5	3 9 984	5 9 975	3 92416	6 91296	59'991	3 105	4	- 11 - 1		$\frac{p}{p}$
2937 2938	58.0	2 + I · 279 B + O · 934	7 9 '765. 2 9 '711	5 250'2 5 32'5	1 87 ° 0	4 9 502 8 9 508	3 9 997 7 9 983	9 9 9 9 9 9 9	19'427	5 9 255	79'992	8 74'	2 -151 +	$\frac{52}{32} - \frac{66}{89} + \frac{8}{9} - \frac{6}{9}$		8 11th
2940	149.9	1,40,130	19'736	2 19.7	688.0	3 9 497	39.980	4 9 977	4 9 400	29 040	2 9 997	3 /-			6 + 32 - 2	
2942	345 2	2 -0 605	3 9 759	0 175 8	1 00'4	4 9 489	29.978	3 9 97 9	3 92487	98.374	0 9 9 9 9	9 107	9 123		6 + 32 - 2 $37 + 83 - 1$ $46 + 16 + 2$	gt
204/	פיססיו	2-1.300	2 0 750	2 310'5	7.03.3	0 0'5IQ	8 0.080	4 9 974	10 9 394	4 97 34	og gog	7.0	71 1	gaporo use gaporo	gay - Linearen	p
2947	51.0	4 -1 · 502	39'710	0 162'1	5 91 8	19'497	0.001	9 9 9 9 7 7	0 0 20	20 02 44	72 9 997	3 78	2 + 7 +	26 - 64 +	24 +117 +	$\begin{array}{c c} - & p \\ - & p \\ 48 & r^{4} \end{array}$
2046	122210	2 +0.028 4 -0.028	701718	7 TTE'S	4 02 0	0.01552	2 0 00	419 970	)5   gn 1 U:	4519 51	4/19 9/3	)/ 9º	5	55	26 + 75 - 42 +	
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2951 2952 2953 2954 2955	27 28 28 28 29	VII VII XII I	r 5	1731	122 299 476 623	18	50.7 3.5	115°658 293'454 105'550 251'858 282'100	+3'25 +0'12 -1'49	23 695	188·108 9'316 163·494	187.779 10.806 161.102	0'6911 0'7443 0'6951 0'7201	9'7634 9'7000 9'7593 9'7296 9'7154	8.7591 8.7063 8.7546 8.7294 8.7178	0.5748 0.5342 0.5589	7.6648 7.6755 7.6638 7.6776 7.6764	8.7858 9.8914 9.9023 0.1717 0.1552
2956 2957 2958 2959 2960	29 29 30 30 31	V XI V XI V	31 24 21 14 10	1731	156 333	9	45'9 21'5 36'8 49'4 21'1	240 · 861 56 · 728 230 · 052	-1'95		356.709 179.244	169·594 357·501	0.7274 0.6973 0.7432 0.6889 0.7414	9.7236 9.7546 9.7038 9.7634 9.7059	8.7223 8.7523 8.7068 8.7610 8.7085	0.5536 0.5442 0.5649 0.5390 0.5638	7.6624 7.6775 7.6626 7.6772 7.6630	0274 9.8708 924999 8.8072 9.6516
2961 2962 2963 2964 2965	31 32 32 32 32	X		1732 1732 1732 1733 1733	834 864 012	20 7 9	48 · 2 14 · 4 17 · 9 34 · 3 49 · 2	7 · 107 35 · 488 178 · 429	+1'17 -1'25 -1'80	23.697 23.697 23.697	343.0010 163.563	189°260 340°684 10°627 165°298 197°378	0.7015 0.7109 0.7230 0.7360 0.7252	9.7419 9.7283 9.7110	8.7476 8.7383 8.7262 8.7137 8.7241	0.5455	7.6766 7.6665 7.6637 7.6725 7.6756	
2966 2967 2968 2969 2970	33 33 34 34 35		9 1 26	1733 1733 1733 1733 1733	366 544 720	10 3 11	5'2 37'3	356.761 167.276 346.445 156.226 335.962	-0.98 +3.05 -0.25	23'696 23'696	171.076 359.971 178.729	350.449 171.007 0.991 176.875 10.688	o'6921 o'7444 o'6922 o'7339 o'7106	9.7616 9.7004 9.7613 9.7140 9.7413	8·7572 8·7055 8·7574 8·7155 8·7386	0.5350 0.5718 0.5361 0.5632 0.5481	7.6692	9n8545 9'9329 7n3944 9'0777 9'8696
2971 2972 2973 2974 2975	36 36 35		17 16 12	1734 1734 1734 1734 1734	223 253 400	1 8	18 · 7 47 · 4 50 · 2	145'523 295'327 325'141 106'857 135'130	+3:39 +4:22 +0:17	23.695 23.695 23.695	344'879 16'445 165'467	184.562 345.926 18.294 165.458 194.334	0 7115 0 7412 0 7333 0 6899 0 6928	9.7648		0.2313	7.6682 7.6753 7.6720 7.6639 7.6669	9n7931 On1555 O:1832 O:0875 On1163
2976 2977 2978 2979 2980	37 37 38 38	XII	1 25 21 14	1734 1734 1734 1735 1735	754 931 109 285	18 10 7 19	36·8 36·1 10·4 0·6 57·4	96.769 272.594 86.530 261.547	-0.37 +0.97 -0.40	23.694 23.694 23.693 23.693	174 126 359 507 182 850 7 375	351 173 176 049 357 216 185 223 5 235	0.5998 0.7256 0.7226 0.7022	9'7021 9'7543 9'7229 9'7292 9'7496	8 · 7498 8 · 7239 8 · 7272 8 · 7476	0.5367 0.5623 0.5505 0.5472	7·6763 7·6632 7·6770 7·6627 7·6774	9n8807 9'7078 8n6581 9n4170 9'8085
2981 2982 2983 2984 2985	39 39 39 40 40	XII IV X	4 29		640 787	10		76'032 220'666 250'700 37'113 209'847	I . 61	23.692 23.692	15 235	167.700	0.6892	9'7066 9'7619 9'7636 9'7107 9'7432	8 7593 8 7612 8 7124	0.5632 0.5397 0.5393 0.5615 0.5500	7 6767 7 6776	021462
2986 2987 2988 2989 2990	41 42 42 43	X IV X II	13 8 2 28	1736 1736 1736 1736 1736	319 496 673	21 18 23		26.607 198.820 16.327 187.570 337.378	-3.08 +0.28 -2.43	23.690 23.690	359 · 191 359 · 191	175 · 282 1 · 215 184 · 791 7 · 016 165 · 985	0.7165 0.7319 0.6956 0.7445 0.6961	9.7359 9.7160 9.7585 9.7003 9.7574	8·7183 8·7544 8·7064	o 5650	7.6644 7.6748 7.6655 7.6736 7.6704	8n8795 $9n7379$
2991 2992 2993 2994 2995	43 44	VIII	23 21 17	1736 1736 1737 1737 1737	998 027 176	7 23 15	8·6 43·3	6 · 126 147 · 062 176 · 334 326 · 767 136 · 506	-1.64 +4.19	23.690 23.690	343'088 14'028	340 · 935 12 · 523 175 · 100	o 6908 o 7286 o 7380 o 7178 o 7051	9.7636 9.7212 9.7089 9.7333 9.7481	8.7595 8.7214 8.7123 8.7323 8.7448	0.5583 0.5679 0.5534	7.6667 7.6684 7.6723 7.6718 7.6671	0n0976 0n1904 0·1204 9·8215 9n8736
2996 2997 2998 2999 3000	46	TTTT	1 25 22	1737 1737 1737 1738 1738	707 884 062	9 21 2	26·6 8·5 25·4	315'783 126'240 304'503 116'077 263'069	+0.70 +4.00 +0.54	23.691 28.691 23.692	0,002	359'516 187'457 10'151	0.6906	9'7638 9'7005 9'7582	8.7118 8.7595 8.7064 8.7538 8.7306	o'5328 o'5738 o'5354	7.6658 7.6744 7.6648	8n7264 6:2314 9n8801 9:8657 0:1708
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Nr.	μ.	γ	$\log n$	G	K	$\log \sin g$	log sin <i>k</i>	$\log \cos g$	$\log \cos k$	$\log \sin \delta'$	log cos δ'	N'	bei⊙Auf gang λ   φ	im Mittag	bei ① Untergang λ   φ	F
								i				,		Grad	0	
2952 2953 2054	15'12 100'53 156'28	+0.0611 -0.7986 +0.7986 +1.4850	9.7022 9.7613	92'99 238'48	91.24 90.45 84.89	9.5738	0.00or 0.0000 0.0000	9'9647	8 8295 8n2707 9n3238	9.5879 9.5820	9 9648	01,7	+157 +	8 +155 + 25 50 - 13 - 73 48 - 100 + 76	2   ' / '	
2956 2957 2958	151.26 324.78 207.08	-1.0652 -0.3161	9.7257	53'67 227'82 43'84	84.23 83.63 83.30	9'6473 9'6546 9'6607	9.9866 9.9818 9.9779	9 '9523 9 '9506 9 '9489	9.3877 9.4531 9.4928	9.5690 9.5453 9.5263	9.9679 9.9715 9.9740	74.8	5 + 1 + 7 + xo5	59 + 41 + 3 35 + 155 24 + 165 - 1 4 + 139 + 4	4 -126 - 1	$t^{\pm 1}$
2961 2962 2963	58.91 126.19 287.50	-0.6230 -1.4880 -1.1837 -1.5337	9.7522 9.7438 79.7304	209 29 5 15 26 33	83 43 88 43 88 72	9 · 675 1 9 · 675 1 9 · 677 6	9 · 9624 9 · 9425 9 · 9590	9 9 9 4 4 9 6 9 9 4 4 8 9 9 9 4 4 8 8 9 9 4 0 8	9n6011 9 6834 9 6834 9 6889	9n4053 48.6963 89.3686	9 9 9 8 5 4 5 9 9 9 9 5 5 9 9 9 8 7 8	114'4 61': 64';	1 - 132	14 - 66 - 5		$egin{array}{c} t \ p \ p \ p \end{array}$
2967 2968	334.84 231.28	3 0 . 002	9.7634	350.50	5 92 9	9 9 688	9 942	9 941	9 680 9 680	3 8 2 9 7 4	09'998	61'	2 + 62 -	75 + 28 - 5 84 + 39 + 8 29 + 129 - 34 34 + 12 + 3 20 - 94 + 4	6 -170 + 2	8 t*
2972 2973	305 ' 42	-0.621 2 -1.430 5 +1.524 7 +1.223 9 -1.307	7 9 . 7 0 6 6 7 9 . 7 6 6	308.7	2 96 ° 0. 4 96 ° 1.	4 9 ' 650; 8 9 ' 676; 6 0 ' 638;	39.984 29.958 49.990	7 9 951 9 9 944 8 9 954	6 g · 618 4 g · 307	8 9 2 5 8 5	19.388 09.362	2 64 2 102	7 - :	13 - 113 - 1	30 - 61 - 6	$\begin{bmatrix} p \\ p \\ p \end{bmatrix}$
2977 2978	331.7	3 -1-0 510 60 045	2 9 · 756.	1 286 6	5 93 4 7 92 7	5 9 6 1 9 6 9 6 1 9	49'995	99 957	4 9 1 1 3 7 5 7 9 1 0 3 8	9,603	37 9 9 9 5 x	8 83	1 - 37 -	54 + 71 - 35 - 99 + 9 + 28 - 10 + 74 + 34 -119 +	26 + 88 + 8 + 130 -	4 1.4 18 1-1
298 298 298 298	2 183 · 8 3 340 · 6 4 159 · 3 5 32 · 6	6 -0.769	3 9 763 7 9 765 7 9 712 3 9 745	9 228 7 6 262 7 8 44 8 2 216 3	4 86 5 5 88 9 9 86 6 9 86 8	6 9 530 5 9 582 2 9 523 9 9 512	8 9 985 6 9 985 6 9 985	9 9 9 7 3 6 9 9 6 5 3 9 9 7 4 5 1 9 9 7 5	33 9 n 3 3 4 57 8 n 6 4 9 13 9 · 3 6 6 56 9 n 4 0 9	9x 9n 579 9x 9n 579 9x 9n 30	90 9 966 47 9 986 10 9 99	5 102 52 92 58 76 1 105	·8 — ·3 + 80 + ·2 — I I 3	· 66		63 r-
298 298	7 150.8	3 -0.075	8 9 . 7 18 9 9 . 7 60	2 203 2 6 20 0 5 180 3	5 88 °C	9'497	9998	9 9 97 94 9 97 39 9 97	739.45 $739.46$ $829.48$	$\begin{array}{c c} 74 & 9n & 11 \\ 80 & 9 & 05 \\ 37 & 8n & 72 \end{array}$	20 9 99 29 9 99 37 9 99	72 72	8 -153 -	- 4 + 98 + - 12 - 151 - - 50 - 98 - - 57 - 161 +	28 - 36 -	x6 t
299 299	3 165 0	53 — 1 · 252 58 — 1 · 550 + 1 · 319 + 0 · 669 - 74	95 9 723 95 9 711	10175	43 93 3 49 90 4	31 9 52 48 9 49 25 9 51	06 9 97 19 9 97 66 9 98	60 9 9 97 60 9 9 97	47 9n39 81 9n49 52 9 38	070 9 ' 33 05 8 ' 40 370 923	128 9 . 98 128 9 . 99 134 9 . 98	94 104 99 108 92 75	3 o — 5 5 —116 -		1	-
299 299	97 320 9 98 130 9	0 - 0 1 7 5	02 9 76 88 9 76 40 0 76	59 115. 27 293.	75 92° 56 92°	90 9 55 74 9 55 94 9 56	98 9 . 99 33 9 . 99	53 9 97 60 9 97 83 9 96	706   9n10 703   9   10 578   8n9	546 9 5 298 925 393 9 5	107 9 97 200 9 97 575 9 9	59 9 48 8 97 9	8 · 9 — 28 · 1 · 8 + 131 · 5 · 3 + 48 ·	- 14 - 134 - + 8 + 39 + - 53 - 128 - + 48 + 148 +	69 - 44 -	38 2

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Nr.				T				$oldsymbol{L}'$	Z	ε	P	Q	$\log p$	$egin{array}{c} \log \ \Delta L \end{array}$	$\log q$	$u_a'$	$\log f_u$	logγ
		ianische alender	r	Julia Tag			elt- eit							from dead				
3001 3002 3003 3004 3005	47 47 47 47 48	VII 1	14 12 11 5	1738 1738 1738 1738 1738	387 416 563	4 15 18	32'9 59'9	77.684 105.821 252.088	-1.42 +0.12	23 693 23 693 23 693	195°323 347'542 17'207 171'372 355'785	349 744 19 652 169 658	0.7288	9.7168 9.7219 9.7354 9.7557 9.7031	8 7 7 1 8 8 8 7 7 2 0 9 8 7 3 2 4 8 7 5 3 3 8 7 0 6 3	o'5651 o'5545 o'5476 o'5438 o'5651	7.6755 7.6625 7.6638 7.6776 7.6624	021508 020606 01863 98704 926077
3006 3007 3008 3009 3010	48 49 49 50 50	XI 1	24 20 14 10	1738 1739 1739 1739 1739	095 273 420	8 0	45°1 51°4 31°7 42°9 18°1	241.271 55.451 230.431 17.704 45.946	-1.04 -3.10 +0.12	23.693	187'100 342'405	2.238	o.6890 o.7407 o.7027 o.7094 o.7217	9.7633 9.7069 9.7489 9.7435 9.7300	8.7609 8.7091 8.7468 8.7396 8.7276	0.5393 0.5630 0.5474 0.5439 0.5502	7 6775 7 6626 7 6772 7 6653 7 6630	8.8226 9.5585 9.7926 0.1879 0.0438
3011 3012 3013 3014 3015	50 51 51 52	XI III 3 IX 2	30	1739 1739 1739 1739 1740	627 774 951	10 18 17	41.2 30.2	219.399 7.432 178.156	-3.49 +1.14	23.694 23.694 23.694	163'264 194'991 350'980 170'678 359'425	197 232 349 95 I	o'7368 o'7262 o'6916 o'7443 o'6928	9'7097 9'7222 9'7623 9'7003 9'7610	8.7129 8.7229 8.7577 8.7057 8.7568	0.5682 0.5626 0.5340 0.5729 0.5354	7.6738 7.6766 7.6665 7.6725 7.6678	0'1941 0n1369 9n8848 9'9516 8n6923
3016 3017 3018 3019 3020	52 53 53 54 54	IX I 2	9 1 27 26	1740 1740 1740 1740 1740	484 660 808	1 2 16	50.6	156.276 306.368	+3.03 -0.26 +4.05	23.694	7 870 186 453 344 665	,	0'7326 0'7119 0'7098 0'7418 0'7344	9.7150 9.7397 9.7421 9.7034 9.7133	8.7167 8.7372 8.7394 8.7082 8.7149	0.5634 0.5482 0.5470 0.5721 0.5643	7.6692 7.6697 7.6742	9'2106 9'8463 9n7584 on1621 0'1739
3021 3022 3023 3024 3025	54 54 55 55 56	VIII 2	- 1	1740 1741 1741 1741 1741	014 162 340	17 ; 15 ;	31.8 31.1		+0.31 +3.36 +0.31	23.693 23.693	164'695 194'859 351'908 173'316 359'436	193'868 350'920 175'329	0'6898 0'6921 0'7419 0'7010	9'7646 9'7619 9'7030 9'7530 9'7244	8.7598 8.7578 8.7082 8.7484 8.7249	0.5320 0.5352 0.5731 0.5377 0.5611	7.6682 7.6753	o'1093 on0991 9n8882 9'7648 8n7154
3026 3027 3028 3029 3030	56 56 57 57 57	V1 2	25	1741 1741 1742 1742 1742	871 048 196	4 18 8	57.5 43.4 45.2 39.3 45.1	86.432 231.863	-3.11 -0.00 +0.00	23.690 23.691	7'350 190'318 343'300	344 323	0.7240 0.7009 0.7418 0.6912 0.6890	9 7275 9 7509 9 7055 9 7614 9 7636	8.7257 8.7486 8.7084 8.7589 8.7613	0.2404	7.6770 7.6627 7.6770	9n2645 9.8058 9n9928 0n1476 0.1063
3031 3032 3033 3034 3035	58 58 59 59 60	XI IV s	4 30 25	1742 1742 1742 1742 1743	550 727 905	22 : 12 : 5 :	22.2	220.997 37.104 209.904	-3.49	23.688 23.688	351 221 176 951 359 040	166.764 353.613 174.499 0.994 184.176	0.7328 0.7328	9.7418 9.7376 9.7145	8.7402 8.7347 8.7173		7.6767 7.6635 7.6758	928912 9'4389
3036 3037 3038 3039 3040	60 61 61 61 62	III z	8 2	1743 1743	407 436 613	11 19 6	5°4 40°7 50°7	198.581 348.181 16.745 187.284 337.627	+2.93 +0.25 -2.40	23.688 23.688	163.933 194.181 13.721	165'619 194'866	0'7445 0'6972 0'6913 0'7371 0'7192		8 7529	0.2680	1	0'1373 0n0784 0'1101
3041 3042 3043 3044 3045	62 63 63 64 64		17 12 6	1744	116 292 470	4 : 17 4 :	53°0 18°2 47°3	147.206 326.705 136.880 315.489 126.656	+4.31 +0.61 +4.18	23 687 23 688	180 224 359 352 187 627	187.074	0.7395	9 7493 9 7070 9 7640 9 7009 9 7570	8.7463 8.7108 8.7600 8.7065 8.7527	o 5685 o 5333 o 5729	7.6684 7.6718 7.6671 7.6732 7.6658	1 = - ,
3046 3047 3048 3049 3050	64 65 65 65 65	VI 2	25 22 21	1744 1744	824 972 001	6 11 23	11.5 13.0 33.1		+3.99 -0.84 +0.55	23.689 23.689 23.689	195'145 346'665	161 023 193 018 348 808 18 876 169 727	0,4303 0,4301	9'7327 9'7184 9'7202 9'7336 9'7566	8'7321 8'7200 8'7196 8'7310 8'7542	0.2634		0'1706 0n1451 0n0911 0'1684 9'8701
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						SIN 9	13,111 10	000.9	00.012				λΙο	p    λ G r a	φ d	<u>}</u>	φ	
3002	252 · 84	1:4150 1:1497 +1:5357	9'7240	63.76 93.82	85.65 90.57	9'5883 9'5883	9,8888	9 <b>9</b> 556 9 <b>9</b> 648	9 · 2424 8 n 3770	9.5940	9.0030	9x.2		54 - 92		  39 +	- 32	<i>p p p p t</i> :
3004	303.32	-0.4022	9.7578	53'29	84.16	9 6484	9.9863	9 9539	9.3930	9.5685	9.9680	74 6	+ 11 -	35 + 60		+117	- 8	r
3007 3008 3009	313'71 189'4 <u>9</u> 239'45	+o'3618	9'7091 9'7454	43.63 218.57 12.94	83 29 83 14 86 28	9.6609 9.6657 9.6829	9'9777 9'9726 9'9468	9'9489 9'9476 9'9426	9'4947 9n5369 9'6684	9.5250 9.4911 9.0871	9.9742	70'0 111'2 62'0	+ 96 -	20 + 32 2 + 43 16 + 164	+ 42		- 13 - 38 - 55 	r-t (p) p
3012 3013	331'34 331'34		9'7242	209'59 5'34 178'68	83'46 88'34	9'6733 9'6885	9'9629 9'9417 9'9402	9'9454 9'9409 9'9402	9n5979 9.6860 9n6908	9n4067 8 : 7158 8 : 1117	9.9853 9.9994 0.0000	114'2 60'9 119'4	-159 - (+ 31)(+	79 — 90 87) — 4 32 + 8	********		- 21 - 34 - 26	
3017	202 ' 75 222 ' 93 62 ' 20	1-0'7020	9'7418 9'7442 9'7055	350.46 350.46	92.89 94.82	9.6876 9.6850 9.6624	9'9436 9'9492 9'9755	9.9412	9.6798 926594 9.5137	9,2087	9'9982	117.5 69.8	+ 70 -	38 — 101 16 — 147 7 — 129	7 40	-149	- 19 - 73 - 61 	1 1:4:
3022 3023 3024	79'33 51'88	+1.2860 -1.2563 -0.7730 +0.5819	9.7639 9.7652 9.7551	154.64 308.61	96 · 13 96 · 04 95 · 08	9.6773 9.6402	9.9581 9.9848 9.9903	9'9442 9'9515 9'9540	9n6218 9'4151 9n3191	3 9 ° 3534 1 9 ° 5613 1 9 ° 5841	9.9886 9.9691 9.9654	103.0	-164 - - 56 -	59 - 45 44 + 152 13 - 95	·l- 59	-134		t**
3027 3028 3029	248·18 99·49	-0.1839 -0.6394 -0.9835 -1.4047 -1.2773	9'7530 9'7634	286.70 100.06	92.77 91.63 86.91	9.6191 9.6088 9.5491	9 9974 9 9991 9 9943	9 9588	3   9 ° 0395 3   8 n 8 1 3 1 3   9 n 2 0 3 4	9n6038 9 6038 4 9n4998	9'9619 9'9'9619	94'	+ 57 +	2 - 30 30 +110 62 -101	I6		- 18 + 42 - 66	$t^{ii}$
3032 3033	161 ° 2 8 ° 8	3 0 ' 000 1	9'7439	229 5: 44 9 216 6	5 86 6 7 86 6 3 86 9	1 9 · 5288 3 9 · 5229	3 9 · 9884 9 9 · 9884 9 9 · 9901	9 9 9 7 3 1 9 9 7 4 3 9 9 7 5	5 92325 4 9 359 8 92406	2 91420 4 9 384 3 91301	9 9 <b>'</b> 9848 5 9'9868 8 9'9911	76.4	7 +114 - 4 - 73 + 1 + 28 +	37 - 166 2 - 11 10 + 87 44 + 146	+ 30 - 17	+ 63 + 153	+ 29 20	2:13 2:13
3038	346.8 3111.9	7 1 · 197 7 1 · 197	7 9 7 7 5 8 9 7 7 1 1 5 9 7 7 1 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	6 345 5 3 20 3 9 188 9	8 91 5 6 87 9 7 89 0	1 9 498 3 9 501 6 9 492	9 9 9 7 9 6 9 9 9 9 8 9 8 9 9 7 8	5 9 9 9 7 7 5 9 9 9 7 7 6 9 9 9 7 7	3 9 482 9 9 47 1 9 9 1 486	7 8 9 1 5 0 9 0 6 3 8 8 1 7 0 7	4 9 ' 998 5 9 ' 997 0 9 ' 999	72 72 72 72 72 72 72 72 72 72 72 72 72 7	7 —	54 + 83 	News 94		+ 21	$egin{array}{c} p \ p \ p \end{array}$
304	2 249 °C	02 -0'02I 09 -0'055	3 9 7 7 6 6 5 9 7 7 6 6	1 306 · 3	93 2 97 93 3 5 93 3	4 9 5 1 5 7 9 5 3 2 12 9 5 3 3	3 9 986 4 9 991 6 9 991	8 9 975 9 9 973 7 9 973	3 9 384 2 9 2 3 0 4 3 1 9 2 8 6	$\begin{vmatrix} 2 & 9n & 343 \\ 4 & 9 & 438 \\ 5 & 9n & 449 \end{vmatrix}$	5 9 9 9 8 3 8 9 9 8 9 8 9 9 8 9	2 75° 0 102°	6 + 47 - 1 - 146 - 4 + 20 -	- 37 +150 - 15 +111 - 9 - 79 - 55 +119 - 48 + 34	- I - I - 6	4 +109 3 - 19 5 -164	15 34	1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
304 304 304	7 270' 8 354'	67 +1 · 481 39 -1 · 396 01 -1 · 233 43 +1 · 473 67 +0 · 74	57 9 72 9 33 9 72 9	25 293 1 23 74 1 55 105	71 92 ° 7 33 87 ° 4 33 92 ° 9	77 9 55 41 9 61 94 9 57	18 9 · 995 75 9 · 995 0 x 9 · 995	39 9 9 979 77 9 9 959 32 9 9 6	9 1 9 '01' 9 1 9 '01' 78 8n 96	38 9 252 09 9 60 22 9 55	11 9 ° 974 38 9 ° 961 54 9 ° 969	6 81 8 83	7 — 6 — 6 —	+ 50 +13	4 + 2	5 -174	+ 31	p p p p p
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Nr.		ianisch alende		Juli Ta			elt- Leit	L'	Z	ε	P	Q 	$\log p$	$egin{array}{c} \mathbf{log} \ \mathbf{\Delta} L \end{array}$	$\log q$	$u_a'$	$\log f_a$	$\log \gamma$
3051 3052 3053 3054 3055	66 66 67 67 68	VI XII V XI V	11 5 31 25 19	1745 1745 1745	503 680 858	18 15 9	22 ^m 7 42'3 20'0 16'6	252.501 66.847 241.643	-1.43 -1.81 -2.47	23.691 23.691	179'200 2'874 187'080	189.289	0'6892 0'7399 0'7038	9.7631 9.7080 9.7475	8.7061 8.7607 8.7100 8.7454 8.7292	0.5395 0.5623 0.5483	7.6625 7.6776 7.6624 7.6775 7.6626	9n6943 8.8321 9.4379 9n7925 0.0106
3056 3057 3058 3059 3060	68 69 69 70	XI IV X III IX	13 10 4 30 23	1746	350 537 714	2 1 19	26 6 28 3 3 6 30 6 28 3	18.041 189.105 7.855	+0.13 -2.53 +1.10	23.691 23.692 23.691	350°291 170°358 358°807	197.119 349.398 170.067 0.075 175.901	0.6912 0.7440 0.6038	9.7629 9.7601	8.7218 8.7581 8.7059 8.7558 8.7179	o:5638 o:5332 o:5736 o:5352 o:5636	7.6772 7.6654 7.6737 7.6665 7.6725	9.9658
3061 3062 3063 3064 3065	71 72 72 72 72	VIII VIII VIII	20 12 7 8 2	1747 1747 1747 1747 1747	245 393 423	10 23 16	49 3	167 · 108 317 · 346 346 · 784	-0.08 +4.3r +3.03	23.691 23.691	186'019 344'380	345°219 17°245	0'7134 0'7083 0'7422 0'7355 0'6899	9'7435 9'7030 9'7121	8.7357 8.7409 8.7076 8.7140 8.7596	0'5471	7.6692	9.8169 9n7268 0n1702 0.1618 0.1287
3066 3067 3068 3069 3070	72 73 73 74 74	VII	23 16	1747 1747 1747 1748 1748	747 925 102 279	23 9 2 20	20'4 30'7 48'3 56'0	156'614 306'059 117'785 294'867 107'440	+4.04 +0.59 +3.34 +0.21	23.690 23.690 23.690 23.689	351.699 359.319	193.478 350.606 174.648 356.948 183.484	0.6913 0.7413 0.7021 0.7234 0.7254		8.7584 8.7086 8.7472 8.7261 8.7243		7.6697 7.6743 7.6648 7.6754 7.6639	0n0833 9n8986 9.8126 8n7962 9n0366
3071 3072 3073 3074 3075	75 75 75 75 76	VII XI XII V	26 21	1748 1748 1748 1748 1748	634 781 811	17 :	14.3 34.4 40.9	283 · 928 96 · 853 243 · 084 273 · 142 57 · 972	-0:34 -2:37 +1:02	23.689 23.688 23.688	189 433 343 285	15.002	0'5918	9.7520 9.7047 9.7608 9.7638 9.7136	8.7497 8.7078 8.7583 8.7612 8.7144	0.5451 0.5647 0.5408 0.5388 0.5594	7.6763 7.6632 7.6775 7.6770 7.6626	9.8014 9n9550 0n1486 0'1055 0'0661
3076 3077 3078 3079 3080	76 77 77 78 78	XI IV X	10 4 30 24	1749 1749 1749 1749 1749	312 490 667 844	19 14 10 14	36·3 4·4 7·1 36·0	47.567 221.039 37.399 209.653	-1.79 -3.49 -1.35 -3.47	23 687 23 686 23 685 23 685	176.127 358.937 184.847 6.214	6.364	0'7137 0'7338 0'6941 0'7446	9'7403 9'7393 9'7133 9'7605 9'6997	8.7390 8.7350 8.7162 8.7560 8.7063		7.6772 7.6630 7.6766 7.6636 7.6757	9n8940 9'5412 9n0000 9n6188 9'7768
3081 3082 3083 3084 3085	79 79 79 80 80	X III IX	13 10 2	1750 1750 1750 1750	198 347 523	7 2 9 2	13'9 20'4 26'9	27.309 198.301 348.417 157.978	-0.05 -3.05 +2.93 -0.35	23.685 23.685	193'449 13'493 171'811	165.171 194.269 11.810 174.214 348.357	0'6918	9.7628	8 7141 8 7293	0'5327	7.6644 7.6691	020564
3086 3087 3088 3089 3090	82 82 83	VIII VIII I	23 16 12 6	1750 1751 1751 1751	878 055 232 379	12 1 17 2 23 3	16.3 17.7 18.6 36.5	337.553 147.590 326.409 137.292 285.423	+0°24 +4°18 +0°62 +2°45	23.685 23.686 23.686 23.686	358 775 187 282 7 187 163 377		0'6900 0'7438 0'6977 0'7163	9'7642 9'7015 9'7560	8·7102 8·7604 8·7068 8·7519 8·7333	0.5340 0.5718		9n8445 9 7929
3091 3092 3093 3094 3095	83 84	VIII VIII VIII VI	3 2 27 21	1751 1751 1751 1751	557 587 734 911	18 6 2 11 5 20 4	6 2 6 4 6 4 7 2	126·897 274·518 87·907	-0.22 +0.72 +1.20 -0.84	23 686 23 687 23 687 23 688	345'805 15'719 171'329 353'946	169 773 354 399	0.7315 0.7202 0.6948 0.7444	9.7187 9.7317 9.7575	8.7210 8.7186 8.7296 8.7550 8.7057	0.5569 0.5509 0.5425	7.6733 7.6632 7.6658 7.6769 7.6627	0n1373 0n1190 0'1511 9'8710 9n7653
3096 3097 3098 3099 3100	84 85 85 86 86	XII VI XII V XI	10 5 31	1752 1752 1752 1752 1752	265 443 620	21 5 18 4 1	3 3	263 · 726 77 · 242 252 · 867 66 · 795 241 · 760	-1'41 -1'42 -1'79	23.687 23.688 23.688	1'961 187'071 10'435	179.777 0.516 189.319 7.994 197.032	0.7391	9.7628 9.7091 9.7462 9.7337 9.7192	8.7444	0.5396 0.5617 0.5492 0.5479 0.5648	7.6774 7.6624 7.6776 7.6624 7.6775	8.8416 9.2711 9n7931 9.9745 on1364
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3051	38°56	-0'4947	9.7049	63°30	85°58	9 6343	9.9930	9.9554	9'2504	9.5936	9.9637	78°8	- 84 -	- 37	— 36 — 102	- 7	+ 18	17 9	1020
3053	51'01	+0.0679	9'7102	53'06	84'14	9.6487	g'9862	9.9521	9'3957	9'5075	0.0083	74'5	113	O	53	7 30	+ 24 + 136	29	7** <del>*</del>
3054 3055	138.30 330,10	0'6201 +1'0247	9'7496 9'7340	43°75	83.33 83.69	9.6597 9.6538	9 9823 9 9779	9.9507 9.9492	914462 914926	915485	9.9710	70.4	~ ,	- 20				_ 51	$\left  egin{array}{c} r ext{-}t \\ p \end{array}  ight $
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3057	210'02	-1.3687 -0.8245	9.7649	13.07	86,18	9'6857	9'9461	9'9417	9'6709	9'0950	9,9966	61,8	- -XI4  -	8o	+152	— 62 —	-147 -125	- 27	t
2050	TTT '80	-0.1054 -0.1054	0'7622	5.62	188'25	a'68a6	0.0414	0.0405	0.6868	8.7300	99993	00.0	-174	- 35	110	4	46	+ 23	t
зобо	219'40	+0.1921	9.7185	178.22	90.47	9.6910	9'9401	9.9401	926909	8.1630	0.0000	119.4	78	+ 41	-17-144	14	-158	x8	7"
3061	319.58	+0.6560	9'7405	358.20	90'56	9.6893	9'9407	9 9406	9.6890	812452	9'9999	60.7		+ 12 3		+ 48 32	+107 + 75	+ 70 - 61	
3063	177'16	-0.5331 -1.4797	9'7051	327'91	96.74	9.6721	9.9655	9'9458	9.2833	924349	9.0833	66.2	_		_		75		p
3064 3065	65.38	+1.4513	9'7141 9'7664	350'44 139'80	96.22	g.6863	9 9440	9.9417	9.0784 $9.5223$	8n 903 1	9.824z	110.2		-		-			$\left  egin{array}{c} p \\ p \end{array}  ight $
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3067	168 30	-1.5112 -0.4018	0.706r	318.22	06'80	0.6630	0 0756	9'9483	9'5134	19n5116	9'9758	60.8	T 74		160	76			r
ვინი	218.02	+0.6496	0.7281	308'48	06.03	0.6506	0 0849	0'0516	9'4136	925617	'g'g0g1	73'8	- 72	18	7-142	25	-102	12	2014
3070	133'48	-0.1088	9.7278	121'41	95.13	9.6408	9.9901	9'9539	923232	9.5836	9.9622	103.5	102		134	IO	79	x8	"
3071	17.79	+0.6330	9'7541	297 '94	94.61	9.6358	9.9923	9'9551	9'2707	925910	9 9642	78 . 3	- 76 117	+ 25 - 49	N #	+ x7	26 172		
3973	89 45	-0.0016	9'7628	254'27	87 93	9.2686	9.998x	9.9680	819720	925542	9'9702	95.8							p
3074 3075	246.07 359.51	+1.1643	9.7658	68.74	87.41	9.2291	919974	9 9588	0.0010	9,5328	9.9619	83'1	1 1	*****	no conf	_			p p
2076	200120	-o 7834	0.7434	242.47	86.00	0.5470	0.0042	0.0711	02180	025016	50'0770	99.4	- 10	40	+ 66	- 7	+173	56	5 1
3077	110,80	+0.3477	9'7414	57'11	86.74	9.5400	9.0928	9'9721	9 2549	9 472	: g.g8oc	79	+170	+ 9	119	1-1- 34	- 42 + 31	7 3	
3070	332 '07	-0'4157	9.7626	45'32	86.63	9'5232	9.9885	9 9744	9'3579	9 387	ilg '9867	70'	28	37	- - 3 x	I	r + 92	x	t
3080	40'66	+0.2981	9,4010	210.37	80.63	9.2100	9.9823	9 9759	92407	1 92 298	99.9912	105	93	- 30	30	7			
3081	106.02	+1.4203 -1.1387	9.7574	358 67	90'14	9.4948	9 9777	9.977	9'494	7,1882	40.000	71	3 2						$p \\ p$
3083	40'30	-1 · 2653	0.7128	202 45	87'70	9'499	0800	9 977	192461	8 92 100	8 9 9 9 9 6	5 107'	O		 64	_		+ 6	p
3084 3085	324'23	+0 7450 -0 8352	9:7325	153'15	92'57	9 4930	9 9 9 7 9 3	9 9776	5 9 470 5 9 2 4 5 0	2 9 . 177	9 9 9 9 9 9 9	106.	ő 32	40	+ 29	- 5	2 + 85	- 7	
2086	7.66	-0.0184	10.708	1332.37	102.57	70.501	20.0826	5 0 ' 077	0.443	3 02 185	70'094	73.	7 65	_ 15	_ 2		8 + 56	5 x	7 1:1
2087	Troo'T	-0.1043	20'7663	140.24	5 03 22	201515	sla•a86:	10'075	3 02 302	ala 1833	o a ' a8a	7 104	7 - 95	8	1-1-100	1777	o∥ 139	] 2	0 6
3089	84 9	5 - 0.620	7 9 758	1   128 ' 60	0 93:39	9 9 5 3 2	4 9 * 9 9 0	8 9 ' 9 7 3	3 92310	8 9 435	3 9 983	3 102.	3 173	+ 48	— 81 —	+ 5	5 - 8	3 + 2	5 t*
3090	175 5	482	3 9 7 3 0 2	2 273 2	90.4	99.500	9999	9 9 904	7 8 - 309	92500	019 904	00							1
3091	29.6	9 — 1 · 37 I <u>9</u> 4 — 1 · 315	9'722	306.3	93'3	9.232 6 9.600	79.991	5 9 ' 972 8 0 ' 062	7 9 289	9 9n45 X	29'981 10'062	9 78·		_			_	*****	$\begin{vmatrix} p \\ p \end{vmatrix}$
3003	272 1	6 +1 · 416	0 9 7 7 3 3 1	6 117'1	4 93 0	3 9 551	8 9 9 9 9 4	8 9 9 70	5 9n 187	2 9 506	999'976	3 99.	4	-	r	+ 2	5 + 5	r   - 4	19
3094	1359 8 134 3	7 -0 582	5 9 7 7 9	4 73.8	2 87.3	2 9 618	49.997	69.958	9 9 025	9,603	79.961	8 83.	4 180	- 38	-132	- I		- 2	_
2006	5 234 . 8	6 +0.069	49.764	9 240 6	6 86 6	19.624	69.006	x 9 ' 957	6 92 128	31 gn 601	49.962	3 98	4 + 66	+ 1	+125	_ 2	0 -16	9	4 t*
300	7 7 48 5	7 +0.186 2 -0.621	70'711	3 63 0	5 85 5	4 9 634	5 9 992	8 9 955	3 9 254	16 g · 593	x 9 ° 9 6 3	8 78	7 + 150	(	o∥ 15¢	1-1-3	4   - 7	8 2	10 1
3000	242'9	9 +0.943	0 9 735	8 53'2	3 84'1	8 9 647	7 9 986	2 9 952	2 9 393	3 I   9 ' 567	4 9.968	2 74	6 + 8	+ 50	— 7c	) (- <del> -</del> 80	o) — 8	3 + 6	8 1'-1'
3100	221'1	1 -1.360	Jg 721	2240.8	103.7	49 052	519 982	9 95	9244	97.54	970	3/20/							
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3101 3102 3103 3104 3105	87 87 88 88 89	IV 21 X 15 IV 10 X 3	1753 1 1753 3 1753 4	76 10 19 6	200 · 123 18 · 462 188 · 884	+0.10	23.689 23.689 23.689	177.236 177.236	169.711 359.206 175.239	0.7438	9.7635 9.7005 9.7593 9.7174 9.7369	8.7584 8.7062 8.7550 8.7189 8.7343	0.574x 0.535x 0.5637	7.6749 7.6654	9n9478 9'9765 9n2089 9'3507 9'7804
3106 3107 3108 3109 3110	89 90 90 90	IX 22 II 18 III 20 VIII 14 IX 12	1753 9: 1754 0: 1754 1:	09 0 4 0 56 1 7 5	328.257	+4'12 +2'10 +0'57	23.689 23.689	344.016 14.985 163.334		0.7366	9.7025 9.7111 9.7641	8.7423 8.7070 8.7129 8.7596 8.7590	o 5639	7.6717 7.6679	9n6992 0n1807 0'1472 0'1453 0n0693
3111 3112 3113 3114 3115	91 91 92 92	II 7 VIII 3 I 27 VII 23 I 15	1754 51 1754 68 1754 86	0 17 4 4 7 10 59 7	305 933	+0.73 +4.02 +0.60	23.687	171.847 359.142 180.403	182.666	0'7408 0'7034 0'7221 0'7268 0'6988	9.7048 9.7500 9.7277 9.7238 9.7532	8.7090 8.7460 8.7274 8.7229 8.7506	0.5405 0.5581 0.5547		9n9126 9'8530 8n8953 8n5719 9'7938
3116 3117 3118 3119 3120	93 93 94 94 94	VII 12 XII 7 I 5 VI 1 VII 1	1	7 2 29 8 6 13 32 9 3 18 14 5	68.372	-1.33	23.686 23.686 23.685	343'276 15'132	164'813	0'7429 0'6924 0'6890 0'7345 0'7419	9.7038 9.7602 9.7638 9.7151 9.7057	8.7577 8.7612 8.7154	0.2415	7.6764	9ng142 0n1494 0'1037 0'0948 0n1931
3121 3122 3123 3124 3125	94 95 95 96 96	XI 26 V 22 XI 15 V 10 XI 3	1755 89 1756 07 1756 25	5 22 17 0	58.004 232.209 47.879	-1.05 -3.14	23.684 23.684 23.684	175'278 358'873	353'591 172'862 0'680 182'823 6'119	0'7119 0'7121 0'7348 0'6934 0'7446	9.7389 9.7411 9.7120 9.7614 9.6995	8.7377 8.7153		7.6775 7.6626 7.6772 7.6630 7.6766	9n8960 9'6255 9n0264 9n5373 9'7677
3126 3127 3128 3129 3130	97 97 97 98 98	IV 1 IV 30 X 23 III 21 IX 13	1756 78 1756 93	8 2 49°2 7 10 58°1 3 22 44°1 2 14 53°5 8 17 33°1	37.823 209.375 359.133	-3.44	23.683 23.683 23.683	192.666 13.326 171.267	164.648 193.627 11.561 173.643 348.016	o 6995 o 6925 o 7352 o 7221 o 7013	9.7544 9.7622 9.7118 9.7290 9.7518	8.7506 8.7577 8.7151 8.7279 8.7488	0'5325	7.6663 7.6636 7.6757 7.6677 7.6713	0'1690 0n0314 0'9957 9'9014 9n9388
3131 3132 3133 3134 3135	99 99 100 100	VIII 23 I 17	1757 64 1757 81 1757 96	8 0.2	337 257 147 997 296 541	+3:70 +0:22 +3:47	23 682 23 682 23 683	186.858 6.610 163.261	358 200 186 084 8 515 160 827	0'7433 0'6990	9 · 7055 9 · 7643 9 · 7022 9 · 7546 9 · 7359	8.7094 8.7607 8.7073 8.7509 8.7345	0'5347 0'5704 0'5392	7.6698 7.6705	8.8209 9n1665 9n8182 9.7580 0.1728
3137 3138 3139 3140	102	VIII 12 I 6 VII 3	1758 17 1758 31 1758 49	2 13 47 1 2 20 43 7 7 3 12 2	109.002 137.519 285.693 98.328	+0'30 +0'60 +2'49 -0'22	23.683 23.683 23.683 23.684	344.980 15.062 171.263 353.052	346.993 17.470 169.792 353.389	0.7279 0.7328 0.7215 0.6941 0.7448	9.7217 9.7169 9.7585 9.7018	8.7222 8.7172 8.7282 8.7558 8.7056	o.2583	7.6719 7.6640 7.6670 7.6762 7.6632	On 1270 On 1443 O'1342 9'8736 9n8253
3142 3143 3144 3145		XII 17 VI 10 XII 5	1759 02 1759 20 1759 38	4 12 32.8 4 23.2 9 2 48.5 5 11 15.2 8 11 12.2	264 082 77 212 252 967	-0'85 -0'12 -1'40 -1'42	23.685 23.685 23.686 23.686	1.058 187.059 9.553 194.860	359 515 189 346 7 113 196 947	0.6902 0.7382 0.7061 0.7172 0.7297		8.7601 8.7117 8.7432 8.7323 8.7197		7.6627	8.8609 9.0024 9.7935 9.9351 0.1367
3147 3148 3149	105 105 106 106 107	V 1 X 25 IV 21 X 14 IV 11	1759 707 1759 885	17 44.6 16 36.9 10 53.2 18 21.2 0 31.2	39'107 211'199 29'016 199'910 18'743	-3.48 -0.78 -3.13	23.687	357 371	169 415 358 883 175 258	0.6956		8·7066 8·7537	0.5315 0.5747 0.5350 0.5635 0.5486	7.6759 7.6644	9n9790 9'9842 9n3550 9'3881 9'7352

Y-A-A-A-A-A-A-A-A-A-A-A-A-A-A-A-A-A-A-A				a de Maria										C	entral	litüt			
NT.			I o o	G	K	log	log	$\log$	log	log	log	N'	bei 🛈 🗛	uf-	im Mitt	tag	bei Unterg	O rang	F'
Nr.	μ	γ	log n	u	I A	$\sin g$	$\sin k$	$\cos g$	cosk	sinδ'	cos o'	71			λ	φ	λ	φ	
								**************************************						G	r a	a l	9		
3101	335 [°] 03	o'8868	9.7655	21°01	84°50	9'6809	9 ' 9534	9'9432	9.6429	9.2841	9.9918	63°4	+ 32 -	79 -	- 36	72	+ 95 +115	- 35 - 43	t r#
3103	228'96	-0.1918	9.7614	13.32	88.00	9.6870	9'9459	9'9414	9'6717	9 1046 827027	9.9965	61.2	(+102)(+ + 72 - - 37 +	37 -	+ 133 - + 26 -	- 3 - 11	162 85	+ 19 - 16	t 2.**
3105	74' 13	+0.6031	9'7390	5.85	88'19	9.6890	9'9417	9*9408	9.6860	8.7555	9,9993	60.0	-143 +	8	- 83 -	F 47	- <del></del>		.
3107	289 99	-0.5002 -1.5160 +1.4033	9.7046	336 59	95.89	9.6796	9 9559	9'9437	9'6324	923251	0.0001	64.0		x	-114 -	- 34 	41 	- 59 	$\left egin{array}{c} t \\ p \\ p \end{array}\right $
3100	199'72	+1 3973	9'7661	148'77	96.63	9.6712	g · g648	9.9460	925874	9'4241	9.9841	113.0					_		$\stackrel{\hat{p}}{p}$
3111	283.36	o.8177	9.4069	327°77	96.48	9.6730	9,8622	9 9456	9.5835	914375	9 9831	66'5	- 49 -	70	+ 87	- 79	+159	30 30	}: }:
3113	341'12	0.0373	9.7299	318'41 121'28	06.31	0 6541	9 9757	9'9483	9.5125	9n5123	9 9757	107.3	+176 + - 52 - + 54 +	14	-121	+ 19	+176	18	7:34
3115	146'48	+0.6220	9'7553	308 56	96.03	9.6503	9.9848	9.9216	9.4142	9,5610	9.9692	73.5	153	21	151	- - I9	104	ľ	1
3117	222 20	-0.8208	9'7622	266.67	89:50	9.2880	0.9999	9.0648	823173	3 9 2 5 8 7 4	9'9049	01.5		38		35	+ 95	- 59	$\frac{r}{p}$
3119	98.87	+1 · 2697 +1 · 2440 -1 · 5600	9 7171	80'25	88 63	9.5776	9.9992	9.9665	8.7734	19'5722	9.9074	80.3			Maryanag Spottan	***			$\frac{p}{p}$
9121	50.38	-0.7870	0.7410	255'12	88.04	9.5682	9 ' 9983	9.968	82.9479	9 9 5 5 5 5	9,0701	95'	-153	43			+ 43		
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3316	5 10.2 7 57.6 8 115.5	0 —0.595 3 +0.558 1 —1.355 0 —1.239 3 +1.263	9 9 74 1 4 9 74 3 7 9 7 1 5	9 298·5 9 107·6 0 286·3	7 93.0 5 92.2 8 92.1	9 · 546 4 9 · 563 3 9 · 566	5 9 994 4 9 997 8 9 997	3 9 ' 97 I 6 9 ' 968 9 9 ' 968	2 9 · 203 8 92016 2 8 · 987	$     \begin{bmatrix}       6 \\       9 \\       7 \\       9 \\       \hline       6 \\       9 \\       \hline       9 \\       7 \\       9 \\       \hline       1 \\       9 \\       \hline       1 \\       9 \\       \hline       1 \\       9 \\       \hline       1 \\       9 \\       \hline       1 \\       9 \\       \hline       1 \\       9 \\       \hline       1 \\       9 \\       \hline       1 \\       9 \\       \hline       1 \\       9 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\      \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\      \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\      \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline       1 \\       \hline $	14 9 · 977 12 9 · 971 12 9 · 979 12 9 · 962	5 80° 5 96° 6 84° 29 80°	6 -	-,0		- 26   t*   - 27   29   29   29   29   29   29   29
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3906 3907 3908 3909 3910	437 437 438 438 439	VII XII VI XII V	13 8 3	1881 1881	019 196 374	17 45	5'5	116.624 263.298 77.729 252.496 67.106	-0'40 -1'15 -1'64	23.641 23.641	166'392 350'119 174'219	14 147 165 447 349 988 175 480 356 351	0.7270 0.6909 0.7448 0.6925 0.7341	9.7238 9.7615 9.7019 9.7597 9.7151	8·7228 8·7591 8·7053 8·7574 8·7155	0.5545 0.5403 0.5659 0.5414 0.5583	7.6642 7.6775 7.6624 7.6776 7.6625	o·o387 o·o6o5 9n9772 9·6936 9n2210
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3916 3917 3918 3919 3920	441 442 442 443 443	high right right	28 20 17	1882 1882 1882 1882 1883	585 761 939	4 8 7 35 16 3	3.1 2.8	189.008 8.146 177.961 357.656 167.292	-1.18	23.643 23.643 23.642	354 · 181 173 · 051 2 · 637	164'302 356'058 170'728 4'992 179'327	0.6994 0.7238 0.7219	9.7037 9.7539 9.7259 9.7285 9.7520	8·7082 8·7499 8·7254 8·7272 8·7486	0.5713 0.5391 0.5575 0.5543 0.5418	7.6730 7.6672 7.6717 7.6687 7.6702	0.1447 927033 9.8044 9.3826 920621
3921 3922 3923 3924 3925	444 444 445 445 446	VII	29 24 20 13	1883 1883 1883 1883	470 618 795 972	2 39 17 30	9'1 9'5	346.797 156.893 305.908 118.140 294.798	-0.24 +3.89 +0.77	23.642 23.641	189 661 346 596 168 046	11'750 189'591 344'923 170'433 351'918	0.6894 0.7365 0.7099	9'7052 9'7644 9'7100 9'7432 9'7360	8.7089 8.7601 8.7133 8.7393 8.7348	0.5342 0.5686 0.5436	7.6700 7.6689 7.6749 7.6644 7.6759	0.0047 9ng121 0n0996 0.0240 9n7038
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4062 4063	92.50	+0'9480 -0'6109 +0'1868 +0'0653 -0'5640	9.7667	267.51 81.56	89'63 88'81	9.5869 9.5778 9.5656	9 9999 9 9994 9 9983	9 9 9 6 4 9 9 9 6 6 5 9 9 6 8 4	817114 817114 819515	925800 9.5738 925523	9.9672	91'0 95'5	+ 26 + -175 - -158 - -135 - - 35 -	33 - 7 - 9 -	- 93 - - 91 - - 78 -	50 9 33 21 17 17	- 35 + 13 - 2	t::: 2:::: t
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4073	346'51	+0.6572 -0.6193 -0.0833 +0.0877 -0.8093	9.7643	358 49	90.16	9 4899	9.9782	9.978	9,487	0.7n303 0.7n929 0.8851	1 0 . 0 0 8 0 3 0 . 0 0 0 0	72	-82 - 6 + 93 - 6	- 23 - 23	- 20 - -+158 +	5 + 40 9 - x40	+ 13	1 1 1
4078	302 90 302 90	+0.8600 +1.1727 -1.4660 -1.2812 +0.5134	9.7653	332.28	93.05 92.62	9 5479	9 9 9 9 4 5	9 9 9 7 1 9 9 9 7 5	9.197	9 9n499 9 9n 187 9 9 542	9 9777 5 9 9948 8 9 9718	3 73 ·	5		Mendalan b	72 114		P P
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4111 4112 4113 4114 4115	524 524 524 524 525	X	13	1912 1912	588 735 764	б: 3 14:	28·9 1·7 21·4	59:394 201:875 231:695	-0.74 -1.63 -3.35 -3.36 +0.08	23.628 23.627 23.627	194'372 344'360 15'944	165'438 196'720 343'232 13'903 172'629	0'7233 0'6926 0'7010	9.7155 9.7285 9.7606 9.75,14 9.7013	8 · 7 · 6 · 1 8 · 7 · 2 6 6 8 · 7 5 7 8 8 · 7 4 9 · 1 8 · 7 • 5 7	0.2211	7.6648 7.6629 7.6742 7.6767 7.6660	021162
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4219	289.22	+oʻ0878 -oʻ8808	9.7539	119.98	93.II	9.5429	9'9939	9.9718	912200	9.4872	9'9785	roo'o	+ 2	+ 14	+ 7x	+ 23	+-133	5	l:4
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4228	120.73	+0.5259 0.6586	9'7043	47'47	83.00	9'6550	9'9814	9'9504	9'4567	9'5437	9'9717	72'2	十170	+ I3 - 20	126	+ 54			
4230	292.27	-1.227	9 7226	15.83	85'59	9.6817	9'9491	9 9430	9.66ox	9.1696	9 9952	62.5		_					p.
4231	134'58	+1.2682	9.2112	38.25	83'17	g'6651	0'0724	0'0478	0.5385	0.4876	0.0785	68.7	وبنشو		i-quarque				p
4232	174'18	+1.4133 -1.3212	9 7331	189'59	87.12	g · 6862	9'9440	9'9417	926783	829642	0.0082	118'6	****		,	*******			$\tilde{p}$ .
4234	77.68	-o'7137	9.7494	8.01	87.56	9.6869	9 9431	9'9414	9'6814	8.8886	9:9987	61'2	-134	- 74	- 67	- 50	8	x7	$\begin{bmatrix} p \\ t \end{bmatrix}$
4235	245:95	+0.7472	9.7090	181'02	89.49	9.0902	9'9404	9 9403	9n 6899	812022	9,8888	110.3	+ 48	-l- 77	+126	58	-176	19	7.**
4236	306.11	+0'0290	9 7654	0'56	89 * 82	9.6894	9 9407	9'9407	9 ' 6894	7.7402	0.0000	60.7	1o	28				+ 31	
4238	192'75	+0.0353 +0.7437	9'7605	353'12	33.11	9.6874	9'9425	9.0412	9 6833	828237	9.9990	gr.r	+ 96	- Ig	+117 +157	+ 54	+175 -136	- 27 + 75	1 th
4239	275 54	-0.6900 -1.3020	9.7215	165'69	94'14	9.6861	9 * 9468	9'9417	926684	9 1334	9,9960	118.1	17	- 15	+ 74	44	+132		r
																			p
4241 4242	27:26 285:10	+1.2137 +1.2132	9 7372 9 7594	345 28 133 76	94'14	9.6817	9'9482	9 9429	9'6630	911397	9'9958	62'3				_			$p \\ p$
4243	20.03	-1.3707	9 7486	157.56	95 70	9.6787	9 9552	9439	026354	0'3074	0.0000	116.5						_	$\mathcal{P}$
4245	179:21	-0.6470 -0.4793	9.7663	124 75	95.24	9 5440	9 9878	9.953r	9 4553 9n3672	9"5445	9.9673	72.3 104.5	+ 53 + 94	+ 39	156 176	- 63 - 52	-135 -106	21	r t [‡]
		+0.0402			1 1				i				l				1		
4247	00.80	-0.2085	9`75.77	114.00	94'12	9 6302	0.0030	0'0563	022100	0.5048	0'0635	100'4	T 2 3	×	62		1 7	24	$t^{**}$
4240	259 69 223 64	-1.0830	9 7310	104 25	93'38 92'34	9.6237 9.6142	9'9961 9'9982	9'9578	9'1292 8"0675	92 6002	9 9625	8x'6	+ 47	+ 34	+ 97	1- 24	+141	+ 49	$p^{i^{*ij}}$
4250	265.01	-1'3453	9.7642	245 44	87.16	9'5538	9 956	9 9702	9n 1475	9n 5 1 75	9'975I	98 6	-	-	ļ —		-	-	p
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Nr.		nische lender		T Julia Tag			elt-	L'	Z	ε	P	Q	$\log p$	$rac{\log}{\Delta L}$	$\log q$	$u'_{a}$	$\log f_a$	$\log \gamma$
4251 4252 4253 4254	578 579 579 580	XII V XI IV	14 11 4 29	1932 1932 1932 1933	520 568 845 022	16 ^h 4 15 21 17	16"0 26.8 5.8	51'830 224'513 41'146	-0°23 -1'56 -3'63 -1'26 -3'69	23.621 23.621	15°878 170'051 351'881 178'095 359'883	169'848 353'248 176'174	0.7450 0.6933 0.7339	9'7017 9'7592 9'7154	8.7522 8.7055 8.7568 8.7161 8.7362	0.5443 0.5666 0.5410 0.5591	7.6774 7.6633 7.6762 7.6640 7.6753	0°1329 9°9804 9n8411 9°2534 8n0217
4255 4256 4257 4258 4259 4260	581 582 582	IV X III IV IX		1933 1933 1933	377 554 702 731	1 16 8 16	55'3 34'6 14'6 38'9	30.678 202.614 351.766	-0'70 -3'38 +2'64 +0'09	23.620 23.620 23.620	186.280	184 · 160 9 · 449 164 · 748 193 · 995	0.4114	9'7417	• "	0'5448 0'5676 0'5346 0'5342	7.6650 7.6741 7.6697 7.6661 7.6692	9n7684 9·8616 0·1064 0n1084 0n1841
4261 4262 4263 4264 4265	583 583 584	X II VIII II VIII	23 17	1934 1934 1934	057 233 411	0 3 11	14'0 21'0 32'6	341'322 151'06: 330'618	-2.76 +3.42 +0.17 +3.97 +0.67	23.620 23.620 23.620	351'847 181'279	174 991 349 519	0'7002 0'7231 0'7231	9'7531 9'7272 9'7270	8.7494	0.2392	7.6729 7.6710 7.6678 7.6725 7.6665	0°1586 9°7802 9 ⁸ 733 9 ⁸ 0596 8°4525
4266 4267 4268 4269 4270	585 585 586 586	VIII XII I VI	25		942 089 119	7 20 14	25'5 15'2 54'2	308'20	+4'15 +0'91 +1'35 +3'93 -0'28	23.620 23.620 23.621	8 · 850 164 · 281 196 · 284	162.577 195.423 350.194	0'6899 0'7358 0'7428 0'7106	9'7644 9'7107 9'7023 9'7429	8.7601 8.7143 8.7077 8.7391	0.5322 0.5696 0.5733 0.5429	7.6654 7.6771 7.6750 7.6627	9.8749 9.8749 0.1666 0.1885 0.0338
4271 4272 4273 4274 4275	586 587 587		16 12 5 31	1935 1935 1935 1935	444 622 798 976	2 0 15 2	25 ° 9 8 ° 9 19 ° 0 25 ° 6	266 · 81 81 · 78 255 · 88 71 · 16	-0 85 -1 36 9 -1 32	23'621 23'622 23'622 23'623	171.964 356.406 179.874 4.543	169'541 358'363 178'547 4'787	0'7133 0'7334 0'6930 0'7446	9.7593	8.736x 8.7x65 8.7568 8.7053	0.5544 0.5578 0.5416 0.5659	7.6774 7.6625 7.6626	9.8567 9.5282 8.0332 9.6412
4275 4275 4275 4275 4286	589 589 589 590	XI XI V	15 13 10	1936 1936 1936 1936	330 478 507 655	3 7 21 0	42.9 17.2 5.3 43.6	60'50 204'29 234'23 21'76	7 -2 · 45 5 -1 · 57 3 -3 · 44 2 -3 · 24 2 -0 · 01	23.62 23.62 23.62 23.62	12.575 4 164.02 4 195.63 4 351.22	188.581 10.962 156.450 197.974 349.003	0.704	9.7108 9.7295 9.7438 9.7482	8   8   7   2   6   8   7   7   8   8   7   7   7   8   7   7	0'5611 0'5570 0'5503 0'5412	7.6629 7.6743 7.6768 7.6659	0°1580 0n1362 9n8860
428 428 428	59x 592 592	IX	30 23 19	1937 1937 1937 1937	009 186 364 549	16 11 9 13	29'7 27'2 11'4 59'4	181.49 181.98 1.70.95	30.88	23.62 23.62 23.62 23.62	3 359 75 3 179 19 3 186 93	0 178'56	9 0.689 8 0.743 3 0.695 9 0.728	9   9 ' 7638 4   9 ' 7010 9   9 ' 757 2   9 ' 720	8 7593 6 8 766 7 8 753 7 8 721	5 0.221 5 0.221	7 6718 7 6718 7 6685 7 7 6704	8n3276 8·8916 9·8463 9n8077
428 428 428 428 429 429	7 593 8 593 9 593 9 594	VIII VIII VIII VIII	8 2 31 27	1937 1937 1937 1938	718 865 894 8048	22 14 23 9	10.3 29.6 50.6 56.6	350.08 350.08 350.08	18 +2'73 18 +0'83 14 -0'45 13 +3'99	23.62 7 23.62 5 23.62 23.62	3 16.56 3 165.00 3 195.22 2 353.05	7 347 05 8 18.96 0 163'49 6 193'00 7 353'58	9 0'717 3 0'695 0 0'705 4 0'743	4 9.733 6 9.758 9.747 6 9.701	9 8.732 4 8.753 9 8.744 0 8.706	0 0'552 9 0'535 4 0'543 6 0'573	0 7.6699 7.6699 6 7.6699 9 7.674	0 0'1706 0'1067 0 0n1223 7 9n8238
429 429 429 429	2 595 3 595 4 596 5 596 6 596	VII VII VII	16 12 5 1	1938 1938 1938 1938	3 397 3 574 3 75 3 929	7 9 1 23 1 13 9 9	28: 26: 59: 53:	5 298.76 3 111.4 7 287.4 6 101.0	08 +3'4' +0'6 92 +2'3 79 +0'2 73 -2'3	23.62 5 23.62 9 23.62 0 23.62	12 0 29 21 182 23 21 7 92 21 190 87 20 343 96	3 358 91 1 184 46 4 5 48 3 193 04	6 0'739 3 0'705 4 0'719 6 0'728	94 9 706 55 9 748 92 9 730 38 9 721	8 · 710 8 · 743 9 8 · 720 24 8 · 760	0'540 0'557 0'555 0'555	7 : 663 7 : 676 0 7 : 663 98 7 : 677	6 9n2937 6 9'8565 0 0n0006 3 0n1294
429 429 429 430	8 597	X	25 21 15	193		3 21	51'	4 62.2 1 235.6		5 23 62 7 23 62	20 169 15 19 351 8	14'07 59 168'83 13 353'26 52 175'26	9 0'74	48 9.70	33 8.753 30 8.705 36 8.75 59 8.71	55 0'560 52 0'54	50 7.662 17 7.676	8 0.0170 9 9n8453

														(	Contr	ılitä	t		
Nr.	μ	γ	$\log n$	G	K	$\log \sin g$	$\log \sin k$	log	log	log sin δ'	log cos ô'	N'	bei⊙ ga		im Mi	ttag	bei Unter	O gang	F
		·				sing	811176	$\cos g$	cosk	SILO	COSO		<u> </u>	φ	λ   * r = ε	φ	λ	φ	
															x 1 0				
		+1.3280											170	-L 58	( TO)	— (+86)	02		$p_{p}$
4253	141.85	-0'6936 -0'1792	9.4613	233.66	86 . 68	9'5335	9.9916	9.9731	9n2884	9114486	9 * 9822	101'7		зх	146	— бі	48	- 52	t
4255	335.82	-0.0102	9.7394	221.07	86.76	9.2155	9.9870	919753	gn3818	9113467	9.9890	104'3	- 35	- - x3	+ 24	13	+ 90	r5	2***
4257	69.93	-0.2867 +0.222	9.7132	207.77	87 42	9.2017	9'9826	9.9770	914433	9n1878	9.9948	rog.3	-123			26 40	1	20 30	1
4259	66'45	+1:2777 -1:2835	9.7636	24'83	87.58	9'5031	9.9812	9 ' 9 7 6 8	9.4567	9'1453	9.9957	73.2	l —			_			$p \mid p$
		-1.5280	i					.											P
4262	181'64	十1	9'7552	337 04	92.23	9'4982	9'9812	9'9773	9.4587	921083	9'9964	73.1	- -II2				-123 +178		
4264	348.86	-0'1174 +0'0283	9.7292	324 04	93'05	9.2093	9'9852	9.9760	9 • 4089	9n2935	9'9914	74 8	56	21	+ 12	18	+ 72	· - 8	7,5\$
4266	44 88	o·8590	7063	310.06	93.36	9.5261	9.9899	9'9740	9:3275	914150	g•g848	77.3	158	67	- 39	- 77	1 45	44	
4268	126.81	+0 7497 9	9'7127	264 95	89.20	9.6000	9 ' 9997	9'9625	815071	9n5986	9'9628	92.0			+ 75 —	+ 67	 	+ 36	p
		-1.0810																	p p
4271	176 71	+1 · 4937 9	7564	109.74	92'46 87'19	9·5624	9'997I	9'9690	9n0633	9'5394	9'9723 0'0522	97'I		+ 47		23	-165	- 35	2) }*#
4273 4274	51'14 51'14	0'3375 9	7185	67.59	86 · 29 85 · 37	9.6351 9.6367	9 · 9952 9 · 9922	9 '9572 9 '9552	9 ' 1708 9n2737	9°5983 9≈5895	9 ' 9629 9 ' 9644	101.8	+125 110	25 + 11	+178 51	+ 3 - 22	-125 + 17	10	1.182 1.181
4275	216.42	+0'4377	7041	57.13	84 69	9.6421	9 9893	9537	9'3430	9.5789	9.9663	76.3	<b>-</b> ⊢ 76	+ 11	- -140	+ 49	136	- - 36	yelli 
4277	233.91-	-0.6550 g +1.1837 g	7129	47.41	83 62	9'6543	9 98 15	9507	9 4566	9:5425	9'9719	72'2		- 23	+ 68 -	- 64 	173 	51	p
4279	x36'08 -	+1 · 4387 g -1 · 3683 g -0 · 7692 g	7457	222.17	83'34	9'6589	9 9766	9'9494	925045	925121	9'9757	109'7	*******		178	52	-123	- 22	$\begin{bmatrix} p \\ p \\ t \end{bmatrix}$
4281		+0.7814	ŀ																
4282 4283	66.60 - 354.13	-0.0213 g	7659 7659	8 24	87 · 48	g ' 6880 g ' 6gog	9'9428 9'9402	9'9410 9'9402	9 ' 6821 9 n 6908	8 · 9022 8 · 1417	o ' o o o o	61'1	128 54	- 30 - 34	66 7	+ 3	- o - 67	+ 28	tili 1 st
4284	314'23	-0.2000 -0.6423	7596	o'86	89.73	g ' 6883	9'9410	9'9410	9'6883	7.9252	0'0000	60'8	~~ <u>2</u> .б	+ 15	+ 36	-I- 54	+119 + 30	+ 74 - 69	t:
4286	300.03	-1 .3320	7214	331'14	96.49	9.6743	9 . 0630	9 9451	9 6026	923988	9.9829	65 6	_	******					p
4288	39 77	+1:4810 g +1:2785 g -1:3253 g	7603	142'99	96.77	9'6647	9 9713	9 ' 9480	925466	9 4759	9.9797	III. 6		processed participal	\$11.00 PM	Annual services	Arresta		$\frac{p}{p}$
4290	327:15	-0.6662	7032	322.07	96.88	9.6667	9 9474	9 9423	9'5422	914865	9.9786	68 5	66	58	+ 41	- 64	+107	19	p P
4292	3 ro n2 -	+0.5469 g	7084	312.11	90'37	9 6547	9.9818	9,9505	9'4526	925459	9'9714	72'4	- 25	- I5	<del>  -  </del> 41	IO	H - 05	14 18	t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1
4293	25.25	+0.2182 c	7326	125 · 13	95'59 95'11	9 6447 9 6397	9.0001	9:9530 9:9541	913721	9'5718	9'9575	76.8	+124 - 82	- - Q	-172	IC	II7	- 24 + 52	l !"
4295	325 43	-1 0014 9	7239	114 93	94'11	9'6299	9 9939	9.9564	92183	9 5946	9.9636	100,4	0	- 62			(+ 22	(-67	(1)
4297	199 23 -	-1'3470 g +1'3523 g +1'0400 g	757312	290'27	93 35	0'6230	0.0060	0'0578	017252	0.,6000	0'0525	81.6	l —			_			p p
4299	273`24 -	+0.3240 c	1.4004 3	240'44	87 27	9 5529	0:0060	0'0703	001205	OFFICE	0.0748	08'0	-L 2	— 34 -1 5	+ 84	- 64	-178 -115	- 49 + 23	
										3 (H3-9	3 3113				1 ^/3	38	1 223	4.5	
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Nr.			T		$oldsymbol{L}'$	Z	ε	P	$Q_{i}$	$\log p$	$egin{array}{c} \log \ \Delta L \end{array}$	$\log q$	u'a	$\log f_a$	logγ
		nischer ender	Julian. Tag	Welt- Zeit											
4301	598	XI 4	1939 78		224°798			359°768		0.2140	9'7357	8.7348	0.5544		8n3201
4302 4303 4304 4305	599 599 600 600	IV 30 X 25 III 20 IV 19	1939 96 1940 14 1940 28 1940 31	0 29'2	213.662	-1.27 -3.69 +1.70 -0.72	23.617 23.617	7.512 164.584	183'430 9'164 164'367 193'418	o.2360 o.2360	9.7434 9.7098 9.7645 9.7624	8.7398 8.7136 8.7579	0.5432 0.5690 0.5339 0.5333	7.6640 7.6753 7.6683 7.6650	9,7140 9.8512 0.1206 0,0877
4306 4307	боо бог	III 10	1940 49 1940 64	8 19 8	202.337 352.160	+2.62	23.617	,	174'640	0.4012		8.7488	0.2412	7.6741 7.6697	0.1201 0.8045
4308 4309 4310	бо1 бо2 бо2 V	II 27	1940 99	3 10 52 8 5 19 24 0 2 22 48 0	341.210	4-3'4x	23.617	180,018	348'944 183'237 357'854	0.7245	9'7286 9'7257 9'7541	8.7256	0.5546 0.5572 0.5393	7.6692 7.6678	9n8997 8n9275 8n3958
4311 4312 4313	боз боз \ бо4	/III x2		23 3 1		+0.62	23.918	8'165	189.672 8.306 162.416	0.6899	9.7036 9.7644 9.7120	8'7602	0.5710 0.5328 0.5684	7.6665	9,9198 9,8401 0,1678
43 ¹ 4 43 ¹ 5	бо4	II 5	1941 70	2 22 21 5	319'228	+4'16	23'618	196.039	195.073	0.4423	9.7030	8.4081	0.2421	7.6737	on 1816 on 0641
4316 4317 4318	бо4		1941 88 1942 02	9 11 2'8	130'778 278'012 92'193	- -x ·34	23.019	171.934	169'521			8.7375	0'5533	7.677x	0'1571 9'8572 9n6259
4319 4320	605	XII 16 VI 11	1942 38	4 0 12'1	267.107 81.262	0.01	23.619	179.854	357°392 178°614 3°747	0'6924	9'7598	1	0.2412		8'0966 9'5422
4321 4322 4323	бот	XII 5 V 31 X 26		8 15 59's 5 10 18's		-x.33	23'620	11.677	188 651 0 978 166 246	0.7367	9'7123	8.7590 8.7275	0.2603	7.6626	928150 0'0408 0'1641
4324 4325	607	XI 25 IV 20	1943 09 1943 24	3 5 44'0	245 424	1	23.620	195 592	197 956	0.7088	9'7422		0'5514	7.6773	0n1363 9n9187
4325 4327 4328	609	X 14 IV 10				-0'04	23.621	359.080	172 703 358 658 178 101	0.6899	9.7641	8.7595	0.5714	7.6659	9.9079 8,8892 9.0514
4329 4330	бто	III 30 IX 22	1943 94	9 17 4.6	i ii.dri	o.82	23.621	7'584	1 '	0'6967	9.7567	8.7526	0.5375	7.6671	9.8151
4331 4332 4333		III 20	1944 30		1'460	+1.81	23.623	16.056	347 28 <u>0</u> 3 18 450 7 162 925	0.7188	9'7324	8.7305	0.225	7.6724 7.6685 7.6666	0'1587
4334 4335	611	IX 12	1944 48	0 7 48.	171.088	-1.58	23.62	194'747	192.580	0.7037	9'7491	8.7456		7 6704	021075
4336 4337 4338	біз	VIII 2 I 26	1944 98	5 15 12 2 2 17 24 0 6 48 0	309 781	+3'97	23.620	0'11	358 64; 183 72	3 0'7388	9'7072	8.711	2 0.2402	7 6747	8.0277
4339 4340	614	I 15 VII 12	1945 33	6 22 23 4 4 16 44	3 298 635	+3.38	23'618	7 82	5.36	8 0.717	9'732	8.731	4 0.5562	7 6758	9.8499
4341 4342 4343	615	XII 6 I 5 VI 2	1945 69	1 10 22	2 287 73	+2'4x	23 61	15 80	343°31 3 14 08 5 167 80	0 695	8 9.756	8 753		7.6766	0.1289
4343 4344 4345	615	Secretary and	1946 01	5 14 42'		2 -2 31	23.01	351 77		0 0 694	5 9 757	8 755	4 0 542	4 7.6773	928480
4345 4347 4348	617	XI 15 V 10 XI 4	1946 54	7 16 32		- 1 55	23'61	7.5	8 182 66	6 0.708	5 9.745		1 0.241	9 7'6633	9n6483
4349 4349 4350	618	IV 1 IV 30	1946 87	3 0 17'		3 -1.78 +0.43	23.61		9 8 93 7 163 91 9 192 79	7 0:690	1 9.764	4 8:760	7 0.570 2 0.533 4 0.532	3 7.667	0 1364
															Special section

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Nr.	μ	γ	$\log n$	G	K	log	log	log	log	log	log	N'	_	Auf- ng	īi	ittag	bei	i 💽	751
	"	′	108/		2.	$\sin g$	sin k	cosg	$\cos k$	$\sin \delta'$	cos o'	1.4	λ	μ	λ	φ	λ	rgang   φ	$I^{n}$
City													r	(	r :	ı d	e		
4301	102°18	0.0209	9.7379	234°11	86°70	9 5333	9.9918	9'9731	9n 2834	9n4507	g'g820	10105	162	+ 10	ro2	18	<b>–</b> 36	- 12	p*
4302	188 94	十0,2000	9'7455	49.83	86.46	9'5277 9'5154	9.9902	919738 919753	9.3216	9'4214 023464	9'9843 0'0800	77'4	12 +-122	42	1 + 11	m 77	-I-TOR	x8	t
4304	00 47	1.33200	10.2002	3.00	89.07	9 4939	9 9 7 7 9	9'9778	9'4932	8.2484	0.0000	71.0							$p \\ p$
4306	187'46	+1.4130	9.7023	207.33	87.43	9.2026	9,9823	9:9768	9 <b>24461</b>	911826	9'9949	106'4				_			p
4307 4308	304.02	-0.2938	9.7541	350'33 157'68	91.00	9 ' 4909 9 ' 4988	0,0810	9.9781	9'4841 924615	827375	9'9994	72'2 107'0	I2 54	35	1 7	40	-t- 60	-	$t^{: i }$
4310	161.91	-0'0846 -0'0249	9.7279	337.20	03.05 03.50	9.4968 9.2091	9.0813	9 9775 9 9761	9 · 4580 9 · 4136	9n 1040 9 ' 2846	9.9918	73.3	-172 +132	- 21 + 14	-107 -162	12 10	47 102	+ 12 16	i. I
4311	159.38	0'8314	9 ' 7057	323 ' 90 !	93.06	9.2092	9 ' 9852	9.9759	9 * 4 0 8 2	912952	9.9 <u>5</u> 13	74'9	+ 97	- 68				- 40	
4313	248.13	+0:5920 +1:4717 -1:5190	9'7140	277 07 9	91'02	9 5807	a agaabi	a *a66oi	8 . 6377	0 9 5 7 7 0	a 'afifici	87'3	*****	54 	42	- <del></del>	+ 34	+ 30 	p
4315	158.13	-1,1230	9 7432	89.67	89.95	9.5921	0.0000	9 9730	7.3131	9.5921	9 9640	77 3 89 9		Winds a			Print Name		$\stackrel{p}{p}$
4316 4317	289 · 80 346 · 29 -	+1'4357 +0'7198	9 7551	121 64 9 264 68	93'24 9 89'16	9'5443	9 9932	9.9715	9n2431	9.4819	9 9 9 7 9 0	100,0	10						p
4310	203 50	-0.4226 +0.0125	9.4141	78.27	88.00	0.0101	9.9987	9.0000	8 8803	9'6024	0.0621	8512	+ 25	27	78	Y	T 32	- r8	
4320	311.20	+0.3482	9.7040	67.29	86.24	9.6271	9.9920	9:9570	9.1767	9.2980	9.9629	80.0	18	+ 10	+ 47	+ 44	+123	+ 27	2.14
4322	334 77	-0.6531 +1.0985	9 7 1 4 4	57'10'6	34 70 0	0.0410	9 9893 (	3 ' 0 5 3 8	0,3430	0'5789	0'0664	76 2	*****	- 27	- 63	- 65	+ 38	47	p   t
4324	00 08 - 264 92 -	-1 4590 -1 3687	9'7297 2 9'7441 2	32.32	33.78	9'6761	9 ' 9593   9 ' 9858	9'9447	926168 924010	923652 025616	9'988o 0'0601	115'2			ptoto-d	Modes IN	Marine Marine		$\stackrel{r}{p}$
4325	306.21-	-0'8292	9.7522	23.89	84 08	9.6779	9.9566	9440	9.6287	9,3311	9.9897	64'2	+ 34	75	+ 64	<b>∸</b> 55	+121	29	
404/1	.03 -1	+0.8090 -0.0775	9 7002	10 04 0	3 47K	3.00471	0 048510	3.0451	0.0024	ומאלדים	0'00501	02 ' 31		99		1	7 Y /7	L. 00	V:11
4329	73.62	+0.6533	9.7588	8.57	37 40 0	9.0892	9 9429	9'9407	926819 916806	8,9515	9 ' 9 9 8 3	61.5	165	+ 35	106	2	45	22	7 til
4330	43 94	0024	9 /241	101 29	9 39 9	9 0090	9 9400	9.9400	926897	82 1016	0,0000	119.3	× 47	8	-155	- 44	- 77	- 66	11.
4332 2	402 23 -	-1'3633 -1'4410	9 7343	1.02	39.08	9 0858	9 9418	0'0418	0:6857	8 10000	0.0000	61 'O			Publicate	_			p
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4335	82 08 -	o · og2o	9.4030	331,13	55 9	9.6759	9.9617	9.9446	9.6039	91:4008	9.9857	65'5	+176	1	73	64			r'
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		9329	, , , , , ,	25 15	30 30 5	9 0442	9-9870	9 9531	9n3720	9.5713	9.9676	104.7	-120	49	- 75	- 52	бі	67	r
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43	_	VIII :	30 1 24 1 22 1 18 1	1950 1950 1951 1951	889 036 065 214	13 6 15	55 7 11 4	343 12' 152' 181' 332'	995 959 931	+0.8 +0.0 -2.1 +3.8	3 2 5 2 1 2 8 2	3.63 3.63	8 19	63 '7 94 '3 52 '4	50 50 62	62.42	29 0	*7314 *7202 *6932 *702 *744	9.73 9.76 9.75 9.75	08 8 · 8 · 03 8 · 8 · 8 ·	7290 7558 7471 7059	0.22	22 7° 36 7° 26 7°	6672 6679 6718 6724	9118598
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4351	303°87	+1'3920	9.7024	220°55	86°75	9'5162	9 ' 9867	9'9752	9n3861	923431	9.0892	104°4			17 + 9 +	_ p
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4355	281'70	-0.0212	9 7572	157.85	92 15	9 4970	9.9811	9 9774	914603	9 . 0926	9.9966	106.0	+ 13 + 1	3 + 78 +	3 +139 -	21 114
4357	165'50	-0.403	9.7663	145'47	93.01	9'5095	9'9846	9.9760	9n4174	9'2790	9.9920	105'4	+109 + 5	8 + 95 - 9 4 - 161 + .	- II I I I I I I I	36 r 24 t* - p
4359	265.38	+1'4793 -1'4883 -1'2345	9'7060	323 73	93'10	9'5118	g'g85I	9'9757	9'4095	922993	9,9915	74.8			_   _	$ \begin{vmatrix} p \\ p \\ p \end{vmatrix}$
4361	44.62	+1:3827	0'7536	133'80	03'43	0'5273	g·g886	9.9737	923534	9.3979	9'9859	103.2				_   p
4362 4363	23.06	+0.7227	9'7422	276 80 80 34	80,00	9'5805	9'9997	gʻ9661 gʻ9640	7.6140	925778	9 9640	89.4	-105 + 4 $-75 - 2$	0 -x15 + 8 - 23 - 3 + 45 -	7 + 29 -	44 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
4365	46:86	+0.525	9.7038	77.92	88 04	0.2330	9.9987	9 9605	8.8933	9,6024	9.9621	85.1	-112 +	9 - 48 +	39 23	
4367	71'45	+1.0115	9.7157	67:27	86 24	9.6269	9.9950	9'957x	9.1770	9 5977	, la , a gac	80.0	+ 83 - 3	+166 -	65 — 98 —	$\begin{array}{c c} 4^2 & t \\ p & \end{array}$
4368 4369	184.67 33.91	+1'4740	9.7282	215 29	83.20	9.6675	9.9693	9 9479	9n5601	9n4531	19.9808 39.9642	101'2	3		6x + 6 -	$ \begin{bmatrix} p \\ p \\ t \end{bmatrix}$
			]	1						1		1		74 + 137 +		- 1
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4374 4375	190.95 264.90	+0.5986 -0.5696	9.7578 9.7255	180.13	85.41	9.6883	9'9499	9.9424	9,681	82945	9 9 9 9 8 3	118.	3 28	9 -1-161 -1- 6 -1- 86	46 172	63 7
4376 4377	174 55	-1.4022 +1.3940	9.7189	347 . 81	93'58	9.6856	9.9456	9'9418	9.672	7 gn 065	4 9 ' 99 <i>7</i> 9	61.				$- \mid p \mid$
4378 4379	274 · 88 57 · 84	+1.3800	9.7620	181'4	95'22	9.6790	9 9529	9'943	9n645 $9n687$	$09.259 \\ 58n136$	8 9 9 9 9 2 °	1119.	I	-     -	65 -123 -	- $p$ $p$ $r$
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4384	274.84	+0.6922	9 7359	321'6	5 96 8	19.665	9 972	59'947	8 9 ' 538	2 9n488	79'978	4 68	7 + 22 +	2x + 78 + 38 -179 -	30 +122 -	- 60 <i>1</i> °°
		-1.3486 +1.3356														$ \begin{vmatrix} p \\ p \end{vmatrix}$
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		6 +0·4±7;										1	2 -102 +			1 24 m
4392	17713	7 -0.030; 2 -0.369; 1 +0.689;	9 748	73.7	587.9	19'564	5 9 998	0 9 9 9 6 8	68.98	2 9 549	1 9'970	9 84	9 - 58 + 1 +128 - 1 -116 +		23 + 68 - 1 - 118 - 25 - 15 -	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
4394	305 '49	+1.423	9 766	28.8	887.2	7 9 507	9 9 982	5 9 976	12 9 444	4 9 209	8 9 994	2 73	6			$\begin{vmatrix} z \\ z \end{vmatrix}$
4396	61.8	9 +x · 376	9.702	233.5	6 86 6	7 9 533	4 9 . 99 1	6 9 973	9128	94 92448	30 9 982	2 101	7 -			-   p
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4400	43.6	8-0.111	9:758	2 171.1	3 90.0	2 9:490	19:978	8 9 978	9,48	44 8 69	97 9 999	5 107	8 -108 +	11 - 45	4 + 19	- 24 t

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Nr	Jı	ulianisch Kalende		Julia Ta			Velt- Zeit	. 1	S <b>*</b> -	2		ε		P		Q	10	$\log p$	$\log \Delta L$	log	$q \mid u_a'$	$\log f$	logy
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4416 4417 4418 4419 4420	645 645 646 646	X 2 IV 2 X 1	5 1 1 4 1	957 2	96 I	5 4 10 2 8 2 3 3	5 · 4 7 · 5 6 · 8	43.4 214.9 33.7 203.7	254	—1 · 3: —3 · 7: —0 · 8: —3 · 4:4	2 2 2 2 2 2 2 2	3, Q16 3, Q16 3, Q16	5 350 5 178 5 185	7 · 58; 8 · 32; 5 · 204 5 · 9 : 8	7 3. 1 1. 4 18	72 · 137 57 · 452 77 · 381 8 · 054 33 · 608	0.6	899 417 993	9.7029 9.7646 9.7027 9.7545 9.7247	8.7597	0'5374	7.6639 7.6639	913121
4422 4423 4424 4425	647 647 647 648	IX X II 2	0 1 4 1 4 1 9 1	957 79	74 2 21 1 51 99	4 0 0 1: 8 3;	6.7	63 · 7 92 · 9 142 · 9	44 01 02	0.6g 2.86  -3.30	2, 2, 2,	3.016 3.016	163	'802   '164   '007	16	46 · 299 2 · 163 2 · 007 1 · 987 2 · 240	0.23	27	9'7294 9'7607 9'7515	8.7569	0'5523	7.6693 7.6690	0n1612 0'1272 0'1526 0n0836 9n8832
4427 4428 4429 4430	649 649 650 650	VIII 13 II 6 VIII 3	7   19 3   19 5   19 8   19	58 68	53 30 2: 57 14 35	8 54 4 44 4 57 5 33	1 · 1 · 3 7 · 0 · 3 3 · 7 · 1	3x 7 43 0 20 7 32 5	45 - 80 - 59 - 54 -	-0 58 -4 11 -0 90	23 23 23	3 615 3 614 3 614	359 180 7 188	'549 '023 '462 '461	35 18	2*546 7*907 2*394 4*991 0*446	0.69 0.73 0.70 0.73	95 53 23	9 7 7 9 7 9 7 7 4 3 2 9 7 3 5 3 9 7 1 6 7	8.7172	0.5674	7.6679 7.6724 7.6666 7.6736 7.6655	9.8580 8n6308 7n3110 9.8267 9n8979
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147 6 148 6 149 6	57 58	II 8	196	io 928 ii 106 ii 283 ii 431 ii 460	15	19	7 17	2 ' 9 I ( 3 ' 2 3 ( 2 ' 3 8 )	5 + 2	44	23	60g	187 ·	294 538	187 7	935	0 1696 0 1743 0 1690 0 1732 0 1740	6 g 0 g 1 g	7023 7637 7162	8 · 7 5 0 2 8 · 7 1 8 1	0.5693 0.5353 0.5643	7 6705	9n 1577 9n 8450 9 '7443 0 '1790 0n 1483

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4402	286.67	-0.7518 -0.5943	9'7661	158.41	92.13	9'4976	9.9809	9'9774	gn4628	9'0827	9'9968	107'0	-100 - 5	66 - - 53	- 15 + 78		- - 50 - - 145	31 19	rafa
4403 4404	18.30	+1.4923	0.4040 0.4164	302.04 336.81	93.24 92.26	9'5421 9'4993	9.9815	9'9718 9'9772	9'2462 9'4590	9n4779	9'9794 9'9963	79'3			********		_	Married W	p
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4407	240'54	+1:3343 +0:7293 -0:5880	9'7437	289.18	92.38	9'5605	9 9973	9'9693	9'0495	925387	9.9724	83'I			I	1	-1-166 74	+ 49	
4409	85.08	+0.1251 +0.0502	9.7633	276.94	00,00	9.5797	9,9996	9,8661	8.6286	925770	9.9666	87'4	-151	— т	86	2I			t st
4411	323'52	-0'650I	9'7624	265'43	89 28	9. 5989	9 9998	9.9628	814630	925977	9 9630				+ 36		+127		
4413	309,80	+0'9254 +1'4847 -1'3727	9.7267	224'95	83'46	9'6567	9'9792	9'9500	92480I	925294	9:9736	108.7 96.4		+ 55	(+- 7)	(- -88)	- 40	61 	2) 2)
4415	170.38	-o.3610	9 7551	41.52	83 28	9.6605	9.9756	9.9489	9,2130	9.2071	9.9763	69.9	(151)	( <del></del> 71)	1		111	50	
4417	57.50	+0'8464 0'2051	9.7667	32.21	83'26	9.6713	9.9661	9'9461	9 5803	9'4385	9,9830	66 17	111	34	- 55	-h 3	+ 69 + 11		1
4419	306.78	+0'1608 +0'5381 -0'5437	9 ' 7566	24.45	83.88	9.6781	9'9572	9.9441	9.6266	9.3403	9,9893	64.3	16	1-1- 7	+ 47	+ 49	+141		1240
		-1.4493												5	- 34	- 47	56	59	
4422 4423	35 · 84	+1.3403 +1.4210	9°73¤4 9°7626	168,12	85 41 93 43	9.6814 9.6831	9'9497 9'9461	9°9430 9°9426	9.6575 9.6711	9 1905	9'9947	62.6		*******	*******	******		participal (	$\frac{p}{p}$
4424	182'85	-1.5155 -0.2645	9.7535	189'30	87.20	9'6862	9'9439	9'9417	926788	829515	0,0083	118'6	******	75	6 ₅	67	+126	- 21	.21
4425	285 08 300 76	+0'7212 -0'0427	9'7642	160.20	95'21	9.6819	9'9518	9'9429	9n6494	9 2534	9'9929	117.0	28	+ 70	+ 84	+ 64	+151	+ 19	(s)
4428 4429	38'30	-0.0050	9'7453 9'7374	330.79	96.38 96.38	9.6763 9.6748	9'9623 9'9623	9'9445 9'9450	926117	9,3814	919870	65.6	+145 103	+ 24	-146	- X4	80		$t^{*\mu}$
4430	275 29	0.4902	9.7188	143.99	96.83	9.6674	9.9700	9'9471	925555	9 4699	9.9802	112.1	+ 22	- 29	+ 76				
4432	228.77	-1'3507 -1'3213	9.7604	321 64	96.79	9.6640	9'9727	9'9481	9 5368	924871	0.0785	68.8				****	Married Log	######################################	$\frac{p}{p}$
4434	305.57	-1.2064 -1.2064 +1.5064	9.7040	134.20	96.49	9.6557	9'9798	9 9503	924746	9 5310	0.0733	108'5	 46	45	E4	60	+142	26	$\binom{p}{t}$
	:	+0:4987																	
4437 4438	285.49 285.49	-0.0328	9 °7503	85.31 821.00	80.31	9.5836 9.5836	9,0000	9.9637	8.0271	915936	9 · 9637	88.3	十 173 十 17	- 2 - 17	- I23 十 74	25 - - 5	61 133	I4	神
4439 4440	62.18	+1.4840	9.7659 9.7659	41.38 41.38	88 · 54 86 · 66	9.5734	9.9868 9.868	9'9673 9'9746	8n 8065 9 3848	9.3552 9.3552	9.9683 9.9885	94.0		+ 43	+170 		-140		p p
444I 4442	164'97 180'86	-1.0197	9.7659	73 86	87.91	9.5657	9'9980	9'9684	8:9803	9.5505	9'9707	84.1							p
4443 4444	297 73 342 83	+0.2995	9 7503 9 7351	197 65	87.28	9.5042	9'9831	9'9766	9.4372	820081	9'9949	73.9	- 19 - 66	- 45	+ 55 + o	- - 66 75	+160 +125		
4445	88.87	-1-0.0591	9.7238	17.01	88.30	9:4927	9.0801	9'9779	9:4713	8.9789	9,9980	72.7	-149	- 14	89	+ g	- 25	- - 2I	21111
4447	130.31	-0'1438	9 7045	3.02	189.02	914877	1919786	9'9785	19:4867	/ 8 * 3080	la 'aaaa	72'1	1-1-163	62	-124	AE	- 62	- 27	2'
4449	247'46	+0.2220 +1.2100 -1.4020	9.7x82	314'82	93.40	9 5249	9889	9'9741	913596	92.3882	9866	76 :		+ 5x	45	+ 38	+ 19	16	p
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•	N	ſr	Julianis Kalene	cher der	T	ian. ag		Volt- Zeit	L	,	Z		ε	P		Q	logį	$\frac{1}{\Delta L}$	$\log q$	u'a	logf	logy
	44 44 44 44 44	52 6 53 6 54 6	59 VI		1961 1961 1961 1962	785 963	12	34.7 53.1	311,	791 424 557	+4.0	3   23 0   23 7   23	. gad . god . god	14'8	58 34	17.070	0.708	9 7489 9 7439 7 9 7105	8.7454 8.7412 8.7124	0 5430 0 5493 0 5621	7.669	0'1114 9'8693 9n8235
	445 445 445 446	57 6 58 6 59 6	51 XII	27 27 27	1962 1962 1962 1962 1962	494 671 819	18 6 16	35'0 13'5	112 · 8 289 · 9 102 · 9 248 · 8 279 · 6	56 25	+2.62 +0.30	23	612	187.26	57 1 38 18 1	0.691 (88.821 7.050 (65.900	0'7449 0'6928 0'7333 0'7252 0'7126	9 7596 9 7161 9 7233	8 · 7056 8 · 7572 8 · 7164 8 · 7243	0.5667 0.5409 0.5581 0.5624	7.6637 7.6765 7.6631 7.6773	8'9427 9'8102 9'9249 0'1741
	446 446 446 446 446	2 66 3 66 4 66 5 66	3 XI 3 XI 4 V	16 12 5 1	1962 1963 1963 1963 1963	173 350 527 705	19 23 18 2 15 5	22'3 57'9	237 4 53 7 226 0 43 6	81 52 23 56	-1.54 -3.61 -1.32	23 23 23 23	613 613 613	W 10	2 1 5 3 9 1 2	71'923 56'786 77'122 7'373	0.6998 0.7422 0.6899 0.7412 0.7004	9'7023 9'7647 9'7034	8.7079 8.7596	0'5364 0'5743 0'5310 0'5732 0'5377	7 · 6769 7 · 6632 7 · 6763	0n0133 9'9332 9n4393 9'2458 9'6745
	446 446 446 447	7 66 8 66 9 66 9 66	5 III 5 IV 5 IX 5 X	14	1964 1964 1964	060 206 236	3 5 22 1 8 3	7 · 2 5 · 6 6 · 4	33°3 174°5 203°9	36 - 65 -	-0 83 -1 53 -3 44	23	613 613	185 · 72 343 · 81 14 · 07 162 · 69 193 · 77	7 3 6 1 9 1 8 1	45'678 16'412 61'657 91'805	0'7230 0'7340 0'7233 0'6921 0'6999	9'7144 9'7278 9'7613	8 · 7262 8 · 7155 8 · 7261 8 · 7575 8 · 7496	0.5597 0.5622 0.5525 0.5368 0.5439	7.6753 7.6683 7.6649 7.6706 7.6742	9n7200 0n1772 0'1073 0'1635 0n0747
	4473 4474 4475 4476	666 667 668	5 IX 7 II 7 VIII 8 II	28 1 25 1 17 1	1964 1964 1964 1965	738 916 092	14 5 16 2 5 2 23	3.5 7.7 0.8 3.7	353'70 164'17 342'62 153'75 331'75	71 - 29 + 56 + 10 +	-3.80 -0.01 -3.31 -0.45	33. 33. 33.	613 613 613	351'55: 170'986 359'159 179'411 7'177	35	72'123   57'433 31'812 4'705	0'7445 0'6919 0'7361 0'7106 0'7141	9'7008 9'7614 9'7110 9'7416 9'7370	8 · 7055 8 · 7574 8 · 7134 8 · 7385 8 · 7349	0.5709 0.5360 0.5655 0.5464 0.5516	7.6696 7.6693 7.6709 7.6679 7.6724	9n9092 9'8851 8n9006 8'7205 9'8087
	4477 4478 4479 4480	669 669	VIII	8 1 3 1 2 1	965 4 965 5 965 6	147 I 194 2 524 I	1 4: 12 10 13 28 15 22	2 · 5   2   3   3   3   3   3   3   3   3   3	143'14 291'31 321'03 103'86	3 + 8 + 4 + 0 +	2'74 4'12 0'40 0'90	23 23 23	612 612 612	187·758 343·816 15·349 165·501 195·672	34 1 16 19	3'503 3'894 4'726 5'881	0.7334 0.6890 0.6935 0.7433 0.7447	9'7152 9'7636 9'7592 9'7038 9'7014	8.7162 8.7609 8.7559 8.7068 8.7053	0'5607 0'5386 0'5397 0'5652 0'5680	7.6666 7.6765 7.6736 7.663x 7.6655	9n8616 0n1322 0'1143 0'1399 0n1742
	4482 4483 4484 4485 4486	670 671 671	VI XII	7 1	965 9 966 1 966 3 966 4	27 03 81	4 4 I 4 I 5	7 2	69:56 83:02 58:27	7 + 0 - 6 -	0.32 0.42 1.13	23·6 23·6	511 509 509	773 743 359 617 182 449 7 154	18	2.014 0.265 8.444	0.6972 0.7275 0.7197 0.7043 0.7398	9'7549 9'7233 9'7298 9'7496 9'7054	8 · 7223 8 · 7298 8 · 7454	0'5538 0'5586 0'5390	7.6771 7.6627 7.6774 7.6625 7.6775	9n8542 9'7627 8n5426 9n3329 9'8329
4	4487 4488 4489 1490	673 674 674	IV X	25   19 22   19 15   19 12   19	966 8. 966 9.	35 83 15 59 18 38	8 9 5 12 8 41 1 8	0 2	- T ,J = 3	5 - 6	2:34 0:92 3:51 0:18	23 · 6 23 · 6 23 · 6	07 3	91'183 14'240 (70'179 149'910 (78'694	17: 34: 18:	3 620 6 2 434 6 7 485 6 0 819 6	0'7436 0'7067 0'7167 0'7298	9'7007 9'7470 9'7344	8 · 7071 8 · 7433 8 · 7334	0'5755 0'5417 0'5542	7.6773 7.6649 7.6743	9n9763 0'1324 9'9365 9n9582 9'0854
4	492 493 494 495 496	675 676 676	VIII 1	1 19 24 19 29 19 20 19 5 19	67 69 67 86 68 01 68 04	58 29 6 12 16 4	37 18 15	'8 18 '1 33	34 · 118 33 · 33 1 2 · 62 3	-3 +3 +1	1.27	23 6 23 6 23 6	07 I 07 I	58.031 86.669 6.152 63.373 94.349	16:	7 194   0 5 814   0 1 307   0 2 978   0	7441 76903 77310 77401	9 7021 9 7631 9 7178	8 7065 8 7601 8 7192	0.2627	7.6719 7.6719	9n2294 9n8068 9'7182 0'1856 0n1322
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		Jender		Tag	5	<i>7</i> 10	eit	·									<u>, , , , , , , , , , , , , , , , , , , </u>			
4451 4452 4453 4454 4455	658 658 659 659 660	558 IX 3 1961 638 6 559 I 28 1961 785 13 559 VII 25 1961 963 3 560 I 18 1962 140					46'9 34'7 53'1	162.7 311.4 123.5	91 24 57	-0'63 +4'00 +0'97	23. 23.	609 609	14'858 171'634 352'966	17.079 169.275	0'7043 0'7086 0'7377	9.7360 9.7489 9.7431 9.7105 9.7617	8 · 7333 8 · 7454 8 · 7412 8 · 7124 8 · 7591	0.5484 0.5430 0.5493 0.5621 0.5393	7.6656 7.6691 7.6746 7.6646 7.6757	0n1384 0'1114 9'8693 9n8235 8'4660
4456 4457 4458 4459 4460	661 661 661 661	560 I 18 1962 140 2 4 560 VII 13 1962 317 4 561 I 6 1962 494 18 1 561 VII 2 1962 671 6 561 XI 27 1962 819 16					36'3 13'5 35'0	289 '9 102 '1 248 '8	31 56 325	+0.75 +2.62 +0.30 -2.14 +1.43	23. 23.	612 612	8 988 163 598	188.821	0.7333	9.7017 9.7596 9.7161 9.7233 9.7379	8.7056 8.7572 8.7164 8.7243 8.7367	0'5667 0'5409 0'558x 0'5624 0'5537	7.6637 7.6765 7.6631 7.6773 7.6771	8'9427 9n8102 9'9249 0'1741 0n1379
4461 4462 4463 4464 4465	662 662 663 663 664	XI I	6 2 5		173 350 527	19 23 18 2	9.8	237 7 53 7 226 0	181 752 923	-1.50 -3.07 -1.54 -3.61 -1.32	23. 23.	б13 б13	356.462	346 · 159 171 · 923 356 · 786 177 · 122 7 · 373	0'7422	9'7544 9'7023 9'7647 9'7034 9'7533	8 · 7495 8 · 7079 8 · 7596 8 · 7088 8 · 7489	0'5364 0'5743 0'5310 0'5732 0'5377	7.6628 7.6769 7.6632 7.6763 7.6639	onox33 9'9332 9n4393 9'2458 9'6745
4466 4467 4468 4469 4470	665 665	III 2 IV 2	2 I 4	1963 1964 1964 1964 1964	030 060 206	3 5	27:3 57:2 15:6	33°3 174°3	565 336 565	-3.72 +1.52 -0.83 -1.53	23 · 23 ·	613 613	343'817 14'076 162'699	183'385 345'678 16'412 161'657 191'805	0'7233	9'7259 9'7144 9'7278 9'7613 9'7526	8 · 7262 8 · 7155 8 · 7261 8 · 7575 8 · 7496	0'5597 0'5622 0'5525 0'5368 0'5439	7'6753 7'6683 7'6649 7'6706 7'6742	9n7200 0n1772 0'1073 0'1635 0n0747
4471 4472 4473 4474 4475	666 666 667 667 668	III r	8	1964 1964 1964	561 738 916	14 16 5	53°5 27'7 20'8	164 ' 342 ' 153 '	171 629 756	+2:48 -0:72 +3:31 +0:01 +3:89	23 · 23 ·	613	170.980 359.159 179.411	351.642 172.123 357.433 181.812 4.705	0.6010	9'7008 9'7614 9'7110 9'7416 9'7370	8'7055 8'7574 8'7134 8'7385 8'7349	0.5709 0.5360 0.5655 0.5464 0.5516	7.6696 7.6693 7.6709 7.6679 7.6724	929092 9.8851 829006 8.7205 9.8087
4476 4477 4478 4479 4480	668 669 669 669	VII	8 6 3	1965 1965 1965	418 447 594	1 12 23	42°5 16°1 28°8	321 ' 321 '	313 038 864	+4'12 +0'40	23° 23°	612 612 612	343'816 15'349 165'501	189'672 343'503 13'894 164'726 195'881	o'6890 o'6935 o'7433		8 7559	0'5607 0'5386 0'5397 0'5652 0'5680	7.6666 7.6765 7.6736 7.663x 7.6655	0'1143
4481 4482 4483 4484 4485	670 670 671	XII I	8	1965 1966 1966	949 127 303	3 4 14	16'4 41'7 15'2	93° 269°	292 567 020	-0.18	23 23 23	. goð . gii	173.745 359.617 182.449	180'255	0.7275 0.7197 0.7043	9'7233 9'7298	8 · 7223 8 · 7298 8 · 7454	o'5538 o'5586 o'5390	7.6627	9'7627 8n5426 9n3329
4486 4487 4488 4489 4490	672 673 673	VI XI 2 IV 2 X 1	25	1965	835 983 159	8 15 18	12.2 41.6	246 34 205	774 816 403		23 23 23	.608 .608	14'240 170'179 349'910	190'714 13'620 172'434 347'485	0'7436 0'7067 0'7167	9'7542 9'7007 9'7470 9'7344 9'7202	8.7071 8.7433 8.7334	0'5755 0'5417 0'5542	7.6773 7.6649 7.6743	0'1324 9'9365 9n9582
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4496 4497 4498 4499 4500	676 677 677	VIII	7 4	1968 1968 1968	223 370 548	14 20 9	44 °C 55 °C 42 °C	173 · 322 · 134 ·	596 456 088	+0'52 -1'46 +4'12 +0'88 +4'02	23 23 23	·бо; •бо;	7 14.39 7 171.42 5 352.20	5 346'410 9 16'668 2 169'093 2 353'744 5 178'662	0'7055 0'7075 0'7386	9'7473 9'7445 9'7092	8 7441 8 7423 8 7117	0'5446 0'5478 0'5634	7.6705 7.6735 7.6656	0.0992 9.8790 9n8689
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4457 4458 4459	94 '80 270 '68 75 '00	+o·o876 -o·6460 +o·8412 +r·4930 -r·3737	9·7617 9·7182 9·7253	277 · 57 88 · 95 235 · 26	91'08 89'84 84'47	9'5791 9'5928 9'6435	9.9879 9.9996	9 · 9663 9 · 9639 9 · 9533	8 · 6657 7 · 8207 9n3667	9n5758 9*5927 9n5723	9 • 9 5 6 6 8 9 • 9 5 3 9 9 • 9 6 7 4	87'1 89'6 104'5	+176 - 16 	+ 8 - 39 + 50	II . —	+ 27 - 62 + 80	9	+ 1 - 34 + 51 -	
4462 4463 4464	113.08 171.48 99.72	-1'0310 +0'8574 -0'2750 +0'1761 +0'4726	9 · 7045 9 · 7668 9 · 7056	224.53 41.39 214.61	83·39 83·25 83·14	9'6585 9'6615 9'6704	9'9787 9'9756 9'9682	9'9495 9'9487 9'9463	9n4852 9·5128 9n5670	925285 9*5092 924597	9.9737 9.9761 9.9812	69'9 112'7	130 136 150	- 34 + 31	169 98	+ 45 + 2 - 6 + 47	- 105 - 35	+ 4 - 12	t
4467 4468 4469	39.52 236.70 158.98	-0.5248 -1.5040 +1.2803 +1.4570 -1.1877	9	3°35 24°74 176°07	88·96 84·00 91·20	9.6876 9.6762 9.6851	9'9415 9'9578 9'9423	9 9412 9 9446 9 9419	9:6867 9:6236 9n6838	8·5128 9·3426 8·5790	9:9998 9:9892 9:9997	60'9 64'5 118'9		6	-156	49	- 64	55 	r p p p
4472 4473 4474	46.05 63.84 260.34	-0.8113 +0.7675 -0.0795 +0.6437	9 · 7635 9 · 7132 9 · 7437	168·59 347·53 160·88	93'38 93'70 95'38	9 · 6863 9 · 6875 9 · 6827	9'9450 9'9452 9'9514	9	9n6750 9'6740 9n6512	9'0384 9%0776 9'2483	9'9974 9'9969 9'9931	117'1 61'6 118'4	-148 -129 + 31	+ 77 - 33 + 30	- 35 - 63 +100	+ 67 - 12 + 14	+ 30 6 +158	+ 22 + 24 - 24	t 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
4477 4478 4479	206 · 21 356 · 65 175 · 75	-0'7272 -1'3557 +1'3010 +1'3800 -1'4933	9	304.66 330.82 117.68	95'50 96'48 94'54	9 · 6428 9 · 6729 9 · 6337	9 · 9880 9 · 9626 9 · 9925	9'9535 9'9455 9'9555	9	925719 924011 95898	9 9675 9 9857 9 9644	75°5 65°7 101°5		_ 21	— 31 — — —	- 39   	+ 13	67 	r p p p p
4483 4484	33.98	-0.7148 +0.5790 -0.0349 -0.2152 +0.6807	9.7320 9.7517	283'56 96'55	91.04	9.6129 9.6017	9.9996 9.9983	9.8601 9.8601	8 · 9450 8 <i>n</i> 62 18	9n6026 9'5994	9.0621 9.0621	84°5 92°6	+ 44	7 9	34	- 26 - II	+ 24	+ 3 14	tili
4487 4488 4489	300.62 51.25 106.34	-0'9470 +1'3563 +0'8640 -0'9082 +0'1217	9'7028 9'749¤ 9'7364	258·85 42·25 210·96	88'47 86'71 87'18	9.5730 9.5181 9.5064	9.9834 9.9834	9 · 9673 9 · 9750 9 · 9764	8n8276 9 * 3759 9n4332	9n5658 9:3591 9n2349	9'9684 9'9884 9'9935	94'I 75'9 106'0	-141 -164	+ 44 - 48	- 57 -114	- 76 - 81	+ 64 + 20	— 十 69 一 77	$\frac{p}{t^{\mu}}$
4492 4493 4494	235 '94 175 '40 4 '89	-0'1696 -0'6409 +0'5226 +1'5333 -1'3557	9'7043 9'7652 9'7198	16'80 185'08 327'76	88·32 89·47 92·93	9.4919 9.4898 9.5105	9 9801 9 9837 9 9837	9 9780 9 9782 9 9760	9'4711 9n4879 9'4307	8 · 9731 8 · 4587 9 · 2546	9'998x 9'9998 9'9929	72'7 107'9 74'1	+ 65 +118 -	<b>- 57</b>	+130	一 37	-171	- 27 - 22 + 14	r
4497 4498 4499	39 27 131 65 326 83	-1'4377 +1'2567 +0'7568 -0'7395 +0'0422	9'7493 9'7466 9'7114	172'19 314'62 124'56	93.36 93.36	9'4950 9'5227 9'5347	9.9781 9.9884 9.9923	9 9777 9 9744 9 9729	9n4906 9'3559 9n2698	8'6499 9n3873 9'4588	9'9996 9'9867 9'9813	108 ° 0 76 ° 5 101 ° 2	 +166 25	- 35	- - 29	- 32	+ 78		r
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4501 4502 4503 4504 4505	679 679 \	/II 24 I 18 /II 13 III 9 I 7	1969 1969 1969	080 256 405	1 0, 15 20, 3 51,	9 123°291 6 301'080 9 112'602 2 260'027 3 290'222	+3.53 +0.74 -0.92	23.607 23.608 23.608	187'469 8'137 163'565	359°744 188'817 6'127 165'823 197'877	0.6936 0.7322 0.7266	9'7591	8.7057 8.7566 8.7179 8.7231 8.7355	0'5671 0'5408 0'5576 0'5633	7.6644 7.6758 7.6637 7.6775 7.6765	9n8054 9'8810 0'1763
4506 4507 4508 4509 4510	680 \ 680 681	VI 2 VII 1 XI 27 V 23 XI 16	1969 1969 1969	610 759 936	3 13. 6 48.	74.252 8 102.232 4 248.652 64.213 237.163	+0.32 -2.16	23.609 23.609 23.609	15.733 170.941 355.911	345 393 14 387 171 739 356 086 176 912	0.7092	9'7556 9'7445 9'7015 9'7645 9'7041	8.7508 8.7404 8.7076 8.7595 8.7094	0.5356 0.5423 0.5750 0.5309 0.5732	7.6625 7.6631 7.6773 7.6628 7.6769	0'1664 9'9377 9n5410
4511 4512 4513 4514 4515	682 683	V 12 XI 5 V 2 IX 26 X 25	1970 1970 1970	467 645 792	6 33	3 225 898	-2·38	23.611 23.611	185 599 13 295 162 315	183 228 15 597 161 380	0'7217 0'7247	9'7521 9'7274 9'7263 9'7619 9'7536	8 · 7477 8 · 7275 8 · 7246 8 · 7582 8 · 7508	o'5380 o'5593 o'5530 o'5372 o'5438	7.6633 7.6762 7.6640 7.6720 7.6752	g.6054 g.n7088 o.0843 o.1718 o.20679
4516 4517 4518 4519 4520	684 ] 685 ] 685 ]	II 21 IX 14 II 10 IX 4 II 28	1971	146 323 501	23 53	3 174 992 353 435	+2.20 -0.24	23.011 23.010	170.216 358.691 178.872	350.956 171.774 356.887 181.295 4.356	0'6925 0'7352 0'7119	9'7008 9'7608 9'7125 9'7399 9'7386	8 · 7054 8 · 7567 8 · 7143 8 · 7371 8 · 7362	0.5700 0.5371 0.5640 0.5481 0.5499	7.6683 7.6706 7.6697 7.6692 7.6710	9n9375 9'9073 9n0918 9'0039 9'7851
4521 4522 4523 4524 4525	687 687 687 V	T 13	1972 1972 1972	003 032 180	10 29 0 20 42 5 5 59 5	3 153.789 5 302.457 6 332.020 8 114.310 142.904	+3.60 +3.87 +0.81	23.609 23.609	343'703 15'065 164'631	188.958 343.501 13.711 163.745 195.031	0.6889 0.6930 0.7426	9'7136 9'7639 9'7601 9'7043 9'7012	8 · 7150 8 · 7610 8 · 7566 8 · 7073 8 · 7055	o 5623 o 5381 o 5385 o 5653 o 5687	7.6678 7.6756 7.6725 7.6638 7.6665	9n8256 0n1350 0.1058 0.1639 0n1538
4526 4527 4528 4529 4530	688 X	II 3 II 28 VI 22	1972 1972 1972 1972 1973	534 712 888	13 11'4 21 32'5	291'721 103'725 280'759 93'457 269'465	-0.10 +1.60 +0.30	23.608 23.608	172 '882 359 '578 181 '584	179 475	0'7259 0'7211 0'7030	9'7540 9'7251 9'7283 9'7511 9'7045	8.7515 8.7235 8.7286 8.7467 8.7098	0.5440 0.5530 0.5592 0.5383 0.5732	7.6765 7.6631 7.6771 7.6627 7.6774	9:8584 9:8:69 8:586: 9:1425 9:8302
4531 4532 4533 4534 4535	691 691	11 6 V 3 X 27	1973	420 558 745	14 1.5 16 13.7 22 35.8 3 1.6 8 11.2	257 957 45 338 216 473	-1.37 -3.75	23.606 23.606	169'410 349'743	189 993 13 451 171 714 347 317 180 020	0.7082	0.7012	8.7074	0'5754	7.6639	0'1300 9'9704 9n9637
	693 694 I 694 VI	X 5 II 31 II 26	1974 1974 1974 1974	277 454 631 779	10 44 0 8 2 1 11 19 7 10 56 6	195.075 13.297 155.405	-0'18 -3'03 +0'75 -0'09	23.604 23.604 23.604	185 970 5 843 193 738	355'390 186'386 6'618 192'273 345'800	0.7443 0.6906 0.7393	9.7586 9.7019 9.7628 9.7083 9.7324	8 · 756 r 8 · 706 r 8 · 7598 8 · 711 r 8 · 7307	0'5678 0'5374	7.6743 7.6659 7.6731 7.6671 7.6680	9n7592 9.6962 0n1128
4542 4543 4544	695 VI	II 15 II 8	1974 1975 1975	956 133 310	5 8 6 16 37 1 19 55 6	184 · 476 333 · 423 144 · 680 322 · 803 133 · 816	+0.23 +0.23 +4.11	23.604 23.604 23.604	351'503 179'288	168 844	0'7062 0'7396 0'6905	9'7459 9'7461 9'7079 9'7628 9'7018	8 · 7431 8 · 7435 8 · 7109 8 · 7599 8 · 7060	0 5464 0 5648 0 5375	7.6718 7.6723 7.6667 7.6735 7.6656	9.8918 9n9069 8.7828
4547 4548 4549	697 X 698	II 19 I 18	1975 ! 1976 !	990	9 24 3 0 44 6	312'181 123'094 271'229 301'362 84'687	+0.97 +0.45 +3.53	23.000 23.000	7'333 163'533 195'357	188 758 5 257 165 743 197 783 344 624	0'7308 0'7277 0'7154	9'7205	8.7557 8.7192 8.7221 8.7343 8.7519	0'5640	7.6644 7.6774	9.8347

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4521	129'16	-a	6693	9'715	7 160	0,01	95.17	9 6827	9 95 14	919427	926512	9 2477	9,9931	117.1	+165	<b>1</b> 5	139	- 39	85	- 67	<b>,</b> .
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4539	345'44	-1	2967	9.704	4 16	5 36	88.44	9.4951	9.9802	9.9776	924696	910176	9976	107 2		+ 47	+ 62	. ° 11	. "	+ 12	$t^{\oplus}$
4540	348 • 24	-x	4945	9 734	4 150	0,00	92.76	9.2065	0.0830 c	9764	9 4744 9n4384	9.2218	9,0030	100,5					Streets.		p
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4542	455 37	0	7795	9'748	2 327	7 62	92'90	9:5078	a • a8 3a c	1.07621	0 4273	000 25 22 4	n · nnanl	7410	+ 39	+ 35	+ 99	44	+155	+ 65	$p_{t^{\dagger !}}$
4544	114.96	+0	0606	9'764	9 314	4.81	93'33	9 5 7 4	9 9070 9	9751	923092	9'3545	9.0860	103 9	-133 ·	- 39	- 77	- 43	0.0	6.1	7. 1:11
4545	77.72	-0	0681	9.704	0 124	4.11	93'24	9'5345	9 9925	9729	92644	9 4608	9.9811	101.1	-140	+ 7	<b>- 78</b>	+ 13	- 22	- 14	1:41
4546	354'44	-0	6273	g • 76o	4 302	2.29	93.22	9 5391	9.9930	9.0723	9.2504	0114722	0.0800	70.2	Ro	_ 47			_L 0,		,
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4554	340'40	+0.1030	9.7071	234'36	84.33	0.6428	0.0841	0'0507	9 2900	9 5007	9 9050	77.4	- 87 -	34 - 34	3	+ 25	- 12	t
4555	281-28	+0*3304	9.7528	51.12	83.99	9.6492	9.9847	9.9219	9'4162	9.5583	9.9696	73.8	+ 13 +	3 + 76	+ 41	+158	+ 33	t*l‡
4556	39'42	-0.2028	9.7311	224'19	83'37	9.6586	9.9785	9	924881	915264	9 ' 9740	100,1	-rog -	10 - 44	- 52	+ 48	- 46	,.
4558	51.44	+1.2003	9.7641	101,06	86'54	0.6854	9 9705	9'9492	9.5057	9.2122	9 9757	70'2		_				p
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4562	286.89	-0.1747	9,4191	2'97	89.00	0.0808 0.0881	9'9415 9'9408	9'9410 9'9405	9116865 g • 68go	8,6131 8,4642	9.9996 9.9996	119'1	+ 23 + + 13 -	86 + 78	+ 72	+141	+ 28	t#
4564	40'01	+o:5687	9.7424	355 32	01'46	0.6880	0.0474	9 9407	9,0003	0 5105	9.9999	119 2	+100 +	37 -x33	+ 11	<b>– 73</b>	- 21	r-t*
4565	238.81	-0. <u>61</u> 74	9'7143	168.86	93.33	9.6873	9 9445	9.9413	926765	9.0293	9 9995	118.2	+ 55 -	- 49 + 111	- 38 - 39	+ 22 + 174	66	35.te
4566	107.09	-1'3782	9.7660	324.57	96.75	9.6662	<b>9</b> • 9 6 9 6	9 9475	9.5581	024628	0.0800	67.8	_	_				
4568	12 42	+1.5325	9 7050	137.11	93 00	0'6585	9.9401	9'9422	9.6712	920702	9.9970	61.8	-   -	-			_	p p
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4573	252'36	-0'0640	9.7546	117'04	04 ' 58	0.6344	9 9 9 9 4	0.0000	9 3002	9115099	9 9078	75 0	150	10 -141	- 24	- 84		
4575	140,40	-0.4994	9.7666	107.67	92.91	0.0100	9'9940 9'997¤	9 '9588 9 '9588	9,2175 9,0635	925950 9.6015	9 ' 9623 9 ' 9635	79'7 97'3	+ 41 + + 112 + + 167 -	29 162 41 143	+ 20 - 30	-153	+ 47	yerife t
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4581 4582	80.28	-0'5021	9 ' 7038	42'41	86 . 74	9.2160	9 9876	9 9753	9:3726	9.3280	919884	76'0	-132 -	43 - 77	18	20	16	r
4583	90.74	-1'2310	9'7117	20.25	87.31	0.5027	0'0820	0.0464	014095	3114705	9 990-	203 0		43 - 67	+ 20	- 6	+ 13	ι τ
4585	284.28	-1.2042 +1.5420	9.7320	103.02	91.43 88.09	9.4970	9 9797	9'9775	914757	8'9816	9 9980	107.5		-   -				p p
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4587	177.12	-0.8684	9.7490	149.20	91.92	9.4972	9'9802 9'9834	9'9774 9'9768	9'4697	9n0342	9 9974	72.7	- 87 + +117 -	35 - 24	+ 52	+ 39	+ 70	t**
4589	179'94	-0.1374	9'7044	136.40	93.27	0.5168	0,0880	0.0250	0	914470	9 9931	74 3	52	11 +117	- 5	十178	+ 20	f.142
4590	122.39	-0.6104	9,7596	315'44	93'34	9.2211	9.9882	9'9747	0.3g11	923797	9.9872	76'3	+118 +	49 <del>-1</del> 79	+ 5 - 53	-125 - 47	- 21 - 23	
459 I	220.71	-⊦o.giie	9.7226	124'07	03'25	0.5356	0.0032	0'0708	005.50									
4593	308.30	-1'3602	9'7359	303 36	03'20	0'5405	0.0036	0,0441	714770	915922	9.9039	90'2		- 143	-i- 55	—145 —	+ 25	p p
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	5	1 2 3403	9 /490	112 00	92.08	9 5550	9.9903	9.9699	911145	9.5251	9'9741	97'9	_   -	1	-		, <del></del>	p
4596 4597	112'94 148'00	0.8796 0.4068	9 7028	257:00	87.88	9.6119	9:9985	9 '9603	8n9261	916024	9'9621	95.3	-146 +	57 -111	+ 38	68	+ 50	7×14
4598	101.42	+0.1991	9'7079	245 20	85.00	0.6301	0.0040	0.0463	9 0920	9.0009	9 9024	82'2	+101	34 -146	7	90	20	t
4600	165.87	-0'4968	9 7513	234.41	84'35	9.6357	9.9918	9 9551 9 9528	9°2852 9n3780	9 * 5875 9n 5704	9 9648	77'9	-154 + - 96 + +123 -	2 - 32 14 - 170	+ 38	+ 45	+ 25	t#
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4.602	180'40		9.7645	200.27	84'73	g'678r	9'9534	9'9441	926429	9112662	9.9925	116.6			bally of the				p p
4603 4604 4605	11.85	1:1467 0:9952 -+0:8688	9.7035	18.67	84 '91	g'683o	9'9509	9'9426	9.6529	9.2391	9'9934	62.8	(+- 57)	(66)			+ 60	- 56	r r
		-0.5351		'														+ 32	
4507	255.28	+0:1779 +0:5213	9.7387	184.41	88.62	9'6892	9'9412	9'9407	9n6875	8,,6340	9,9996	119'2	+ 43	l- - 39	+107	- - g	+168	19 61	r-t1:
4609	350'43	-0.5724 -1.3980	9'7129	176.64	91'05	9'6893	9'9410	9'9407	9,,6884	8.5165	9.9998	110.5	56	- 6	o			64	$\frac{r}{p}$
4611	12'20	-1.3023 -1.3023	9.7637	355.52	91,38	g:6868	9,9419	9.9414	9.6851	8, 6376	9.9996	gr.o	w	s./ms			<b>⊕a</b> torina		p
4613 4614	183.43	0.7487 0.8002	9'7542 9'7301	325.17	96 · 67	9.6593	9.9687 9.9687	9'9468 9'9493	9.5642	914598 9 5175	9.8813	ნე:5	十141 十 57	+ 64	99 175	7x +- 77		25 32	14
4615	265.60	0.0555	9'7277	315.83	96.64	9.6588	9.9782	9'9494	9,4893	9115258	9'9741	70.0	+ 25	21	+ 95	23		- - 15	r ^{all}
4616 4617	313'48	+0.0078	9'7053	305.67	95.67	9'6456	9'9871	9:9527	9,3201	9115703	9.9677	75.1	II	+ 25	+ 4x	2 X	+ 85	- 14 51	沙
4619	300'45	0'7273 1'3347 0'7273	9'7044	294'36	94.03	9'6291	9'9943	9.9566	9'2080	9n5954	9.9634	79.9		- 32	+104	25	+148	- 52 	$\begin{bmatrix} t \\ p \\ p \end{bmatrix}$
4621	143.47	r · 4830	9.7561	107.23	92.88	9.6186	9'9971	: g*g58g	9,,0596	g · Gor3	9 9623	97.2		Spekking		_	<b>Bootiering</b>		p
4623	120.20	-0'9292 +0'3443 -0'2122	3,4181	66.88	87.3x	9.5525	9.9962	9'9704	9'1212	9.5204	9.9747	81.0	142	+ 11	152	+ 40	78	- - 26	
4625	179.81	0'4235	9.7037	54.72	86.73	0,2330	0.0031	9'9731	9.2763	9'4535	9,8814 8,848	78.6	+129	- 35	-177	30	41	- 22 - 13	
4627	194'57	+0.4633	9.4130	41.87	86.72	9.2120	9.9872	9'9750	9:3775	9 3550	9'9885	75.8		-l- 40 	+162	+ 14	137	+ 14	p
4629	138.38	1 1 1 1 8 7 7 1 0 1 8 4 4 7 - 0 1 9 2 2 4	9,4211	354 '04	go'63	9.4918	9.9783	9'9781	9.4892	8115296	9 9998	72'0	1-147		-146 66		II *	-l- 75 82	P 13# 11
4631		+0.1100													ì				
4632 4633	284 ' 59 248 ' 92	-0'1997 -0'5874	9.7047	328 47	92.74	9.2020	9 9837	9.9769	9,4299	9:2276	9.9937	74'I	十 14 十 30	+ 4 51	+ 74 + 115	48	+131 176	27	profi.
4634 4635	311.00	10.2420 1.2.220	9.7198	281 · 72	91.60	9.5182	9,9880	9.9750	9#3659 8 · 8489	9°3692 9″5646	9'9686 9'9686	85.Q	49 	+ 45	+ 35	48	+102	-l- 19	p
4636 4637	72'17	1.3457 1.3113	9.7344	316.11	93'38	9.5232	9.9879	9'9744	9.3682	913770	9.9873	75'I		Quarter q		_		_	$rac{p}{p}$ .
4638 4639	232.35	+0.8880	9.7508	268 85	93,30	9 5370	0.0000	9'9539	912725 718600	9.4610 9.5925	0,0630 0,0811	30,2	 + 89	 55		+ 40	168	 54	$p_{r^{\oplus}}$
		0.2712												- 34		,	+155	- 29	
4642	138'63	+0'203 <u>0</u> +0'1786	9.7500	71.47	86.94	9.6202	9.9967	9.9584	9.0847	0.0010	9 19623	82'4	- <b>⊢</b> ≖57	+ 2	139	1- 34		+ 16	t ^{riti}
4644	293 43	+1.2385	9.7233	3 Gr 36	85.32	9.6350	9 9920	9'9553	9 2804	9'5878	9.9648	78'I	68			, ,,,,,,,,,	(-xo5)		
		-x · x40;													_		_	_	p
4648	188.20	- 1 · 0593   + 0 · 8898   - 0 · 2959	9'760:	200 . 39	84.6	9'681:	9 9528	9'943	1 911 6452	912723	9.9922	116.4	r 7 9			+ 74 - 10		 35 10	1) t#
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4656 4657 4658 4659 4660	742 743 743	VIII VIII	[ 3o	199 199	2 11 2 29 2 46 2 64 2 82	0 8 1 4 1	7 20 4 8 9 45	5 I	24'97 35'23 14'13 24'90 02'90	7 + 0 + 4 +	0 '87 4 '03 1 '01	7 2	3 60 3 60	4 I 2 3 2 I	70°5 59°2	23 26	353 · 18 168 · 12 1 · 50 177 · 27 7 · 68	2 5 5	0'7015 0'7216 0'7248 0'6991	9.7299 9.7242 9.7547	8 7278 8 7247 8 7504	0'5518	7.6656	9'9367 8n8549 8'8804
4661 4662 4663 4664 4665	744 745 745 745 745	VII VII	7 4 4	199; 199;	2 999 3 176 3 324 3 354 3 501	4 20	13,	5 2	4.78 91.47 76.69 04.69	7 + 9 - 7 +	2.72 1.02 0.47	23	3 · 60: 3 · 60:	1 16	13 ' 9 ! 56 ' 8 ! 96 ' 4 :	54 89 :	187 · 89 12 · 91 169 · 29 198 · 42 347 · 13	X 0	0'7417 0'7125	9'7031	8.7086 8.7371 8.7482	0.5375	7.6765	0'1219
4666 4667 4668 4669 4670	746 746 747 747 748	V XI V XI V	17 14 7	1993 1994 1994	8 679 8 855 9 033 210 387	18 6	34° 27° 57° 54°	6 23 9 3 2 22	56 · 32 39 · 07 5 · 66 8 · 32 4 · 96	4 -3	3 ' 0 g 1 ' 5 3 3 ' 5 9	23	5599 5599 5599	35	7'45 3'53 5'32	51 3 31 1	77 300 56 32 83 59 6 40 89 78	# C	1592x	9.7610 9.7616 9.7606	8 · 7582 8 · 7585 8 · 7585	0'5406	7.6628 7.6769 7.6632 7.6763 7.6640	9'6306 9n3381 9n5325 9'6574 0n0348
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4658 4659	28'32 115'51	+0.	0716	9.7264 9.7568	325 43	96.83	9.6698	9 9683	9.9465	9,5667	9 4502	9.8813	67.4	- 73   <del>+</del>	71 +13 72 + 7 26 - 2 23 -11 20 - 7	9  + 86 7   21	+156 + 28	+ 35 + 18	4 5 8
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4711 4712 4713 4714 4715	765 766 766 767 767	XI V XI IV IX	7 3	2000 2001 2001	972 150 297	14 8 12	37'I 9'0 52'I	228.639 16.59		23.596 23.595 23.595	190.682 13.205 169.238	188.857	0'7356	9'7137	8.7146		7.6769 7.6632 7.6668 7.6668 7.6721	9.6522 0.0015 0.0684 9.9709 0.0039
4716 4717 4718 4719 4720	768 768 769 769 770	III	15 12 5	2001 2001 2002 2002 2002	828 006 183	21 21 0	21.0	176'54' 355'933 165'613	+1'37 -1'69 +2'30 -0'81 +4'06	23.594 23.594 23.594	356 861 186 020 4 730	177'431 355'970 183'819 2'441 165'072	0'7426 0'6986	9.7641 9.7033 9.7549 9.7238 9.7154	8 · 7604 8 · 7680 8 · 7516 8 · 7247 8 · 7177	0.5700 0.5398 0.5568	7.6682 7.6707 7.6696 7.6693 7.6744	9.2963 9.4789 9.7172 9.6394 0.1939
4721 4722 4723 4724 4725	770 770 770 771 771		25 20	2002 2002 2002 2002 2002	508 537 685	3 11	2 · 2 48 · 9 17 · 8	126.600 155.050 304.450	+3.13 +1.00 -0.06 +3.67	23 594 23 594 23 595	343'017	195.714 341.792 11.051 170.742 352.541	0'6940	9.7296 9.7606 9.7514 9.7000 9.7628	8 '7290 8 '7563 8 '7479 8 '7062 8 '7582	0'5340 0'5411 0'5749	7.6709 7.6648 7.6679 7.6755 7.6638	on 1128 on 1576 o 0559 g 0606 gn 8537
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4708	350.65	-0'9286 +0'5125 -0'2206	9'7154	89'95	89.99	9.2906	0'0000	9.9642	6.4614	9.5906	9.9642	90'0	- 69 + 65	+ 28 9	(+158)  + 9  +133	+ 54 - 35	+ 88 156	+ 28 - 14	$t^{il}$
4710	13.84	0'2543	9.7037	78.42	88.43	9.2711	9,9990	9 . 9676	8 8424	9.2633	9*9688	85.7	68	18	x3	+ 7	+ 44	- 10	7:41
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4723 4724	354'36 108'49	+1'1373 +0'9132 -0'7140	9 ° 7534 9 ° 7022	149'59 293'49	92.41 95.41	9.5058 9.5517	0.00 <u>0</u> 0	9 9764 9 9705	9,4352	9,2274 9,5186	9 9937 9 9750	81.8 100.0	159	+ 53 - 37		+ 48	CI .	46	
4726	104'24	o.5181	0,2110	28o'64	91.46	9.2726	9,9991	9'9674	8.8073	9 <i>1</i> ,5661	g·9684	86:0	163	+ 8	-105	9	49	+ 15	7.112
4728 4729	186.87	+0.0275 0.4844 0.8330	9.7367 9.7367	268.55 82.52	88.81 88.81	9.5930 9.6030	o'oooo 9'9995	0.0010 0.0038	7×9592 8 · 6798	9:5929	9 · 9638 9 · 9625	90 ° 6	+123	- 26	+ 6 +173 -136	- 52	-ro8	1	$r_{\perp}$
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4732 4733	87.79 87.79	0'4381	9.7583	35.17	83.12	9.6647 9.6685	9'9725 9'9690	9'9479 9'9468	9 <i>n</i> 5380 9'5619	914873 9'4630	9.9809	67.6	84 39	+ 72 - 46	+ 12	II	+ 71	3	l:1:
		+0'2451 +0'3423																	
4737	252.01	-0'4782 -1'4940 -1'0546	9.7659	358.03	00,00	9.6856	9'9419	9'9418	9.6852	82790	9,9999	61,0		2	+ 16	<del>- 43</del>	+103	54	. 'r 2' 1'
4739	330.38	-1'1820 -0'8335	9.7029	192'09	86.43	9.6865	9'9453	9'9416	926738	920631	9 9971	118'4	******	 83	110	- 77	- 44	— 28	p
4742	268.43	-0'1231	9 ' 7237	342 68	3 94.83	9 6843	9'9494	9'942	g · 6584	9:2102	9 9942	62.5	十 23	34	+ 93	- 17	- 61 +150	+ 20	1.
4743 4744	346'14 304'51	0'1971 0'5283	9 7590	334 20	96 · 10	9.6784	9'9577	9 944	9n6241	9.3489 9.3613	9 · 9889 9 · 9882	64.6	- 6a - 8	+ 36 + 12	+ 16 + 47	+ 26	十 75 十 98	- 14 + 60	tile print
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4748 4749	114'94	+1'3253 -1'2877 -0'9280	9.751	137 7	3 95 · 6. 2 92 · 6.	4 9 658; 5 9 616	9 9 9 7 6 7 4 9 9 9 7 7	9 9 9 4 9 9	6 92503; 3 9 022	7 9 '511 <u>9</u> 1 9 n 6 o 1 <u>9</u>	9 9758 9 9622	109.7	+ 73		(+ 31			1: "	1
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4756	130.76	+0.9895	9'7553	33.04	87.05	9'5095	9 9841	g'9761	9'4255	0.3636	0.0030	74.0	+121 + 6			8-1/1	· ·
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4766 4767	238·73 224·06	-0.7805	9.7644	116'74	92'94	9'5481	9.9951	9'9711	911778	9.5045	9.9766	99, I	+ 64 - 4	811-	- 34 +	166 - 50	5 t
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4780	85.70	-1'1540	9.2033	200,36	84.62	9.6817	9.9525	9.9429	9n 6463	912707	9.9923	116.8				xo3) (- -67	p
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4783	25'33	-o'x598	9 7324	350 66	02 84	0.6881	0.0433	9 9410	920784	8 9459	9.9983	118.6				35 + 19	p
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4786	353'61	0'4713	0.7657	155.28	06.05	0.6778	0.054	0.0447						EI . I			
4788	85'27	+1'4037	0.7375	121.66	05'10	0.6580	9 9590	9 9444	9.0180	923045	3.3880	64.8		2 + I	- 19	57 - 5	$\begin{vmatrix} t \\ p \end{vmatrix}$
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4795	238,33	-0.835o	9.4188	89.30	89.00	9.589	0.0000	964	7 604	9.5897	9 9644	89.7	- 64 + 2 + 78 - 5	0 +122	- 34 +	166 - 5	6 th
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4806 4807 4808 4809 4810	807 807 808 808 809	VIII	7 31	2016 2016 2016	033 210 388	11 11 2	31.0 31.0	315'226	+0'84 +4'05 +r'03	23'591 23'591	350.106 177.378 358.716	170 042 351 304 175 628 1 138 182 766	0'6929 0'7117	9.4612	8.7379	0.5340 0.5677 0.5448	7.6733 7.6657 7.6745 7.6647 7.6755	9°9821 9n9258 9°3937 9n0600 9n6685
4811 4812 4813 4814 4815	809 810 810 810	VII VI VII XI	9 5 5	2016 2017 2017	919 066 096	6 21 12	43°9 8°9 35°3	116.891 293.309 77.956 106.214 252.483	+2.85 -0.91 +0.57	23.592 23.592 23.593 23.593 23.593	345°324 15°265		0'7342 0'6929 0'7432 0'7449 0'6980	9.7150 9.7595 9.7040 9.7018 9.7541	8.7158 8.7569 8.7069 8.7053 8.7518	0.5410 0.5647 0.5663	7.6638 7.6765 7.6625 7.6631 7.6774	9.8310 0.0492 0.1449 0.1633 9.9690
4816 4817 4818 4819 4820	811 811 812 812 813	V XI V XI V	26 19 14 8 4	2017 2017 2017 2017 2018	598 775 953	22 12 2	3'6 9'8 6'0 7'4 19'5	241'499	-1.49 -3.54	23.592 23.593 23.593 23.593 23.594	2,381	0,108 0,108	0'7270 0'7207 0'7037 0'7403 0'6901	9.7285 9.7500 9.7049	8 · 7225 8 · 7286 8 · 7454 8 · 7098 8 · 7592	0.5591 0.5391 0.5725	7.6627 7.6770 7.6632 7.6763 7.6640	9n6492
4821 4822 4823 4824 4825	813 814 814 815 815	X III IX III IX	25 17	2018 2018 2018 2018 2018	455 631 809	11 13 21	59 7 37 8 24 6	218'825 8'390 178'068 357'760 167'529	+1.20 -1.81 +2.14	23.594 23.594 23.594	349 475 168 223 357 803	191'181 351'747 165'800 359'892 175'135	0.4122		8·7427 8·7338	0'5440	7.6754 7.6681 7.6708 7.6694 7.6694	0'0233
4825 4827 4828 4829 4830	816 816 817 817 817	VIII VIII VIII VIII	18	2019 2019 2019	340 517 666	19 23 0	35 ' 8 37 ' 2 35 ' 6	345.768 157.195 335.605 118.478 146.870	-0.20 +3.68 +0.95	23.594 23.593	184.933 13.035 163.474	185.650	0'6904 0'7391	9.7013 9.7633 9.7071 9.7338 9.7469	8.7311 8.7100 8.7311	0'5343 0'5686 0'5485	7.6708 7.6681 7.6723 7.6640 7.6667	9'7281 9n6228 0'0903 0'1702 0n0696
4831 4832 4833 4834 4835		VII XII VI XII	7 31 26	2020 2020 2020	020 197 374	6 ; 5 ; 8	57.2 35.7 0.2	294'755 107'973 283'932 97'286 273'148	+0.64 +1.89 +0.15	23.291 23.291	171 885 357 324	347'078 *73'366 356'584 *79'477 6'6*3	o'7388 o'6899	9°7094 9°7625	8.7500 8.7500 8.7057	0.5621 0.5395 0.5658	7.6632 7.6770 7.6627	9'8864 9n3570
4836 4837 4838 4839 4840	820 820 821 821 821	VI XII V VI X	9 5 3	2021 2021	906 053 082	9 11 3	53'0 35'4 11'0	262.209 48.314 76.347	-0.75 -1.39 -1.00	23.590 23.589 23.589	13'082 167'079 196'672	185 980 15 505 165 259 194 312 349 350	0'7151 0'6984 0'7089	9.7182 9.7352 9.7558 9.7450 9.7014	8.7345 8.7512 8.7409	0'5556 0'5361 0'5417		9x8751 0.0679 0.0459 0x1646 0x0363
4841 4842 4843 4844 4845	822 822 823 823 824	IV X IV X IV	18 14 8	2021 2021	584 762 939	20 20 20 2	1'4 14'9 18'4	209 ' 338 28 ' 009 198 ' 232	-3 68 -0 42 -3 24	23 588 23 588 23 588	355'855 184'255 3'576	175 866 354 652 186 296 1 189 195 052	0'7405 0'7023 0'7214	9.7050 9.7514 9.7289	8 · 7598 8 · 7100 8 · 7478 8 · 7287 8 · 7247	0'5713 0'5396 0'5567	7.6647 7.6745 7.6657 7.6733 7.6669	925706
4849	_	VIII	21 17 10	2022	441 618 795	18 1 19 1 18 5	8.8	148,236 326,234	+3.61 +0.38 +4.01	23 588 23 588 23 588	169'659 349'444 177'132	9.919 169.582 350.763 175.303 0.436	0'7448 0'6936 0'7349	9.7505 9.7127	8.7514 8.7059 8.7563 8.7155 8.7367	0'5725 0'5353 0'5662	7.6669 7.6733	9°9968 9n9544
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4803 4804	14.64 66.29 184.34	-0'3717 -0'4283 +0'3558 -1'2185 +1'0472	9 · 7547 9 · 7297 9 · 7287	21'36 189'03 8'42	89.11 89.07 89.81	9'4968 9'4888 9'4935	gʻ980g gʻ9790 gʻ9784	9'9775 9'9783 9'9778	9.4628 9.4828 9.4883	9.0775 827055 8.6811	9 '9969 9 '9994 9 '9995	73.0 107.7 73.0	- 75 - -128 + -	42 -	- IX  -	20	+ 51	8	t
4807 4808 4809	354°27 343°17 212°69	+0'9596 -0'8430 +0'2476 -0'1148 -0'4661	9.7636 9.7135 9.7434	128.91 305.80 116.92	93'36 93'28 92'94	9'5299 9'5321 9'5467	9,882 <b>0</b> 8,8818 8,8808	9 '9735 9 '9733 9 '9713	9n3115 9'2814 9n1795	9'4311 9n4500 9'5025	9 · 9836 9 · 9821 9 · 9769	78'5 99'2	- 4x + - 55 44 + + 83 + - x59 -	43 - 3 - 2 -	- 15 - 15 -147	- 44 - 2 + 12	+ 46 + 71 -155	- 65 + 25 - 15	t 7ポ じゅ
4812 4813 4814	275°30 142°14 4°05	+0.6777 -1.1200 -1.3960 +1.4563 +0.9312	9.7615 9.7060 9.7038	281'42 64'13 93'65	91.56 85.75 90.54	9 5729 9 6308 9 5855	9'9935 9'9939	9'9652 9'9562 9'9653	8.8382 9.2345 8n3548	925654 9:5926 9:5847	9'9685 9'9639 9'9653	85·8 79·3 91·4		_	_	_	-107  62	_	p p p
4817 4818 4819	214'08 214'08	-0.5926 +0.2642 +0.2002 -0.4459 +0.9277	9.7307 9.7521 9.7071	228'15 44'31 218'21	83.40 83.14	9'6535 9'6579 9'6659	9'9820 9'9786 9'9722	9 * 95 ° 7 9 * 94 97 9 * 94 75	9n4490 9'4865 9n5396	9n5462 9 5264 9n4881	9 · 9713 9 · 9740 9 · 9784	71.0 71.0	+ 154 + - 64 - + 81 -	30 - 7 - 5 -	154 4  -141	5 + 32	- 92 + 73	- 29 - 45	tik r
4822 4823 4824	1'16 29'04 139'60	1'1320 0'9252 +-1'0550 0'2048 +-0'2944	9.7482 9.7378 9.7211	6.02 178.61 358.40	90'43 90'50	9 6877 9 6870 9 6898	9'9421 9'9414 9'9406	9'9412 9'9414 9'9405	9.6846 9.6869 9.6895	8.7664 8.1301 8.1943	9 9999 9 9993	60.2 113.1 91.0	(+ 72)(- - +158 -			— — — 14 + 25		 + 17	p
4827 4828 4829 4830	113'08 167'07 191'87 341'59	+0.5347 -0.4196 +1.2310 +1.4797 -1.1737	9.7654 9.7092 9.7358 9.7489	163'45 342'26 131'47 155'41	94.63 94.88 96.24 95.97	9.6838 9.6832 9.6516 9.6760	9'9490 9'9502 9'9826 9'9577	9'9423 9'9426 9'9513 9'9446	9n 6601 9 6560 9n 4439 9n 6240	9 1907 9 2183 9 5463 9 3399	9'9947 9'9940 9'97¤3 9'9893	115.2 102.3 102.2	180	3 -	-119  	+ 32 - 19 	58 	+ 61 - 51 -	$egin{array}{c} t \ p \ p \ p \end{array}$
4832 4833 4834	285 · 89 262 · 86 299 · 95	-0'9320 0'7698 0'2275 0'0119 0'4440	9.7043 9.7043	111,28 508,01	95°17 94°59 93°57	9.6402 9.6342 9.6250	9'9899 9'9923 9'9955	9 ' 954 I 9 ' 9554 9 ' 9575	9n3301 9r2705 9n1536	9.5806 9.5892 9.5987	9 96660 9 9645 9 9628	78'3 98'9	- 35 + + 22 -	56 -1 23 -1 9 -1	- 79 - 98 - 60	+ 75 - 36 + 24	+161 +163 +117	+ 34 - 1 - 8	garle garle
4837 4838 4839 4840	325 ° 91 358 ° 02 119 ° 99 135 ° 41	-0.7500 -1.1692 -1.115 -1.6072	9'7372 9'7578 9'7479 9'7479	275°30 57°60 88°96	90.84 86.76 89.84 86.65	9'5998 9'5411 9'5898 9'5259	9'9997 9'9930 0'0000 9'9900	9'9626 9'9720 9'9644 9'9739	8 · 5284 9 · 2497 7 · 8 x 27 9 n 3243	9n5982 9'4754 9'5897 9n4166	9'9629 9'9797 9'9644 9'9846	87'9 79'3 89'5 102'6			- 20   	Andrews Surfaces	+ 65 	- 47  	p p
4842 4843 4844 4845	130.67 186.87 296.21	0.3667 0.3956 0.3721 0.3268	5 9 . 7274 9 . 7274	216.03 34.20 202.20 21.44	86.97 87.03 87.83 487.83	9:5076 9:5081 9:4957 9:4994	9 9853 9 9846 9 9813 9 9807	9 · 9762 9 · 9762 9 · 9776	9n4070 9'4178 9n4579 9'4651	9n2923 9 2739 9n0975 9 0819	9.9968 9.9968 9.9958	74'5 105'8 72'9	+170 +172 -115 +	· 8 - · 37 -	-128 -128	— 35 — 12	- 53 - 66	— 38 — 6	$\begin{array}{ c c c } r \\ t \end{array}$
4847 4848 4849	101.00	5 0 · 120 0 · 992 5 0 · 270 5 0 · 180	9 · 702 4 9 · 762 4 9 · 714	332'24	4 92 '5' 1 93 '1' 4 93 '2'	9,5005 9,5138 3,9,5143	9'9827 9'9860 19'9872	9 9 9 7 7 9 9 7 5 4 9 9 7 5 5	9'4422 9n3968 9'3794	9n 1863 9	9.9948	73 7 104 8 75 8	-159 + -176 - -163 +	- 48 - - 1 -	-103	+ 3	(—143) — 80 — 46 + 93	- 74 + 29	t
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4856 4857 4858 4859 4860	829 829 830	XII r VI XI 3 V 2 XI 1	5 2	2024 2024 2024	005 184 360	7 . 6 .	54 ° 37 ° 3 24 ° 4	77 · 820 252 · 68 <u>0</u> 67 · 565	-0.56 -0.92 -1.83 -1.31 -2.87	23.200 23.200 23.200	352'708 177'058 1'430	171'108 350'417 179'438 359'333 185'710	o.6988 o.7257 o.7220 o.7026 o.7407	9'7256	8.7240	0.5451 0.5525 0.5601 0.5380 0.5733	7.6775 7.6625 7.6774 7.6627 7.6770	9.9707 9.8271 9.4301 9.0977 9.6396
4861 4862 4863 4864 4865	831 832 832	$\mathbf{x}_{\mathbf{I}}$	8 : 4 : 47 :	2024 2025	892 040 216	9 19 21	23'6 41'1	19.067 188.958	4-0.58	23'592 23'592 23'592	167 845	9'831 190'918 351'183 165'427 359'276	0'7425 0'7081 0'7140	9'7447 9'7372	8.7074	0'5311 0'5743 0'5441 0'5513 0'5601	7.6632 7.6763 7.6668 7.6722 7.668x	9 19337 020476 929919 0 10354 924099
4866 4867 4868 4869 4870	834 834 835		7 3	2025 2025 2026	749 926 103	6 3 7	51'4 37'6 7'5	357 557 167 953	$\frac{1}{1}$	23.591	184 397	185*238	0.4383	9'7594 9'7012 9'7628 9'7082 9'7454		0'5705 0'5353 0'5672	7.6594	9.5222 9.6876 9.5732 0.0760 0.0512
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4876 4877 4878 4879 4886	838 839 839	VI XII V VI XI	20 16 15	2027 2027 2027 2027 2027	491 638 668	18 19 3	28'I 2'I 22'2	273'41 58'80 86'78	5 +0.63 -1.46	23 588	3 166 264 3 166 264 3 195 808	185 027 15 478 164 542 193 492 349 095	0'7165	9'7570	8 · 7332 8 · 7522 8 · 7423	0.5563 0.5352 0.5408	7.6774 7.6631 7.6625	021406
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	4901 4902 4903 4904 4905	849 849 850 850 850	XI IV V	18 16 15	2031 2031	477 626 655	17 2 3 1	3.6 3.7 8.1	241.06 29.68 57.80	9 -2 0 -0 4 -1	91 52 45	23.288	191.590 17.974	190'699 350'549	0.7421 0.7096 0.6990	9'7433	8.7398 8.7503	0'5744 0'5442 0'5363	7.6769 7.6656 7.6632	9' on or o'
	4906 4907 4908 4909 4910	851 852	TTT	28 24 17	2032 2032 2032	156 334 511	19 2 13 5 11 4	0 4 5 2 7 8	189°25 8°27 178°77	$     \begin{array}{c c}       3 & -2 \\       7 & +1 \\       9 & -1     \end{array} $	21 89	23'589	175 741 4'482 183'938	184,801	0'7443	9 7010	8.7054	0'5602 0'5382 0'5697 0'5362 0'5658	7.6722 7.6682 7.6707	9° 9° 9°
	4911 4912 4913 4914 4915	854 854 855	$\mathbf{v}_{\mathbf{I}}$	1 28 21	2033 2033 2033	013 190 367	8 1 20 1 23 1	8·8 5·8	316'95 128'92 306'25	7 +4 r +1 o +3	'05 '04 '71	23 589 23 588 23 588	349'101	194.630 346.872 171.503 356.602 177.482	0.404	9'7437 9'7481 9'7070 9'7632 9'7028	8 · 7604	0'5463 0'5643 0'5384	7.6693 7.6744 7.6648 7.6755 7.6639	9n 9n 9
	4916 4917 4918 4919 4920	856 856 857	VII XII V	5 31 27	2033 2033 2034 8034 2034	899 077 224	3 2 2	1'0 6'3	284 ' 60 69 ' 25	9 +0 9 +1 8 -1	·65 ·94 ·25	23.586 23.585	186.278	6.669 184.098 15.429 163.804 192.681	0.7292 0.7177 0.6964	9.7566 9.7213 9.7325 9.7582 9.7480	8.7205 8.7319 8.7532	0'5553 0'5569 0'5344	7.6627	0,
	4921 4922 4923 4924 4925	858 858 859	XI V	16 9 6	2034 2034 2034	578 755 933	19 8	37.8 33.8 13.7	59 ' 23 231 ' 50 49 ' 09	3 -3 7 -3 7 -3	44 3.5 I	23'584	355 51 182 76	348.88x 174.559 354.123 184.940 0.750	0.4391 0.4391	9'7005 9'7640 9'7066 9'7489 9'73 ¹ 7	8.7593 8.7113 8.7450	0'5313	7.6631 7.6639	9 °
	4926 4927 4928 4929 4939	860 861 861	$\mathbf{X}$	18 15 8	2035 2035 2035	464 612 789	4 4 8 4 11 1	47·6 45·6 12·0	359'00 169'6	36   -3 59   +3 99   -3	2.01 5.40	23.583	11, 22; 168, 73; 348, 33;	193.552 9.553 168.436 349.875 174.445	o · 6965 o · 7447 o · 6949	9.7009	8.7537 8.7059 8.7552	0'5705 0'5376	7.6648 7.6744 7.6693 7.6696 7.6707	9,
	4931 4932 4933 4934 4935	863 863 864	VIII	21 18 11	2036 2036 2036	320 498 675	7 8	25 · 6 18 · 5 38 · 5	337 2 148 5 326 5	23   +: 30   +: 84   +:	3.00 3.00 3.00	23.282	184.52 4.96 192.69	7 191 658	0.7374	9.7617	8.7130	0'5635	7.6668	9,
No.	4936 4933 4938 4939 4949	865 865 866	XII	25 21 16	2037 2037 2037	176 354 531	21 23 10	39 ' 7 32 ' 9 1 ' 3	98 6 275 0 88 4	61 + 92 + 38 -	0'24 0'83 0'32	23.58 23.58 23.58	350'94 175'99 359'68	5 171'168 6 348'59'3 3 179'30'6 6 357'766 4 185'369	0'7228	9.7289 9.7243 9.7541	8 · 7252 8 · 7252 8 · 7494	0'5508	7.6628	91
	494 494 494 494 494	2 867 3 868 4 868	XI IV V	30 26	2038	063	10	27 7 38 3	252'2 40'2 68'3	38 — 37 — 52 —	1,30 1,10	23 · 58 23 · 58 23 · 58	6 347 45 6 17 12	8 8'41' 5 190"51' 3 349'84' 2 19'05' 6 164'92'	0.411	9 7 7 0 2 8 9 7 7 4 1 8 9 7 7 5 3 9	8.7084 8.7384 8.7499	0.5306 0.5743 0.5444 0.5368 0.5514	7.6773 7.6646 7.6628	3 O
	494 494 494 494 495	7 869 8 870 9 870	X IV IX	9 4 28	2038	3 742 3 919 9 096	3 20 20	45 4 49 :	1 200 2 1 18 9 6	21 - 25 + 78 -	3'33 0'30 2'69	23.58 23.58 23.58	6 175 43 6 3 84 6 183 55	2 357'80 7 174'32 7 3'95 5 184'63 0 9'89	0 0 692; 5 0 744; 1 0 691;	9 7606 9 7013 9 7616	8 · 757 8 · 705 8 · 757	4 0.5386 3 0.5696 9 0.5373	7.6734	4   9 8   9 2   9
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Nr.	μ	γ	$\log n$	G	K	$\sin g$	$\sin k$	$\cos g$	$\cos k$	sin ô'	coső	N'	gra	ng		<del></del> -	Unter	rgang	F
i													<del>\</del> \	Ι φ	∥ λ ≯r:	ı φ ı d	В	Ι φ	
													<u> </u>						
4901	110019	+0.7862	9.7666	54°37	84°37	9.6445	9.9872	9.9530	9:3777	9.2693	9.9679	75° 1	+160	+ 34	<b>x</b> 16	+ 76	+ 5	+ 59	t ^{;jt}
4903	531.00	-1.043 -1.043	9 7454	21.79	84139	9.6796	9.9544	9'9436	9.6387	9'2959	0'0013	63.6	=	_		_	_	_	p p
4904 4905	272 · 58	+1.1022 +1.2363	9.7571	45°57 194°48	85.89	0.0231	9°9800 9°9477	9'9508 9'9425	9.4723 9n6649	9'5301 9n1344	9'9735 9'9959	71.6 117.8		_		_	_	_	$p \begin{pmatrix} p \\ p \end{pmatrix}$
4906	1.11	-0.3168	9.2186	13.40	85 ' 98	o:6862	0.0464	0'0415	0,6604	דאדזים	0.0060	6r:o	5fi	_ 46	_ ,	_ 74	-l- 62	-t- TO	,
4907 4908	113.00	+0.3644	19.2021	190.03	87.90	9.0879	9'9423	9'9411	9n 6841	828085	100010	IIO.0	I75	+ 50	801	- - 2 T	+ 63 - 47	- 8	111
4909	357 97	-0:3355 +1:1447	9 7042	179.13	90.27	g'osssi	9.0400	0'0400	02 6887	7'0208	0.0000	110.5	I 6∡	+ 10	- 33	T 33	+ 67	T 35	t
														_					p
4912	303.11	-0.0814	9.7501	327.53	96.68	9'6698	9 9663	9'9465	0.2201	024363	0.0833	66 8	(-134)	 (-73)		*****		46	$v_t$
4913	154.89	-0.3305 -0.2435	9.7653	140'99 318'65	96.82 96.75	9'6643 9'6614	9'9732	9'9480 9'9487	9n5326	9'4932 925088	9 9779	60.0	+ 67 +118	+ 72 32	(+ 65) 163	- 34	28 102	+ 44	r# t
49 ¹ 5	133'56	o·1820	9.7050	131.00	96.30	9.6534	9.9823	9 ' 9508	9114465	9.5475	9.9711	107.4	+155	+ 26	-132	+ 32	- 75		7**
4916	40'50	-1-0'4363	9.7587	308.99	96.03	9'6493	9.9846	9 9519	9'4178	925576	9.9697	73 ' 7	-104	+ 9		1	1 .		t ^{i‡}
4910	220.30	-0.5834 -1.1707	19 7345	298 32	94'62	0'0340'	0'0021	0'05551	0'2748	025870	0,0648	78.2		21		I4	-137	- 44	p
4920	335.39	+1.3043	9.7500	110.08	93'46	9 5/75	9,868	9.3228	9n 1402	9.5986	9.9628 9.9628	98.2 86.6		_			-		$p \mid p$
4921	12.76	-1.1155	9.7026	254'77	88'02	9.5654	9,9983	9 ' 9685	8,,0552	025518	0.0705	95'5						_	p
4923	3,35	-0'5031 -0'4264	9.7088	70 42	87.59 87.01	9'5589	9'9972	9'9695 9'9716	9.0269	9 * 5362 0 » 4056	9'9727	83'0	+167	+ 22 15	-119 - 5	51 44	一 35 十 72	+ 35 - 33	$t^{i \dagger i}$
4924 4925	350.68	0 · 2434 0 · 2885	9 . 75 ro	58.95	86.85	9'5406	9 9 9 3 6	9'9721	9.2323	0.4805	0.0702	79'7	53	23	-l- a	3	-l- 66	- 4	12111 20141
					l					**				7.0	/*	1			
4927	253'12	-1'0482 0'9627	9 7584	215.01	86.94	9'5104	9'9851	9 9 9 5 9	024103	922042	0.0014	105'2	X T X	+ 79	+114	+ 75	ー 十172	+ 57	$p_{t^{\oplus}}$
4929	351,20 315,20	-0.0002	9.7608	358.85	91,30	9'4881	9'9785 9'9791	9 9785	9*4880 924800	7n8129 8 8545	0.0000	72 I	70	- 57			— (— <b>6</b> 6)		$\frac{p}{t}$
4930	332'34	-ho:3358	9.4179	345 20	91'49	9,4908	9'9797	9'978x	9.4746	819184	9.9985	72.6	- 35	+ 2	+ 25	<b>+ 16</b>	+ 87	+ 37	7** 1
4931 4932	190'11	-0'2942 -0'4025	9.7382	154'41	92'41	9'4986	9'9821	9 9772	924492	9'1522	9 ' 9955	106.2	+106	_ x	+167				
4933	287.87	1 · 0752	9.7128	141.21	93'14	9.2113	g'g862	9 9758	023052	9'3108	0 '0003	104.7		- 39 十 42	- 89 + 76	- 34 + 4x	25 139	+ 13	
4935	299.59	+1'2237	9.7034	128.80	93.35	9.2291	9,0002	9 9736	913105	9,4303	9 9836	75.2			-		_		p
4936	21,50	-0'9452	9 ' 7530	273:35	90,20	9 5853	9 9999	9.9652	8.3191	925847	9'9653	88.7	- 57	+ 6o	22	- <del> -</del> 48	+ 10	+ 62	t st
4937	140.32 140.32	0'8272 0'2767	9.7310	85.43 261.27	89'28 88'60	9'5983 9'6046	9,9998	9'9629 9'9617	8 * 4631 8 27 486	9 ' 597 I	9'963x	93.5	+171	- 51 18	-146 -173	- 33 - 7	-ror	- 48 + II	r
4939	330.23	-0'0273 -0'4236	9.7562	74'50	87'46	9'6153	9 9977	9'9595	0.0045	o foro	9'9622	83.7	3r	- 7	+ 20	+ 22	-l- Q5	+ 4	t*
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4942	200.29	+0'7127	9.7049	238 23	84'86	9.6397	9 9899	9'9541	923269	925810	9659	103.3	_	+ 32	+134	+ 70 -	-120	<u> </u>	p
4944	112.22	-1'1115 -1'4703	9 ' 7558	55'2I	84'51	9.6420	9 9879	9536	9'3660	9 5795	9 9677	75.5		_			_		p = p
4945	37.27	-1.1245	9'7419	202.85	84'27	9'6777	9.9558	9'9442	916328	9n3132	9.9906	116.0		-		_	-		p
4946 4947	107 ' 92 240 ' 67	-0:3832 -0:3898	9.7174	21.74	84.35	9.6811	9 9 9 5 4 0	9 9 4 3 2	9 6464	9 2978	9.9913	63.5	-158	- 48 - 50	-102	- 14	- 44	+ 4	g.
4948	x30.02	+0.3031	9 ' 7033	13,01	86.05	9 6867	9'9461	9'9414	9.6706	9'1131	9 9 9 6 3	61.8	+167	- 6	-x37	+ 32	— бо	+ 49	2 st
4950	141.36	+1.0002	9.7128								9 9993				-120	- 24	54 	<b>- 4</b> 5	p
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		anisch ilende		Juli Ta			olt- oit							ΔLI				
4951 4952 4953 4954 4955	871 872 872 873 873	IX VIII VII VII	18 12 8 1 28	2039 2039 2039 2039 2040	598 776 953	16 3 7	41'2 1'9 52'2	179°112 327'984 139'463 317'338 128'643	+3.94 +0.78 +4.05	23.586 23.586 23.586	348 · 862 169 · 450	356'538	0'7097 0'7026 0'7409 0'6893	9.7421 9.7495 9.7059 9.7635 9.7032	8.7392 8.7465 8.7087 8.7604 8.7067	o·5478 o·5448 o·5656 o·5376 o·5664	7.6707 7.6732 7.6658 7.6744 7.6648	0n0192 9n9865 0'0015 9n4128 9'4173
4956 4957 4958 4959 4960	874 874 875 875 875	$\mathbf{v}\mathbf{n}$	21 17 11 7 6	2040 2040 2040 2040 2040	484 662 809	7 11 9	5'4 28'5 50'1	306.664 117.992 295.772 79.702 107.668	+0'97 +3'02 -0'80	23.584 23.584	185 445	15'344 163'054	o.6965 o.7277 o.7189 o.6955 o.7046	9'7557 9'7228 9'7309 9'7592 9'7494	8.7531 8.7219 8.7306 8.7541 8.7450	0'5426 0'5548 0'5574 0'5338 0'5395	7.6755 7.6639 7.6764 7.6625 7.6631	g.6306 gn7028 o.0673 o.1193 on0890
4961 4962 4963 4964 4965	876 876 877	V IX V IX V	1 27 19 16 9	2040 2041 2041 2041 2041	164 340 518	19 19	7 9 59 4 3 5	69 · 674 242 · 655	-1'22 -2'81 -1'44	23.283 23.281	173'232 355'422 181'948	353'937 184'186	0'7440 0'5910 0'7381 0'7065	9.6999 9.7638 9.7076 9.7475 9.7330	8.7065 8.7588 8.7122 8.7434 8.7325	0'5759 0'5313 0'5713 0'5406 0'5562	7.6774 7.6627 7.6770 7.6631 7.6763	
4966 4967 4968 4969 4970	878 879 879	X III IX III	6 29 26 19 14	2041 2042 2042 2042 2042	049 197 374	13 15 19	48'1 19'6	220.571	+1'07 -2'01	23.580 23.580 23.580	190.570 11.057 168.164 347.901 175.954	9'475 167'745 349'536	0.7296 0.6955 0.7445 0.6956 0.7317	9.7208 9.7572 9.7014 9.7577 9.7172	8 · 7205 8 · 7547 8 · 7062 8 · 7545 8 · 7184	0.5559 0.5418 0.5695 0.5389 0.5610	7.6639 7.6755 7.6680 7.6709 7.6693	9n9910 9'9762 0'0544 0n0149 9'5782
4971 4972 4973 4974 4975	880 881 881 882 882	VIII VIII VIII	8 4 28 21 17	2042 2042 2043 2043 2043	906 083 260	14 17	28'2 23'3 4'3	159.130	- -2'91 0'31 - -3'58	23.280 23.280	184 · 159 4 · 342 192 · 401	5 908 191 469	0.7083 0.7383 0.6910	9'7344 9'7440 9'7093 9'7623 9'7014	8 · 7327 8 · 7414 8 · 7123 8 · 7592 8 · 7058	0.5466 0.5650 0.5370	7.6695 7.6707 7.6682 7.6722 7.6668	9.6153 0n0209
4976 4977 4978 4979 4980	883 884 884 884	VII VI XII	8 2 25 21	2043 2043 2043 2044 2044	762 940 116 294	4 7 17 10	38 4 57 2 21 7 27 3	274*931	+0'73 +2'12 +0'27	23.281 23.281	169.036 350.093 176.942 358.821 184.359	179 215 356 997	0.7212	9'7307 9'7228 9'7552	8 · 7285 8 · 7241 8 · 7507	0'5500 0'5624 0'5359	7.6632	9'4507
4981 4982 4983 4984 4985	885 886 886 886	VI VI X	7 6 30	2044 2044 2044 2044 2044	648 796 826	9 17 2	34 ° 6 55 ° 2 59 ° 7	263.426 50.745 78.792	-0'64 -1'40 -0'83	23.283	191.441 346.664 16.251	190'354 349'084	0.7410 0.7012	9'7528	8 · 7368 8 · 7479	0'5740 0'5449 0'5374		0n0364 0n0736 0'1465
4986 4987 4988 4989 4990	887 888 888	IV X IV X IV	20 15 9 4	2045 2045 2045 2045 2045	327 505 682	3 4	36.3	211 · 257 29 · 512 200 · 646	-0'49	23'584 23'584	175 ° 203 3 ° 104 183 ° 251	184'434	0.7446	9'7612 9'7011	8.7581 8.7052 8.7575	o'5389 o'5681 o'5386	7.6646 7.6746 7.6656 7.6734 7.6668	9.6117 9.4760 9.4435
4991 4992 4993 4994 4995		AIII AIII	23 19 12 8	2046 2046 2046 2046 2046	184 361 538 715	9 16 10	56 · 6 54 · 1 24 · 8	190'000 338'940 150'065 328'366 139:181	+3'49 +0'28 +3'93	23.584 23.584 23.584	348.551	169 834 356 408	0.7015	9'7508	8 7475 8 7082 8 7605	0'5434 0'5669 0'5369		9n9973 0'0299 9n4455
4996 4997 4998 4999 5000	892 892 893 893 893	VII VII VI VII	27 21 17	2047	069 247 304	14 19 17	5'6 51'0 13'2	306'895 90'139	+1.05 +3.73 -0.23	23.582 23.582 23.581	4.780 184.649 12.832 163.659 193.275	182'367 15'207	0.7203	9.7243 9.7295 9.7601	8.7293	0.5544 0.5577 0.5332	1	
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Nr.	μ.	γ	$\log n$	G	K	$\log \sin g$	log sin k	$\log \cos g$	log cos k	log sin ở	log രേട <i>ർ</i> ′	N'	$\frac{\text{bei} \odot \text{Auf-}}{\text{gang}}$ $\frac{\lambda + \varphi}{}$	λ   φ	bei () Untergang λ   φ	
4952	227.62	-hr.0032	9.7212	336.33	95'86 96'61	9'6774 9'6734	9'9566 9'9635	9'9443 9'9454	9.6292	9,,3266	9'9900	64'2	(+ 74) (-73 (- 87) (+60	d l	29 48	p t (r)*
4955 4956 4957 4958	170°24 283°95 346°01	+0.5014	9.7054 9.7578 9.7249 9.7329	318.98 131.35 308.98	96'75 96'27 96'00	9.6646 9.6615 9.6526 9.6483	9'9733 9'9753 9'9826 9'9847	9'9479 9'9487 9'9511	9"5319 9'5156 9"4437 9'4160	9.4947 9.5064 9.5480	9.9777 9.9764 9.9711	69.8 107.3	+ 15 - 12	+130 + 3 -174 +	4 173 5 8 122 43	1 ⁴¹
4960 4961 4962 4963	132'28 229'66 123'93	-1.2275 -1.1197 -10.5759 -0.4345 -0.1721	9 '7514 9 '7020 9 '7659 9 '7098	267.09 82.03 254.58	95'06 89'57 88'87 88'00	9'5383 9'5858 9'5778	9'9902 9'9999 9'9995 0'0082	9'9544 9'9651 9'9665	9,,3207 8,,2567 8,6867 8,,0500	9.5811 9.5853 9.5742	9 · 9652 9 · 9652	91'1 87'0 95'6	+ 48 + 30 + 165 - 19	125 4	7 - 48 - 29	7°
4965 4966 4967 4968 4969	258.20 22.30 59.28	-0.9795 -0.9467 -1.1335	9 7352 9 7229 9 7593 9 7035 9 7598	58'93 229'00 12'07 180'66	86 · 83 86 · 63 88 · 76 89 · 93	9'5441 9'5415 9'5266 9'4910	9 9946 9 9936 9 9900 9 9792	9.9716 9.9739 9.9781	9" 1959 9 ' 2333 9" 3283 9 ' 4803	9"4953 9'4814 9"4152 8'8324	9 · 9776 9 · 9791 9 · 9847 9 · 9990	99'5 79'7 102'7 72'4	35 + 74	+161 - 5	7 +149 - 62 1 + 35 + 55	,t
4971 4971 4972 4973 4974	306.00 213.14 34.93 69.86	-0'3780 -0'3418 -0'3687 +0'4124 -1'0492	9 · 7 · 7 · 9 · 7 · 6 · 5 · 7 · 6 · 5 · 7 · 6 · 5 · 7 · 6 · 5 · 7 · 6 · 3 · 7 · 6 · 3 · 7 · 6 · 3 · 6 · 6 · 6 · 6 · 6 · 6 · 6 · 6	358 57 167 59 345 31 154 33 332 59	90°15 91°26 91°48 92°41	9'4873 9'4902 9'4978 9'5029	9 9 9 7 8 5 9 9 7 9 4 9 9 7 9 6 9 9 8 2 2	9°9785 9°9782 9°9780 9°9773	9'4872 9"4788 9'4755 9"4482	7,19069 8,8431 8,19160 9,1527	9 · 9989 9 · 9985 9 · 9955	72'1 107'6 72'5 106'5	10 2 78 30		7 115 - 37 148 4	7-31
4976 4977 4978 4979	150.66 251.29 297.98	+0.9540 -0.9540 -0.9018 +0.2823 -0.1023	9 · 75 × 9 9 · 73 2 7 9 · 72 5 0 9 · 75 73	285.69 96.79 273.25 85.48	92.03 90.97 90.48	9.5652 9.5802 9.5849	9.8991 9.8999 9.89999	9'9684 9'9662 9'9653	8 · 9678 8 · 9678 8 · 9042 8 · 4577	9×5509 9 '5775 9×5843	9°9706 9°9666 9°9654	84·3 92·6 88·7 88·2	+ 56 - 55 + 5 - 14 -141 - 7	+108 - 42 + 62 - 6 - 80 + 13	+118 + 16 - 18 - 4	<i>p</i> t*!*
4981 4982 4983 4984	333.71 321.08 93.34	-0.4178 -0.6387 -1.0875 -1.1847 -1.1847 -1.1352	9 · 7667 9 · 7057 9 · 7423 9 · 7547	75.03 249.28 38.91 65.33	87 · 55 86 · 58 83 · 22 85 · 96	9.6145 9.6235 9.6633	9 '9979 9 9 '9960 9 9 '9732 9	9'9597 9'9579 9'9483	8'9887 9"1348 9'5325	9.6020 9:5992 9.4911	9 9 5 2 2 9 9 5 2 7 9 9 7 8 1	83.9 98.5 69.0		+ 25 + 64	+x19 + 4x	ι* ν ν ν ν
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5038	234 38	+1'1482	9,7301	328 33	06.64	0.6703	0.0624	9 9454	925928	9.4180	9'9845	113,0		+ 3 	-141	- 8	- 87	43 	$\begin{vmatrix} r \\ p \end{vmatrix}$
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5043	7.37	0'4430	0.2118	278'87	QI'42	0.0048	0.0003	0.0017	8.7554	0.,6004	0.0604	26.4	+108 84	+ 45 - 27	- gr		— т + 66	+ 37 - 21	t**
5045	94.09	-0.0213	9 7405	93 84 266 78	89.25 89.20	9 5968 9 5850	0,0000 0,0008	9'963x 9'9653	823864 823000	9.5960	9'9633 9'9633	ATIE	27	0	十 37	+ 22	+ 99 - 36	3	$t^{\eta_1}$
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5056 5057 5058 5059 5060	919 920	II 3 VII 29 I 24 VII 18 I 12	2056 756 2056 932 2057 111 2057 287 2057 465	18 53'3 0 29'8 8 13'2	130.098 308.247	+1'04 +3'79 +1'03	23'575		346.092 178.912 355.545	0'7049 0'7186 0'7282 0'6968 0'7433	9'7339 9'7201 9'7574	8'7452 8'7316 8'7216 8'7530 8'7071	0'5491 0'5630 0'5352	7.6743 7.6649 7.6754 7.6640 7.6762	9,9930 0,0163 9,4823 9,3903 9,6021
5061 5062 5063 5064 5065	921 922 922 922 922	VII 8 I r V 29 VI 27 XI 21	2057 642 2057 819 2057 967 2057 996 2058 143		285.787 71.662 99.668	+2'03 -1'11 +0'33	23.576 23.577 23.577 23.577 23.577	5.801 191.302 344.979 14.509 166.977	347 431 16 685	o.6906 o.7398 o.7158 o.7041 o.7076	9'7642 9'7051 9'7371 9'7499 9'7437	8.7593 8.7103 8.7339 8.7453 8.7420	0'5312 0'5727 0'5462 0'5390 0'5503	7.6632 7.6770 7.6627 7.6627 7.6770	9.6932 0.0299 0.1274 0.1011 0.0585
5066 5067 5068 5069 5070	923	V 18 XI 11 V 6 X 30 IV 25	2058 675	5 43'4 16 47'9 21 39'2	50.524 222.773	-3'42 -1'37 -3'79	23'577 23'578 23'579 23'580 23'580	174'918 1'482 182'845		0.7370 0.6905 0.7447 0.6930 0.7335	9'7115 9'7621 9'7015 9'7592 9'7153	8.7126 8.7594 8.7052 8.7563 8.7158	0.2400 0.2608 0.2400	7·6632 7·6764 7·6639 7·6755 7·6647	9n7899 9'6358 9'1552 9n3866 9'9491
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5081 5082 5083 5084 5085	930 930 931	I 2 VI 29 XII 22 VI 18 XII 12	2060 742 2060 920 2061 096 2061 274 2061 451	1 29'7 20 35'7 16 40'1	276.217	+0'39 +0'93 -0'16	23°577 23°577	170.614 355.257 179.366		0.6926	9.7622	8.7570	0'5322 0'5696 0'5428		020576 9'9030 926509 8'7524 9'4211
5086 5087 5088 5089 5090	932 933	VI 7 XI 30 IV 27 V 27 X 21	2061 629 2061 805 2061 953 2061 983 2062 130	15 44 5 12 8 9 3 52 8	254.094 41.539 69.917	-1'74 -1'13 -1'19	23.575 23.575 23.575	187 981 10 844 166 017 196 094 347 046	9'520 165'258 196'314	0.7334 0.6930 0.7436 0.7449 0.6982	9'7594	8'7166 8'7572 8'7068 8'7055 8'7517	0.5414 0.5664 0.5660	7.6625 7.6774 7.6645 7.6627 7.6747	9n8738 9°9654 0°1247 0n1857 0n0467
5091 5092 5093 5094 5095	934 934 935 935 936	IV 16 X 11 IV 6 IX 30 III 25	2062 307 2062 485 2062 662 2062 839 2063 016	7 56 8 1 54 2 12 24 6	202.642 20.363 191.594	-3 48 +0 19 -2 85	23.573 23.573 23.573	174'106 355'128 182'594 2'919 191'051	357°539 180°363 4°200	0.7281 0.7210 0.7047 0.7404 0.6904	9'7293 9'7486	8.7219 8.7289 8.7451 8.7101 8.7598	0.5565 0.5417 0.5694	7.6656 7.6735 7.6667 7.6723 7.6681	9.7375 9.6479 9.3583 9.4451 9.9709
5095 5097 5098 5099 5100	937 937 938	VIII 9 II 3 VII 29	2063 193 2063 341 2063 518 2063 696 2063 872	23 32'9 2 11'5 8 35'4	330.506 140.664 319.608	+3:87 +0:76 +4:02	23.573 23.573 23.573	10:364 168:517 347:783 176:543 356:386	170*782 345*358 178*671	017437 017062 017170 017295 016958	9'7020 9'7463 9'7354 9'7189 9'7585	8 · 7070 8 · 7439 8 · 7332 8 · 7205 8 · 7543	0.5467 0.5488	7.6708 7.6731 7.6659 7.6743 7.6649	9'9966 o'0032 on0406 9'5076 9n4933

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5052	91,30	-0'4168 -0'2815	9.7493	11.07	88 78	9 4902	9'9793	9.9782	9'4797	8 8277	9'9999	72.4	153	- 34	8a	13	-114 - 27	-t- I	
5º53 5º54	318.27	-0.3100	9 ' 7090 9 ' 7652	180'90 359'12	00,00 80,01	9'4862 9'4904	9 ' 9786 9 ' 9782	9.9786 9.9782	9#4861 9 4903	7n7024	0,0000	72.0	+ 43 (+139)	H- 36	+r08	- <del> </del> 19	+167	+ 1	7**
5055	253.70	+1.0392	9.7039	167.18	01,30	9.4902	9 9 9 9 9 4	9.9782	9114782	3.8570	9,9989	107.6	****		· · · · · · · · · · · · · · · · · · ·				p
5056 5057	46'35 105'04	1 03840 1 0382	9.7497	311.03	93.36	9.5262	9.9899	9.9740	9.3283	924146 0'4856	9.9848	77'3	100	+ 63		********	( бг)	(+75)	
5058	184.23	+0.3036 -0.2456	9.7223	208.11	92'99	9 5437	9 9946	9,0216	9'1945	9n4952	9.9776	80.2	+115				-13I		
5060	213.27	-0'4000	9.7032	285.23	91.97	9.5645	9.9983	9 9686	8 9544	9,5509	9 9706	84.2	+ 73				-144	17	
5061	197.73	+0.4934	9.7663	97.35	91.02	9.5787	99996	9 9664	8,, 6524	9.5756	9.9669	92.8	4 8 r	-l- <b>3</b> 0	- <b>+163</b>	52	119	+ 25	t#
5003	307.82	-1.0712 -1.3410	9'7391	57 99	84'85	9 6392	9.0800	9 ' 9543	9'3297	9'5794	9 9662	76.6	****		Water		desi and	porter.	p p
5065	60.04	+1.5650 -+1.1445	9 7518	231.12	84.02	9.2903	9.9848	9.9522	8.2922 9:4152	9.5958 9.5569	0,0608 0,0033	88.8 2 88.8	******	PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT AND ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESIDENT ADDRESS OF THE PRESID	particular to the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the		BA comid	*****	p = p
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5007	72.38	+0.4323	9.7642	38.42	83.125 83.126	9'6614	9'9754	9'9487	9"5145 9'5379	9115072 914895	9'9763	110'2 68'7	+ 41	+ 43	├ 94 75	9 27	+155 - 2	+ 28	14
5009	147 95	0'2436 0'8894	0.4013	212,00	83 28 (	3'6714	9656	9'9460	925828	914341	9'9834	113'4	-150	+ 9	I 5 I	3 T	7I	- 36 + 75	$t_{r^{\oplus}}$
1	ı	-0.9732			1		1		'			i				Britarium	(-122)		
5072	77.20	-1.1862 c	7555	0'46	39 86 0	6865	9415	9415	g • 6865	7 ' 6495	0,0000	60'0		79	Armonda .				$p \\ p$
5074	315'58 -	-0.3301 c	7664	352.99	2'15 0	6878	9424	94 X X	9.6835	8n8321	0,0000	6x · x	- 26	- 49	+ 49	- 27		+ 9	t 1:4:
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5079 3	304'82 -	1.210 g	7636	24.22 0	5'41 9	6410	9. 6883 (	9538	913584	9 5720	9'0674	104'2			product-o	<b>20</b> 00000	North-Mann	p	$\frac{p}{p}$
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5082	204.00	-1.1412 c	7643	114 94 9	34' IO	0293	9940	g'9566	922181	9 5939	0.0637	100'3	+ 43	+ 55	+160	+ 78	110	+ 39	$r_{t^{**}}$
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5087	55 51	-0.7478 c	9.7015:	206'84[8	39.23	5857	9,0000	9.9621	82923	9n5851	0.0652	01'2	or	42 59	+157	25 45	-157 - 17		r t#
5088	235'00	-1.3327 G	9.7032	50.07	88.87	9'5285	9'9994	9'9737	9:3201 8:6852	9 4236	9.9841 9.9670	77 5				Process Process	******	processes (	$\frac{p}{v}$
5090	132.82	-1,1132	9.7565	220.58	86.75	5162	9.9867	9.9752	9113859	923434	9'9892	104'4	#Annapari		* Bertany			ar non	p
5091 5092	54'85	+0.5464 g	9'7243	37.62	86.88	9.5112	9'9857	9.9758	9 4007	9.3118	9'9907	75'1	-125	- - I8	- 59	+ 46	+ 24	+ 47	palit l
5093 5094	207:70	-0.2282 c	9.7507	25'04	87.63	9'4983	9,9819	9'9773	9'45 x3	9.1434	9'9958	73'4	+ 93	- 20	-154	6	143	+ 3	t st
	80.41	-0.9325	9.7658	12.34	88.43	9 4927	9 9790	9.9778	9.4814	8 8 8 4 3 5	9:9989	72'3	-109	- 85	- 73	<b>-</b> 75	T 54	- 51	
5096	3'14	+0'9922	9'7041	180'53	89.94	9.4871	9 9785	9 9785	924871	7n4742	0.0000	107.0	(+ 90)	(-1-79)			+ 83	<b>-</b> 65	2+11:
5098	215'01	-1'0074 -1'0980	9'7374	132.67	93.39	9 * 5260	9 9893	9.9740	923425	9'4939	9.9855	103'11	Sanata Januaria				-		$p \\ p$
5100	56'52	-0'3114 -0'3114	9'7605	310,30 150,43	93'12 93'33	9 5244 9 5414	9.3638 9.3600	9.9742 9.9720	9°3253 9n2248	9n4135 9.4839	9.9849 9.9788	77 3	- 7 -119	6 8		+ 4 - I		· ·	
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5151	49°31	-0 2287	9.7596	231°52	84°03	9 6486	9.9850	9'9520	924118	925596	9.9694	10001	113	3	— 51		+ 27	27	
5 I 53	233'32	+0°7323 -0°9540	9.7361	221.89	83.31	9'6597	9'9763	9'9491	9115073	925110	9'9758	100.0	+ 22	+ 27 - 49	+ 48	-+- 7x	十162 (一 54)	/ >	1
5154 5155	314'55 86'03	-1.1247 +1.4330	9'7579 9'7470	38.41	85·53 83·24	9.6815 9.6627	9'9493 9'9731	9'943I 9'9485	9'6592 9'5334	9'1767 9'4887	9'995I 9'9784	ба 5 бо о	,						p p
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5150	47'10 200'54	+1·2727	9°7037 9°7664	189'44 8'47	87 · 16	9.6868 9.6868	9.9438	9'9415 9'9413	9:6791 9:6808	8n9585 8'9123	9'9982 9'9985	21.5 118.2	-l- 99	- 54	+165	24	 133	+ 4	$\frac{p}{t}$
5158	42.59	- -0°5606 - -0°2959	9.7084	181.40	89,26	9 6894	9.9407	9'9407	ე₁68ევ	8n 1374	0,0000	110.3	107	+ 63	- 33	+ 39	+ 23	+ 5	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
5160	113.28	0.1303	9.7324	173.62	9I.97	9.6885	9.9420	9.9409	926850	8.7925	9.9992	110.0	-177	- - I8	-117	- 9	- 54	- 40	
5161	233 48	+1.0222	9.7261	353'37	92.02	9.6864	0.0427	9.0415	q·6826	828063	0.0001	61.1							p
5162 5163	294 · 8 I	-0.3047	9'7574	165.65	94'04	9 ' 6844	9'9471	9'9421	9116672	9'1243	0,0001	118.0	8	- 36		******	(+ 34)	(-82)	t
5164	68.62	+0'9425	9.7627	134'73	96.20	9.6557	9.9796	9'9503	924766	9'5304	9'9735	108.6	+r23	+ 70	(+120)	(-1-76)	- 35	+ 48	
5105	12.29	-0'4614	9'7153	311.89	90.31	9.6531	9.9820	9,9208	9'4491	925450	9.9714	72.5	96	4I	8	49	+ 55	- 9	1'
5166	284 10	+0.2104	7415	125'55	95.63	9.6446	9.9873	9 9530	913769	9.5698	9.9678	104.9	- 2	+ 25	+ 77				t*
5168	41.57	+0.2201	7156	115'48	94'19	9.6302	9 9937	9 ' 9563	922277	9'5933	9.9638	100.6	98	- 23	45	- 7 - 13	+ 3	42	
5169 3	319.25	+1.4820 c	9.7627	290 48 73 75	93 37 8 87 90	9 6227	9'996r 9'996r	9 ' 9580 9 ' 9685	9 * 1293 8 * 9827	915991 95497	9'9627 9'9708	81'6 84'1	6 	+ 5 I	+ 37	+ 44	+ 65	+ 62	$\left  egin{array}{c} t^* \\ p \end{array} \right $
5171	30.08	-1'3623 <u>c</u>	7543	104'48   246'32	92 · 36 9	9.6137 9.5526	9.998x	9'9599	829739 921312	g*6019 g25189	9'9622 9'9749	95'9 98'2		, from	positros.	Promise.			$\frac{p}{p}$
5173 2	66 78	+o 6836 g -o 4816 g	7280	62 08	87.00	9'5455	9 9946	9'9714	0.1633	9'4977	9'9774				+ 90 +168	-I- ба 46		+ 49 38	20:31
5175	76.07	-o 1051 g	7536	50.27	86 65	9.5273	9.9904	9'9738	9.3170	9,4236	9'9841	77 6	-r35	1 7	11	1	- 11		
51762	39.38	+o'2243 g	7058	221.11	86 . 80	9.5129	0.0872	9'9756	923791	023443	0.0801	104'2	4- 66	-h 26	+122	I	I 78	х	y:#
5177 3	18.19	-0.8280 g	7664	38:12	36 84	3.2130	9 9859	9 9756	9'3992	0.3183	9'9904	75'I	3	67	+ 47	47	+107	40	t
5179	57.46	+1.0737 €	7459	350.55	90.08	9'4910	9 * 9 7 8 8	9'978r	9 ' 4844	827276	9,0004	72'2	********	79	1.130		161	+ 50	$p^{\oplus}$
5180	82.35	-1'1987 <u>c</u>	7404	158.04	92.17	9.2002	9.9808	9 9771	924641	9 '0924	9.9966	107.1	***************************************			News			27
51811	82.70	+0.3782	7186	337'17	92'18	9 4951	9.9812	9 9777	9 ' 4562	911027	9.9962	73 2	+115	+ 5	-h·174	- <del> </del> - 16	-125	+ 39	
5183 2	202 20	-0.3385 c	3.4026	323 58	93.03	9 ' 5 0 7 3	9 ' 9855	9 ' 9762	9 4042	922959	0,0013	75 0	+ 88	- 34	- -16o	15 32	128 139	- 40 - 5	1
51841	181.09	+0.2972 c	9.7649	133'17	93'35	9 ' 5228	g ' 989 r	9'9744	923440	9'3973	a'a850	103'2	ros	+ 29	180		115		$egin{array}{c} t^{; \mathfrak{h}} \\ p \end{array}$
																			1
5186 5187	48·99 88·28	+1.0640	9'7470 9'7496	121'66 264'88	93'20 89'20	9 5415	9 9934	9 9720	9n2409 8n5123	9.4788	9'9793	100.2		income		parameter (			$\left  egin{array}{c} p \\ p \end{array} \right $
5188	349.76	-0.8766 +0.4433	9.2101	78 60	88,16	9 * 6088	9 9988	9'9609	8.8671	0'6015	0'0623	85 4	24	- 57					1.
5190	2.30	-0.1148	9.7049	67.48	86.58	9.6262	9 9973	9 9591	9,1724	9.5974	9,8631	80.2	- 56	- 15	+ 55 - 2		+112		
STOT	180'44	-0.2254	0.7587	242'22	85.45	0.0334	0.003	0'0556	0266=	0., 580.1	0.064	10115			l + hr O				,
5192	46.20	+0.0491	9.7222	57 25	84'73	9.6408	0.0803	9'9539	9'3404	9'578x	9 9664	76.3	126	+ 25	5 X	+ 64	+ 50	+ 49	211
5194	70'60	-0.9497	9.7592	24.24	84.09	9'6758	9 9574	9'9447	9.6253	9'3342	9.9896	64'4	***************************************	50	(+173 —	) (78) 	+165	69 	$\frac{r}{p}$
5195	195'36	1.3622	9 7487	47'94	83.45	9.6213	9,9830	9.9512	9'4497	9'5432	9'9718	72.5			_	_			$\hat{p}$
5196	161.11	+1.3047	9.7031	197.51	85'18	9.6828	9.9500	9'9426	916563	9n2126	9'9941	117.4		_					p
5197	320'21	-0.4789 -0.5983	9.7661	16.30	85.43	9.6835	9'9489	9.9424	9:6606	9.1842	9.9949	62'4	- 15	- 55 65	+ 46	- 24	+107	I	t
5199	195'16	+0.2493 -0.1487	9'7515	8.74	87.35	9'6869	9'9434	9'9413	9 6803	8.9258	9.9984	61.3	+102	- I4	+16x	21	-126	+ 43	t 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
5200	~3. Ug	- 140/	a 1239	35	-9 3/	3 0091	9 9400	3 5400	y roogo	on1213	0000	1.49 3		7- 21	7-127	- 11		- 38	3

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Nı	Jul	ianischer alender	Tulian.	Welt-Zeit	L'	Z	ε	P	Q	$\log p$	$\log \Delta L$	$\log q$	u'u	$\log f_a$	logγ
520 520 520 520	92 98; 93 98, 94 98,	IX g II 4 VII 31	2080 350 2080 498 2080 676	1 11 33 45 5 3 20 8 3 6 0 4 6 8 13 9	171'316 320'938 132'509	+3.03 +1.03	23'572 23'572 23'572	189·972 347 547 158·177	13°430 188'275 347'286 169'620 198'718	0.7267 0.6968 0.7442 0.6944 0.6898	9'7565 9'7002 9'7596	8.7526 8.7058 8.7548	0.5741	7.6693 7.6696 7.6742 7.6649 7.6682	9129332
520 520 520 520	9 986 9 986	VII 20 I 13 VII 9 I 2	2081 030 2081 207 2081 384 2081 561	21 3 0 14 8 3 4 36 6 21 33 3 18 21 6	122'268 298'581 111'801	+3.12	23.240 23.240	176.839 2'798 185'316	352 984 179 277 0 392 187 004 9 700	0'7325 0'7148 0'7096 0'7367 0'6g11	9'7145 9'7376 9'7416 9'7121		0'5662 0'5465 0'5510 0'5605	7.6753 7.6640 7.6762 7.6633 7.6768	9,6754 9,4541 9,3961 9,7015 9,9597
521 521 521 521 521	2 987 3 988 4 988	XI 23 V 18 XI 12	2081 886 2082 063 2082 241	23 0'4 22 21'9 12 31'0 8 34'7 0 27'6	62:348 235:877	-2 50 -1 35 -3 34	23.568 23.568 23.567	346.736 171.743 354.638	193.211 348.798 169.385 356.956 178.398	0.7449 0.7009 0.7240 0.7244 0.7011	9.75II	8 · 7258 8 · 7252	0.5461 0.5516 0.5612	7.6628 7.6770 7.6632 7.6764 7.6638	0n 1060 0n 0594 9 8791 9n 6928 8n 5662
521 521 521 521 522	7 990 8 990 9 991	X 21 III 18 IV 17	2082 595 2082 772 2082 949 2083 097 2083 127	17 1.0 10 56.6 23 42.7 9 40.2	41'938	-1.1.67 -3.81	23.566 23.566 23.566	9 · 364 167 · 360	3 · 127 188 · 895 8 · 408 169 · 728 199 · 449	0'7421 0'6901 0'7422 0'7103 0'6995	9'7029 9'7646 9'7031 9'7423 9'7546	8.7084 8.7600 8.7085 8.7399 8.7506	0.5317 0.5725 0.5468	7.6756 7.6646 7.6746 7.6692 7.6656	9'3139 9"8845 9'9514 0'0483 0"1782
522 522 522 522 522	991 3 992 4 992 5 993	X 10 III 7 VIII 30 II 24	2083 274 2083 303 2083 452 2083 628 2083 806	7 56'8 15 8'8	352.392	-3 45 +2 57 -0 55	23'566 23'566 23'565	346 '037 16 '995 175 '552 354 '428 183 '158	177 485 353 279	0.7125 0.7246 0.7331 0.6933 0.7447	9 7252 9 7153 9 7608	8 · 7254 8 · 7170 8 · 7571	0.5485 0.5590 0.5629 0.5360 0.5723	7.6698 7.6734 7.6705 7.6684 7.6718	0,0931 0:1884 9:6205 9,6784 9,4835
5226 5226 5226 5226 5236	994 994 995 995	VIII 9 I 4 VI 30	2084 485 2084 662	9 31.8 22 57.2 2 28.2 17 39.3	141 704 289 150 102 875	+3 · 86   : +0 · 76   : +2 · 36   : +0 · 53   :	23'565 23'566 23'566 23'566	11'360 166'846 349'874	188 956 13 742 164 691 351 139	0'5920 0'7372 0'7097 0'7029 0'7409	9 7434 9 7490 9 7070	8.7131 8.7399 8.7469 8.7094	0.5344 0.5677 0.5442 0.5473 0.5633	7.6670 7.6732 7.6658 7.6768 7.6628	9:3829 919996 0:0021 0:0580 919838
5233 5233 5233 5234 5235	996 997 997	XII 13 VI 7 XII 2	2084 839 2085 016 2085 194 2085 370 2085 548	8 48·5 2	267·521 - 81·617 -	-0'17 2 -0'69 2	3.568	182.591	184 306	0.7437	9'7032 9'7557 9'7217	8.7064	0.5652 0.5437 0.5547	7·6773 7·6625 7·6775 7·6625 7·6774	913147
5236 5237 5238 5239 5240	998 998 999 999	V 28 X 23 IV 18 X 12	2085 873 2086 050 2086 227	5 45 6 2	71.321 - 33.089 - 103.787 -	-1'09 2 -3'83 2 -0'68 2	3.569 3.570 3.570 3.570	14 ' 772	12.523 166.508	0.7055 0.7440 0.6903	9.7482 9.7639 9.7639	8.7534 8.7436 8.7062 8.7592 8.7114	0.5399 0.5741 0.5327	7.6645 7.6628 7.6747 7.6656 7.6735	0n1040 0'1100 0'1239 9n7305 9'7979
5241 5242 5243 5244 5245	1000 1001 1001 1002	IX 30 III 27 IX 19 II 15	2086 405 2086 581 2086 759 2086 935 2087 084	23 52 9 I 3 44 9 3	92'784 - 12'310 - 82'145 - 31'918 +	-2'92 2 -0'88 2 -2'15 2 -3'78 2	3'570 I 3'570 I	2 2 2 2 6 (81 2 5 9 10 6 6 0 (89 5 2 1 1 47 2 4 9	178 826   12 824   18 87 921   18	0.282 0.288 0.6928	9 7331 9 7214 9 7572	8.7444 8.7319 8.7211 8.7537 8.7060	0.5537 0.5580 0.5392	7.6667 7.6723 7.6680 7.6709 7.6731	9.2922 9n0573 9.9932 9n9122 on0858
5246 5247 5248 5249 5250	1003	II 4 VII 31	2087 261 2087 290 2087 438 2087 615 2087 792	2 3 3 3 3 T	71 '732 - 20 699 +	1 31 2 3 99 2	3 570 I	67.456 x 97.794 x 54.742 3 76.065 x 2.677	52 717 0	0 6898 0 7317 0 7163	9 7639 9 7160 9 7359	8.7540 8.7597 8.7179 8.7332 8.7411	0 · 5348 0 · 5648 0 · 5479	7 ^{.6743}	0.0300 0n1731 9n6917 9.5507 9.3754
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Nr.	μ	y	$\log n$	G	K	$\log \sin g$	log sin <i>k</i>	$\log \cos g$	$\log \cos k$	log sin ວ່′	log cosð'	N'	bei ⊙. gan λ	Auf- g φ	im M	ittag   φ	bei Unter, λ	O gang	F
5202 5203 5204	55.40 121.59 182.68	+1'0320 -0'8574 -1'1907 +1'0090	9.7586 9.7618	173'77 330'90 143'86	96.21 96.21	9.6873 9.6660 9.6660	9 · 9423 9 · 9623 9 · 9703	9'9413 9'9452 9'9476	9.6839 9.6011 9.5535	8.7808 924014 9.4694	919992 919857 919803	55.6 112.0	-130 - (- 47)	30	- 68	75	- 38	- 86 + 58	$(t)^{\dagger}$
5206 5207 5208 5209	133°32 31°76 245°32 140°99	-1.5325 -0.4736 +0.2845 +0.2489 -0.5029 +0.9114	9·7167 9·7397 9·7437 9·7142	321'63 135'17 311'87 125'60	96.83 96.56 96.31	9'6550 9'6571 9'6530	9°9725 9°9791 9°9821	9 9478 9 9498 9 9509	9.5377 9.4814 9.4489	9n4884 9°5291 9n5455	9.9784 9.9736 9.9714	68.7 108.8 72.5	+142 -109 + 50	+ 33 - 3 - 14	- 29 +113 -145	37 5	+ 31 +166 - 06	- 2 + 30	r-t**
5211 5212 5213 5214	160°95 160°94 11°16 313°39	-1.2763 -1.1465 +0.7570 -0.4930 -0.0368	9·7039 9·7532 9·7297 9·7267	115'10 258'85 73'85 246'89	94°12 88°47 87°92 87°32	9.6296 9.5727 9.5644 9.5518	9:9939 9:9991 9:9980 9:9962	9'9565 9'9674 9'9686 9'9705	9n2209 8n8277 8'9795 9n1206	9.5937 9.5655 9.5492	9.9637 9.9685 9.9709	100'4 94'1 84'1 98'0	-101	 + 40 20	 13 + 45	+ 70 - 49	87 126	+ 50 - 35 + 7	p p r# r
5217 5218 5219	74.45 345.32 176.97	+0.2060 -0.7665 +0.8942 +1.177 -1.5073	9 · 7053 9 · 7444	50'56 220'63 3'85	86 ' 64 86 ' 80 89 ' 59	9.5287 9.5132 9.4898	9'9904	9'9736 9'9756 9'9783	9'3156 9#3827 9'4887	9 · 4268 9 · 3406 8 · 3389	0.0000 0.0803 0.0830	77.6 104.3 72.1	121 17	+ 22 - 59 + 72	70	36		- 36 - 47	1
5222 5223 5224	32.80 297.83 48.97	-1.2390 +1.5430 +0.4174 -0.4769 -0.3044	9 · 7272 9 · 7629	350.29 128.33	87 · 45 90 · 96 92 · 12	9 · 5027 9 · 4878 9 · 4965	9.821 9.821 9.821	9	924481 9:4813 924612	921768 827237 0:0851	9'9951 9'9994 9'9968	72.3 106.0	r r	II	- 53	- 23	- - II	+ 42 - 45 - x	t
5228 5229	160.83 214.60	+0.2415 -0.9990 +1.0048 +1.1430 -0.9634	9 7117 9 7510	277.02 277.02	01.01 03.32	9 · 5092 9 · 5240 9 · 5799	9.9854 9.9888 9.9996	9'9760 9'9742 9'9661	9°4051 923509 8°6334	922996 9:3940	9'9912 9'9862 9'9666	75.0 103.4 87.3	(146) 	(-78)	paparahan Raisera kap	+ 25 - 52	+149	- 1 - 61  - 62	$\begin{pmatrix} r \\ p \\ p \end{pmatrix}$
5233 5234 5235	311.71 147.79 126.32	+0'4457 -0'2064 -0'2236 +0'5652 -0'9486	9 · 7578 9 · 7238 9 · 7330	253.51 67.46 242.68	87 · 29 86 · 28 85 · 53	9 · 6326 9 · 6326	9'9975 9'9952 9'9927	9'9593 9'9574 9'9558	8.8841 9.0322 9.1727 9.2587	9.6016 9.6015 9.5972 9.5898	9'9623 9'9623 9'9631 9'9644	85.7 80.7 80.4	152 19 +135 +118	- 15 - 6	- 97 + 48	- 37	- 39 + 121	- 7 - 18	t t
5237 5238 5239 5240	276 · 65 78 · 00 271 · 75	-1.2707 +1.2882 +1.3300 -0.5376 +0.6279	9 7502 9 7025 9 7099	57.69 205.96 24.40 197.24	84.81 83.81 84.00 82.21	9.6394 9.6765 9.6839	9.9897 9.9588 9.9572 9.9495	9'9543 9'9445 9'9442 9'9423	9'3337 9n6185 9'6265 9n6582	9.5784 9.3615 9.3391 9.2076	9 9664 9 9882 9 9894 9 9943	76'5 115'3 64'3	-127 + 41		-⊦- 98	+ 36	+154	1	1
5243 5244 5244 5245	236.05 128.38 101.38	+0.1960 -0.1141 +0.9845 -0.8170 -1.2185	9 7332 9 7593 9 7026	8 · 87 181 · 54 339 · 48	87 : 33 89 : 52 95 : 40	6, 6800 6, 6881 6, 6860	9 9434 9 9438 9 9411 9 9529	9'9417 9'9417 9'9411	9n6803 9'6792 9n6879 9'6446	8n9469 8 9306 8n1751 9n2746	9'9983 9'9984 0'0000	63,3 110,5 61,3	- 52 +168 +106	+ 22	+_7	13	+ 75	一 35 )(+71)	) r:
5247 5248 5249	253'24 140'50	+1:0715 -1:4897 -0:4917 +0:3554 +0:2374	9.7380	330.76	96.84	9.6744	9 9432 9 9624 9 9608	9'9423	9,6810	8 7596 3 924036	9'9993 9'9856	65	23	1 A T	1 TOM	1 1 4			p p r r-t**
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Nr.		T		L'	Z	ε	P	Q	$\log p$	$\log \ \Delta L$	$\log q$	$u_a'$	$\log f_a$	log y
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5251 5252 5253 5254 5255	1005 I 1 1005 VII 1005 XII	9 2088 324 4 2088 472	3 9'9 5 25'6 7 6'8	122°263 298'911 111'549 258'086 72'785	+3.20 +0.87 -1.33	23 567 23 567 23 567	184°472 10.671 192.443 346.700 170.880	186°070 9'720 192'198 348'816 168'492	o 6908 o 7448 o 7019	9.7107 9.7617 9.7498 9.7498	8 · 7591 8 · 7055 8 · 7477	0.5617 0.5395 0.5664 0.5470	7.6640 7.6762 7.6633 7.6774 7.6628	9.9562 0.0761 0.0616
5256 5257 5258 5259 5260	1007 V 1 1007 XI 1 1008 V	3 2088 826 9 2089 003 2 2089 180 8 2089 358 1 2089 534	7 51'2	62.550 235.721	-1.36 -1.36	23 565 23 565 23 565	188.361	2'882	0.7256 0.6999 0.7427 0.6902 0.7415	9'7229 9'7544 9'7020 9'7646 9'7035		0.5623 0.5366 0.5741 0.5312 0.5728	7.6770 7.6632 7.6764 7.6639 7.6755	8.5407 9.2853 9.8455
5261 5262 5263 5264 5265	roog IV 2	2089 888	8 56 °0 22 19 '5	42°334 183°574 213°095	-1'12 -2'27	23 · 564 23 · 564 23 · 564	196.877 345.608 16.765	169 * 213 198 * 810 343 * 236 14 * 410 176 * 922	0'7119 0'7009 0'7110 0'7234 0'7343	9.7410 9.7533 9.7412 9.7264 9.7141	8.7383 8.7493 8.7391 8.7267 8.7160	o:5468 o:5380 o:5484 o:5590 o:5630	7.6679 7.6647 7.6710 7.6746 7.6692	0,1618 0,1045 0'1814
5266 5267 5268 5269 5270	1011 III 1011 VIII 3 1012 II 2	2090 568 4 2090 745	16 37.5 15 56.2 17 11.6	352'154 162'709	+2·59 -0·57 +3·36	23.563 23.563 23.563		352 885 182 813 3 389 188 540 13 116	o'6925 o'7447 o'6925 o'7363 o'7110	9'7614	8.7139	0:5363 0:5715 0:5354 0:5663 0:5459	7.6697 7.6706 7.6683 7.6719 7.6669	9.2820 9.19849
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5276 5277 5278 5279 5280	1015 XII 1. 1016 V 1016 VI 1016 XI	2091 956 2092 134 2092 281 2092 310 2092 458	5 1.0 7 35.3 15 40.8 13 44.1	267 753 53 750 81 759 226 157	-1:36 -0:61 -3:75	23'566 23'566 23'567 23'567	344'310 13'903 165'853	192 870 342 833 11 718 166 198	o 6950 o 7042 o 7441	9'7233 9'7296 9'7594 9'7497 9'7002		0.5537 0.5587 0.5342 0.5389 0.5750	7.6626 7.6774 7.6637 7.6626 7.6757	0,1301 0,0830 0,1301
5281 5282 5283 5284 5285	1017 X 2: 1018 IV 1: 1018 X 1: 1019 IV 1:		13 34.8 16 24.8 19 19.2 2 16.4	214'797 33'452 203'747 22'967	-3.83 -0.68 -3.54 +0.01	23 567 23 567 23 567 23 567	173'125 1'540 180'960 10'027	171'590 3'792 178'525 12'139	0.7374 0.7062 0.7162 0.7295	9.7086 9.7467 9.7345	8 7589 8 7123 8 7430 8 7331 8 7198	0.5694 0.5423 0.5535	7.6645 7.6747 7.6656 7.6735 7.6667	9'8133 9'1334
5286 5287 5288 5289 5290	1020 VIII 2: 1020 VIII 2: 1020 IX 20 1021 II 12	2093 876 2094 023	11 13 9 15 29 4 0 27 9 12 57 0	342.830 153.739 182.567 331.692	+3.24 +0.08 -2.20 +3.80	23.567 23.567	346 880 166 798 197 340	345 402 168 465	0'7439 0'6959 0'6808	9.758x 9.7577 9.7577 9.7635 9.7176	8 7547 8 7061 8 7531 8 7597 8 7188	0.5395 0.5720 0.5371 0.5358 0.5631	7.6722 7.6717 7.6671 7.6708 7.6731	020978
	1022 VII 31 1023 I 24 1023 VII 20	2094 377 2094 555 2094 732 2094 909	10 59.2 11 53.5 11 55.5	320.777 132.764 310.043 122.004	+3.97 +1.03 +3.80 +1.10	23.566 23.566 23.566 23.565	183 665 10 546 191 578	0'146 185'175 9'694 191'219	0'7384 0'6904 0'7446	9.7342 9.7446 9.7094 9.7622 9.7020	8 · 7315 8 · 7423 8 · 7114 8 · 7594 8 · 7055	o · 5483 o · 5630	7.6659 7.6743 7.6649 7.6754 7.6640	9.6247 9.3434 9.5418 9.9508 0.0451
5297 5298	1024 VI 9 1024 XII 4 1025 V 29	2095 057 2095 234 2095 412 2095 588 2095 766	2 23'4 1 19'5 15 12'8	83 211 258 234	-0'54 -1'33 -1'01	23.565 23.564 23.564	170 : 006 354 : 523 178 : 750	348.839 167.596 356.755 176.908 2.676	0'7210 0'7268 0'6989	9.7486 9.7311 9.7215 9.7555 9.7014	8 · 7466 8 · 7285 8 · 7229 8 · 7508 8 · 7077	0 · 5495 0 · 5633 0 · 5357	7.6774 7.6626 7.6773 7.6628 7.6770	020635 9'9584 927044 9'0356 9'2628
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5252	221,00	-0'4239 -0'9040 -1'1915	9.7638	312.05	96.30	9.6525	9 9820	9'9511	9'4499	925440	9.9717	72.5	+ 80	- 6 + 43	+115		+164 +148		
5254	291'02	-1'1523 -+0'8326	9.7519	271'10	90.17	9.5925	0.0000	9,9639	7.8383	925924	9.9639	89.6		 + 49	II6	+ 79	9	+ 52	p
		0'5006 0'0347										93.9	154 2						(
5258 5259	189.51 189.60	十0.1002 一0.1002	9 · 7042 9 · 7667	62.70	87.34 87.03	9.5510 9.5467	9·9963 9·9949	9'97¤7	921196 911852	925189 9'5011	9'9749 9'9770	98.0	170 122	+ 18 50	115 174	8 27	56 130	+ 3	1:1: t
		+0.8742		.		1	.							- - 66	g8	+ 47	- 45	- <del> -</del> 47	
5262 5263	76.19 319.24	+1:1692 -1:4513 -1:2720	9 · 7552 9 · 7432	50.51	86·58 :	9.5322 9.4931	9.9904	9'9733 9'9779	9'3193 924917	9'4301 823966	9.9837 9.833	77.5	*****	****	parame maram	version	Particular Section 1		$\left. egin{array}{c} p \\ p \\ p \end{array} \right $
		+1.2183 +0.4642		3'94	86·76	9.2129 9.4863	9.9865	9'9752 9'9786	913890 9.4852	9n3390 8:3453	9'9894 9'9894	72.2	-115	+ 10	<b>5</b> 5	+ 30	+ I5	+ 45	p
5266 5267	65 99 65 99	-0'5194 -0'2631	9.7634	171.43	90.89	9.4899 9.4867	9'9788	9'9782 9'9786	9n4845 9'4797	8 · 6842 8 · 7370	9'9995 9'9994	72'4	122 129	13 33	175 64	3o 1g	ro6	1 .	$\frac{t}{r}$
5268 5269	59'12 71'75	+0'1914 0'9658 +0'9504	7635	336 60 g	92.07	9 4954 9	9.8819 6 9.8810	9'9776 9'9776	9×4616 9 4553	9'0749 9n1139	9.9963 9.9969	73.3	127 (+103)	+ 28 (-82)	- 58	r8	+ 5	- 6 - 57	r
		+1.1467		1			,							~ -	87)	(-1-89)	177	+ 55	
5272 5273	184 · 80 -	-1.0480 5	7081	246.84	90.99 6	9.5787 g	3.333g	9.0 <u>6</u> 22	8n8255 8 6298	9°5649 9≈5760	9 ' 9 6 6 8 9 ' 9 6 6 8	94°1 87°4	+ 92			+ 5		 + 27	1) 1) 1)
5274 5275	82.78	-0.2941 c	7059	89.21 85.26	39.88 g	. 5981 0	.0000	9.9630	7.6931 824785	9,5968 9,5968	9 9 9 6 3 2 9 9 6 3 2	85.4 86.4	十111 一152		83		139 12		
5277	252 83 -	+0 4811 g -0 9482 g	7317 2	53 97 8	7 37 9	9.6160	9977	919595	920194	gafors	9'9623	96.5	+ 35 14		+110 ( 76)		-16g	+ 30 64	y.: s
5279	52.68	-1.3337 5 -1.3493 5	7517	67.94 8	36.37 5	6248	9954	9.9576	9'1627	9.5973	9,9631	80.0		-	Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salahan Salaha				$\frac{p}{p}$
5281	193 . 84 -	-o·6o16	7657	32.86	33.28	9.6699	9666	9'9464	9 5770	9.4408	9.9828	66 · g	+122	56	+173	- 25	128	13	t
5282	29 42 - 66 52 -	+0.0200 0	7488	205 · 65   8	33.82 g	9.6776	9 9 5 8 3 9	9 9442	9n6209 9 6255	9n3582	919884 919892	64.4	70 126	53	20 68	+ 33	+ 35 + 5	+ 15	t:li
5285	211.20	+0.9294	9.7221	16.41	35.36	9.6825	9.9494	9 9424	9.6584	9,1931	9 9943 9 9946	62.2	172 61	+ 40	114	15		32 (+79)	- 14
5287	348'90 -	-0.7838 c	7031 3	347. QI	93 ' 63 <u> </u>	9.6853	9'9458	9'9419	9 ' 6720	920720	9,0020	61,8		- 23	+ 46	- 68	+158	79	$\left  egin{array}{c} t \\ p \end{array} \right $
5289	185.62	+1.1287 9 -1.4527 9 -0.5154 9	7654	181.82	39'43	9.6849	9'9421	9'9420	9n6846	82530	9.9999	118.0		- 56	- 5	 46	— + 54		$\frac{p}{r}$
5291	250.43	+0.4214	7363	152.86	96 34	9.6759	9 ' 9 6 o x	9'9447	926126	9:3776	9.9873	115.0	20	48	+115	+ 41	+175	0	1014
5292 5293	342'77	+0'2205 g -0'3482 g +0'8928 g	7407	330.83	96 · 53 (	9.6679	9.9623 9.9696	9'945I 9'9470	9'6010 925580	9n4027	919856 919805	65 6	+155 - 46	- 11	-141	I	85 65	+ 36	1-14
5295	354 53	-1.1002	7041	134.89	g6 53	9.6564	9.9793	9,8200	9n 4786	9,5302	9.9735	108.4	— <u>55</u>	T 40	I		+ I3	7º	p
5297	218.82	-1.1575	9.7331	96.21	01.03	0.6011	9.9997	g · g624	8n6185	9.5987	9.9628	92.6	+ 18						$p_{r^*}$
5299	49'49	-0.2002 -0.1082 -0.1831	9.7576	85.76	89 ' 38	9.5834	9.9998	9 9655	8,4178	9 ' 5824	9.9657	88 4	+ 79 -115 + 70	+ 4	- 50	+ 29	+ 17	+ 7	$t^{*}$
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Nr.	Julian Kalei		Julian. Tag	Welt- Zeit	$m{L}'$	Z	ε	P	Q	$\log p$	$egin{array}{c} \log \ \Delta L \end{array}$	$\log q$	u'a	$\log f_a$	$\log \gamma$
5301 5302 5303 5304 5305	1026 1027	V 19 XI 12 IV 9 V 9 X 2	2095 943 2096 120 2096 268 2096 298 2096 444	2 45'7 15 1'9 0 42'6	235 407 24 514 52 854	-1,32 -0,13 -3,35	23'562 23'561 23'561	9 026 166 199 196 098	187°581 7'868 168'616 198'111 342'906	0.7409 0.7133 0.7020	9'7042	8 · 7597 8 · 7096 8 · 7359 8 · 7481 8 · 7404	0.5310 0.5729 0.5469 0.5382 0.5485	7.6764	9n8002 9°9342 0°0888 0n1430 0n1135
5306 5307 5308 5309 5310	1028 1028 1029	XI I III 28 IX 21 III 17 IX 10		22 39 9	183·899 2'929	+0'74 -2'29 +1'70	23'561 23'561	353'484 182'220	176 '274 352 '562 182 '186	0.7355 0.6918	9'7278 9'7131 9'7619 9'7606	8 · 7279 8 · 7149 8 · 7587 8 · 7058 8 · 7571	o·5589 o·5627 o·5367 o·5707 o·5366	7.6755 7.6679 7.6710 7.6692 7.6697	0°1758 9°7149 9″7446 9″3308 9°1701
5311 5312 5313 5314 5315	1030 V	III 7 III 31 I 25 VII 22 I 15	2097 655 2097 833	14 5'3	311'436 123'766	-0.20 +3.80 +1.13	23.561 23.561 23.562	10 118 165 646 348 141	188'052 12'549 164'600 349'198 174'439	0.7124 0.7009 0.7421	9 7125 9 7400 9 7514 9 7050 9 7635	8.7147 8.7375 8.7490 8.7081 8.7612	0.5646 0.5475 0.5449 0.5651 0.5385	7.6706 7.6683 7.6752 7.6641 7.6761	9n9666 9'955x 0'0624 0n0528 9'6600
5316 5317 5318 5319 5320	1033	I 4	2098 187 2098 365 2098 541 2098 719 2098 866	13 30.7	278.952	+2.42 +0.53 +1.21	23.562 23.563	182'516 4'318 190'430	355'173 184'375 2'035 192'814 342'125	0.4212 0.4213	9'7044 9'7538 9'7250 9'7281 9'7603	8 · 7075 8 · 7516 8 · 7237 8 · 7284 8 · 7553	0.5650 0.5443 0.5530 0.5596 0.5333	7.6768	9#5786 9#3386 9*6007 9#9768 0#1462
5321 5322 5323 5324 5325	1034 1035	VI 18 XI 13 V 10 XI 2 IV 28	2099 043	21 37.7 8 20.7 21 32.4	237 270 54 173 225 868	-3 28 -1 36	23'564 23'564	165 · 704 352 · 127 172 · 934	165 941 352 913 171 317	0.6013	9'7511 9'6997 9'7631 9'7096 9'7454	8.7466 8.7059 8.7583 8.7132 8.7417	0.5382 0.5756 0.5320 0.5694 0.5424	7.6637 7.6757	0.0540 0.1347 9.8259 9.8244 8.8490
5326 5327 5328 5329 5330	1037	X 22 IV 18 X 11 III 8 IX 1	2099 930 2100 106	9 23.3 18 33.0	204'023	-0.69 -3.54 +2.47	23'565 23'565 23'565	9 326 188 850 346 433	178'300 11'375 187'443 345'847 167'977	o'7308 o'6941 o'7436	9'7359 9'7186 9'7586 9'7016 9'7564	8 · 7345 8 · 7185 8 · 7555 8 · 7662 8 · 7522	o:5536 o:5583 o:5397 o:5708 o:5383	7.6656 7.6735 7.6704	8n8196 9'9384 9n8791 on1118 o'0720
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5336 5337 5338 5339 5340	1041 X 1041 X	VII 30 XII 26 VI 20	2101 317 2101 494 2101 643 2101 819 2101 997	9 21.0	132 494 280 510	+1 03 +1 37 +0 05	23 563 23 563 23 562	346 648 169 127	9:619 190:282 348:856 166:700 356:665	0.7040	9'7629 9'7021 9'7475 9'7329 9'7202	8.7598 8.7060 8.7454 8.7300 8.7218	0 5671 0 5482 0 5485	7.6649 7.6772 7.6627	9'9429 ono130 ono654 9'9931 9n7084
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5346 5347 5348 5349 5350	1045	X 13	2102 883 2103 030 2103 059 2103 208 2103 384	1 15 2 14 54 5 5 45 9	205 452 235 296 24 534	-3.40 -0.11	23'559 23'559 23'559	344 977 16 489 173 858	197:373 342:659 14:077 175:546 352:323	0'7083 0'7207 0'7365	9'7509 9'7437 9'7292 9'7119 9'7623	8:7465 8:7418 8:7293 8:7139 8:7593	0.5484	7.6632 7.6737 7.6764 7.6665 7.6724	0n1224 0n1199 01717 917636 9n7667
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530	302°52	-0.6313	9.7667	74°56	87°99	g'5654	9.9982	g · g684	8.0612	9'5515	0.0705	84°4	+ 7	41	+ 59	10	+114	31	t
530	3 222,33	+0.8594	9'7064	246 41	87.29	9.5507	9,9960	9,9706	921281	925173	9'9751	q8°2	+101	+ 6 r		+ 41		+ 47	7:1
530	188.22	-1.3987	9'7541	62'59	86.99	9'5490	9'9947	9,0400	0.1888	0 5032	0.0768	80.6						-	$\stackrel{\mathcal{P}}{\stackrel{\mathcal{P}}{=}}$
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5307	100.24	+1.4990	9.7153	17.30	88.30	9'4914	9,9803	9'9781	9.4695	8.0820	9 9980	72.8	+133	+ 14	165	+ 38	 89	+ 48	2)
5308	294'40	-0'5554 -0'2142	9.7640	184.81	89.50	9'4889	9 9785	9 9783	9114872	824342	9 99998	107.0	3	16		- 37	-136 -114		1 a B
5310	180.00	十0'1479	9.7627	171.94	90.83	9.4889	9.9788	9 9 9 7 8 4	924842	8.6568	9.9996	107.8	+114	+ 26	179	- - I2	-117	- 9	
5311	185 59	-0'9260	9 7146	349 96	91'03	9 4889	9.9791	9 9783	9.4815	817513	9'9993	72.3	<b>+</b> 60	84	177	- 80	гоз		1.
5313	114.85	+0'9018 +1'1545	9'7534	302.02	93'22	9.2409	9 9932	9'9721	9.2453	924766	9.9796	79 * 4	*******	+ 79 	22	+ 77 	56 	+ 47	p p
5314	342'18	1'1292 0'4571	9.7656	289.39	92.98	9 · 5529 9 · 5583	9.9963	9 ' 9704 9 ' 9695	921167 9'0521	9 5216 925361	9.9746	83.1 38.0		1g	16	+ 7	72	+ 32	$t^{p}$
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53×7	213.30	-0.3084 +0.3084	9'7559	277'40	01.02	9.2481	9 9996	9 9665	8.6548	9115750	9.9670	87.2	+ 76	X4	+147	35	¥45	9	t
5310	18.89	-0'9480 -1'4003	9.7302	265.72	89.33	9'5974	9 9998	9*9630	824334	945964	9.9632	9x'7	147	6o	(+160)		+ 83 +115	- 62	9.
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5325	178.89	-1-0.0706	9 7475	33.11	83.25	6701	9.9668	9463	9 : 5757	9 4437	9 9825	66.9	-123	18	180		108	' -	
5326	237 12	-0.0660	7380	205 . 64	83'82	6775	9 . 9 5 8 3	9442	926209	9×3579	9.9884	115'4	<b>⊹</b> 65	- - 21	+122	- 17	I67	- 28	
3320	09.00	+0.8678	3.40041	197 47	85 . IO 6	3.0830	9.50010	0.427	G2 5553	0 2 2 1 1 5	0'0042	64'4 117'3	- 44 - 146	+ 34 22		+ 87 68		+ 77 74	t t
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5334	203.10	+0.4824 +0.1084	9 7480	339 41	95 ' 43 !	9'6813	9 9530	0.0431	0.6447	022764	0,0021	63.3	-l- 30	T5	-l- 04	-1- 2	T52	+ 37	r-t#
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5336 5337	121.83	+0.8768 -1.0304	9 · 7650 ;	330.99 144.01	96 48 9	9·6734 9·6671	9 9624	9454	g · 6010	923995	9.9858	65 7	+171	- <del>-</del> 36	132	+ 60	-117	+ 75	
5338	130,88	-1'1625 -0'9842	9.7496	294'42	94'01	9 6284	9 9943	9568	9 ' 2085	925945	0.0636	79 9			(	(			p
5340	327 13	-0.2110	9.7224	283 48	92.19	6120	9.9983	9.0602	8,9419	926018	9 9 9 6 2 2	84.2	49	33	+ 34	- 54	+174 +109	+ 6x - 23	1
5341	159.67	-ho:1832	9.7588	96.98	91.11	9 6016	9.9996	9.9622	8n6492	915989	9.9627	92 8	+131	+ 12	-159	- - 34	- 92	+ 7	t ^a :
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5349	268 26	+1.4850 +0.5802	9.7141	30.51	87:29	9.2014	0.0836	0.0770	0.4320	0.2200	0.0030	74 T	22	 + 19	+ 87	 + 47	 170	- + 50	$r^*$
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5356 5357 5358 5359 5360	1049 1050 1050	VIII I	2104 2104 2104	418 595 772	13 :	24'2 41'5 56'1	311.	271 827 485	+2.61 +1.01 +3.86 +1.13 +3.33	23° 23°	558 559 559	347.337 174.480 355.200	195.093 348.290 174.420 354.212 184.367	0'7117 0'7429 0'6891 0'7422 0'6994	9.7404 9.7042 9.7640 9.7049 9.7527	8.7379 8.7077 8.7612 8.7081 8.7505	0:5486 0:5660 0:5378 0:5651 0:5446	7.6706 7.6649 7.6752 7.6641 7.6761	011884 010816 9.6701 916626 913259
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5366 5367 5368 5369 5370	1053 1054 1054 1055	XI 13 V 10 XI 2 IV 29	2106 2106 2106	983 161 337 515	5 3 7 1 11 5 16 2	37°1 36°3 31°8	236 · 54 · 54 · 64 · 64 · 64 · 64 · 64 · 6	986 513 855 096	-1'26 -3'30 -1'35 -3'77 -1'15	23.	562 562 561- 562	172.800 0.004 180.568 8.563	10.547	0.6919 0.7357 0.7093 0.7134 0.7320	9'7627 9'7105 9'7372 9'7372	8.7576 8.7140 8.7401 8.7359 8.7173	0.5320 0.5693 0.5427 0.5533 0.5583	7.6632 7.6764 7.6638 7.6757 7.6645	9,8698 9.8317 6.5512 8,7075 9.9027
5371 5372 5373 5374 5375	1056 1056 1056 1057	III 19 IX 12 X 11 III 8	2107 2107 2107	840 017 046 194	1 4 7 2 17 1 4 2	4'0 0'1 2'9 2'7	4 1 175 1 204 1 353 1	438 221 445 478	+1.57 -1.59 -3.56 +2.47	23 23 23 23 23 23 23 23 23 23 23 23 23 2	562 562 562	345'907 165'705 196'661		o 6931 o 7434 o 6977 o 6907 o 7281	9'7593 9'7023 9'7554 9'7624 9'7208	8.7564 8.765 8.7514 8.7590 8.7210	0.5401 0.5697 0.5397 0.5378 0.5597	7.6747 7.6691 7.6698 7.6735 7.6705	9,18668 0,1278 0.0883 0,1462 9,17649
5376 5377 5378 5379 5380	1058 1058 1059 1059	IX 1 II 25 VIII 22 II 15 VIII 11	2107 2107 2107 2108	548 726 903 080	0 4 5 1 1	1.0 4.0	342 ° 2 153 ° 2 332 ° 2 143 ° 0	734 921 149 036	-0.71 +3.23 +0.10 +3.77	23°5 23°5 23°5	562 562 562 561	1.929 182.220 10.115 189.986	359 663 183 537 9 484 189 398	0'7046 0'7400 0'6897 0'7437	9'7305 9'7474 9'7069 9'7633 9'7025	8.7289 8.7443 8.7097 8.7599 8.7062	0.5530 0.5452 0.5657 0.5369 0.5676	7.6684 7.6718 7.6670 7.6731 7.6659	9'7305 9'2297 9n3259 9'9321 9n9807
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5391 5392 5393 5394 5395	1063 1063 1064 1064 1065	X 13 IV 8	2109 ( 2109 ( 2109 ( 2110 )	644 793 970 147	23 2: 12 4: 0 10 13 4:	3.1	246 · 4 35 · 1 205 · 8 24 · 2	63 18 01 77	-2:56 -0:76 -3:63 -0:08	23.5 23.5 23.5 23.5	557 557 556 556	344'774 16'420 173'147 352'849 180'977	13'990 174'745 352'153	0.7070 0.7194 0.7875 0.6905 0.7449	9.7450 9.7307 9.7108 9.7626 9.7012	8.7305	0.5483 0.5579 0.5626 0.5376 0.5688	7.6748 7.6770 7.6655 7.6736 7.6666	0n1244 01687 98120 9n7836 8n9745
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5300	343.05	-0.3118	9.7548	289.81	92'41	9.5575	9 9971	9.9697	9 0605	925343	9.8430	83.0	- 54	18	+ 18	- 32	- - 8 ₃	5	
5362	144'40	+0.3186 -0.3186	9.7288	277 84	gr'rr'	9 5778	9 9995	9 9 9 5 6 5	8.6800	925743	9.0621	87:0	ー167 十 82		- 94 (+ 37)		- 25 - 20	+ 14 - 59	
5363 5364	270.38	-1.4683 +1.0555	9 7530 9 7545	61.30	85 35 8 89 96	9.6335	9.9920	9 9557	9'2801 7'2630	9'5860 9'5910	9'9651 9'9642	28.1	#*************************************	_	- 3//			-	p.
5365	270.6x	+1.3740	9.7016	234 ' 72	84.42	9 6437	9*9875	9.953r	913730	9n5702	9 9677	104.7	processor		_	-	Begannet	-	p p
5366 5367	61 16 260 54	-0.7410	7648	51.25	84.02	9.6482	9 9849	9.9522	9'4144	9'5577	9.9697	73.8	- 97	- 57	- 56	- 29	I	29	
5368 5369	289 28	+0.0210	9'74bi	42'02	83.50	9.0003	9 9764	9'9491	9'5059	9'5126	9'9757	70.1	14	IO	7I	+ ro	-LTAT		l**
	64.35	+0.4993	9. 7 x 93	33.23	83.26	9.6696	9 9670	9 9465	9'5745	9 4444	9.9825	67.0	- 146	-h 29	- 74	+ 75	+ 57	24 69	
5371	198.10	-0:7358g	7614	205 '94	3,81	6764	9588	9445	9n6185	923611	9 9882	115'3	+ 84	2I	+153	б8	89	68	t
5373	294.72	-1 3420 g	7574	176:56	) r , o g   č	3 . 6899 . S	9418	9415	9n6856	8 5225	180001	110.0	Breedom .				- Francisco		$p \\ p$
5374	78 37	-1'4003 5 -0'5820 9	7229	355.33	1.42	0.9881 0	9512	9437	9.6863 9.6863	9n2186   8n6571	9.9940	60.0	+ 43	- 6 ₅	+124	- - 44	 178	— б	$r = \frac{p}{r}$
5376	15.24	+o.2376 g	. 7326 r	68.99	3 · 28 g	. 6867 9	9446	9415	926762	0.0237	9.9976	118.5	+167	- <del> </del> - 60	107	44	- 48	4	21111
5378	90.26	-0,5118 d	7495 3	61'06	5'14 9	6831 g	9457 9 9511 9	9417	9.6725 ( 9.6521 (	920743 9	9'9969 9'9932	61'7	- 93 - 106	18 15	29	+ 4	+ 32	+ 38 30	$t^{*!}$
537912	50.081-	-0.82255 -0.8225	705413	330.0110	5 30 C	08036	1 0 5 3 0 0	.0434 0	3'6445	102712	100001	62.2	40	+ 31 46	+ 99		+120 (+127)	+ 78	t _{it} :
5381	320.04	-1'1702	7484	305'31	5.28	6434	9875	0.532	9'3732	n 5508	0.0678	75.3	_		******	_			<b>J</b> )
5383	67 57	+1.0280 c	7366	331.05	94.23	6329	9 9 6 2 8 9	9462	9.5987	923954	9.0861	65 ' 8		-	powers.	_	Production	positive processed	$\stackrel{(p)}{p}$
5384	91,18	-0.2579 s	7210 2	294'87 9	)4 ' 0 9   c	0.6204 0	0.0040	0.0565	0.2160	205042	2.0626	70.7	-176 + 16	- 37 + 20	8g	- 55 - 39	17 - -158	一 19 十 7	r t*
		+0'1697			1	.											_		
5387	100.08	-0.4859 -0.8408	7662	97.37	31.12/5	6022	9995	9621 8	8n 6733	5002	0.0627	92.0	-173 +137 -146	- 24	-167	6		- 29	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
5389	271 25	-1,3202 c	7386	54 76 8	36 ' 70   9	5353	9920	19728	9 2780	9'4561	0'0815	78 6			-103	+ 34	— бт	+ 51	29
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5392	r 68 ' 83¦∙	-1:3317 9 +1:4747 9 +0:6487 9	7327 2	258.31 8	38 4 1   9	9'57I9 9	9 ' 9 9 9 0   9	9675	8n 8473	9n 5640	9'9687	04 . 3					mann.	_	$p \\ p$
5394	187 '83  ·	-0.6076 c	7647 2	2 X I ' 56 8	37'18 9	5048	9 8889	9767	9n4287	92404	9 1 9 9 3 4 1 :	105'8		- 21	- -168	49	-105	+ 52 - 52	riii t
	l		1	1	1							74 I		- 21		T 4	+ 37	+ 10	7 ^{1.1} 1
5397	48'03	+0'0806 g	7175	10.20	38.35[9	9'4915 9	9 980 r g	9'9780	9 4712	8 0666	11800'0	72 ' 7	105	- 72	4I	1 54	4 22	- 12 - 38	t ^{ali}
5399	8 48	+0.8232 0	9 7558 3	327.90	)2 ' go g	5087	9 8 8 8 9 1	9762	9 4296	92500	0.0030	74'1	+ 27	+ 73 	+102 -	+ 58	-⊹168 	+ 37	p
3400	. 09 OI	1 * 5000 9	7439	3 33	, y 05 5	9 4910	9761	9780	9 4908	0 2774	9.9999	72'0	-			-	· <del>-</del>		p
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n	onkschri	ften der ma	themna	turw. Cl.	LII, Bd.												28		

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INT.	Julianischer Kalender	Julian. Welt- Tag Zeit			ε	T	, V.	$\log p$	$\Delta L$	$\log q$	u _a	$\log f_a$	logy
5401 5402 5403 5404 5405	1068 II 6 1068 VII 31 1069 I 25	2111 357 20 35 4 2111 535 19 45 7	322.903 133.985	+3.86 +3.86	23.556 23.556	174 '295 354 '391 182 '313	347°433 174'351 353'298 184'307	0.6894	9'7639 9'7656 9'7518	8.7072 8.7611 8.7088 8.7495 8.7265		7.6660 7.6742 7.6649 7.6753 7.6640	0n 1067 9.6847 9n7293 9n3042 9.3848
5406 5407 5408 5409 5410	1070 VII 10 1070 XII 5 1071 V 31	2111 890 6 20 0 2112 066 13 35 8 2112 214 13 38 1 2112 391 23 20 1 2112 568 13 47 4	259'596 75'113	-0.84 -1.16	23'557 23'558 23'558	11'319 165'515 350'435	192.618 9.379 165.539 351.502 170.936	0.7238 0.7004 0.7444 0.6927 0.7347	9'7538 9'6994 9'7620	8.7260 8.7493 8.7061 8.7570 8.7150	0.5370	7.6762 7.6633 7.6773 7.6628 7.6770	9"9737 9'9911 0'1405 9"9111 9'8361
5411 5412 5413 5414 5415	1072 XI 12 1073 V 9 1073 XI 2	2112 746 14 26 2 2113 277 2 43 6 2113 277 2 43 6 2113 425 8 46 2	236 993 54 586 226 158	-3'30 -1'33 -3'30	23.559 23.559 23.560	7 747 188 457	1 · 561 178 · 046 9 · 662 187 · 247 344 · 507	o'7109 o'7122 o'7334 o'6923 o'7430		8.7386 8.7372 8.7163 8.7573 8.7068	0.5433 0.5530 0.5586 0.5403 0.5684	7.6632 7.6764 7.6638 7.6756 7.6678	8n8672 8n6157 9.8610 9n8577 On1452
5416 5417 5418 5419 5420	1074 IX 23 1074 X 23 1075 III 19 1075 IX 13		186 069 215 484 4 264 175 442	-2:43 -3:85 +1:60 -1:59	23'560 23'560	165 '272 196 '433 353 '229	15'959 167'204 197'422 350'984	0'7446 0'6987 0'6910 0'7270 0'7216	9'7015 9'7541 9'7618 9'7225 9'7288	8.7053 8.7505 8.7585 8.7222 8.7276	0.5673 0.5411 0.5387 0.5581 0.5547	7'6646 7'6712 7'6746 7'6691 7'6698	0'1771 0'1019 0n1407 9n7965 9'7681
5421 5422 5423 5424 5425	1076 IX 1 1077 II 25 1077 VIII 21 1078 I 16	2114 488 13 28 1 2114 665 8 1 8 2114 813 17 55 4	164 595 343 102 153 639	-0'70 +3'20 +0'12	23'559 23'559	181'593 9'792 189'279	359,316 182,816 9,276 188,581 348,797	0'7034 0'7407 0'6896 0'7433 0'7065	9'7489 9'7058 9'7636 9'7028 9'7450	8.7455 8.7092 8.7601 8.7066 8.7429	0.5436 0.5673 0.5361 0.5682 0.5491	7.6705 7.6684 7.6718 7.6670 7.6760	9'1289 9'1825 9'9'81 9'9486 0'0723
5426 5427 5428 5429 5430	1078 VII 11 1079 I 6 1079 VII 1 1079 XII 26	2114 989 23 26.4 2115 168 2 22.6 2115 344 13 20.2 2115 522 3 42.5	291'800 104'335 280'411	+1 01 +2 57 +0 64 +1 35	23 '558 23 '558 23 '557 23 '557	167 412 354 373 176 149 1 694		0.6961 0.7164 0.7302 0.6957 0.7437	9'7362 9'7176 9'7587 9'7001	8.7331 8.7195 8.7539 8.7066	0'5471 0'5654 0'5340 0'5758	7.6732 7.6634 7.6767 7.6629 7.6772	9.2122
5432 5433 5434 5435	1081 V 11 1081 VI 9 1081 XI 3	2115 699 6 37'3 2115 876 3 6'5 2116 024 12 56'3 2116 053 22 38'4 2116 200 18 8'5	56 162 84 227 227 591	-0'06 -1'34 -0'43 -3'74	23.556 23.556 23.556 23.555	8 8 8 0 2 163 9 8 2 193 5 7 1 344 6 2 7	7'360 166'416 195'795 342'381	0.6909 0.7388 0.7176 0.7061 0.7056	9'7067 9'7349 9'7480	8.7114 8.7323 8.7437	0.5720	7.6626 7.6774 7.6637 7.6626 7.6758	9'9214 0'1564
5436 5437 5438 5439 5440	1082 IV 30 1082 X 24 1083 IV 19 1083 X 14	2116 910 0 48.4	45 644 216 851 34 852 206 222	-1.19 -3.88 -0.75 -3.64	23 555 23 555 23 554 23 553	172'374 352'635 180'249 0'657	13.935 173.881 352.046 179.872 2.213	0 7181 0 7385 0 6902 0 7447 0 6948	9.7099 9.7628 9.7015 9.7580	8.7117 8.7602 8.7060 8.7551	0.5625 0.5380 0.5679 0.5402	7.6773 7.6645 7.6748 7.6655 7.6736	0 1664 9 8592 9n7960 8n3806 8 7522
5441 5442 5443 5444 5445	1084 X 2 1085 II 26 1085 III 28 1085 VIII 23		195 516 344 460 13 459 155 437	-3.14 +0.80 -0.10	23.553 23.553 23.553 23.553	165 903 196 537 345 902	11'266 164'056 194'155 346'635	0'7324 0'7161 0'6981 0'7093	9'7350 9'755x 9'7437 9'7026	8 · 7336 8 · 7518 8 · 7406 8 · 7068	0.5527 0.5409 0.5453 0.5685	7.6666 7.6723 7.6716 7.6680 7.6673	9n8837 9'8996 0'0827 0n1616 0n1282
5446 5447 5448 5449 5450	1086 VIII 12 1087 II 6 1087 VIII 1	2118 121 4 16·6 2118 297 8 34·5	333 919 144 540 323 292 133 895 312 399	+3.97 +1.05	23'553 23'553 23'554	353 643 182 134 1 858	352'444 184'193	0 6895 0 7409 0 7018 0 7219 0 7249	9'7064 9'7508 9'7297	8 · 7096 8 · 7484 8 · 7281	0:5654 0:5447 0:5514	7.6730 7.6660 7.6742 7.6649 7.6753	9'7034 9n7829 9n2707 9'2329 9n9691

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5401	125011	-1.2785	9 ' 7055	137°26	03°28	0'5175	o'0876	0.0751	a» 3716	0.3633	0 0882	10400							21
5402 5403	129,39 153,45	-0.4839	0.2028 0.2028	314.95 124.39	93'32 93'24	9.5200	9 · 9884 9 · 9924	9'9747 9'9730	9°3561 9°2671	923822 9'4587	0.881 <b>3</b>	201.1	+ 54 +172	- 20	-132	<b>— 16</b>	- 79	41	te 1
5405	200 03	-0.3426 -+0.3426	9 7303	112.31	92. <u>6</u> 2	9.5375	9.9965	9*9725	9°2475 9n1068	914712 9:5234	9'9743	97 8	+ 89	2I 2I	-+161	- 29 + 34	- 48 -135	+ 6	
5407	20'44	-0'9412 -0'9797	9.7559	101,15	91'52	9.5725	9,9991	9.9674	8,18263	9 5654	9'9685	94'I	-176	67 -+ 67	(- 86) (+161)	(-88) (+79)	-155 117	— 57 + 64	$t^{:::}$
5409	172.96	+1:3820 -0:8148 +0:6857	9,7641	δ1'22	85.35	9.6344	919919	9'9553	9'2819	9 ' 5868	9'9649	78.0	+154	- 58 + 52	169 26	- 34 + 23	-117 + 26	- 39 + 26	p t
5411 5412	37'97 120'55	0'0736 0'0413	9'7445	51'44	84 · 03	9'6484 0'6570	9.9850	9'9521	9.4126	9.5589	9'9695	73'9	~ 93	19	- 37	- - I7	+ 29	+ 11	ℓ#: 2·#:
5413 5414	327·46	+0.7262 -0.7262	9'7 ¹ 79 9'7622	42'10	83 · 30	9 • 6599 9 • 6678	9 ° 9 7 6 5 9 ° 9 7 6 5	9'9492 9'9470	9 ' 5060 9 2 5628	9.5128 914598	9'9757 9'9812	70'2 112'4	+113 - 47	十 25	-175	+ 70	- 59 - 61 +140	20 60 63	21.112 t
		+1.2032 -1.3040	[												_				$\mathcal{P}$
5417 5418	56.99 207.00	+1.3827	9'7561 9'7561	184°36 206°49	88 · 66 83 · 84	g:6865	9'9420	9'9415 9'9454	9n6848 9n6133	8n6259 9n3655	9 · 9880 9 · 9996	115.0	breeded.	_					$p \\ p \\ p$
5420	230.53	0.259 0.2863	9.7309	176.24	91'02	9.6886	9'9413	9'9410	910873 9n6877	8.2010	9,9998	119'2	+ 58	+ 65	+ 11	44 44	69 163		144
5422	297.00	+0.1346 0 -0.1522 0 +0.8282 0	7080	,68 · 96 6	93'3I	9.6875	9 ' 9444	9'9412	926769	9 '0260	9'9975	118'5	o	+ 20	-∤- бі	4	+119	- 37	2'
5424	297'72	-0.8884 g	7050	rбо 82  c	25 . 17 9	9 6823	9 95 16	9429	gn6506	9'2491	9'9931	117.0	— 29 — 7	- 35 			+ 50		
5426 2 5427 1	73 57	+1.230 c	7587	339 ' 73 5	95 · 24 g	9.6772	9 9 5 3 6	9 9443	9.6420	92551 95605	9'9925	63'5	turen.	_					p p
5428 2 5429	20.26	-0'5242 g -0'3317 g -0'1630 g	0.2608 3.2188	305 · 68 <u>c</u>	95.65 g	9 6349 9 6340	9.9872	9.9530	9:3787	915695 915879	9 9 9 6 7 9	75'I	58 99	42 28	149 18		+ 48	+ 7	1.41 3.
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5433	19 23	-0.4116 +0.8344 -1.4337 -1.1870	3.7309	00.72	37 29	9 5535	gʻggbri	9'9702	9'1250	9'5211	9'9746	81,0	+ 88	+ 46	+134	+ 33	+173	+ 54	p
5435	99.26	-1.3400	7482	236.60	86.73	9'5398	9.9927	9'9722	9n2597	9n4698	9'9802	101,0		_			_	_	p p
5437	(16,33	+1'4670 g +0'7232 g -0'6251 g	9.2121	55 15 8	86 * 75	9'5333	9 9 9 9 2 2 0	9'9730	9 2717	9'4550	9'9815	78.7	162	+ 33	— —121	 + 64	- 22	+ 54	p $t$
5439	(27.28	-0'0240 -0'0565	9.7037	42'07	80.20	9'5146	gʻg8781	9'9755	9'3694	9 ' 3586	gʻq884	76°I	176	- 15	I27	I2	l 64	12	21
5441 5442	156.62 25.41	-0.7650 q	9.7190	29'57 199'04	87 '32 88 '10	9'5013 9'4954	9 · 9833	9 ' 9770	9'4349 9n468s	9,2118	9'9942	74.0	+152 - 82	64 60	150 10	43 50	- 91 44	- 33 - 35	2°
5443	133.31	+1 · 2097 -1 · 4507 -1 · 3433	9 7571	15.46	91.91 88.32	9 4982 9 4957	9 9800 9 9797	9'9773 9'9776	9'4715 9'4756	9n0296 8 9685	9'9975 g'9981	72.7				_			p p
5446	10.55	+0'5051	9.7661	328.06	92.83	9 . 5047	9.9839	9 9766	9'4256	9n 2447	9'9932	74 3	- 76	+ 14	- 14	+ 22	+ 47	AR	$p$ $t^{*}$
5447 5448	239'59 231'89	—0'1710 —0'1865 +0'1710	9.7086	312,32	93 27	9.2101 9.2100	9 '9879! 9 '9883	9'9752 9'9749	913669 913587	9 3652 9n3781	919880	76.4	+ 67 + 50	- 23 - 24	+124 +122	- 25 - 25	+179 -176	- 49 + 3	1. t#
5450	32'49	-0'9314	9.7260	302.86	93 . 22	9.5378	9.9929	9'9724	9.2526	9n4699	9,0803	79'2	-170	- 70	T 54		+115	— I	r
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5451 5452 5453 5454 5455	1088 1088 1089 1089	VII 20 XII 15 VI 11 XII 4 V 31	2118 65 2118 79 2118 97 2119 15 2119 33	3 22 1 6	270.776 85.555 259.325	+0.10	23.555 23.555 23.555	165'443 349'557 172'643	8°664 165:356 350'766 170'799 0'730	o.6992 o.7445 o.6934 o.7338 o.7125	9'7550 9'6995 9'7613 9'7129 9'7408	8.7507 8.7062 8.7562 8.7160 8.7371	0'5368 0'5763 0'5326 0'5685 0'5441	7'6640 7'6774 7'6626 7'6773 7'6628	9.9580 0.1427 9n9496 9.8391 9n1780
5456 5457 5458 5459 5460	1090 1091 1091 1092 1092	XI 24 V 21 XI 13 IV 9 V 9	2119 68	6 5 57°1 2 18 28°7 0 15 40°6	237.301	-1.53	23.556 23.556 23.556		8 · 725 187 · 234 343 · 729	0.7107 0.7346 0.6918 0.7427 0.7447	9.7398 9.7145 9.7606 9.7039 9.7016	8.7385 8.7150 8.7580 8.7074 8.7052	0'5525 0'5590 0'5404 0'5673 0'5668	7.6770 7.6632 7.6764 7.6664 7.6638	8n5438 9.8x16 9n8513 0n1639 0.1540
5461 5462 5463 5464 5465	1092 1092 1093 1093	XI 2 III 29	2120 21 2120 35 2120 54	7 23 39 6 7 10 25 7 4 19 19 8 2 10 51 2 9 6 3 6	226.582 14.982 186.272	一3.77 十0.67	23'557	352.664 173.136	350,326	0.6995 0.6913 0.7257 0.7228 0.7024	9'7529 9'7612 9'7243 9'7270 9'7504	8.7496 8.7581 8.7235 8.7263 8.7466	0.5426 0.5397 0.5561 0.5566 0.5421	7.6725 7.6756 7.6678 7.6691	0'1129 0n1367 9n8298 9'7981 8'9675
5466 5467 5468 5469 5470	1094 1095 1095 1096 1096	III 8 IX 1 I 28 II 26	2121 07 2121 25 2121 39 2121 42	8 13 56.1	353.987 164.302	+2:42 -0:68 +3:88	23'557 23'557 23'557	9'391 188'642 346'377		0.7412 0.6893 0.7427 0.7080 0.6974	9'7047 9'7639 9'7030 9'7438 9'7557	8.7087 8.7601 8.7070 8.7414 8.7523	o'5686 o'5352 o'5689 o'5492 o'5405	7.6698 7.6705 7.6684 7.6751 7.6718	8n9979 9.8999 9n9173 0n0779 0.1763
5471 5472 5473 5474 5475	1096 1096 1097 1097 1098	VIII 20 I 16 VII 11 I 5	2121 75 2121 92 2122 10	4 18 26.6 3 10 36.2 9 20 47.5 7 11 43.3	302.943 114.802 291.573	+0'14 +3'43 +1'04 +2'52	23.556 23.556	196'623 354'270 175'301	194'353	0'7149 0'7266 0'7311 0'6947 0'7441	9'7379 9'7237 9'7164 9'7597 9'7000	8.7346 8.7229 8.7185 8.7550 8.7063	0.5465 0.5562 0.5657 0.5338 0.5756	7.6642 7.6670 7.6760 7.6634 7.6767	0.0778 0.1811 9.7282 9.6060 9.1870
5476 5477 5478 5479 5480	1098 1098 1099 1099	V 22 VI 21 XI 15	2122 46 2122 60 2122 63 2122 78	9 5 51 4 6 2 44 7	280 · 107 66 · 625 94 · 661 238 · 737	+1.30 -1.18 +0.14 -3.51	23.554 23.553 23.553 23.553	192.699 344.529	7'211 165'574 194'977 342'327	0.6914 0.7378 0.7192 0.7073 0.7044	i	8.7584 8.7121 8.7305 8.7424 8.7455	0.5315 0.5714 0.5486 0.5408 0.5479	7.6629 7.6772 7.6631 7.6626 7.6765	9"5290 9'9173 0'1794 0"0474 0"1286
5481 5482 5483 5484 5485	1101	XI 3 IV 30 X 24	2123 14 2123 31 2123 49	0 17 27 3 8 3 5 9 5 9 19 3		-3 74 -1 18	23 552	352.485 179.465	352'007	0.73931	9.7088	8.7606 8.7606	0.5566 0.5627 0.5385 0.5669 0.5414	7.6774 7.6637 7.6758 7.6645 7.6748	0°1644 9°9044 9°8043 8°7126 8°5868
5486 5487 5488 5489 5490	1102 1103 1103 1103	X 13 III 10 IV 8 IX 3	2124 02 2124 17	9 21 42 3 7 5 3 3 6 15 1 0 4 9 58 6	206 '485 355 '332 24 '132 166 '116	-3.65 +2.32 -0.05 -0.80	23.221 23.221 23.221	8,536 165,505 195,933 345,286	163'743	0.2122 0.2080	9'7332 9'7562	8.7190 8.7322 8.7527 8.7420 8.7066	0'5582 0'5543 0'5395 0'5437 0'5695	7.6655 7.6736 7.6703 7.6666 7.6685	9n8440 9'8869 0'0937 0n x446 0n x468
5491 5492 5493 5494 5495	1105	VIII 22 II 16 VIII 11	2124 52 2124 70 2124 88	3 11.8 1 21 16.3 8 10 19.6 5 12 39.0 2 15 49.4	344'808 155'153 334'302 144'468	+3.68 +0.67	23.551 23.551 23.550 23.550	173 719 352 961 181 888	174.009 351.663 184.006	o · 6898 o · 7400 o · 7030	9'7638	8 · 7606 8 · 7104 8 · 7472	0.5681 0.5359 0.5658 0.5446 0.5512	7.6723 7.6717 7.6673 7.6730 7.6660	0' x870 9' 7268 9n8262 9n2187 9' 0220
5495 5497 5498 5499 5500	1106 1107	XII 27 VI 22	2125 23 2125 38 2125 56	5 43'0 2 14 10'9	134'126	+1.05 +1.53 +0.25	23.551 23.551 23.552	165 368 348 681	7 ⁹⁹⁴	0.7444	9.7560 9.6996 9.7605	8 · 7518 8 · 7555	0.5367	7:6742 7:6649 7:6772 7:6627 7:6774	9n9625 9'9245 0'1447 9n9850 9'8408

Nr.	μ	ÿ	$\log n$	G	K	$\log \sin g$	log sin k	$\log \cos g$	$\log \cos k$	log sin δ'	log cosδ'	N'	_	)Auf- ng   φ	im M	ittag   φ	be Unter	i⊙ rgang   φ	F
5452 5453 5454	149'10 284'12 153'60	+0'9078 +1'3890 -0'8904 +0'6904 -0'1507	9.7016 9.7634 9.7150	257.00 71.70 245.17	87 89 86 99 85 92	9 6111 9 6191 9 6111	9'9985 9'9969 9'9940	9 ' 9504 9 ' 9588 9 ' 9565	829255 9'0787 922157	926016 9'6003 925040	9'9622 9'9625 9'9636	95°3 82°5 100°3	+ 46 +166	— — бо + 48	+ 79 -150	- 40 + 21	- 26  +124 - 99 - 81	- 49 - 30	$rac{p}{t}$
5457 5458 5459	98.63 59.20	0'0350 0'6480 0'7100 1'4583	9 · 7 · 6 6 9 · 7 6 2 7 9 · 7 · 6 5	51.49 224.51 18.86	84 ° 04 83 ° 44 84 ° 95	9 · 6482 9 · 6570 9 · 6805	9 9850 9 9788 9 9787	9'9521 9'9498 9'9434	9'4119 924840 0'6400	9'5591 9n5268	9'9595 9'9739	73.0 108.0	180 	+ 12 + 23 - 25 -		+ 64			91 ¹ 11
5463 5464	336.83 111.14 346.97	- -1 · 2970   x · 3700   o · 6758   o · 6282   o · 6282   o · 6288	9 7631 9 7264 9 7291	215.27 10.79 184.48	83 28 9 86 79 9	9.6650 9.6859 9.6884	9'9699 9'9448 9'9414	9'9478 9'9418 9'9409	9n5562 9 6758 9n6867	924629 9'0142 826401	9 * 9809 9 * 9977 9 * 9006	61.2	— —164 — 49	- - 68				+ 10	2.74
5468 5469 5470	43'38 215'94 22'17	0'0995 g +0'7942 g 0'8266 g 1'1965 g +1'5007 g	7052 77459 77576	355.09 9 168.73 9 325.11 9 347.98 9	93 · 33 9 93 · 36 9 93 · 45 9	0.6842 0.6869 0.6673 0.6817	9 · 94 · 8 ! 9 · 94 4 7 ! 9 · 96 8 9 !	9 9413 9 9472 9 9472	9'6856 9n6758 9'5626 9'6693	8n6219 9°0339 9n4588 9n0546	9'9996 9'9974 9'9813 9'9972	61'0 118'5 67'6 62'0	+145 -114	24	153	- 5 + 63 - 64	+ 14 - 83 - 17	4 44	tili
5473 5474 5475 3	92'38- 337'16- 31'86- 352'84-	+1.1962 g -1.5173 g -0.5348 g -0.4036 g -0.1538 g	7257	305.60 g	5 16 g 5 93 g 5 65 g	6477 9 6451 9	9 9523 9 9 9784 9 9 9852 9 1 9872 9	9 9434 9 9 9496 9 9 9523 9 9 9528 9	9n6475 9°4881 9n4092 9°3778	9°2515 9n5256 9°5596 9n5701	9'9929 9'9741 9'9694 9'9677	70'9 106'0 75'1	- -×45 56	47 37 6	-129	54 + 45 13	+ 93 - 63 + 58		t'ili
54773 5478 I 5479 2 5480 2	25.65 64.82 27.80	-0.3381 9 -0.8266 9 -1.5113 9 -1.152 9 -1.3447 9	7099 2 7353 7486 7494 2	78 · 37   8 78 · 37   8 408 · 27   9 449 · 36   8	4.01 9 3.00 9 7.48 9	6285 g 5722 g 6189 g 5587 g	9943 9990 9969 9968 9	9567 9 9574 8 99588 9	3.8453 c 3.8453 c 3.0778 c	)n5948 ( ) '5644 ( ) '6002 ( )n5335 (	9'9635 9'9686 9'9625 9'9731	79'9 85'7 97'5 97'3	- 37 - -			+ 34 + 34 -	-	— 29 十 57 — —	t* r* p
5483 5484 5485 3	87°19 - 87°81 - 227°81 -	-1.4600 g -0.8024 g -0.6373 g -0.0516 g -0.0386 g	7109 7652 7043 7591	67.14 8 237.63 8 54.99 8 225.31 8	7°34 9 6°81 9 6°76 9 6°68 9	5521 9 5381 9 5321 9	9.9963 9 9.9931 9 9.9886 9	9705 g 9724 g 9732 g 9748 g	0°1162 g 0n2467 g 0°2725 g 0n3539 g	0 5208 9 9 4724 9 9 4539 9 9 13838 9	9'9747 9'9800 9'9817 9'9869	82'0 78'7 78'5	+ 52 -167 + 74 - 24	- 26 - 8 + 15	+132 +37	- 58	+ 3	47	T ast
5488 2 5489 5490 3	47 15 - 41 69 - 334 53 -	-0.6982 9 -0.7707 9 -1.3950 9 -1.4022 9	7353 2 3 7582 3 7473	354 30 9 29 37 8 62 93 9	7,53 d	'4933 9 '5049 9 '4937 9	9840 g 99829 g 99829 g	9705 9	014259 5 014909 8 014393 5 014722 8	3.0817 ( 3.0817 ( 3.0817 (	9 9930 9 9998 9 9941 9 9980	105.7 73.8 73.8	47 162 	- 56 + 64  	+101 -141 -	- 33 + 43  	+159 - 82 -		
5493 3 5494 5495	37 32 - 36 86 - 5 64 - 56 39 -	-1.5380 9 -0.5331 9 -0.6702 9 -0.1655 9 -0.1052 9	7059 2 7092 1 7517 3	341.36 9 449.46 9 328.49 9 36.71 9	1.85 9 2.74 9 2.80 9 3.27 9	14939 9 15023 9 15037 9 15169 9	9804 g 9836 g 9838 g	9778 g 9'9769 g 9'9767 g	3°4681 g 3°4312 g 3°4278 g 3°3669 g	9n0183 ( 9'2251 ( 9n2386 ( 9'3658 (	9'9976 9'9938 9'9934 9'9880	72 · 8 105 · 9 74 · 2 103 · 8	- 40 - 74 -124	- 26 - 25 + 19	+ 18 - 4 - 56	- 34 20 20		- 57 + 6 - 8	2° 1°* 2°-1°*
5498 2 5499	68 30 - 34 91 -	-0.9172 9 -0.8404 9 -1.3953 9 -0.9660 9 -0.6931 9	75017 2	68 · 86 8 82 · 60 8	9.83 9 8.82 9	5348 9	00000	1 9729 9 1 9640 7	n2729 0 n8543 0	0,4576 0 0,5921 0	9'9814 9'9640	90'4	+ 3	+ 63	+119	+ 76 	153 	+ 43	p = p

Nr.	( )		T		L'	Z	ε	P	Q	$\log p$	$\log \Delta L$	$\log q$	$u'_{\alpha}$	$\log f_a$	logy
		nischer lender	Julian. Tag	Welt- Zeit											
5501 5502 5503 5504 5505	1108	VI 11 XII 4 V 31 XI 24 IV 20		13 38,1	259 363 75 466 248 485	-0.82	23.553 23.553 23.554	180°348 6°005 188°274	359°880 177'972 7'761 187'258 342'887	0.4328 0.4328	9'7412 9'7612	8.7398 8.7140 8.7587	0'5519 0'5596 0'5403	7.6626 7.6773 7.6628 7.6770 7.6654	8n491 9.753 9n847
5506 5507 5508 5509 5510	1111	XI 13 IV 10	2126 625 2126 773 2126 802 2126 950 2127 127	7 59 1 19 9 7 2 37 8	207.972 25.632	-3.70 -3.26 -0.15	23.554 23.554 23.555	164 635 196 152 352 027	197.339	0'7007 0'6920 0'7246	9.7515 9.7605 9.7259	1	0.5546	7.6632 7.6737 7.6764 7.6665 7.6724	0'128 0'121 0'134 9'864 9'821
5511 5512 5513 5514 5515	1112	IX 22 III 19	2127 304 2127 481 2127 659 2127 835 2127 984	22 I6 2 5 53 8 22 9 3	186'144 4'800 175'038	-2.44 +1.55 -1.56	23.554 23.554 23.554	180'562 8'000	8.650 187.170	0'7417 0'6894 0'7422	9.7517 9.7037 9.7641 9.7035 9.7426	8.7081 8.7603	o'5698 o'5345 o'5694	7.6679 7.6710 7.6692 7.6698 7.6741	8.646 8.731 9.877 9.888 0.084
5516 5517 5518 5519 5520	1114	VIII 2 IX 1 I 27 VII 23	2128 013 2128 160 2128 190 2128 338 2128 515	13 54.0 1 49.4 18 43.1 4 18.5	135.232 164.161 314.039 125.301	+1.11 -0.66 +3.88 +1.01	23 554 23 554 23 554	17'219 165'834 196'020 354'114 174'489	356.060 193.707	o.6981 o.7133 o.7252 o.7322 o.6938	9 7393	8 · 7360 8 · 7243	0.2623	7.6705 7.6650 7.6684 7.6752 7.6641	0'167 0'164 0"164 9"740 9'674
5521 5522 5523 5524 5525	1116	VII 11 VII 1 XI 25	2128 692 2128 869 2129 046 2129 224 2129 371	21 35'4 19 25'5 13 3'5	115.225 201.270 105.100	+1'05 +2'49 +0'70	23'552	8,662	7'049	0.7442 0.6918 0.7371 0.7087 0.7031	9.6997 9.7629 9.7088 9.7449 9.7486	8.7060 8.7579 8.7128 8.7409 8.7465	0'5320 0'5705 0'5418	7.6761 7.6634 7.6768 7.6629 7.6770	9'150 9"425 9'912 0"018 0"128
5526 5527 5528 5529 5530	1117 1118 1119 1119	XI 15 V 11 XI 4	2129 726 2129 903 2130 080	8 49.5 2 14.2 9 38.7 17 56.0	239'107 55'853 228'372	-1'16 -3'20 -1'32 -3'73	23.551 23.549 23.549 23.549	170.684 352.382 178.629 0.300	171'996 352'010 178'024 2'019	0'7441	9'7077 9'7633 9'7026 9'7560	8.7062 8.7534	0'5388 0'5661 0'5425	7.6772 7.6631 7.6765 7.6637 7.6757	0'162 9'947 9n809 9'120 8'413
5531 5532 5533 5534 5535	1120 1121 1121 1121	III 20 IV 18 IX 13	2130 257 2130 435 2130 582 2130 611 2130 759	13 5.4 22 33.0 17 6.1	6 138 34 748 176 862	+1.42 -0.73 -1.71	23 548 23 548 23 548 23 548	165 · 034 195 · 262 344 · 746	163.357 192.957 345.254	0.2062	9'7316 9'7575 9'7467	8.7200 8.7310 8.7535 8.7432 8.7063	0.5559 0.5382 0.5422	7.6645 7.6747 7.6690 7.6656 7.6699	9n797 9.877 0.106 0n125 0n162
5536 5537 5538 5539 5540	1122 1122 1123 1123	IX 2 II 27 VIII 22	2130 937 2131 113 2131 291 2131 467	5 32.6 17 24.7 20 53.8 23 13.2	355'747 165'832 345'243 155'097	+2.30 -0.48 +3.08 +0.03	23.548 23.548 23.548 23.548	173°320 352°350 181°571 0°499	173 734 850 956 183 743 358 083	0.6900 0.7393 0.7043 0.7188	9'7638 9'7081 9'7485	8 · 7459	o * 5353 o * 5660	7.6735 7.6704 7.6685 7.6717 7.6671	9n861 9n140
	1125	I 6 VII 2 VIII 1	2131 646 2131 822 2131 970 2132 147 2132 177	13 43'1 21 36'5 5 4'6	293 120 106 451 134 536	+2.65 +0.77 +1.02	23 549	9'027	7°381 164°969 349°289	0'6971	9'7570 9'6999 9'7595	8 · 7063 8 · 7547	0.5367 0.5356 0.5336	7'6731 7'6559 7'6767 7'6630 7'6649	9n952, 9'8900 0'147, 0n017; 0'168,
5547 5548	1126	XII 15 VI 11	2132 324 2132 502 2132 678 2132 856 2133 033	11 45 8 22 18 3 10 12 7	96 · 293 270 · 574 85 · 877	+0'28 +0'14 -0'31	23 549 23 550 23 550	180.320	170:565 359:020 177:967 6*775 187:312	0.7155 0.7369	9'7375 9'7426 9'7119	8 7 18 1 8 7 3 4 1 8 7 4 1 0 8 7 1 3 0 8 7 5 9 2	0.2428	7.6772 7.6627 7.6774 7.6626 7.6773	9.842; 9n490; 8n453; 9.683; 9n844

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Nr.	μ	γ	log	$i \mid G$	K	log	log	log	log	log	log	N'		)Auf- ng	im M	littag	be Unte	i ⊙ rgang	F
						$\sin g$	sin k	$\cos g$	cosk	$\sin \delta'$	cos ô'		λ_	φ	1	Ι φ	λ	Īφ	
													<u> </u>	1	3 r	a a	<u>е</u> 	1	<u> </u> 
5501	251°53	0.220	5 9 741	2 71°80	87°01	9'6191	9 9969	9'9587	9'0762	9 6005	9.9624	82°5	+ 54	19					t esta
5503	8'40	-0.203 -0.203 -0.203	6 9 715	2 61,30	85'34	9'6345	9.9920	9'9555	9'2797	9:5874	9'9649	78'1	- 84	+ 21	- 26 - 12	+ 58	+ 42 + 80 -126	+ 42	15%
5505	162 14	-1.524	3 9.706	8 27.09	83.4	9.6739	9.9604	9 9532	9,6109	913744	9.9875	65 2			+125			53	p
5506 5507	31'27	+1.343 +1.324	79.703	7 51.41	84 · 64 84 · 64	9.6479	9.9850	9,0432	9'4125	9.5582	ე ' ენენ ი ' ენენ	73'9	-			_			$p \\ p$
5508 5509	221.63 102.33	-1.363	2 9 . 7 6 2 2 9 . 7 6 2	4 225 25 0 18 70	83 ' 54 84 ' 95	9'6543 9'6815	9 ' 9797 9 ' 95 ¤ 4	9'9506 9'9431	9n4756	9n5287	9'9737 9'9934	108.5 62.9	+ 99	 _ 71	+149	_ _ 45	 154	- 20	p
5510	105'42	- -0.663	6 9.727	6 192.36	86.36	0,0861	9'9456	9'9417	916729	920718	9 9970	118.3	-x57	- <del>-</del> 69				+ 13	2*
5512	126,35	-0'044 -0'053	8 9.705	184.38	88 63	9 6896	9'9411	9'9406	926879	8n6311	9 ' 9996	119.5	+ 144	+ 26	157	6	+ 39 94	32	1.
5513 5514	151,20 521,00	十0.723	7 9 7 7 6 6 7 9 7 7 6 6	3 44 7 176 46	88.83	9'6874 9'6890	9.9416	9'9413	9.6864 9.6879	8 5242 8 5386	9 9998	бо'9	+ 21	+ 20	+ 84		+177 - gr		"
		-1.519				ļ		l						*******					l P
5517	30'76	+1.471	9'741	146.22	96 68	9.6670	9 9 680	9 9473	925590	9'4470	9 9823	112.7	_			B	********		$\frac{p}{p}$
55 T 9]	98.47	1'458 0'550 0'472	5 9 . 2 z 24	325 38	96.81	g 66go	9 9 6 8 4	9 9466	9 5657	9 4582	9,9813	67:4	+172	- 53 - 45	- 92 +120	- 53 - - 49	- 29 -175	10 8	
- 1		+0'141		1	- 1	.					į.			İ					
5522 1	42'13	-0.2663 +0.8186	9 7650	128.71	95 98'9	9 6483 g	9849	9'952 rig	224140	9'558x	9.9696	106'2	I52	- 10 1	-112 -144 -113	一 II 十 5 十 36	- 60 - 90 - 78	- 29 - 60	2#
5524	12'49	-1 · 0442	9 7469	118.48	94 ' 67   9	3 6340 9	, gorolc	9555	22817	1.863	0.0040	102'0	_			******			p p
5526 I	89.59	+1 '4527	9.7370	293.89	3.92	6273	9945	9570	1983	20,5949	9635	80.1	-		****		-		p
55273 55282	18.30	0'8858 0'6453	9 7098	78.81	8.48 9 7.59 9	) 57 I 5 9 ) 5579 9	'9991 9	9676 8	8 · 8281 g	0.5642	9'9687	85.0 85.0	+ 59	— зт	1-140	- 61	-128	- 44	2 ·**
5529]3 5530	92.65	+0'1321 +0'0259	9.7581	238.23	37 · 34   9 36 · 84   9	3.2383 6 3.2211 6	9934 9	9707 9	n2394 9	0.2193 0.4751	9749	82.0	27 153	+ 11	+ 33 - 93	+ 27 - 16		- 15 - 9	1.44 1.44
5531	8.89	-0'6270	9.7223	54.60	36 . 73 9	5325 9	9920	9731 9	2772	4524	8186.6	78 6	58	- 47	- 5	- 23	- <del> -</del> 51	<b>– 2</b> 6	<b>3.</b>
5533]	18.00	+0 7540 +1 2777 -1 3335	9 7594	7 49	39 '20 9	1 5212 9	9880 9	9740 9	1.4808	6306	9 9807	72 0	43	- 59	95	-l- 37		+ 34	$p \\ p$
5535	82.47	1'4533	9.7035	176'13	90 40 9	4893 9	9784 9	9749 9	1114882	3398	9999	07.9	Money	******	******	-			p
55363 55372	42.25 62.30	+1:5125 +0:5670	9'7091	212'10 8	37.129	5077 9	9838 9	9763 9	n4286 g	2498 g	9,0030	05.8	- 20	_			164	52	$p_{t^*}$
5538 5539 I	30.01	0.1381 0.2568	9.7102	341 79 9	74 9 1 80 9	14922 9 14929 9	9802 9	9779 9	4683 9	20076 9	9979	72.8	-151 -164	- 29 - 25	- 91 -129	- 44 - 14	25 67	— бз +- g	<i>t</i> ∗
55401	68.12	0'0454	9.7350	149'41	2.24 9	.2023 0	·9836 9	9768 9	n4309	2258	9937	05.0	<b>⊹12</b> 6	+ 18	-168	+ 12	-108	— тз	かーだ!
5542	0,41	—о·89бо +о·7773	9'7591	137.14	3 28 9	5176 9	.9877 9	975x 9	n3708 g	3632 9	188g'	04'0	- 35 100	76  - 62			+173 + 83	- 47 36	r. Lik
5543 5544 I	27.22 46.00	+1'4037 -1'0404	9.7615	281.08 ¢	1 5 5 9 10 5 7 9	5722 9 5842 9	.0001 0	'9675 8 '9654 8	·8245 9	n5651 9	9686	85°9	_		_				p p
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5547 3	57125	+o'5965 o'5965	9.7396	82 : 65 8	8 83 9	'601g	19995 9	96218	67139	'5989 9	.9627	87'1	- 53	- rg	+ 3	+ 5	+ 61	- 14	£#
5549 I	07 ' XO	-0 0284 -0 4830 -0 6983	9.7140	71.76 8	7.00 0	61919	99699	9588 9	'0771 9	6004 9	9625	82'5	-179	+ 20	-109	+ 53	26	- 6 - 33 - 48	r*
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5551 5552 5553 5554 5555	1128 1128 1128 1129	X 25 XI 24 IV 20	2133	358 388 535	3 58.0 9 50.7	75°224 219°022 248°909 36°225 208°143	-3'87 -2'36 -0'81	23.551	164.424 196.077 351.327	166'558 197'361 348'969	0'7447 0'7017 0'6925 0'7232	9'7504	8.7053 8.7476 8.7571 8.7260 8.7241	0.5661 0.5452 0.5411 0.5530 0.5599	7.6628 7.6749 7.6770 7.6654 7.6737	0.1287 0.1330 9.8995
5556 5557 5558 5559 5560	1130 1131 1131	IV 9 X 4 III 30 IX 23 II 18	2134	067 244 421	13 55°2 5 27°7	197°028 15°543	-3'19 +0'63 -2'42	23.552 23.552 23.552	180'160 8'353 187'600	357.873 181.083 8.229 186.585 348.296	0.7002 0.7422 0.6895 0.7415 0.7104	9.7530 9.7030 9.7644 9.7040 9.74x3	8 · 7489 8 · 7077 8 · 7601 8 · 7082 8 · 7389		7.6665 7.6724 7.6679 7.6710 7.6729	8n0045 8nx860 9 8496 9n8607 0n0947
5561 5562 5563 5564 5565	1132	III 19 VIII 12 IX 11 II 7 VIII 2	2134 2134 2134 2134 2135	745 775 924	9 21.9 2 42.1	5'202 146'116 174'909 325'081 135'842	-1.55 +3.93	23 ' 552 23 ' 552 23 ' 552	165 ' 120 195 ' 489 353 ' 898	18.610 162.724 193.140 355.778 172.587	0.4118	9'7538 9'7408 9'7255 9'7141 9'7612	8.2162	0'5460 0'5561 0'5658	7.6692 7.6661 7.6697 7.6741 7.6650	0'1570 0'1195 0"1483 9"7575 9'7298
5566 5567 5568 5569 5570	1134 1135 1135	I 16 VII 12	2135 4 2135 4 2135 6 2135 8	455 632 809	5 8.0 3 31.2 20 16.5	313'791 125'728 302'417 115'562 261'123	+1 17 +3 37 +1 07	23.550 23.549	8,226	1'415 183'337 6'857 193'363 342'329	0.7443 0.6921 0.7362 0.7101 0.7020	9'6999 9'7622 9'7099 9'7433 9'7497	8.7059 8.7573 8.7135 8.7392 8.7478		7.6752 7.664x 7.676x 7.6634 7.6773	9'0942 9n2950 9'9065 9n9887 0n1287
5571 5572 5573 5574 5575	1136 1136 1136 1137 1137	I 5 VI 1 XI 25 V 21 XI 15	2135 9 2136 9 2136 2 2136 4	134 311 488	15 20.9 11 5.0 16 8.0	291'252 76'991 250'297 66'298 239'519	-0.44 -1.14	23'548	352'316	13.811 170.997 352.048 177.039 1.993	0.7409 0.6891 0.7438	9'7364 9'7068 9'7635 9'7032 9'7550	8.7352 8.7092 8.7611 8.7064 8.7525	0.5632	7.6768 7.6627 7.6770 7.6631 7.6765	0.1597 9.9874 9.8131 9.3342 8.2337
5576 5577 5578 5579 5580	1138 1139 1139 1139	XI 4 III 31	2137	167 197	6 0.1 6 0.3	228'602 16'870 45'307	-3.43 -1.19	23'546 23'546 23'546	8 169 164 481 194 532	183 · 723 10 · 576 162 · 902 192 · 277 344 · 676	0.7199 0.6956	9'7220 9'7300 9'7584 9'7483 9'7008	8'7544 8'7444	0.5551 0.5575 0.5369 0.5407 0.5718	7.6637 7.6757 7.6677 7.6645 7.6713	9n7411 9.8704 0.1211 0n1028 0n1753
5581 5582 5583 5584 5585		IX 13 III 10	2137 6	599 877	0 40 8	176 581 356 112	+1.39 +1.39	23 546 23 546 23 546	351 818 181 175	17.157 173.379 350.327 183.399 357.492	0.7384	9'7637 9'7089 9'7472		0'5347 0'5663 0'5446	7'6690 7'6699 7'6704	0'1740 9'7840 9n8895 9n0152 7n8764
5586 5587 5588 5589 5590	1143	I 17 VII 14	2138 2	555 733	19 57 9 21 39 0 5 3 0	304 246	+0'01 +3'49 +1'12	23.545 23.546 23.546	8°378 165'144 346'984	191'523 6'838 164'734 348'571 17'427	0'6960 0'7441 0'6960	9'7004	8 · 7064 8 · 7539	o'5368 o'5751 o'5344	7'6717 7'6671 7'6760 7'6635 7'6659	9n9388 9'8574 0'1509 0n0466 0'1506
5591 5592 5593 5594 5595	1145	VII 2 XII 26 VI 22	2139 0 2139 2 2139 4	087 264 142	18 50 0 6 59 0 1 46 8	292.883 106.729 281.780 96.286 270.913	+0.79 +1.49 +0.28	23.547 23.548 23.549	355°707 180°289 4°193	170 · 435 358 · 157 177 · 965 5 · 779 187 · 379	0'7169	9'7357 9'7439 9'7106	8'7121	0'5469 0'5502 0'5610	7:6767 7:6630 7:6772 7:6627 7:6774	9.8459 9n5890 8n4079 9.5998 9n8419
5596 5597 5598 5599 5600	1146 1146	XI 6 XII 5 V r	2139 9 2139 9 2140 1	973	12 48 5 16 58 5	230 · 124 260 · 117 46 · 754	-1.12	23'550	196.032	11'949 166'464 197'406 348'183 174'511	0'7028 0'6932	9'7490 9'7590	8'7465 8'7564 8'7275	0'5416	7.6626 7.6758 7.6773 7.6644 7.6749	0'0684 0'1338 0n1325 9n9345 9'8541
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5551	127019	+x'2580	9.7038	61°27	85°32	9.6344	9 9920	9 9554	9.5815	9.2869	9'9649	78°0	_	_		_	_	-	$ _{p}$
5553	238.22	+1'3450 -1'3583	9.7617	235'57	84'56	9.6414	9 * 9882	9'9537	923612	9n5715	9'9675	104'3				_		_	$p \choose p$
5554 5555	330.05	-0'7934 -0'6917	9.7259	20.89	83.73	0.6813 0.6220	9.9528 9.9528	9'9449 9'9430	9 6128 9 2 6449	9°373x 9n2752	9.9875 9.9921	116.4	+ 3 + 93	一 71 十 68	+ 40 +145	- 47 + 40	+ 95 -159	- 27 + 17	
5556	144'60	-0,0101	9'7551	18.80	84.02	a·6820	0.0213	0.0430	a · 65 1 6	0.2406	0.0034	62'0	+157	27	-144	<u></u>	- 76	- 26	t ^{ele}
5557	268.83	-0.40123	9.7025	192,51	86.38	9 ' 687 r	9 9452	9'9413	926742	920682	9'9970	118'4	+ 34	+ 27	+ 91	- 8	+155 + 65	- 29	$r^{**}$
5559	262,51	-0.7257 -1.2437	9 ' 7062	184 . 12	88.70	9.6891	9'9412	9 ' 9407	gn 6875	816097	9 9996	119'2	+ 27	- 17	+ 86	- 59	+177	T 72	r
i i					i						·								p
5561 5562	267.28 142.62	+1,4323	9°7557 9°7427	3 76 154 77	96.01 98.89	9 · 6842 9 · 6744	9 · 9426 9 · 9586	9 · 9422 9 · 9452	9:6830 9:6830	8 · 5 5 9 1 9 · 3 4 7 8	9'9997 9'9890	61'2		******				_	$p \\ p$
5563 5564	318'19 218'26	-1.4070 -0.2721	9 7285 9 7163	334 · 28	91'13 96'20	9 · 68 68	9.9418	9'9414 9'9442	9,16856 9.6207	8·5497 9n3593		64.6	+ 54	58	+150	53	150	g	$\frac{1}{p}$
55 ⁶ 5	359°24	+0.2367	9,4633	146.71	96.43	9.6692	9.9671	9 9466	915739	9'4446	9 9825	113.0	<b>– 89</b>	+ 52	+ 7	+ 52	+ 72	+ 9	
5566	228 25	+0'1242	9'7021	325 ' 24 !	96 · 83	6695	9 9685	9 9466	9.5653	924500	9'9812	67 . 4	+ 67	- 15	+130	- g	177		
5568	227.09	-0.1925	9.2121	315'38	96.27	3.6574	9.826.6	9 '9498	9'4835	925279	9'9738	21.1	+ 73	+ 33	+125		+158 +159	- 29 + 64	2:14
5579 5570	127.06	-0.3420	9.7453	273.08	30. 65 6	9.6475	9'9849	9'9523 9'9631	924142 8 4016	9,5568 9,5962	9 9633 9 9633	88'4	-172 	55			(—135) —	(—69) —	p
5571	316.60	+1·4443	7384	818.00	25'50	6424	0870	0.0535	0 ' 3665	02.5700	0.0676	75.5	_		************				47
5572	53.82	+0 9714 9 -0 6503	7089	90'17 9	30.03	5902	0,0000	9643	720387	9 . 2002	9 9 9 5 4 3	30.1			(+126) + 9		+ 87		$r^*$
5574	63'80	+0.2159 c	7054	78 67 8	38·46 g	5706	9990	9677	8 8327	3'5632	9*9689	85.8	-128	+ 8	- 64	+ 34	+ 4 -157	- 39 + 15	9+1
	v :				1									7			157	5	"
5576 5577	34.54	-0.5509 g -0.7420 g	17321 2	38 35 8	6.83 9	5393	9934 9	9723	3n 2388 [9	n 4766	9 9796]:	100.2	163 80		— 30 — 111	- 15 + 32		24 35	2" 2" :
5578 5 5579 2	37 · 82 -	⊢ι.3212 ∂ ⊢ι.3212 ∂	7503	20'49 8 54'36 8	7 94 9 86 69 9	5346	0.0010	977 x 9	9'4687	9'0641	9'9971	72·8 78·5		<b></b>	,				p p
5580	92'49	-1.4973 g	7029	89 45	39.02	14908	9.88	9781	224843	317274	9 9994	107.8			******		-		$\hat{p}$
5581	99 16	+1'4927	7080	25'17	36.64	5223	9884	9745	3573	923853	9868	103.6							$p_{ab}$
5583	194.12	+0.6081 c	i. Arroll	75 7719	0 44 9	14874	9786	9785	3n4861 8	3.3770	9 9 9 9 9 9	107 '8	+ 95	- 33	+ 150	- 53	126	+ 55 69	r
55841	252.12	-0.0022 c	7493	355 · x9 9	90.2010	1.4870	3.8466	978419	9'4859	3n4328	9.9998	72.2	+ 44	- 24	1-109	i— 81	- -x7x	+ 12	$t^{**}$
		o 8686 <u>c</u>		į			.			ŀ		ŀ							
5587	117'62	+0.7202 c	760x	(49 . 85   6	92°73 9	5031	9.0833	9767	9n4338	9.2217	9 ' 99 39	106.0	+153	+ 61	-112	+ 58	<b>-</b> 40	- 43 + 30	t ^{ide}
5589	257'43	-1'1132 g	9.7606	105 45	32 ' O I   C	5656	9.9982	9684	Bn 9616	9.5517	9.9705	95'6	_		_	_		_	$\begin{vmatrix} p \\ p \end{vmatrix}$
			-											-		September 1			p
5592	102.20	+0.2013 c	7378	93,86 8	90.57	5836	9,0000	9655	Bn 3777	9 5827	919656	91.2	-159	20	103	o	48	+ 44 22	
5593	283'20	0'0256 0'3979	7460	268 • 46   8	39 ' 76   9	5924	0,0000	9639	729847	925922	9'9639	90.6	+ 13	r	+ 77	24	+141	2	r-t*
5595	133.03	-o · 6948	7642	257 08	37.00	6107	9985	9505	82226	926014	9.9623	95 2	+137	— 35	-136	- 68	- 38	- 44	
5596	222.56	+1.1702	7042	71.63	36.98	6191	9968	9587	0.0801	9 ' 6002	9 9625	82 ' 5							p
5598	9.93	+1'3567 9	9'7609	246 ' 52 8	36 · 15 g	6262	9.9947	9572	921900	925950	9.9635	99'7		-					p p
5599	78.14	-0'8600 9	9'7316	35.21	33.53	6664	9696	9474	9 5578	9 4639	9 * 98 08	67.8	- 91 - 22	ー 71 十 65	68 + 23	- 51 + 37	- 15 + 78	- 35 + 21	r
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5601 5502 5603 5604 5605	1148 1149 1149	IV 20 X 14 IV 9 X 3 III 1	2140 652	13 17 5 21 49 4 12 55 9	207.978	-3'72 -0'19 -3'17	23'550 23'550 23'550	179 833 7 725 187 198	357°267 180°655 7°741 186°079 347°982	0'7426 0'6897 0'7409	9'7644	8.7499 8.7072 8.7599 8.7089 8.7375	0.5378 0.5725 0.5329 0.5703 0.5495		
5606 5607 5608 5609 5610	1150 1150 1151	III 30 VIII 24 IX 22 II 18 VIII 13	2141 331 2141 360 2141 500		336.060	-0.09 -2.42 +3.57	23'550 23'550	164'474 195'039 353'613	18.143 162.107 192.658 355.419 172.000	0.7103 0.7223 0.7342	9.7527 9.7421 9.7278 9.7129 9.7619	8.7489 8.7390 8.7270 8.7152 8.7572	0.5402 0.5458 0.5561 0.5658 0.5341	7.6729 7.6710 7.6729	0.1441 0.1360 0n1344 9n7783 9.7758
5611 5612 5613 5614 5615	1152 1152 1153 1153 1153	VIII 7 VIII 26 VII 23 XII 17	2142 040	3 31.5	313.214 313.214	+1.18 +3.80 +1.01	23'549 23'549 23'549	8,338 8,238	1'066 182'699 6'620 192'584 342'356	0.6927	9.6998 9.7616 9.7114 9.7415 9.7510	8 · 7058 8 · 7568 8 · 7146 8 · 7378 8 · 7488	0.5739 0.5338 0.5681 0.5443 0.5464	7.6650 7.6752 7.6641	9.0069 9n1193 9.8976 9n9574 0n1281
5616 5617 5618 5619 5620	1154 1154 1155 1155	I 15 VI 12 XII 6 VI 1 XI 26	2142 896 2143 073 2143 251	21 49 0 19 59 1 22 34 3 11 22 0	261.209 76.413	-0.32 -0.36	23*548 23*546	168.878 352.280	13.732 169.980 352.117 176.024 2.002	o 6889	9'7378 9'7059 9'7637 9'7037 9'7538	8 7364 8 7083 8 7612 8 7069 8 7517	0.5533 0.5636 0.5392 0.5649 0.5445	7.6761 7.6626 7.6773 7.6627 7.6770	0.1564 0.0249 928150 9.4805 8.0840
5621 5622 5623 5624 5625	1156 1156 1157 1157 1157	V 21 XI 14 IV 11 V 10 X 5	2143 428 2143 605 2143 753 2143 782 2143 930	22 32 2 4 49 2 13 23 8 7 47 1		-3'17 -0'28 -1'30 -3'17	23.545 23.545 23.545	193.751	182.835 10.451 162.386 191.557 344.173	0'7273 0'7212 0'6948 0'7040 0'7446	9'7237 9'7284 9'7594 9'7500 9'7005	8.7550	0.5539 0.5588 0.5358 0.5395 0.5728	7.6631 7.6765 7.6664 7.6637 7.6725	9n6739 9.8663 0.1370 0n0780 0n1857
5626 5627 5628 5629 5630	1157 1158 1158 1159 1159	XI 4 III 31 IX 24 III 21 IX 13	2144 107 2144 284 2144 452 2144 638	21 40 9 8 6 3 12 54 7 14 29 3	187.402 6.910 176.556	+0'49 -2'54 +1'36 -1'66	23 544 23 544 23 544 23 544	351'366 180'704 359'414	172'959 349'782 182'974 356'986	0.4160		8 · 7594 8 · 7131 8 · 7431 8 · 7341	-	7.6757 7.6678 7.6713 7.6690 7.6699	0'1696 9'8165 9n9117 8n7944 8n7237
563x 5632 5633 5634 5635	1161 1161 1161	, 111 22	2145 141 2145 318 2145 347	5 29 6 12 32 5 20 37 7	315.332 127.429 155.771	+3.90 +1.19 -0.02	23 544	164.969	164.450	0'744I 0'6969	9.7587	8 7551 8 7567 8 7529	o'5609 o'5371 o'5742 o'5355 o'5338	7.6704 7.6685 7.6751 7.6642 7.6671	9n9206 9'8256 0'1559 0n0730 0'1342
5636 5637 5638 5639 5640	1163 1163 1163	VII 3 XII 27	2145 673 2145 849 2146 027 2146 204	8 20 7	117'186 292'970 106'702 282'129	+1'14 +2'63 +0'80 +1'52	23.545 23.544 23.545 23.546	180°240 3°298 188°158	357'318 177'949 4'789 187'441	0.2388 0.2388	9'7339 9'7454 9'7093	8 · 73 15 8 · 7436 8 · 7111	0'5493 0'5619	7.6760 7.6634 7.6767 7.6630 7.6772	9.8505 9n6680 8n3262 9.4965 9n8398
5542 5643 5644	1164	XI 16 XII 15 V 12 XI 5	2146 381 2146 529 2146 558 2146 706 2146 883	21 39'7 0 3'0 18 51'4	57 260 230 261	-3'04 +0'21 -1'29 -3'68	23 546 23 546 23 547 23 547	196 000 1 196 000 1 149 768 3	197'459 347'361 174'301	0.7040 0.6940 0.7204 0.7275	9'7477 9'7583 9'7313	8 · 7455 8 · 7557 8 · 7289	0.5478 0.5423 0.5498	7.6627 7.6765 7.6774 7.6637 7.6758	0'0345 0'1376 0n1324 9n9679 9'8641
5647 5648	1166 1167 1167 1168	X 25 IV 21 X 14	2147 000 2147 237 2147 415 2147 591 2147 740	21 0 6 2 5 36 2 20 33 5 2	207 673 -	-3.89 -0.83 -3.69	23 548 1 23 548 1	79 577 1 7 032 86 871 1	7.130	0'7431	9'7015 9'7544	8 7068 6 8 7597 6 8 7097 6	0.5324	7 · 6748 7 · 6655	9n1298 8.6091 9.7754 9n8157 on1196
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Nr.	μ	γ	$\log n$	G	K	$\log$	log	$\log$	$\log_{\mathbf{r}}$	log	log	N'	bei ⊙ gai		im M	ittag	bei Unter	O Canc	F
	ļ.,	<b>'</b>	108/	<u> </u>	11	$\sin g$	$\sin k$	$\cos g$	cos k	$\sin \delta'$	coso′		$\frac{\delta}{\lambda}$	φ	<del>-</del> \( \lambda \)	Ιφ	\\	φ	1
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5601	259°93	-0.0201	9 ' 7565	27°00	83°70	9'6755	g · g6aa	9*9449	0.0120	913752	9*9875	65°o	+ 44	28	+101	· <del> </del> 9	4169	- - 20	<i>t</i> *
5002	23'14	+o.orgo	9'7042	200,33	84.28	9.6824	9'9524	9'9427	gn6467	912728	9'9922	116.8	78	+ 27	23	ro	+ 42	- 25	1.**
5004	12.11	+0.6866	9'7069	192'00	86'44	g • 6868	9'9451	9'9414	926743	9n0605	9.997x	118'4	+141 - 85	- I5	-		- 52 + 73		2.
5005	228.23	-1'2767	9'7420	350.29	92.81	9 6854	9 9442	9.9418	9.6777	8n9552	9.9982	61,4		_					P
5606	27.11	+1,3933	9.7546	11.00	86.64	g·6823	9.9461	9*9428	9.6707	9.0402	9.9974	61.0		******				-	p
5007	256.81	-1.3624 -1.3624	9.7440	162.96	94'64	9.6799	9.9504	9'9435	926549	9'1977	9'9945	117.5	-		******				$\frac{p}{p}$
5009	336.52	-0.0001	9'7151	342 66	94.81	9.6837	9.9496	9.9423	0'6577	922098	9.9942	62.6	62	бз		- 52		9	.1"
5010	115.20	+0.2967	9.7040	155.30	96.03	9.0708	9.9577	9*9444	920239	9'3441	9.9891	115.0	152	- - OO	108	+ 54	- 44	1 I	t ^a
5611	344 18	+0.1019	9.7020	334'14	96.53	9.6781	9.9584	9 9440	9'6205	923619	9.0885	64 6	49						
5613	347'05	+0.1310	9'7136	324'92	96 82	9'6684	9.9689	9.9468	9'5623	924620	0.0810	67.6	5°	+ 15 + 28	- II + 3	+ 8 + 42		一 29 十 67	
5614	229.26	-0.3430	9'7435	138.38	96 67	9 6593	9'9762	9'9494	925084	9'5092	9'9761	100,0	+ 70	<b>- 42</b>		56		- 7I	
00	~37 33	1 3430	9 /329		92 50	9 0151	9 9977	9 9590	g UIIO	gnoori	9 9023	03 0							P
5616 5617	83'34	+1'4337	9 . 7398	315.07	96.50	9.6555	9 9793	9'9503	9'4793	925280	9'9738	71'3					. paragona		$p_{\cdot}$
5018	122.41	+1.0230	9'7658	274'89	90.76	9.2981	9,9998	919630	8,4910	915967	9'9632	88.1		- 39	-122	- 64		- 35	
5019	100'24	+0.3054	9.7059	90.05	30.01	9.5897	0,0000	9'9644	625073	9'5897	9'9644	90'0	+131 - 55	1	- 16o 十 7	+ 40	91 + 72	1 !	10.00
										9					' '		' ' "		
5621 5622	216'33 150'10	-0.4720 +0.7350	9.7258	78.36	88 42 87 66	9 5705	9.9990	9'9677	8 8442	9.5627	9.9689	85.7	十 92 十155		+145	- 7 + 28	l	22 38	4 11
5023	255.93	1.3710	9.7613	33'25	87.02	9.2109	9 9840	9'9759	9'4257	9 2665	9.9925	74'3		+ 49	-157				p
5024 5625	304 53	-1.1967 -1.2337	9.7520	66 41 202 75	87 27 87 79	9 5525	g ' g g б о g ' g 8 1 2	9'9704 9'9774	9°1297 9n4592	9'5191 9n1044	9°9749 9°9965	100.0		_		house			10
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5020 5627	217.37 146.39	+1.4777 +0.6554	9.7072	238.03	86'80 87'93	9'5399	0.0810 0.0810	9'9723 0'0776	9n2434	9n4759	9.9797	73.0	140	+ 24	-152	- 50	- 65	+ 57	$r_{t^{iji}}$
5028	300.47	-0.8160 -0.8160	9.7120	189,12	89'06	9.4887	9'9790	9'9783	9114825	817114	9'9994	107.7	- 22	- 37	+ 45	- 62	<b>+136</b>	- 72	2,
5630	30.13	-0.0223	9.7380	175.43	90'44	9'4871	9.8489 9.8489	9 9785	9 4830 9 4858	8.3801	8.8888 8.8888	107.8	- 74 102	+ I5	- 12 - 40	- 2	+ 23	+ 14 21	1°-6'#
562T	T 48 · 8 2	-0.8000	0.7009				0 -												
303*	43/ 14	-0.8330 -0.6693	9.7000	102.93	91.72	9 4930	9.9801	9.9779	Qn4712	8'9832	9.0000	107.3	1 - 43	一 74 十 59	-141 +128	50	- 73 - 164	+ 25	t*
5033 5634	202.00	-1.1830 -1.4350	9.7030	306.27	93,31	9.5328	9'9917	9.9732	9'2871	924483	9.9822	78.4	-		grounds.			-	$\begin{bmatrix} p \\ p \end{bmatrix}$
5635	126.15	+1.3620	9.7654	150 66	92.24	9 5068	9.9828	9 9764	9n44I3	9.2147	9 9941	106.3		-	_			province#	p
5636	284'48	+0.7088	0.7204	203'12	02.68	0.2221	0.0063	0'070F	011010	05200	0'0748	81.0	+ 20	-1- 0-	+ 70	- ne		+ 40	1 44
5637	208.68	-0.4656	9'7360	105.30	91,99	9'5645	919982	919685	829589	9:5597	9 9706	95 6	1- 94	21	+150	- 7	- r 56	- 31	1-6
5939	303.40	-0'0212 +0'3137	9.7112	93'71	90'54	9.5836	9'9999	9.9655	823606	9 5828	9.9656	gr'4	- 14	- 5 + 18	- 52 + 57	+ 41	+ 10	+ 3	1 1.1"
5640	265.82	-o'6915	9.7646	268.98	89.84	9.2918	0,0000	9.9640	718079	925917	9'9640	90'4	+ 3				-174		
5641	317.88	+1.0827	9'7044	82.40	88 . 79	9 6023	919995	9.9621	8.6864	9.2001	9'9627	87.0							$  _{p}$
5042	330.50	+1.3727	9'7497	228 28	83.75	9.6213	9'9824	9'9514	924461	925445	9.9716	107'4	*****		-		-		p
5044	184.22	-0.0588	9'7333	44.62	83'47	9'6561	9.9790	9.9502	0.4824	0'5264	0'0740	71'2	x 7 7	- 70	-176	- 59	-126	- 46	j 2'
5045	109.00	+0.4313	9 7229	218'28	83.18	9 6648	9'9725	9'9479	925381	914874	9'9785	III.3	-142	+ 62	-101	+ 34	- 46	+ 24	1 11:18
5646	13'77	-o'1348	9'7578	35 60	83.20	9.6671	9.9697	9 9472	9.5578	9 4655	9 9806	67.8	- 68	- 29	_ 12	+ 9	+ 55		t lik
5047	139.12	+0.0406 +0.5962	9'7037	208.88	83.47	9'6753	9.9618	9.9448	926034	924003	0.0858	114'	+168	+ 26	5   r a a	- 12	2 73	21	1 1 th
5049	130.13	-0.0242	9.7074	200.13	84.63	9'6822	9 9524	0'0420	926472	0 2684	0'0024	1116:8	31 + x 50	- 12	-140	- 58			r
35,50	349 /3	-1.3170	9 /400	350 42	90 49 	9 0808	9 9415	9-9414	9.6865	811847	9.9999	90.0	1				1		p
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5653 5653 5653 5653	1168	X	3 2147 3 2147 8 2148	910 946	0 57 18 12	7 26°61 167'46 16 196'62 5 346'97 4 157'08	-0.90 $-3.16$ $+2.94$	23'548 23'548 23'548	163.893 194.663	161.260 192.260	0.7088	9'7514 9'7436 9'7293 9'7119 9'7624	8.7405	0.2424 0.2561 0.2626	7.6665 7.6686 7.6724 7.6716 7.6673	0.1201 011222 018033
5656 5658 5659 5660	1170	VIII 1 VIII XII 2	3 2148 5 2148 3 2148 3 2149	625 802 980 127	20 26 19 28 10 49 13 42	5 335 799 9 146 862 7 324 559 0 136 582 8 283 542	+3.92	23'547 23'546 23'546	180 · 822 8 · 187 189 · 423	182'107	0.7344	9'7605 9'7605	8.7559 8.7153 8.7364	0'5347 0'5667 0'5458	7.6660	
5661 5662 5663 5664 5665	1172 1172 1173 1173	XII 12 XII 12 XII 6		305 482 659 836	4 15 4 53 5 0 20 9 ·	6 313.525 3 97.805 272.728 1 87.116 3 261.916	+0'36 +0'38 -0'22 -0'97	23'545 23'545 23'545 23'544	167 963 352 246 175 942 0 104	2'032	0'7423 0'6888 0'7427 0'6991		8.7074	0'5642 0'5391 0'5643	7'6774	0'1517 0'0594 9"8168 9'5903 7'9559
5667 5668 5669 5670	1174 1175 1175 1175	XI 26 IV 22 V 21 X 16	2150 2150 2150 2150	191 338 367 515	6 56. 12 31. 20 44. 15 20.	6 76.575 4 250.908 4 38.145 7 66.302 9 209.526 4 239.622	-2:20 -0:89 -1:14 -3:78	23 543 23 543 23 543 23 543	8.001 163.167 192.929 343.579	161 810 190 808 343 748	0'7222 0'6940 0'7029 0'7447	9'7268 9'7605 9'7514 9'7000	8'7240 8'7274 8'7558 8'7468 8'7061	0.5601 0.5346 0.5382 0.5737	7.6628 7.6770 7.6632 7.6632 7.6738	9x5922 9.8638 0.1538 0x0507 0x1940
5672 5673 5674 5675 5676 5677	1176 1177 1177	X 4 III 31 IX 23	2150 2151 2151	869 047 223	15 42°; 20 41°; 22 21°;	198.294 17.639 187.393	-0 38 -3 28 +0 47 -2 54	23 541 23 541 23 541 23 541	350.33x 180.123 358.388	172'464 349'320 182'471 356'566	0.6917 0.7363 0.7085 0.7145	9'7628 9'7108 9'7445 9'7373	8.7356	0'5338 0'5668 0'5446 0'5507	7.6764 7.6664 7.6725 7.6678 7.6712	0.1666 9.8508 9.9289 8.1497 8.19595
5679 5679 5680 5681 5682	1179 1179 1179	VIII 10 VIII 4	2151	756 903	7 39 5	176.839 326.363 356.018 137.977	-1.70 +3.90 +2.27 +0.99	23°541 23°541 23°541 23°541	7,295 164,735 196,205 345,430	5'966 164'107 196'563 347'230	0.6979	9 7595 9 7014 9 7012 9 7564	8 · 7562 8 · 7070 8 · 7063 8 · 7521	0.5373 0.5732 0.5712 0.5367	7.6651 7.6621	9,8978 9,7958 0,1621 0,1881 0,0965
5683 5684 5685 5686 5687	1180 1181 1181	I 17 VII 13	2152 d 2152 d 2152 d	258 435 612 780	9 0.7 0 14.7 14 55.4	127.677 304.129 117.141	+1'19 +3'46 +1'14	23'542 23'542 23'542		355·503 177·905 3·819	0.7398 0.7398	9'7321 9'7467 9'7082	8 · 7299 8 · 7446 8 · 7104	0.2031 0.2480 0.2620	7.6751 7.6642 7.6760	o'1190 9'8576 9'7326 8'1379 9'3639
5688 5689 5690	1182	XI 27 XII 27 V 23	2153 1 2153 1 2153 2	144 144 150	5 49°2 8 15°1 6 30°5 7 5°2	106 '436 252 '458 282 '547 67 '724	+0.80 -2.04 +1.55 -1.09	23.544 23.544 23.544 23.544 3.544	10:387 164:118 195:965 348:928 5	9'884 (66'396 (97'510 (46'507	0 7442   0 7052   0 7052   0 6949   0 7193   0	) '7026   8 ) '7464   8 ) '7574   8 ) '7331   8	3 7444 3 7549 3 7304	0.5658 0.5489 0.5426 0.5485	7.6629 7.6771 7.6772 7.6631	9n8367 9'9981 0'1404 0n1324 0n0007
5693 5694 5695 5696	1184 1184 1185 1185	XI 5 V 1 X 25	2153 6 2153 8 2154 0 2154 1	23 23 27 77	4 49 6 3 17 5 4 20 8 8 56 7	230 065 47 395 218 688	-1 27 2 -3 70 2 -1 18 2 -3 89 2	23 544 5 23 544 1 23 544 1 23 545 1	357 048 3 79 379 i 6 275 86 6r6 i	55°94X 0 79°993 0 6°585 0 85°308 0	9:6972   9 9:7433   9 9:6902   9 9:7394   9	7568 8 7008 8 7643 8 7059 8	3 7521 0 3 7068 0 3 7594 0	0.5354 0.5746 0.5318 0.5708	7 · 6637 7 · 6758	9'8716 9'87161 9'7267 9'7287
5698 5699	1186	IV 21 IX 14 X 14 III 12	2154 3 2154 5 2154 5	01 2 31	0 26 3 9 0 3	37 *218 178 *235 207 *584 357 *807	-1'81 2	3 545 I	53 390 I	61.084 C	7030 g	7503 8 7449 8 7306 8	7420 0 7296 0	2 5403 2 2 5457 2 2 5560 2	7 6655 6 7 6700 6 7 6736 6	0n1349 0'1107 0'1617 0n1121 0n8318
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Nr.	μ	γ .	$\log n$	G	K	log sin g	log sink	$\log \cos g$	log cos k	log sinδ'	log cos oʻ	N'	bei ⊙ gan λ	Auf-   ng   φ	im M	ttag     φ	bei e Unterg	Ogang φ	F
5652 5653 5654	13'24 193'96 92'04	+1.3453 +1.4130 -1.3250 -0.6357 +0.6507	9'7455 9'7314 9'7141	170.90 192.01 350.66	92.69 86.49 92.82	9.6831 9.6845 9.6875	9'9447 9'9458 9'9435	9'9426 9'9421 9'9412	926760 926720 9.6799	8 · 9381 920579 829546	9.9984 9.9971 9.9982	118.4 118.3 61.3	-172 + 35		 82 +135	_ _ _ 52 + 56	  23 161		p p p r t*
5657 5658 5659	125'99 106'04 339'03	+0.0723 -0.0705 +0.7686 -0.8412 -1.3430	9 . 7627 9 . 7149 9 . 7418	155.58 333.84 147.25	96.00 96.68	9.6777 9.6770 9.6777	9 · 9572 9 · 9590 9 · 9667	9'9442 9'9444 9'9467	9n6264 9.6181 9n5769	9 · 3392 9n3649 9 · 4386	9 ' 9894 9 ' 9880 9 ' 9830	115'7 64'7 113'1	-171 - 44	+ 21 + 24	-127 -117	+ 8 + 45	- 69	29 + 70	$t^{ii}$
5662 5663 5664	247 ° 05 254 ° 58 256 ° 39	+1.4180 +1.1465 -0.6559 +0.3893 0.0090	9 · 7068 9 · 7068	111.86 111.86	91.49 93.60	9 · 6245 9 · 6165 9 · 6079	9 ' 9955 9 ' 9974 9 ' 9989	9'9576 9'9592 9'9610	9n1585 9.0365 8n8539	9:5975 9:6010 9:6010	9 · 9630 9 · 9623 9 · 9623	99°0 83°2 94°5		- 43 - 25 - 2		65 46 23			1) 1) t t*
5667 5668 5669	284'29 12'21 129'43	-0.3910 +0.7308 +1.4250 -1.5630	9·7289 9·7624 9·7534	263'44 45'68 78'16	86.90 86.60 88.39	9.5711 9.5252 9.5711	9'9997 9'9885 9'9989	9'9563 9'9740 9'9676	8,6036 9,3558 8,8521	9.3921 9.3631	9'9667 9'9669 9'9669	92°5 76°5 85°6		- 21 + 45 - -	+ 41 + 77 — —	+ 25  	+ 96 + 126 	- 21 + 40 	424
5672 5673 5674	265 36 61 34 120 81	+1.4677 +0.7093 -0.8490 -0.0141 -0.0911	9 · 7649 9 · 7129 0 · 7466	34'13 202'53	87.04 87.83	9'5074 9'4959	9 9846 9 9813	9 · 9762 9 · 9776 9 · 9777	9.4175 914580	9'2724 9n0982 0'0828	9'9966 9'9966 9'9922	74.0 73.1	+ 17 142 169	IS	69 130	- 70 6	-175 + 38 - 65 - 94	+ 59 - 73 + 16 - 23	r t ^{sis}
5677 5678 5679	18:59 18:59 288:17	-0.7903 +0.6249 +1.4523 -1.5420 -1.2487	9.7616 9.7034 9.7032	176'09 319'20 355'11	90'41 93'24 90'51	9:4880 9:5158 9:4905	9°9786 9°9869 9°9783	9'9785 9'9781 9'9781	9,4869 9,4887	8 · 3428 9n3448 8n4430	0.0008 0.0801 0.0000	75.6 72.0	- 7º  	- 70 57 		- 53 + 42 	и.	- 34 - 21	4414
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5687 5688 5689	53·58 99·40 272·72	-0.6866 +0.9956 +1.3817 -1.3563 -1.0016	9 · 7047 9 · 7484 9 · 7593	93.54 238.76 269.97	90.52 84.97 90.00	9'5840 9'6374 9'5909	9'9999 9'9904 o'0000	9 9654 9 9547 9 9642	8n 3406 9n 3183 6n 2061	9.5833 9.5807 9.5909	9.9655 9.9660 9.9642	90'0	+140						
5692 5693 5694	126.31 226.31	+0.7440 -0.2034 +0.0597 +0.5330 -0.6290	9	44.68 217.98 35.98	83.46 83.15 83.21	9 6565 9 6659 9 6663	9'9790 9'9720 9'9702	9 9501 9 9475 9 9475	9'4823 9"5411 9'5548	9.5274 9.4861 9.4683	9 9 7 3 9 9 9 7 8 6 9 9 8 0 4	71.2	-179 + 51 - 91	- 29 + 24 + 10	-125 $+104$ $-25$	+ 52 + 52	+170 +71	+ 5	7 1" 1" 1" 1" 1" 1" 1" 1" 1" 1" 1" 1" 1"
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5711 5712 5713 5714 5715	1192 1192 1193 1193	VI V	6 2 2 1 2	2156 2156 2156	598 776	15	56 23 8	0 2	73 · 12 36 · 99 32 · 10 76 • 75	I -	-0°2: -0°9:	2 2 2 2 2 2	3.54 3.54	1 18 1 16	33°35 7°95 32°41	57	2.06 10.28 10.28 161.18	4 6 3 6	0'7000 0'7245 0'7235 0'6934 0'7016	9'727	8 · 725 8 · 726 8 · 756	3 0.55	0 7.677	6 9 <i>n</i> 4899 3 9 8626 3 0 1716
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5721 5722 5723 5724 5725	1196 1196 1197 1197 1197	III 31 IX 23 II 18 III 20 VIII 15	2 2	158 158	311	20	49 6	5 33	7 · 7 1 6 9 6 · 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 • 7 9 1 6 •	+ +	2:56 3:53	2;	פכוני כ	16	0 87 4 43 5 68	6 1 9 1	5 646 5 701	0	7327 75934 77434 77447 76988	9'7162 9'7602 9'7020 9'7010	8.757	6 0.560 0.537 3 0.572 0.570	7 7.6678 7 7.6728 1 7.6728 4 7.6699	3 9n8689 3 9'7691 3 0'1700 0n1747
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5702	210'99	+0.0358 -0.0146	9.7026	350.20	92'88	9 6882	9'9435	9'9411	9.6804	829631	9 9982	61'2	+ 86	- 27	+148	- 3	-154	+ 3 r	r#
5704	223'78	+0.7408 -0.7807	9'7162	342'26	94.89	9.6833	9,32or	9'9425	9.6561	9n2185	9'9940	62'7	<b>-</b> ⊢ 6g	+ 20	+125	+ 47	十 1 7 5	+ 72	2** <del>!</del> :
		-1'3450										74'3					_		p
5707	334'62	+1:3980 +1:2330	9'7429	333.68	96 · 18	9.6747	9'9595	9'9450	9.6152	923644	9 9880	64.0	berrow that		hyrr- <b>G</b>				p p
5709	26'67	-0.6592 -0.4764	9.7659	297.94	94.26	ე . ნკვკ	9'9924	9'9557	9.5682	9n5884	9'9647	78.4 99.0			- 23 + 10	- 65 + 52	II . =	- 27 + 18	t.
5711	253'70	+0.0060	9.7538	287.21	92.82	9.6174	9.9972	9 9591	9.0208	926008	9'9624	83'0	+ 40	— б	+106	- 23	+167	+ 7	
5713	49'70	0'3089	9'7276	275.55	90.87	0.2990	9.9998	9.9628	8.5475	9n5973	9,0631	87.8		+ 40	52 50		- 8 - 3	- 20 + 44	
5714 5715	238.04	+1.4847 -1.0478	9'7547	89.65	89.82	9.5897	0,0000	9.9719	7:3334	9.2897	9'9795	79°3 89°9			*****				$\stackrel{\mathcal{P}}{p}$
5716	g6'02	+1'4500 +0'7684	9 ' 7053 0 ' 7645	263'10 46'60	89'01 86'65	9'5792	9,9996 9,666,6	9.9662	8n6253	915765	9.9667	92'6		36	- 27	-l- 67	 十 77	fo	$p_{t^{11}}$
5718	178'39	-0.8752 +0.0412	9'7140	215.75	86.32	9.2083	9.9852	9'976x	914092	922904	9.9915	105.2	+ 94	45	+175	- 76	- 64 - 79	- 72	r
		0'1220															+147		
5722	122'30	0 · 7395 0 · 5876	9.7623	189.20	80.05	9.4892	9.8480	9'9783	914826	827279	9.9994	107.2	十173	- 64 + 54		- 44 + 35		- 31 + 18	1
5723 5724	36.43 36.43	十1'4790 一1'4953	9 ' 7040 9 ' 7040	8.32 8.32	92'59 89'13	9	9 · 9825 9 · 9787	9.976g 9.976g	9 ' 4443 9 ' 4856	9n 1874 8 6742	9'9948 9'9995	73.6		B000-00					p p
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5726 5727	167.06	+1'2747 +0'7375	9 7233	318.81	93.53	9.5148	9.9871	9'9754	9.3804	923470	9'9890	75'7	+130	+ 32	-172	+ 37	-119	+ 59	
5729	307.73	-0'6115 -0'0024 +0'1509	9.4201	305.85	93.58	9.2318	0.0010	9'9733	9'2823	9114490	9'9821	78.5	14	X X	+ 52	16	+112	48 + 11 0	<i>(</i> **)
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5732 5733	150'40 228'54	-0'6784 +0'9110 +1'3880	9.7050	104'98 249'86	86.69 82.02	9'5649 9'6215	9.9983 9.9961	9.9685	8n9479 9n1212	9.5518	9'9705	95'4 98'3	+ 86	+ 62	148	+ 87	- 41 	+ 54	)***** ])
5734	43'50	1 · 0747	9.7585	282.53	91.06	9.5716	9.9988	9 ' 9675	8.8665	915530	9 9689	85'5	-	=			\$ Process		p
5736	354 58	+0.7532	9.2200	238.50	84.01	g·6387	9.9902	9'9544	923227	925810	9.9659	103.1	30	55	- - 10	+ 28	+ 61	+ 33	2.112
5738	14 44	-0'2752 +0'0737	9'7026	227.21	83.64	9'6539	9'9817	9 95 97	914535	925440	9'9717	107.7	- 67	2C	- 14	16	+ 51	- 13	1:18
5739 5740	2.80	+0'4652 -0'6103	9.7089	217.78	83,16	9.6657	9'9794	9'9476	9:4784	9 5294 9n4841	9.9736	111,2	+150 - 78	- I5	— I37 — I3	49 59	- 47 + 88	55	
5741 5742	222.03	-1'4190 +1'2307	9'7376 0'7577	14.01	86.00	9.6830	9 9475	9'9426	9'666x	9'1206	9.9962	62'I					_		p
5743	253 27	+1.4827 -1.2703	9'7482	186.29	88.03	9'6835	9 9437	9 9425	926797	827997	9.9991	118.6	******				_		$\begin{bmatrix} p \\ p \\ p \end{bmatrix}$
5745	316.24	-0'7295	9.4121	6.13	88.11	9 . 6883	9 9419	9'9499	9'6850	8.7748	9.9992	6x.c	— тз	- 75	+ 55	- 53	+112	18	
5747	321.33	+0.7412 -0.0085	9.7029	358.25	90.55	9'6898	9'9406	9 9405	g 6895	82344	9'9999	60'7	- 22	30	∯ + 39	2	⊪ - 98	+ 29	) r*
5748 5749	339,88 3,16	+0.0323 +0.0023	9.7508	350.29	92.26	9 6869 9 6872	9'9433	9'9415	9n6808	8,9110	9,0081	118.8	- 70 - 48	+ 31	- 3 9	+ 48	+ 58	- 27 + 73	t **
5750	202 93	-0.7247	9 7383	103.87	94 50	9.0827	9 9490	9'9427	911 5602	9'1787	9,9950	117.6	<del> </del> - 89	- 19	+147	- 46	<b>—160</b>	- 72	$r^{-t}$
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5756 126 5757 126 5758 123 5759 123	09 XII 28 10 VI 22 10 XII 17	2163 183	13 42.7 23 2.7 23 49.3	284.337 97.421 273.301	+1.72 +0.41	23.540 23.540 23.539	0.046 182.475 7.923	180.031	0.7246	9'7062 9'7507 9'7288 9'7242 9'7541	8·7086 8·7485 8·7267 8·7251 8·7494	0.5637 0.5463 0.5507 0.5619 0.5366	7.6630 7.6771 7.6627 7.6774 7.6626	9'7499 7'6036 9"3561 9'8619 9"9870
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786   122 787   122 788   122 789   122 790   122	V 12 2 X 6 2 XI 5	1	1 31.3 2 20 19.1 12 38.0 2	29'945 58'279 - 200'006 - 229'701 -	-0.41 -1.25 -3.38 -3.72	23 539 3 23 539 23 540 3	186 · 287 343 · 452 13 · 336 162 · 617 193 · 974	345'892 15'569 160'417	0.7061 0.7047	9.7342 9.7476 9.7475	8 · 7119 8 · 7317 8 · 7434 8 · 7446 8 · 7323	0.5499 0.5407 0.5457	7.6765 7.6663 7.6637 7.6726 7.6758	9x7753 0x1703 0'0671 0'1781 0x10977
91 1223 92 1223 93 1224 94 1224 95 1225	4 III 21 2 4 IX 14 2 5 III 10 2	2167 850 2168 027 2168 204 2168 381 2 2168 558	3 45 1 1 16 43 1 20 9 5 1 18 34 8 3	89'450 - 8'301 - 79'015 - 157'312 -	-2'70 : -1'26 : -1'88 :	23 540 3 23 540 3	351.687 70.830 359.378 779.082 7.130	170'340 358'949 180'695	0.6898 0.7441 0.6953	9.7634 9.7577	8 · 7598 8 · 7056 8 · 7539	0'5383	7.6676 7.6713 7.6690 7.6699 7.6704	9n8962 9·8901 8n7776 8·8979 9·8228
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5756	89.52	+0.5622 +0.0040	9.7084	121'96	95'15	9.6393	9.9899	9'9542	923291	9'5798	9.9661	103.3	178	+ 43	86	+ 58	- 16	+ 10	y.: t
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5766	121'44	-o.6816	9.7172	34.70	87.03	915070	a'a84a	0.0763	0,4130	0.8480	0,0030	74.7	T/11.2	F7					
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5773	172.33	-0.6770	9 7250	141'87	92 59	9.2010	9'9827 9'9860	9.9770	9'4416	9n1904	9'9947	73.8	+ 8	- 27	+ 67 -177	+ 43 - 32		+ 64 55	7 · 16 ·
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3//4	33/ /3	+1 3940 g	9 74591	201 48	88 0416	0 0 0 37	0.0003	0.0018	8,7270	0.5007	0.0606	93,4			-			+ 44	$p_{\perp}$
5780	140'17	-1'1485	7386	75.02	87 56	9. gr38	9.9980	9.8288	8.9874	9.6017	9 9753	81.4			200000	_	Process		$\frac{p}{p}$
5781	300'58	-l-1 ' 5390 g	9.7250	105 27	01.00	2'5550	0.0082	0.0684	80570	A . E E A 9	0:0704	05.6				·			
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5784	133 28	+0.0843	9.7020	238 00	84 85 6	0299 0 6306	0.0800	9 9504	0.2291	9.5925	9.0039	79'4	4I	- 28	+ I3	+ 2	+ 73	- 9	(1)11
3/35	-40 10	+o.3942	7058	54.09	84 '42	9.6434	9'9875	9.9532	9'3732	9.2698	9 . 9678	75.3	+ 44	- <del> -</del> 8	+111	H- 46	164	+ 35	t**
5786 5787	125.81	-0.2961 c	7097	227 . 52	83 64	6538	9.8816	9 ' 9507	914551	9115427	9,8418	197.7	+161	18	-131	- 59	- 33	50	,
5788	123'05	+1.1620	7302	45 68	84 40 9	0.6538	9.0800	9'9441	9.6350	9'2997	9'9912	63'8			P		_	_	p p
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5794	24'44	-o.o200 g	7598	79 30	0.33	6882	3 9410	9 9407	g 0800	o 700g	9 9993	00.9	-128	32	69	1	- 8	+ 26	7
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	Julianischer Kalender	Julian. Tag	Welt- Zeit			ε	.#.	Q	$\log p$	$\Delta L$	$\log q$	u'a	$\log f_a$	logγ
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5806 5807 5808 5809 5810	1229 XII 17 1230 V 14 1230 XI 6	2170 301 2170 449 2170 525	10 42 0 4 30 4 15 26 1	59 637 231 367	+0.38 -1.23 -3.67	23'536 23'536 23'535	169.425	16.103 170.617 348.394	0.6991 0.7425 0.6935 0.7331 0.7128	9.7610 9.7610	8.7505 8.7078 8.7565 8.7169 8.7370	0.5358 0.5750 0.5332 0.5670 0.5453	7.6527 7.6774 7.6636 7.6758 7.6644	9n9511 0'1613 9'9551 9n9577 9'2315
5811 5812 5813 5814 5815		2171 158 2171 334 2171 482	3 11.8 12 51.6 11 37.0	38 · 940	-0'90 -3'77 +2'01	23'534 23'534 23'534	186.547 6.241	188 · 347 5 · 230 162 · 663	0.7104 0.7350 0.6919 0.7426 0.7450	9.7139 9.7512	8.7396 8.7151 8.7585 8.7081 8.7057	o 5504 o 5609 o 5384 o 5696 o 5688	7.6749 7.6654 7.6737 7.6701 7.6666	9n2147 9n7899 9'7261 0'1911 0n1394
5816 5817 5818 5819 5820	1233 IX 5 1233 X 5 1234 III 1 1234 VIII 26 1235 II 19	2171 689 2171 836 2172 014	5 8.6 15 1.9 6 42.8	199'035	-3 · 33 +2 · 88 -0 · 26	23'534 23'534 23'533	14'320	15'505 169'118 354'320	0.7009 0.6924 0.7254 0.7240 0.7018	9.7612	8 7489 8 7578 8 7246 8 7259 8 7481	o 5408 o 5380 o 5582 o 5545 o 5439	7.6688 7.6724 7.6715 7.6674 7.6729	0n1512 0.0837 9.8971 9n8679 8.5628
5821 5822 5823 5824 5825	1235 VIII 15 1236 II 8 1236 VIII 3 1236 XII 29 1237 I 28	2172 545 2172 722 2172 870	16 56.6 11 27.0 20 18.7	326.686 137.837	+1.00	23'534 23'534	0'039 187'680 7'838 164'021 195'692	7,000	0.7420 0.6893 0.7430 0.7088 0.6978	9'7637	8 7085 8 7608 8 7074 8 7410 8 7523	0.5664 0.5373 0.5663 0.5511 0.5430	7.6661 7.6741 7.6650 7.6771 7.6752	7.5728 9.8131 9.8755 0.1466 0.1280
5826 5827 5828 5829 5830	1237 VI 24 1237 VII 23 1237 XII 19 1238 VI 13 1238 XII 8	2173 225	3 58.8	99'021 127'183 274'942 88'878 263'508	+1.21 +0.60 -0.07	23'535 23'535 23'536	355.077	13.730	0'7148 0'7256 0'7319 0'6946 0'7442	9'7245 9'7151	8 7349 8 7234 8 7178 8 7549 8 7063	0.5454 0.5541 0.5672 0.5332 0.5762	7.6627 7.6641 7.6773 7.6626 7.6773	0n0868 0'1649 9'8843 9n6261 8'9653
5831 5832 5833 5834 5835	1239 XI 27 1240 IV 23 1240 V 23 1240 X 16	2174 081 2174 111 2174 257	4 25 1 17 21 4 3 36 4	40'528 68'751	-1.05 -0.09 -1.05	23.537 23.537 23.537	3.767 186.186 342.744 12.501 162.344	345 177	0 6913 0 7370 0 7193 0 7075 0 7035	9 7632 9 7086 9 7327 9 7462 9 7487	8'7582 8'7129 8'7302 8'7419 8'7460	0.5316 0.5708 0.5502 0.5413 0.5457		9.5068 9.7672 0.1895 0.0408 0.1834
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5841 5842 5843 5844 5845	1243 IX 15 1244 III 10 1244 III 10 1244 VIII 5	2175 646	6 22.2 6 22.2 6 22.2	328.061 357.399 139.626	-1 · 90 +3 · 82 +2 · 16 +0 · 93	23	14'891 164'509	342°159 12°548 165°069	0'7301 0'7181 0'6959 0'7066 0'7440	9.7188 9.7328 9.7566 9.7456 9.7023	8 7191 8 7310 8 7532 8 7422 8 7060	0'5600 0'5525 0'5412 0'5456 0'5674	7.6690 7.6699 7.6739 7.6704 7.6652	9'7899 9n7998 0n1377 0'1145 0'1687
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5804	268 62	-0'0011	9.7325	121.82	95'13	9.6390	9.9899	9'9543	923275	9 5799	9,0661	103'3	- 27	+ 4	+ 00	+ 14	96 145	- 20	2-11
5805	299'74	+0.7253	9.7248	298.22	94'64	9.6340	9.9920	9 9555	9'2778	925872	9 9649	78 · r	+ 5	+ 32	+ 56	+ 25	+ 99	+ 52	2***
5806	97'74	-0.8935	9.7573	111.20	93'55	g · 6237	919955	919578	921526	9.5974	g'g6gr	08'9	-147	48	101	- 41	_ 7r	61	t
5807	335'92	-⊦1'4497 -⊦0'9018	9.7039	286.96	92.77	9'6167	9'9973	9'9592	9.0440	926006	9'9624	83.1					· —-		$p_{\perp}$
5809	57.77	-0.3023	9 7162	241.28	86.99	9.5437	9'9945	9.9717	921990	9114940	9'9778	99.6			+105 62			+ 63 66	
5810	108.80	-l-0'1704	9'7423	59'47	86 . 89	9.2399	9,9938	9'9722	9 . 2248	9.4819	919790	79'9	-172				- 39	+ 19	$t^{:  }$
5811	168.35	0'1639	9.7433	228 92	86 - 67	9.5243	9.9899	9'9742	923269	924123	9 ' 9850	102'7	+129	+ 3	r 6 g	25	99	- 21	2°-1*
5812	227.03	-0.2322 +0.2322	19.2100	47.27	86 ' 67	9.2222	9.0893	9 9744	9'3396	9'3996	9 9858	76'9	- <del> -</del> 83	- 49	I37	25	166	- 24	r
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5815	240.97	-1,3482	9:7031	34'31	87.03	9.2078	9.9847	9.9763	9,4169	9'2747	9.9922	74.6	********		P TOPM				2)
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5821	345 °00	+0:0037	9'7073	141 56	93.11	9.2092	9 9862	9.9760	923935	9'3171	9'9904	104.7	- 49	+ 15	+ 15	12	+ 73	- 14	
5823	348.54	—о б5оз +о 75о8	9.7060	128 83	93'31	9 5268	9'9908	9'9739	923079	9'4282	9.9838	75.0	- 150 - 85	- 53 + 57	04 - - 16	- 55 + 66	+ 8 + 93	- 25 + 35	494
5824	126.42	+1'4017 -1'3427	9 ' 7446	273 50	90'52	9.5847	9'9999	9'9653	8'3363	9115840	9.9654	88.7				_		_	p
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5828	241'29	+0.7662	9'7173	261 11 2	88 * 58	9 6042	9 ' 9993	9.9618	817559	925997	9'9626	93.6	+ 76				+r68	+ 42	P
5830	252 49	-0'4228 -0'0923	9.7018	249'10	86.26	9.6232	9'9979	9 9 9 5 9 8	8.9887 9n1384	9°0012 925985	9.9628 9.9628	98.6	-152 $+ 53$			- 2 - 18	- 41 +169	· '	444
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5840	447 52	+0'1162	9.7588	187.07	87 84	9.6873	9 ' 9426	9 9 4 1 3	g <i>n</i> 6830	8,18352	9,9990	118.0	+ 51	+ 35	+114	+ 4	+178		t**
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5851 5852	64°01	+0.4213	9.7235 9.7584	309°12	96°01	9.6486 9.6387	9 ' 9846 9 ' 9899	9'9521 9'9544	9.4186 923280	9n5562 9'5793	9 ' 9 6 6 2 9 ' 9 6 9 9		123 96			+ 28 35	- 28 -176	+ 56 59	rii: t
5853 5854	95'57	+1.4437	9.7622	298'19 82'41	94°59 88°92	9 · 6334 9 · 5779	9.9923 9.9996	9 9557 9 9665	9:2724 8:6660	9"5876 9"5746	9.9648	82.1	-140	+ 63	+175)	(18+)	+145	+ 66	$rac{p}{t^*}$
		-1.217				ľ						•		l	-I-178	- 88	- 54	63	
5857	217'67	-0'9158 +0'2421 -0'1762	9'7407	71'39	87.20	9'5590	9 9975	9.9695	9.0323	9.2380	9.9724	99 5	+ 2	I	+ 64	T 34	+135	19	6.
E850	220154	0'5457 0'5140	0 7740	50'52	86'00	0.4308	0.0038	0'0722	9 2240	9'4820	9'9790	79'9	20 162	41 42	141	16 17	81 81	— 22 + 18	
5861	348.84	-1,3100	9.7035	46.85	86·66	9.5226	g · g8g r	9'9744	9.3436	9:3972	0,0000 0,0800	76 .8							p p
5863 5864	24'42 161'34	+1.1912	9.7621	216.34 358.67	86'go go'14	9 5123 9 4886	9 985 x	9'9757 9'9784	924095	9n3005	0'0000	72'1		— + 38	. 1			 - - 74	$p_{j}$
5865	35'42	-0.7922	9.7271	167.79	91.54	9.4891	9'9794	9.9783	914782	8.8350	9.9990	107.5	-100	- 35	- 42 - 25	— 52 — 7		70	
5867	89'42	0.0611 -0.0611 -0.6286	9.7062	154.38	92'38	9 * 4958	9 9824	9.9776	9n4404	9'1490	9.9920	100.7	-152	一 14 十 13 一 54	90	+ 4	+ 98 - 32 -123	- 20 - 22	gails t
586a	90.78	+0.6786	9'7065	141'29	93,13	9.2101	9 9862	9'9758	913925	9.3200	9.9905	104.6	-177	+ 55	- 86 	+ 57 	16	+ 27	p
5871	71,00	-1.3300	9.7559	320'36	93'25	9.2170	9.9863	9'975	9.3930	913362	9 9 9 8 9 5	75 3						11	p p
5873 5874	151'12 4'07	-1.3887 +0.7736	9.7281	129'07	93'35 90'45	9.5290	9,9999	9 9 9 7 3 6	8.3122	9.4292	9.9837	88.8	- 52	1 1	. 1		+ 42		$p_{p}$
5875	209'93	—o'4968	9.7628	86'02	89.38	9'5964	9 9998	9'9632	8.4017	9.2920	9 9034	88.4	96		+150	7		- 26	etile
5877	100,01	+0.0998 +0.2468 -0.5780	9.7648	75'40	87.62	9.6133	9 9981	9'9600	8.8441	9.6013	13.3053	84"	- 68 - 178 - 86	+ 8		+ 38	+ 48 - 36 + 79	+ 2 + 18 - 40	$t^{*}$
5870	340 ' 28	+1.0280 +1.2385	9.7464	65 45	85.08	9.6278	9 9942	9.9568	3 9 2 1 0 0	9'5935	9.0037	79	3						p p
5881	95'97	_I.2287	9.7381	238.51	84.89	9.6384	9,9900	9 9544	923262	925795	9'9661	103'			_			- 42	$\begin{bmatrix} p \\ r \end{bmatrix}$
5883	134'92	-0.9245 +0.8285 -0.1845	9.7659	203'10	84.22	9.6778	9.9500	9 9442	0.640	30 2052	0'0013	63	28	- 36	+ 83	. ~	1	11	t:11
5885	12'22	+0'1467	9.7576	195'03	85.22	9 6842	9 9478	9.9422	920040	911518	9.995	117	] - 70	7 30	10		T 55		
5887	101.13	+0.5614 -0.5933 -1.3937	9'7332	187'26	87 79	g 6867	1919429	9'941	5 92082	1 82845	99999	dira.	o waror	+ 6 - 8	+ 33	47 47	+122 -115	+ 61 - 65	$\left\{egin{array}{c} r^* \\ r \\ p \end{array} ight.$
588a	101,07	+1.2570 +1.5447	9.7491	5 90	88'20	9.6859	9.9426	9'941	7 9 682	918.755	3 9 999	3 or.	T —		_	_	_		p p
#80T	264:55	, — I · 3683	0.7002	170'4	00'18	30.686	0.041	0'041	5 92686	5 7 741	0.000	119.	<u>.</u>					Y 5	$\begin{bmatrix} p \\ t \end{bmatrix}$
5892 5893	29.07	+0.7037	9.7654	336.81	95.81	9.6782	9 9 9 5 5	9 9 9 9 4 4	0 9 631 8 9 <i>n</i> 593	9 9 n 3 1 9 0 9 ' 4 1 5	7 9 ° 990; 1 9 ° 984; 6 0 ° 083;	8 113 8 66	0 + 08 $0 - 149$ $0 - 121$	- 24	- 19 - 50	- I	1 + 51	+ 2	B 2***
5895	120.61	+0.0048	9.7358	140'87	96.70	9 663	9'973	9 948	2 9 1 5 3 0	99'493	9 977	9 110.	91-1-170	- 20	-121	"	1 - 03		
5897	319.21	+0.7132 -0.7438	9.7595	131'73	96 26	9.651	8 9 982	19.951	3 92446	59'544	9 9 971	5 107.	4 - 20	+ 24 - 29	+165 + 35	+ 3	+ 76	+ 60	
5899	114.48	+1 ·4360 +1 ·0482 -1 ·4517	9.7614	93'72	90 58	9 596	9.999	9 9 9 5 3	3 82371	69.595	39.963	4 91.	5 —				_	-	$\begin{array}{c} p \\ p \\ p \end{array}$
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5901 5902 5903 5904 5905	1267 1267 1268	XI 28 V 25 XI 17 V 13 XI 6	218 218 218	3 79 3 97 4 15 4 32 4 50	4 9 0 15 8 16	31'5 57'0 48'6	70° 242° 59°	403 567 948	-1°9; -0°9; -2°9; -1°2; -3°6;	23	3'531 3'530 3'530	176 47 357 92 184 95	3 178° 2 355° 3 186°	899 590 580	0.7128	9'7438	8.7340 8.7421 8.7129	0'5461 0'5500 0'5611	7 6766 7 6636	9n9641 9'5027 9n2649 9n6713 9'6996
5906 5907 5908 5909 5910	1269 1269 1270	V 27 IX 27 X 26 III 23 IX 16	218	4 03 4 85 5 00	9 22 7 6	19.7	221	606 075 699	-2.87 -3.93 +1.14	23	529 529	342.65 13.83	9 344 5 15 168	823 214 130	0'7450 0'7029 0'6936 0'7228 0'7265	9 · 7499 9 · 7593	8.7468 8.7566	0'5402	7.6644 7.6714 7.6749 7.6689 7.6700	0n0919 0n1754 0'0702 9'9377 9n9243
5911 5912 5913 5914 5915	1271 1272 1272	III 12 IX 6 III 1 VIII 25 I 20	218 218 218 218	5 53 5 71 5 89 6 04	9 0	57.0 50.7 6.8 28.0	348 · 6 359 · 6 308 · 4	988 540 012 105	-1'12 +2'83 -0'22 +3'63	23 23 23 23	528 528	358.75	359	637 039 356		9'7031 9'7642	8.7075 8.7608 8.7086	0'5410 0'5689 0'5356 0'5670 0'5520	7.6702 7.6687 7.6715 7.6674 7.6759	8.9999 9.0775 9.7786 9.7870 0.1533
5916 5917 5918 5919 5920	1273 1273 1274 1274	VII 5	2186 2186 2186	5 217 5 247 5 395 5 572	7 18 7 5 6 20 2 9	29 5 35 x 27 7 23 5	109.7 297.2 148.2	75 93 77	+0.52 +0.98	23 23 23 23	529 529 529 529	171'656 353'339	342° 12 173° 352°	250 161 508 231	0.7001 0.7119 0.7237 0.7341 0.6932	9 7529 9 7417 9 7276 9 7129 9 7615	8.7380 8.7262 8.7159	0'5427 0'5441 0'5536 0'5681 0'5326	7.6636	0n1182 0n1335 0'1205 9'8936 9n7556
5921 5922 5923 5924 5925	1274 1275 1275 1276 1276	XII 18 VI 13 XII 7	2187 2187 2187	927 103 281 458	20 17 3	49 5 59 3 3 7	99 7 274 4 89 6	43 06 35	+0.55 +0.52 -0.01	23	531 531	178 885 2 014 186 060 10 770 193 749	184	928 145	0.7444 0.6925 0.7354 0.7105 0.7131	9 6994 9 7621 9 7107 9 7430 9 7375	8.7571	0'5761 0'5320 0'5697 0'5427 0'5542		9'0314 9'2362 9"7567 9'9800 0"0870
5926 5927 5928 5929 5930	1277 1277 1278 1278 1279	IV 12	2187 2187 2188 2188	783 960 137 314	5 13 20 16	20.6 56.4 35.9	222'4 40'1 211'7 29'4	35 82 83 41	3'90 0'92 3'84 0'36	23. 23.	532 532 532 532	349'472 169'984 357'335 178'023 5'396	169 '8 356 '5 179 '8 3 '1	347 584 394 668	0.7278	9'7220	8.7608 8.7067 8.7514 8.7215	0.5644 0.5376 0.5669 0.5422 0.5568	7.6750 7.6653 7.6738 7.6665	0n0004 9'9273 9n4085 9'2334 9'6989
5934 5935	1280 1280 1280 1281	IV 1 IX 25 II 20	2188 2188 2188	669 846 994	13 9	52'5 8'1 15'7	18 g: 190 o: 339 4:	23 · 28 · 76 ·	+0·38 -2·73 +3·37	23 23	532 532 532	13'851 194'038 351'409	11.6 195.3 352.0	501 305 14	0'7043	9.7486	8 · 7447 8 · 7096	0.5388 0.5423 0.5689	7.6725 7.6714 7.6678 7.6713 7.6727	9n7503 on1524 o 0814 on1229 9n8623
5938 5939 5940	1282 \ 1283 1283	I 30 VII 25	2189 2189 2189	525 703 879	3 9 16	21'0 1'2 58'9	139 3 317 90 129 06	29 -	+3.45 +0.84 +3.87 +1.51	23 23 23 23	532 532 531 531	359 55 1 179 182 7 547 187 831	1.7 176.7 9.6 186.2	93 38 49 91	0.4346 0.436 0.4363 0.4363 0.6353	9.7099 9.7461 9.7353 9.7188 9.7584	8 · 7437 8 · 7325 8 · 7202	0 5473 0 5484 0 5636	7:6662 7:6740 7:6651 7:6751 7:6642	9.9369 8.5976 8.8695 9.8456 9.8281
5942 5943 5944 5945	1285	VII 14 XII 8 VI 4	2190 2190 2190	234 381 559	10 16 16	7'1 10'0 35'5	91 00 118 97 264 84 80 84	3 -	-0.21 -0.67 -0.21	23.5	530 1 530 3 530 3	75.615	168'4 197'0 347'9 178'0	19 0 32 0 52 0 45 0	0.6962 0.6907 0.7298	9'7008 9'7585 9'7641 9'7178 9'7354	8 · 7534 8 · 7591 8 · 7198	0'5341 0'5315 0'5657	7 · 6626 7 · 6634 7 · 6773	0'1539 0'0510 0n1410 9n9652 9'5986
5947 5948 5949	1285 1286 1286 1287 1287	XI 17 V 14	2191 2191	090 268	14 5	3 7 2		7 -	-2 · 97	23 5 23 5 23 5	527 I 527 I	57.864 84.086 5.786 92.064 42.318	185 6: 5 0:	27   C 81   C	7381 6 6904 7448	9 7 102 9 7 6 2 6 9 7 0 1 7	8.7120 8.7601 8.7056	0'5614 0'5393 0'5665	7.6631 7.6637	9n2757 9n5887 9 6918 0n0628 0n1845
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III to more a secondario			1											Gr 1	ı di	6		
5901	302°35	0.9206	9.7185	266°44	89°48	g·5840	0,0000	919654	8,3431	925833	9 ' 9555	91°4	- 61 - 5	+ 57	go	-179	59	1.
5902 5903	324.70 62.74	+0'3182 -0'1840	9 7393 9 7459	83.00 254.34	89.00 87.08	9.5780 9.5637	gʻggg6 gʻggg6	9 9664 9 9688	8.6305 8 _n 9658	9	9.8408 9.8669	95'7	- 35 + 1 -128 - ;	63	31	+ 7	15	r-t
5904	71,00	-0.4691 -0.5007	9'7x35	71'46	87.71	9'5587	9'9974	9'9695	9.0336	9.2382	9.9724	83.4	-123 - 31 + 33 + 3	- 70	8 12		20 20	
5906	88.73	I·2357	9.7038	50.00	86.87	9.2399	9 9936	9.9722	9.3398	9 4804	9 ' 9792	79:7		-	_			p
5908	152.67	-1.4977 -1.1755	9.7613	229'34	86.62	9.5280	9.9900	9'9737	923264	914188	9'9845	105.2	*****	 76	— — — 69	十177	77	$p \\ p$
5909 5910	276'15 149'43	0'8654 0'8400	9.7301	181'13	89.88	9'4912 9'4866	9.9792	9.9786	914865	718012	0.0000	107.9	+ 4 + 4		- 62		- 75	
5911	86.55	+0.1000	9'7554	358.00	00.11	g'486g	g·9786	9:9786	9.4868	7n7924 8 ' 8414	0,0000	72.1	-151 - 1: +103 + 1	87	+ 6		+ 24 24	ate I
5913	323'32	-0.6006	9.7663	345 99	91'42	9'4910	9'9795	9'9781	9.4766	828956	9.9987	72.2	- 39 - 5 + 87 + 5	1 42	44	- - 108	19 21	t pili
5915	22.11	+1.4233	9.7420	298'41	93.03	9 5449	9'9945	9 97 15	0,1999	924953	9 9776	80.4	g. 100 mg	A0-10-14		payri while		p
5917	99'63	—1:3127 —1:3600	9.7436	100,18	92*38	g·5608	9.9973	9'9692	920497	9'539I	9'9723	30.0		_	_		\$70Accon	p p
5918 5919	259.66 126.27	+1'3197	9.7297	141'46 285'40	91.88 91.19	9'5129 9'5637	9.3861 9.3861	9,9756	9n3963 8 9585	g:3220 9:5499	0,0208 0,0003	84.4	-178 + 4		- - 3I		+ 52	p 1** t
1		o·5696												-1- 38	x3		- 34	
5922	220'70	+0'1723	9'7642	86'39	89'44	9:5957	9,0999	9'9634	8.3282	9'5949	9.0632	88.6	+ 171 + + 71 + + 150 - 2	3 + 139	+ 33	-152	+ 10 - 35	1,4,
5924	87.34	-0.5711 +0.9550 -1.2217	9'7450	76'03	87.73	9.6121	9.9982	9'9602	8.9571	0.6013	9,3653	84 3	+x47 + 5	3 (+ go)	(+83)			$p^{t^{t \mathbf{i}}}$
		-1,0010											(+- 21)(6 <u>c</u>	)		+ 42	54	(o·)
5927	254'15	+0.8428	9'7659	20187	83.35	9'6701 9'6738	9'9656 0'0631	9'9463	925826 0'5070	924304	9'9836 9'9851	65.8	+ 80 + 7 - 71 - 3	7 18	+ 52 - 1	- -162 - - 42	+ 33	t**
5020	128.20	-LO' 1711	0'7566	203'34	84 15	0.6787	0'0560	0'0430	026318	923228	9'9902	TIO.O	+166 + 3 -134 +	5 136 75	- 1 + 45	71 14	- 16 + 55	
5031	310.40	0:5627	0.2315	105'22	85 60	ი 6836	0'0481	0'0424	on 6636	9n 1559	9 ' 9955	117.8	- 18 -			<b>.</b>		l l
5932 5933	75°25	-1.4203 +1.2062	9 7 7 5 0 6 9 7 5 0 6	352.74	92.17	g ' 6835 g ' 6832	9 9438	9 9425 9 9425	9.6670	9'1121	9.9990	62'1						p
5934 5935	317.39	-1.3270 -0.4283	9.4621 9.4621	345 13	94.55 94.55	9.6835 9.6835	9 9431	9'9417 9'9424	9,6644	921460	9 9989	62.2	- 57 - 7	3 + 52	63	+118	- 19	r t
5936	133 13	-ho:8648	9.7120	157 95	95 65	9·6792	9 9546	9 9436	926374	9.3012	9.0011	116.3	+ 80 + 7	8 -121	+ 86	- 50	+ 33	地
5038	220'52	-1-0'0740	0.7374	740 ' 63	06 . 20	o'6724'	a'a638	9 9456	025030	0'4152	9 9847	III3.0	+113 - 2 $+60 + 2$ $-13 + 2$	71 131	T 20	-172	- 19 - 63	1-13
5940	71.81	-o · 6731	9.7605	141.02	96.77	9.6629	9 9733	9 9484	925316	9.4913	9'9781	III.G	-r35 - 2	o — 79	- 28	- 33	- 58	t
5941 5942	333 40 224 80	+1 · 4253 +1 · 1245	9 · 7029 9 · 7605	318·83 104·68	96·70 92·39	9 6 6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	9 9756 9 9980	9 ' 9490 9 ' 9599	9 · 5131 8n 9792	9 <i>n</i> 5058	9'9764 9'9623	69 g		Printer	_	_		$\begin{bmatrix} p \\ p \end{bmatrix}$
5943 5944	327:21	-1.3837 -0.0230	9.7660 9.7660	131'74 278'43	96'21 91'34	9 · 6502 9 · 6033	9'9825 9'9993	9'9517 9'9618	9n4453 8 · 7321	9'543I 9n5994	9 9626	86.6	+167 - 6	0 (+116)			- 56	
5945	70.45	+0.3968	9.7375	94.32	90.67	9·5 <b>9</b> 66	9, 9998	9 9632	8n4367	9.5956	9 9634	91.7	-146 + 2	3 - 70				
5947	171 65	-0.3848 -0.1884	9.7124	83.10	89 02	9.5780	9 9996	9.9664	8 . 6248	9.5753	9 9669	87 4	+135 - 2	9 +168 3 -171	x	и.	<b>– 19</b>	2.14
5949	186.87	-1'1555	9.2038	71.04	87.66	9 5586	9'9974	9.9695	9.0428	9.5374	9'9725	83.2		2 - 44	+- g	+ 13	+ 22	$\left  egin{array}{c} p \\ p \\ p \end{array} \right $
5950	.20 14	-1'5293	y /5º4	20/ 42	·/ 42	y J∨34	9 9023	9.9708	yn4405	3111040	9 9949							
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5961 5962 5963 5964 5965	1292 1292 1293	VIII 25 I 21 VII 15 I 9 VII 5	2192 2192 2193 2193 2193	981 157 335	4 35 16 53 4 48	3 308 3 120 7 297	423 252 022	-0'19 +3'62 +1'25 +2'90 +1'01	23 528 23 527 23 527	171.538 352.502 178.781	173.318 351.530 178.753	0'7351 0'6925 0'7445		8 · 7278 8 · 7150 8 · 7576 8 · 7661 8 · 7566	0.5534 0.5683 0.5325 0.5758 0.5326	7.6673 7.6759 7.6636 7.6766 7.6630	928060
5966 5967 5968 5969 5970	1294 1294 1295	XII 29 VI 25 XII 18 V 15 XI 8	2193 2193 2194 2194 2194	867 043 191	1 7 11 40 19 22	8 100 7 274 9 61	066 410 450	+1.82 +0.58 +0.52 -1.17 -3.57	23 529 23 529 23 529	9 · 897 193 · 715 348 · 627	184 193 12 302 191 291 349 705 169 809	0.7110	9'7411 9'7389 9'7056	8.7376 8.7376 8.7082	0.5437 0.5534 0.5644	7.6627 7.6636	9 9452 0n0847 0n0345
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5976 5977 5978 5979 5986	1298 1299 1299	IV 12 X 6 III 3 VIII 27 II 21	2195 2195 2195	431 579 756	17 37 3 45	7 200 1 350 8 160	.915 .406 .551	-0'36 -3'43 +2'68 -0'34 +3'36	23 '53 23 '53 23 '53		194.815 351.782 168.546	0.7407 0.6905 0.7368	9 7049 9 7628 9 7110	8 · 709 I 8 · 759 2 8 · 7127	0.5363	7.6725 7.6714 7.6675	0n1114 9n8799 9'9665
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599 599 599 599	2 1305 3 1305 4 1306	V 24 XI 17 IV 13	2197 2198 2198	853 030 177	7 3 15 28 21 10	1 4 70 3 5 243 5 7 3 1	3 33	5 -2 95 3 -0 46	23 52 23 52 23 52	6 191 18 6 13 58 6 169 30	4 5 12 5 190 73 9 15 14 8 166 88 5 352 29	5 0.744 0 0.694 5 0.720	6   9 · 702 9   9 · 757 3   9 · 731	8 · 705 8 · 755 8 · 729	0.566 0.542 0.551	7 663 7 646 7 666	9 6865 0 00302 5 0 0639 9 9867 7 9n9615
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5951	282°01	+1.1620	9'7606	242°13	86°99	9'5463	9'9946	0'0713	921033	024087	0'0773	99°5		_	_	_	_	p
5952 5953	29'29 265'34	+0.8808	9'7317 9'7239	24'96 194'53	87·62	9'4995 9'4901	9'9818	9'9772 9'9783	9'4527 9"4745	9'1435 8 ₂ 9100	9'9958	73'4	-117 + + 14 -	49 — 37 44 + 87				1:41
5954	207'30	0'1416	9'7565	12.24	88.76	9'4894	9'9794	9'9783	9'4784	8 8 3 6 6	9'9990	72'4	+ 89 - - 5 +	9 +152	+ 12	-141	+ 26 28	$t^{iji}$
5956	88.02	0.5666	9'7663	359:39	90.06	9'4876	9.9785	9 9785	9.4875	7n5342	0,0000	72.1	-157 -	52 - 83	- 37	<b>– 19</b>	r7	t
5957 5958	302°14 148°35	十0.5537	9'7078 9'7405	311.51	91.28	9.4876	9'9797	9 9785 9 9740	9n4756	8.8538 9n4137	9 · 9989 9 · 9849	77.2	- I3 + -	51 63 	+ 40	+125 —	+ тб 	p
5959 5960	208.81 355.33	-1.4233 -1.4233	9 7539 9 7450	121,13	93.18 81.38	9.4952	9,8832	9'97¤7 9'9770	9,4819	9.4827	0.0480 0.0084	100.4				-		p
5961	10,20	+1.522 +0.402	9.7312	154.17	92.44	9'4998	9'9820	9'9770	924495	9.1573	9 9954	106 5		_				$p_{j}$
5963	73'70	0.6397	9.7643	100,03	92'35	9.2200	9'9974	9.9695	920448	9.2376	9'9725	96.8	+ 56 + -131 - + 50 +	31 - 76	20	- 24	- 43	t
		+0'0986											- 40 +					.ate
5967	194'06	-0.8814 -0.8814	9'7431	86.99	89.23	9'5950	9 9999	9'9535	8:2788	9 5945	9.9636	88 8	+ 27 - + 54 +				— 31 + 55	
5968 5969	351'42	-1.0822 -1.0822	9.7410	260'85 48'21	88.54	9.6045 9.6522	9'9992	9'9512 9'9512	827684 9'4474	9%5999 9'5449	9.9626	93 7			`	,		p p
5970	34'60	0.8582	9.7659	221.27	83.30	9.6599	9'9757	9.9490	915122	9n5066	9.9763	i io.	- 52 +	68 - 27	- <b>+</b> 47	+ 28	+ 37	T _{alt}
5972	265 84	+0.1896	9.7554	212'12	83.31	9 6708	9 9658	9 9462	925820	924337	9 9834	113.7	- 169 - + 41 +	33 4- 96	4		I2	L181
5974	71,10	-0.2381 -1.4230	9'7299	203'53	84.13	9.6782	9'9563	9 9441	926306	913254	9,9901	115'9			+ 43 - 49	- 94 + 14	56	
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5977	129'13	7 +1:1490 3 -1:2923 0:7584	9.2020	195'18	85'72	9 6830	9.9483	9'9426	9,6630	921538	9 9955	1 x x 7 ' 1	7	78 - 73	64		- 20	$p \\ p \\ t$
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5981	340 . 63	+o'1377	9.7389	157.96	5 95 · 65	9.6795	9 9546	9 9436	926377	9.3017	1 9 ' 9 9 x :	1116'	3 - 51 +	33 + 21	+ 20	+ 78	18	2-2
5982 5983	186.1	2 +0 · 6822 1 -0 · 6064	9.7614	337'2	95.77	9 · 678	9 9 9 5 5 4	9'9438	9.6342	923138 794128	3 9 990 3 9 984	63 63 5 3 114 5	0 +108 -	17 - 79	+ 38	- 29	+ 56 58	2013
		+1.4003 +1.5000													_		_	p p
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5988	175'2	5 +0 · 4776 -0 · 1914	9.7359	105.5	8 92 49	9 9 6 14:	2 9 9978	9.959	7 82 997:	2 9 601	9 962	3 96	$     \begin{array}{c cccccccccccccccccccccccccccccccc$		+ 52	-100	+ 20	
5990	269,5	-0.3040	9.4113	94'4	i 90 · 6	9 9 5 9 6	9999	9 963	2 8 1 4 4 6	9.595	6 9 963	4 91'	7 + 34 -					7:11
5991 5992	176.7	4 +0.4850 3 -1.0720	9.7649	267.0	3 89 · 5	6 9 584 6 9 577	8 9 9999 5 9 9999	9 9 9 6 5 5 9 9 6 6	3 8 n 2 6 4 6 8 · 6 4 0	6 9n584	3 9 ' 965 5 9 ' 967	4 gr	1 +128 +	28 -176	+ 6	-121	+ 20	$\begin{bmatrix} t^* \\ p \end{bmatrix}$
5993 5994	52.1	8 +1 · 1585 2 +0 · 9698	9'759	5 254 7 5 37 7	0 86.8	5 9.212 6 9.212	8 9 · 998: 3 9 · 985	2 9 · 9 6 8 8 9 · 9 7 5	3 82957 7 9 401	$\frac{3}{9}, \frac{9}{3}, \frac{5}{3}$	2 9 · 970 6 9 · 990	4 95° 6 75°	6 — 1 +116 +		_	 (- - 36	) (+78	p
5995	22.7	9 -0.012	9.7222	207:8	8 87 4	49'499	5 9 982	9.977	2 92440	7 92 186	9 9 994	8 106.	2 -112 -	49 - 30		+105	- 7	r
5992	7 54'6	0 -0 2150	0 9:703	8 194 4	0 88 5	7 9 487	6 9 980	0 9'978	59n472	3 82903	2 9 998	6 107'	5 — 30 — 3 — 115 +	5 - 57	- x	3∥- - q	- 3·	
599	3 210 g	2 -0.525 2 +0.502	1 9 . 766; 1 9 . 766;	3 12'7 4 180'5	3 88 · 7 4 89 · 9	0 9 490 4 9 484	2 9 979 7 9 978	4 9 9 9 7 8 8 9 9 7 8	2 9 478 8 9 484	3 8 854 7 7n 494	3 0 ' 000	0 107	4 + 86 - 8 -116 +	49   +×53	- 29	- I 44 2 + I 3	x	2 101
0000	×73 0	0 +1 . 4620	9 739	4 3 4 4 2	4/93.0	Jy 510	49 985	9 975	919 411	2 92292	9 9 991	5 74'	8	_				p
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Nr.		anisch alende		T	ian. ag		Velt- Zeit	L'	Z	ε	P	Q	$\log p$	$\log \Delta L$	$\log q$	$u'_a$	$\log f_a$	logγ
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6006 6007 6008 6009 6010	1311	VII	9 5	2200 2200 2200	097 274 452	17	42'4 14'3	308'147 120'579 295'757 110'508 285'513	+1.26 +2.87 +1.03	23.524 23.525 23.525	0'314 185'919	184 040	0'6941 0'7337 0'7133		8 7060 8 7559 8 7162 8 7362 8 7389	0.5751 0.5334 0.5679 0.5447 0.5524	7.6759 7.6636 7.6766 7.6630 7.6771	9.1164 8.4308 9.7448 9.9073 0.0823
6011 6012 6013 6014 6015	1313 1313 1314 1314 1315		15 8	2201	953 131 308	22 2 14	42'8 33'6	71 · 888 244 · 710 61 · 172 233 · 949 50 · 559	-2.83 -1.16 -3.56	23.526	169.730 157.665	348'718 169'818 354'719 179'677 1'602	0 6889	9'7049 9'7638 9'7046 9'7521 9'7256	8.7077 8.7610 8.7076 8.7495 8.7242	0.5645 0.5386 0.565x 0.5447 0.5536	7.6630 7.6766 7.6636 7.6759 7.6643	0n0672 9'9379 9n6165 9'3078 9'5577
бо1б бо17 бо18 бо19 бо20	1315 1316 1316 1316 1317	X III IV X III	24 22 17	2201 2201 2201 2202 2202	810 839 017	9 18 4	7.6	40°18g	-3'91 +0'96 -0'90 -3'85 +1'84	23.528 23.528 23.528	342 320 12 520	194.401	0'7231 0'5931 0'7020 0'7413 0'6911		8.7260 8.7561 8.7470 8.7085 8.7585		7.6750 7.6687 7.6653 7.6737 7.6700	9n7160 0n1736 0'0360 0n1019 9n9006
6021 6022 6023 6024 6025	1319	IX VIII VIII : VIII :	3 25 21	2202 2202 2202 2202 2203	519 695 874	18 81	29°3 12°8 55°2	171°245 350°751 160°559 339°912 150°204	-1.22 +2.65 -0.33 +3.36 +0.39	23'527 23'527 23'527	358 934 177 828	0,010	0.7356 0.7083 0.7137 0.7315 0.6939	9,7383 9,7383	8 · 7139 8 · 7410 8 · 7355 8 · 7179 8 · 7558	0'5639 0'5472 0'5480 0'5637 0'5352	7.6689 7.6714 7.6675 7.6727 7.6663	9.9908 829758 9.2902 9.8177 927362
6026 6027 6028 6029 6030	1320 1320 1320 1321	XII s	5 30 26	2203 2203 2203 2203 2203	375 405 552 730	17 1 8 6	33'9 19'5 51'1 34'8	140 · 029 287 · 232 101 · 700	+1.05 +0.65 +1.07 +0.66	23.526 23.526 23.526 23.525	165'124 194'881 349'951 173'864	195 741 347 747 176 276	0'7441 0'6980 0'6914 0'7276 0'7201	9'7631 9'7205 9'7319	8.7293	0.5354 0.5330 0.5639 0.5489	7.6740 7.6630 7.6651 7.6771 7.6627	0'1420 0'1055 0"0990 9"9673 9'7469
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037 038 039 040	1324 1324 1325 1325 1326	X IV	8 2 3 2 7 2 3 2	204 205 205 205	940 117 294 472	21 17 3 22 3 10 1	0.4 30.3 31.2 2.7	21.043	-3 90 -0 48 -3 54	23 521 23 522 23 521	168.606 349.841 177.181 357.385 185.631	351.952 175.458 357.940	0.7100 0.200 0.6020 0.441	9.7182 9.4182	8.7528 8.7528	0'5631 0'5369 0'5724	7.6652 7.6738 7.6664 7.6726 7.6676	0'0127 9n9743 9'3867 9n4011 9n6800
042 043 044 045	1327 1327 1327 \ 1327	III 2 III 1 IX 1	2 2 4 2 7 2 6 2	205 ( 205 ( 205 ( 206 (	797 827 973 903	14 2 1 5 16 4 4	7 · 8 7 · 8 0 · 5 · 3 4 · 7 · 1	10.690 51.574 80.377	+3'26 +1'05 +0'33 -1'97	23 521 23 521 23 521	194.038 342.394 12.778	10.360 10.360	0.7037	9.7359 9.7495 9.7459	8 7454	0.5524 0.5425 0.5431	7.6689 7.6664	9.6613 0.1731 0n0865 0n1861 0.0622
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0005	10/ 3/	-0'7060	9 7048	120.98	93 14	9.2401	9.9936	9.9721	922310	9'4804	9'9792	100.3	- -x13	- 33	+159		-139		
6005 6007	7'73	+0:1307	9'7019	297 '45	92.93	9.5429	9 9949	9.9718	9.1840	914967	9.9775	80.7	- 69	2	- 8	_ rr	+ 47	r6	7×#
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бобі	47°64	+0,4360	9'7400	109°88	92°42	9.5577	9.9971	9.9697	920522	9'5343	9'9730	97°1	-145	+ 50	- 45	+ 68	+ 40	+ 37	t#
6053	309,36	-1'2540	9.7064	68.38	86.43	9 6238	9'9954	9'9577	9'1552	9.5972	9,9631	84.5 81.0			ga mark				$p \\ p$
6055	297'42	+1.2282 +0.8224	9.7657	241'98	85.44	0.0330	9'9994	9.9528	9n2697	9,5720	9 9648	03.2	+ 36	- - бх	+ 67	+ 40	+116	+ 44	(⅓) t**
6056 6057	318'45 163'21	-0'4972 +0'2122	9.7076	57.56	84.79 84.05	9'6397	9.9895	9'954I	9.3356	9'5783	9'9664 0'0605	76.5	3	- 39 - 36	+ 45	9 8	+100	- 15 - 4	2° L#
6059	316.14	-0.2021	9 7293	221.66	83'29	9.0528	0.0421	9'9510 9'9491	9 4520 925096	9.5431	9'9718	72'4	- 90 - 25	I	— 30	- - 38	- <del> -</del> 49	+ 3 ² - 47	1:11
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6061 6062	330,15	-1.2427 -0.8390	9'7641	8.68	87.39	9'6857	9 9438	9'9418	9'6792	8.0210	9'9985	61.4	2	 84	+ 42	68	+103	- 28	$\frac{p}{t}$
6054	185'60	+1.0257 -0.1329 +0.2458	9.7444	1,14	. 89 ' 64	9 6882	9'9411	9'9411	9.6881	8.0473	0,0000	60.8	+112	- 37 - 43	+176	8 20		+ 22 - 15	
		+0'6244											i				+-114		
6067 6068	60'66 320'94	-0'4888 -1'3583	9.7629	345°28	93'98 94'18	9'6843 9'6833	9'9469 9'9479	9'942I	9n6677 9 6646	9°1167 9n1417	9'9962 9'9958	62.3	128	- 1		- 26		- 56	
6069	196'71	+1'3473	9.7560	134'97	96'47	9'6547	9'9795	9 95 95	9114777	9:5277	9 9738	108.6			, Lepondord potentials	******			p p
6071	77:22	-0.9320	9'724	311.25	96'23	9.6512	9 9825	9'9514	9'4444	925454	9'9715	72.7	+124	<b>— 69</b>	(+111)	(-82)	+ 26	- 47	2°
6073	219.72	-0.1316 -0.1361 -0.6331	9 '7509	301.35	95.05	9 6381	9,9903	9'9545	9'3202	925809	9'9659	76.8	+ 67	22	+141	34	-157	2	r-t
бо75	80'88	+0.4790	9'7655	290.63	93,39	9.6223	9.9960	9.9581	9,1333	975983	9 9629	81,2	-140	+ 18	- 83	- <del>-</del> 6	- 30		
6077	313,63	-0'8974 -1'1545	9.7578	279 0	91'44	9'6044	9.9992	9'9617	8.7636	9115999	9.9626	86'4	14-18941	- 51	118	- 41	86 	- 59 	$\frac{r}{p}$
6079	261'78	+1.0927 +0.3031	9'7192	234'0	86.43	9.2312	9,9919	9'9734	922826	924481	9.9822	TOI'5	13	59	( 87)	(84)	103		11
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6082	90,41	-0.2817 -0.4253 -0.4221	3 9 7658	38 38 6	5 86 . 85	9.2115	9.9862	9'9757	9'3942	9.3216	9'9902	75 3	I 48	39			25	- 10 + 9	t
5084	156.82	+1.5250 -1.1767	9 7366	350'7	3 90.97	9,4917	9'9787	9'9780	9'4854	817202	9 9994	72.2				_	_		$p \over p$
6086	358 41	+1.1122	9 735	193'8	88.60	9.4900	9 9795	9.9781	924769	8,8899	9.9987	107.5	-						$p_{}$
6088	59.80	+0.8666 -0.8266 +0.1721	9'765	3 145 '8	92.97	9.5078	3 919846	9.9762	914175	9 2736	9 9 9 9 2 2	105 4	-126	- 39	- 66	48	- 13	+ 75 - 68 + 24	$t_{}$
6ogo	311.00	-0.1062	9.760	133 5	193'3	9 5200	9 9 9 9 3 7	9 9747	923453	9, 3928	9.9863	103.3	18	+ 7	+ 47	+ 8	+107	- 19	
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6099	131,2	-0.4979	1 9.431	57.5	3 84 7	9 639	7 9 9895	9 954	9.3359	9 9 5 7 8 1	9 9664	76	<b>+166</b>	1	133	+ 35	59	+ 23	$r \cdot t^{::}$
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6	igi 139 ig2 139 ig3 139 ig4 139 ig5 139	2 III 2 IX 2 II	24 2 17 2	229 (	569 746 303 1	7 43 8 51 7 44	7 12 9 182 2 331	. 16; . 80; . 65;	3 +0° 2 -2° 9 +3°	94   23° 19   23° 67   23°	518 12 518 192 518 349	446	193 7	90 0.69	32 9 76 228 9 72	66 8 7	62 0.23	7 · 67 7 · 67 7 · 67 7 · 67 7 · 67 7 · 67 7 · 67 7 · 66	00 0n0 37 9n9
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0152	190,20	+1'4840 -1'0990 -0'9515	9.7629	174.24	91.75	9'6850	9.9429	9'9420	926821	8 7442	9.9993	118.8		_			_	p p
6154	234'36	+0.7934	9.7289	144'47	96.79	9.6669	9.9697	9'9473	9115582	9'4646	9'9807	112'2	+ 6 + 67	·F135	 7б 31		- 46 + 29 + 9	1.04s
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0157	344'53	+0.4694	9.7657	312.12	96'30	9.6524	9'9819	9'9511	9.4510	925431	9.9718	72'5	- 8 + 20 - 48 + 10	+ 12	+ 22 + 9 - 27	+ 63	- 16 + 42	l**
0159	215'05	+1.1537	9'7557	301.75	95'08	9'6376	9,0001	9'9547	9'3251	925788	9'9663	76.8		+ 47		+ 88	- 54 	$\frac{r}{p}$
6161		-1.4437																
6162	144'50	0.0030	9.2164	259 19	88'53	9'5714	9,9990	9'9675	8,8130	925647	9 9686	94'0 84'4	+ 66 - 66 -140 + 19				£8 + 29	$r$ $t^*$
6164	154'03	-0'302I	9'7020	246.75	87 '34	9'5497	9.9962	9'9708	921211	915172	9'9751	98.0		155	38	83 +100	- 25 8	r
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6167	192.67 241.40	-1.0210	9'7475 9'7382	220.32	86 · 64 86 · 79	9 * 5301 9 * 5136	9.9868	9'9735	9'3102 9:3852	9'4320 9≈3384	9'9835	77'8				- -		$p \\ p$
6169	108.03	+0'9484 0'9247	0,2001	3.00	89.29	9.4861	9.9787	9'9786	9'4849	8 ' 3496	9 ' 99 99 9	72.2	+x69 H- 54			十 33 十 1 1 0	+ 89 85	1:4
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6173	134.36	-0'2212 -0'4793	9.7211 9.7286	336 51 356 51	92.03	9'4939 9'4946	9.9812 9.9812	9'9777 9'9777	914612 9'4533	9 ° 0665 9n x x 36	9 ' 99 70 9 ' 99 63	106,0	+110 4		- 7	-125	- 29 12	lili
6174	14.82	+0:5404 -1:1540	9'7347	145'50	92'91	9.5057	9'9845	9.9764	914193	9'2637	9'9925	105 5 74 9	93 + 47				<u>1</u> 7	1-t* P
6176	237.25	-1.2143	9.7045	101:62	91.28	9.2211	9.9990	9 ' 9676	818440	9 ' 5633	g · g688	94'3					_	$ _{p}$
6177 6178	99'90 333'54	+1,3403 +0,8838	9'7105 9'7652	134'07 277'11	01.01 03.32	9·5223 9·5781	9 • 9887 9 • 9996	9'9744 9'9664	923510 8:5376	9'3907 9n5752	919864 919669	103 4 87 3		+ 25	 + 40	- + 66	- 57	$p_{t^*}$
6179	249'63	0'7535 0'2254	9.2106	89 • 65	89'95	9.2900	0,0000	9'9643	7:3397	9 5900	9'9643	80 . 0	+ 64 - 44 +110 14		26 10	+157	44	r-th
6181	339.21	0'0467	9'7347	78'49	88'15	9.6080	9.9988	9.9610	8 · 8703	9 · 6006	9.9624	85 ' 4	- 41 - 2	- <del>-</del> 20 -	- 26	- - 85	+ 7	リー七米
6183	327.82 175.29	-0.4888 0.4888	9 7223	253'54 68'19	87'31 86'42	9.6158 9.6158	9 9975	9'9594 9'9578	9:1569 9:1569	9≈6006 9:5969	9'9624 9'9632	81.0	- 42 - 21 + 89 + 40	+ 3r	- 53	+114	- 33	1'
6184 6185	355°30 324°66	-1.2047 -1.0078	9'7620	33°24	85 47 83 31	9.6683 9.6683	9.9672 9.9622	9 ' 9558 9 ' 9468	9n2660 9'5733	925884 9'4430	9 9647 9 9826	67.1	(+ 86) (-67)	_	_	 96	 - 57	$p \atop (t)$
6186	70.57	+1'5040	9 7665	58.78	85.00	9.6363	9.0002	9 9549	9,3141	9'5796	9,9661	77.0			_			p
6187 6188	88 48 173 66	+1'1182 -0'2893	9'7185 9'7401	205.73 24.84	83'88 83'95	9'6753 9'6774	9 <b>·9</b> 589 9 <b>·9</b> 576	9 19449 9 19443	916185 9'6243	9n3566 9'3455	9°9885 9°9891	64'4	+134 - 41	-170	6	-108	g	p r-t
6190	279.91	0'3556 0'4813	9 7459 9 7139	16.24	85°23 85°34	9.6833 9.6834	9 <b>· 950</b> 0 9 <b>· 949</b> 3	9 ' 9428 9 ' 9425	9n6565	9n2073 9 1948	9'9943 9'9946	62.5	+ 94 + 47 + 15 + 1		+ 14 + 42	-146 +158		
біді	67:39	o'358g	9.7644	189.21	87:14	g <b>·686</b> 3	9 * 9439	9'9416	9n6785	829609	9 9982		_r33 <del> -</del> 8	- 72	- 29	+ 5	- 49	t
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6195	341,30	+0'8656	9'7272	153 05	95 40 96 29	9 6752	9.0000 9.0000	9 9438 9 9449	9 0419 9n6128	912775 913741	9 9921	03'5	(+ 53) (-74) -127 + 75	+ 30	+ 86	+104	- 48 + 34	- 14
6196	246 17	-0'2221	9'7545	330 81	96 49	9 6733	9 ' 9625	9 9454	o.0000	924017	9 9857	65 . 7	+ 39 - 36	- <del> </del> -116	- 29	- -175		
6198	115'74	+0.4603	9'7659	321'96	96'79	9 6642	9'9724	9'9481	9'5392	914846	9'9788	68:7	-109 + 28 +179 + 6	120	- 12	- 68	- 15 + 46	$t^*$
6200	45 49 345 39	-0.6370 -1.1212	9'7548	312.31	96.26	9.6211 9.0207	9.9820	9 9499 9 9514	914504	9 5285 9n5414	9 9737	72 5	-105 - 20	— 52 —	- 23 -	7	- 53 -	p
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6306 6307 6308 6309 6310	1443 XI 21 1444 V 17 1444 XI 10	2248 616 21 14	8 248 003 0 65 333 9 236 984	-2.61 -1.02 -3.45	23.209 23.209	354·486 175·372	16.066 165.296 356.923 173.168 4.297	0'6913 0'7279 0'7189 0'7042 0'7390	9.7203 9.7335 9.7475	8·7585 8·7218 8·7307 8·7452 8·7107	0'5475	7.6627 7.6767 7.6635 7.6760 7.6643	0'1116 0'0624 926995 9'6089 9'4374
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6331 6332 6333 6334 6335	1455 IV 16 1455 X 11 1456 IV 5 1456 IX 29	2252 602 23 33.	34 975 2 206 350 2 24 213	-0.05 -3.74 +0.02	23.504 23.504	175'222 355'675 183'283	347 773 174 211 357 737 180 953 6 181	0'7424	9'7045	8 · 7081 8 · 7489 8 · 7249	0.2667	7.6662	ono198 9:6608 9:5764 9:4807 9:5494
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370	271'93	+1.2743 g	7141	67.21 8 97.80 9	7 35 9	5521 g	9963 9	9704 g	1148 g 16975 9	,6007 9 5210 9 5989 9	9624 9746 9627	84'9 82'1 93'1	- 177	35 - 16	+ 59	150 +	48 56 1
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6665	12'0	2 +	9427	9.7017	287.08	93.02	9.6163 9.6238	9'9954 9'9973	9 9578 9 9594	9 1635 9 0467	9°5961 9°5999	9 '9633 9 '9626		+ 76 - 53	18 55	+133 - 15	6	-175 + 7	- 35	t
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5741	1633	X 3 III 29	23	17 7	77	6	1'2	190'	215	-2.7	7 3	3 486	187 544	358.691		9 7219	8.7277	0.5537	7 6584	0,0001
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6756 6757 6758 6759 6760	1640 XI 24 1640 XI 13	2320 198 20 36	5 242'570 50'161 231'840	-1.03 -3.12	23.483 23.481 23.481	352'795 180'015 0'759	174.085 350.802 181.093 0.708 187.020	0'7417 0'6892	9.7518 9.7055	8'7252 8'7497 8'7086 8'7612 8'7071	0'5516 0'5451 0'5648 0'5379 0'5664	7.6761	9.8793 9n7966 7n1575 8.8092 9n8778
6761 6762 6763 6764 6765	1641 XI 3 1642 III 30 1642 IV 29 1642 IX 24 1642 X 23	2320 877 12 14 5 2320 907 0 44 6	38.655	+1'13 -0'74 -2'02	23'480 23'480 23'480	165'566 195'958 345'888	10.696 163.128 193.686 347.831 19.249	0'7271	9'7535 9'7372 9'7235 9'7150 9'7282	8.7509 8.7351 8.7229 8.7167 8.7279	0'5430 0'5500 0'5558 0'5624 0'5570	7.6697	g'8802 0'1095 0n1643 0n186 0'1830
6766 6767 6768 6769 6770		2321 409 3 52 2 2321 586 18 4 9 2321 763 4 45 8	359 · 288 170 · 066 348 · 798 159 · 158 338 · 172	-1'07 +2'74 -0'14	23'480 23'480 23'480	353'636 182'048 1'395	172.433 353.880 182.762 359.780 192.493	o'6943 o'7448 o'6908 o'7373 o'7071	9.7593 9.7010 9.7627 9.7108 9.7449	8.7597 8.7131	o'5380 o'5697 o'5369 o'5633 o'5476	7.6709 7.6680 7.6723 7.6667 7.6735	9.7199 9.17873 9.2418 9.1215 9.19533
6771 6772 6773 6774 6775	1645 VIII 21 1646 I 16 1646 VII 12 1647 I 5 1647 VII 2	2322 265 23 43 6	297 · 113 110 · 228 285 · 633	+2'71 +1'22 +1'62	23.481 23.481	165°304 348°629 173°418	7.280 167.649 348.225 172.847 358.977	o'7158 o'7395 o'6905 o'7436 o'6969	9.7367 9.7057 9.7643 9.7005 9.7576	8.2108	0.5480 0.5722 0.5311 0.5754 0.5346	7.6656 7.6769 7.6629 7.6772 7.6627	9'9407 0'1118 9"9833 9'8006 9"3653
6776 6777 6778 6779 6780	1647 XII 26 1648 VI 21 1648 XII 14 1649 V 11 1649 VI 10	2323 152 0 48	263.153	+0.33 -1.02	23.482	6.072 188.577 344.467	186 · 321 345 · 029	0'7184 0'7051 0'7440	9.7188 9.7341 9.7461 9.7025 9.7094		o'5650 o'5478 o'5489 o'5671 o'5619	7.6773 7.6630 7.6630	8n8413 9'7407 9n8765 0n1697 0'1361
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6811 6812 6813 6814 6815	1661 1661 1662 1662	III 36 IX 23 III 26 IX 13	0 2 2 2 2	327 327 328	172	9 10 2	54': 23'(	3 18 5 35	0 127 0 780 9 708	7 -1	00	23 .	478 478 477	173'438 353'051 181'681	18 95 172 09 353 186 182 509 359 049	0'	5936 7448	9'7601 9'7006 9'7621	8.7566 8.7058	0.5369 0.5365	7.6741 7.6697 7.6692 7.6710 7.6679	9'7494'
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6807 6808 6809	36'06 122'22 295'24	-0.6766 +0.7442 +1.3287 -1.3920 -1.3607	9'7545 9'7408 9'7272	242 '49 25 '03 58 '99	87 · 04 87 · 59 86 · 87	9.5446 9.5013 9.5395	9 9949 9 9817 9 9935	9 9716 9 9770 9 9722	9,1864 9,4542 9,2308	9:1465 9:1465 9:4796	9 9773 9 9957 9 9793	99°3 73°3 79°7	82  		-1-127 - 33 	23 31	+178 + 22 	- 33 + 36	
6812 6813 6814	327'71 347'58 213'59	+1.5060 +0.5616 -0.6688 -0.1434 +0.0714	9 7622 9 7028 9 7642	12 50 180 97 359 64	88.73 89.90 90.04	9'4894 9'4839 9'4856	9'9794 9'9788 9'9787	9'9782 9'9788 9'9787	9'4779 9"4838 9'4856	8 · 8454 7 · 7343 7 · 3076	9 9989 o oooo	72.5	- 37 - 56 + 82	24 26	- 6 - 148	g	+ 81 149	6o 10	P P
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6837 6838 6839	340 · 11 306 · 07 170 · 95	-1 · 1887 +1 · 4070 -1 · 3652 -1 · 4963 -0 · 5204	9.7660 9.7208 9.7092	14.28	85 · 99 93 · 96 87 · 88	9 · 6805 9 · 6814 9 · 6853	9 · 9483 9 · 9432	9'9433 9'9433 9'9419	9 6629 9 6644 9 9 681	9 1255 9 1191 0 818290	9 9961 9 9961	62.3 117.8 118.7		58		- 44		- - - - 3	p p p p
6842 6843 6844	128·74 314·86 126·64	+0.5576 +0.1971 -0.1961 +0.8992	9.7651 9.7651	328'2	95 78 96 52 96 67	9 · 6793 9 · 6721 9 · 6709	9'9553 9'9633 9'9654	9 9432 9 9452 9 9462	9 6340 7 9 5 5 5 5 5 5 6 5 6 6 6 6 6 6 6 6 6 6 6	5 9 1 3 1 4 2 5 9 1 4 0 8 5 9 9 1 4 3 9 1	9'9906 9'9852 9'9837	63 °9	+167 23 +169	- 14 12 39	-132 + 43 -138	+ 1 + 2 + 63	— 76 +100 —131	+ 37 - 34 + 74	t rii
6847 6848 6849	136 61 265 68 66 93	1 — 1 · 3773 1 + 1 · 5447 3 + 0 · 9202 3 — 0 · 6350 5 + 0 · 1658	9 7 1 6 5 9 7 2 6 9 9 7 7 5 5	318'4 105'50 278'54	96 65 92 53 191 3	9 6587 9 6137 9 6026	9 9 9 7 6 1 9 9 9 9 7 7 9 9 9 9 9 3	9 949 9 959 9 962	9 · 5 0 8 · 9 · 9 · 9 · 9 · 9 · 9 · 9 · 9 · 9 ·	8 9 <i>n</i> 5075 7 9 6001 4 9 <i>n</i> 5986	9 9763 9 9623 5 9 9628	70° 96°: 86°:	3 - 38 5 - 157	39	- 66	- 6g	4 I I	- 33	3 t
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6876 6877 6878 6879 6880	1687 1687 1688 1688	XI 15 V 11 XI 5 IV 30 X 24	23 23 23 23	37 1 37 3 37 5 37 7 37 8	55 33 10 87	5 2 2 6 5	3.4 4.0 7.0	223 40 211	.000 .515 .796	4 0 3	'02 '81 '92	23 23 23 23	476	3 3 1 5	59'102 7'709 38'031	3:	56.657 82.576 6.061 88.481	0 0	7070 7176 7306 6959 7438	9'7443 9'7345 9'7172 9'7577 9'7007	1	0.5488 0.5640 0.5362 0.5729	7.6650 7.6742 7.6660 7.6730	9'8173 8n9107 8n6787 9'8213 9n8868
6882 6883 6884 6885	1689 1689 1689 1690	111 10	23 23 23 23	38 2 38 2 38 3	64 I III I 41 89 2	8 5 5 2 6 5 2 5	2 · 4 3 · 3 6 · 9 0 · 3	30 171 200 350	.383 .201 .830	-1 ·	46 59	23 23 23	'479 '479 '479	16 19 35	5'464 5'464 3'908	16 19 35	2.458 4.011 6.338	0 0 0	7293	9.7582 9.7639 9.7203 9.7080 9.7346	8.7543 8.7595 8.7201 8.7111 8.7331	0.2332	7.6681	0n0876 0'1335 0'1518 0n1623 9n7400
6887 6888 6889 6890	1692 1692	IX 3 II 28 VIII 23 II 17 VIII 12	233 233 233 233	18 56 18 74 18 92 19 09	14 20 1 28 75	6 4 4 3 9 4	6·6 8·4 9·7	150 328 140	577 564 428	+3;	23 50 63 07	23 23 23	478 478 477 477	18	1'555 9'160 9'160	18	0'755 3'338 0'940 8'798 1'612	0 0	7375 6907 7443 6951	9'7470 9'7087 9'7035 9'7001	8.7433 8.7121 8.7588 8.7059 8.7542	0.5329	7.6734 7.6657 7.6746	9'7894 9'2362 9n1221 9'9440 9n9376
	1693 1694	I 6 II 5 VII 3 XII 27 VI 22	233 233 233	9 60 9 77 9 95	7 1	2 23 1 ! 5 6	3 · 2 5 · 1 5 · 5	102 · 276 · 91 ·	042 133 474	+o +o -	89 48 33	23 · 23 ·	476 476 476 476	16 35 17	9,112	17	2'291 4'527 1'341 0'816 8'117	0.	7317 7278 6972	9 ' 7297 9 ' 7157 9 ' 7232 9 ' 7549 9 ' 7037	8.7295 8.7178 8.7219 8.7525 8.7067	0'5657	7.6772 7.6756 7.6627 7.6773 7.6627	0n1391 0'1844 0'0018 9n8045 9'4035
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6851	297°бо	+0.0423	9'7657	267°16	89°58	gʻ5839	0,0000	9 ' 9654	8n 2448	925835	9 9655	9101		- - 3	+ 62	20	+126	+ 1	· /#
0852	334'18	0.2348	9.7074	83.12	89'03	9.5769	9'9997	9.9667	8 6208	9'5742	9 967x	87.4	- 24	- 36	+ 27 -162	- 14	+ 78	- 31 + 39	r
0854	230.79	-1.3184 -1.3223	9.7425	37.73	86,83	9'5140	9'9857	9'9755	9'4026	9.3157	9'9905	75'0				-		~	p
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6857	318.33	-1.4007 +1.4923	9.7269	242.28	87'00	9 5464	9'9947	9 9713	QuIQII	02/4003	0.0772	00.4			graning -			entered to	$\frac{p}{p}$
6859	96.31	-0.2122	9 7630 9 7026	25'65 194'37	87.59 88.57	9'4979 9'4875	9'9822 9'9800	9 9773 9 9785	9'4484	9,1525	9.9955	73.5	161 168	+ 21 - 28	93 103	+ 47 53	• .	+ 53 - 63	l:li
6860	337 10	o.1028	9.7640	13.06	88.69	9 4885	9.9796	9.9783	9'4759	8.8629	9.9988	72'5	- 40		+ 24				
6861	108.26	+0'0176	9.7152	180.65	89 93	9 4838	9 ' 9788	9 ' 9788	9114838	715532	0,0000	107.7	-169					- 17	
0803	219.30	-0.8464 -0.7518	9'7416	167.41	91.27	9 4885	9 9795	9 * 9783	924768	8.8473	0,0080	107'5	-I- 6o	76 + <b>6</b> 6	+175 +147	63 + 56	116 145	+ 31	
6865	319,15	-1.1012	9.4666	310.42	93.32	9'5393	9'9901	9 ' 9742 9 ' 9723	9:3235 9:2385	9:4140 9:4768	9'9848 9'9796	77 4 100 5						_	$\frac{p}{p}$
6866	70.60	+1'4290	9.7628	155.00	92'40	9'5007	9.0817	9:9770	024537	0.1454	010057	106.2							p
0807	44'24	+0'6510 -0'3821	9.7038	297'31	92'92	9.5428	9'9950	9'9719'	0.1810	924971	9.9775	80.8	IOI		47			+ 47	
0809	77.24	-0.0582 -0.3946	9.7238	284.54	ðr,88	9.5641	9 ' 9984	9 9687	8 9344	925517	9.9705	84'7	142	8	+ 148 77	24	16		7:4
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6872	120'89	-0'7417 -1'2047	9'7094	87.20	89:57	9 5935	9 9999	9.9637	8.2454	9.2031	0 0638	88.0	+ 45	- 44	- -141	70 	- 125	- 42	r-t P
6873 6874	80'16	-1.3727	9'7643 9'7655	231 '51 261 '47	84'11	9'6459 9'6028	9'9851	9 · 9526	924097 8273 <b>6</b> 7	925567 925988	g'9698 g'9627	106.0 93.4			# Propert				$\stackrel{\cdot}{p}$
6875	276'41	-0.8780	9'7120	48.17	83.75	9.6512	9.9823	9 ' 95 14	9'4470	9 5437	9,8212		- - 68 -	67	92	46	+141	4x	
6876	139.91	+0.6566	9'7464	221'54	83.31	9.6596	9.9760	9492	925100	915082	9 9762	110.0	179	+ 56	133	26	77	+ 20	1-1*
0878	204 74	0'0814	9`7194 :	212'19	83.31	9'6705	9.9659	0.0463	au 58141	0 » 4 3 4 T	0.0834	T T 2 ' 2	-l- 40	-l- 20	L OF	- TO	1.754	- 15 - 25	1*
6880	285.88	+0.6627	9.7598	30,30	84.16	9.6785	9,8200 9,8030	9 9480	9.5924 9.6318	9'4129 9n3220	9 9849	110,0 20,1	十 75 2	+ 17 24	+142 + 63	71		+ 61 72	$i_{i_{i_{i}}}$
6881	330'00	-1'2235	9.7602	1.05	80.68	a·6856	9'9418	0.0418	0.6855	8.0055	o topón	fr'o			, <u></u> ,				. 40
б882	100,10	+1.3600 +1.4183	9'7658	22'40	84'41	9 6757	919558	9447	o • 6326l	0.3030	0,0010	64.0		****		_			p = p
0884	283'53	-1·4530 -0·5495	9'7101	194'93	85.79	9.6824	9 * 9483	9.9428	92663xl	921464	0'0057	エエク・ク					_		p
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0007	240 42	+0.1723	9.7109	345 49	94.10	9'0847	9 ' 9473	9'9421	0.65651	021374	0'0050	62 T	+ 50	тЯ	-I-YYY	-l- 0	-L- T 60	27	$r^{\mu}$
6889	243'34	-0 1325 -0 8790	9'7050	336'98	95 54 95 80	9.6788 9.6788	9 9543   9 9557	9.9438	926391 916331	g'2916 g ₂ 3176	0.0004	63.0	-139	+ 18	- 72	+ 3	14	22	
6890	324.17	-o · 8662	9,4610	150.37	96'46	9.6709	9.9634	9 9 9 6 1	9n5956	9 4044	9 9855	114.0	- 31	- 35	+ 25	- 57	+ 45	- 74	t
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6893	7.70	+1'5290	9'7253	116.10	94 25	9 6295	9 9934	9 * 9564	92372	9 5906	0.0642	100.8	_			_		_	p p
6895	62.05	-0.6376 +0.2532	9 7570 9 7059	290.14 102.20	93'29 92'55	9 6206 9 6140	9 9961 9 9977	9 · 9584 9 · 9598	9°1205 9n0088	9n5978 9 ' 6002	g g630 g g630	81.7 95.4	+ 69 -132	43 19	+165 61	- <b>6</b> 3 + <b>3</b> 8	-114 + 3	29 + 8	t 1°*
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6906 6907 6908 6909 6910	1699 1699 1700	X 4 III 31 IX 23 II 18 VIII 14	2341 6 2341 8 2342 6	597 373 521	8 57.8 10 23.4 23 34.1	191'315 10'875 180'564 330'416 141'724	+1'05 +1'05 +3'58	23.472 23.472 23.472	7.866 165.831	357 825 191 491 5 473 166 888 346 209	0'7341 0'7114 0'7115 0'7416 0'6901	9'7141 9'7411 9'7409 9'7039 9'7647	8 · 7386 8 · 7090	0'5637 0'5477 0'5476 0'5720 0'5318	7.6706 7.6697 7.6692 7.6745 7.6647	8n4638 9n9088 9*8457 0*1283 0n0667
6911 6912 6913 6914 6915	1701	11 7	2342 5	375 553 730	9 27.6 1 38.5	170'140 319'050 131'593 307'770 121'323	+3.68 -1.1.38 -1.3.37	23 472 23 473 23 473	354 778 180 541	172°176 356°738 178°258	0'7426	9'7615 9'7023 9'7539 9'7232 9'7288	8 7080 8 7495 8 7241	0'5372	7.6679 7.6755 7.6640 7.6763 7.6633	0'13E7 9'8230 9'6570 8'6984 9'5019
6916 6917 6918 6919 6920	1703 1703 1704	VII 14 XII 8 I 7 VI 2	2343 4 2343 4 2343 4	262 109 139	2 50°2 15 29°4	296.760 110.791 255.928 285.943 71.846	+1 · 26 -1 · 93 +1 · 62	23.474 23.475 23.475	11.801 164.467 196.335	165 410 196 049	0'7019 0'7412 0'6906 0'6890	9'7499 9'7063 9'7619 9'7636 9'7111	8 · 7478 8 · 7088 8 · 7592 8 · 7611 8 · 7123		7.6769 7.6629 7.6767 7.6772 7.6634	9n8667 0 0498 0 1164 0n1361 9n9804
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	1710	III 11 IX 4 II 28 VIII 24	2345 5 2345 6 2345 8	329 506 583 360	0 34'0 12 18'1 17 26'0	350 795 161 202 339 564 150 997	+2'50 -0'28 +3'24 +0'49	23 476 23 476 23 476	1.477 180.866 8.883	180'388	0,2384	9'7638 9'7638	8.7112	0.5683 0.5332 0.5733	7.6723 7.6667 7.6735	9'1474
	1711 1711 1712 1712	I 18 II 17 VII 15 I 8 VII 3	2346 0 2346 1 2346 3 2346 5	85 62 39	13 47 4 19 10 6 9 52 8 22 30 9	298.296 328.331 112.468 287.344 101.880	+1.30 +1.30 +0.90	23'475 23'475 23'475 23'473	16.370 168.229 352.569	342 · 215 14 · 283 170 · 402 350 · 847 177 · 084	0'7185 0'7306 0'7290 0'6963 0'7438	9'7313 9'7172 9'7214 9'7558 9'7030	8 · 7307 8 · 7189 8 · 7205 8 · 7534 8 · 7062	0'5574 0'5643 0'5550 0'5435 0'5654	7.6768 7.6746 7.6629 7.6772 7.6627	0n1395 0'1786 0'0365 9n8059 9'5344
6941 6942 6943 6944 6945	1713	XII 28 VI 22 XII 17 V 13 VI 12	2347 c 2347 c 2347 2 2347 2	93	23 21'4 16 12'6 18 25'2 4 53'5	91'200 265'713 52'487 80'695	+0'33 -0'82 -1'04 -0'25	23 473 23 472 23 472 23 471	8°311 163°073 192°804		0.7030	9'7634 9'7072 9'7487 9'7439 9'7304	8.7610 8.7095 8.7466 8.7402 8.7282	0'5392 0'5630 0'5474 0'5435 0'5500	7.6773 7.6627 7.6771 7.6649 7.6630	8.5573 gn6259 g.8609 g.1717 on0651
6946 6947 6948 6949 6950	1714 1715 1715	XI 7 XII 7 V 3 X 27 IV 22	2347 4	26 73 750	1 44'3 9 30'7 8 54'0	224 609 254 671 42 244 213 338 32 023	-2.08 -0.86 -3.98	23 47 x 23 47 x 23 47 x	16'181 171'665 351'751 180'126	170.666	0'7268 0'6920 9'7446	9.7093 9.7220 9.7624 9.7002 9.7608	8 · 7 · 3 · 0 8 · 7 · 2 3 · 1 8 · 7 · 5 8 · 0 8 · 7 · 7 · 6 · 9 8 · 7 · 7 · 6 · 9	o'5686 o'5629 o'5336 o'5732 o'5352	7 6743 7 6767 7 6659 7 6731 7 6671	0n1648 0'1699 9'8511 9n8991 8n0337
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6912	162'57	+1.3763	9'7045	310.12	93.29	9.5232	9 9904	9'9743	9'3174	924157	9.9846	77'0	+138	+ 28	-167 + 36	+ 28 - 10	-115 + 92	+ 51 - 35	p 1:#
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6927	218'12	-1.2645 -1.3065	9.7657	30.87	83.50	9.6686	9 9 5 4 9	9.9467	9.2869	9.4167	9.9846	66 4		_	******	_	\$100,00 <b>1</b>	_	$p \\ p$
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6951	335°60 68'65	-0'7670	9.7173	207°39	87°50	9'4967	9.9828	9'9775	924401	9n1770	9'9951	106°2	- 35 - 733	+ 12 - 65			+ 89	- 20	1.
6953	95'09	+0.6243	9'7445	194.02	88.59	9'4889	9'9798	9'9784	9n4744	8n8949	9.9987	107.4	-×57			- 45 - 39			r-t#
6955	178.91	+1.3212 -1.2650	9 7035	13.33	88.63	9 4953	9.979I	9 9777	9 4502	8.8773	9.9988	73.3	_	_	_			_	(p)
6956	130,18	-1.5260	9.7665	146 36	92'95	9.2078	9 ' 9844	9 ' 9762	9n4206	9'2674	9.9924	105.5	_	_				_	p
6957	310.39	+1:3290 +0:6843	9.7640	181.00	89.88	9'4900	9.9782	9 9782	924899	727904	0,0000	108.0	<u> </u>	_ + 28	+ 75	+ 34	 131	- + 56	$p_{\perp}$
6959	74. 17	-0.5232 -0.0383	9'7546	133,06	93,30	9,2192	9.9890	9'9749	9n3475	9.3884	9 9866	103.3	-137	- 18	- 77	x8	- 20	- 43	t
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ნენ2	118.10	+0 2422 -0 7278	9.753x	297.52	92.94	9'5436	9'9949	9.6118	9'1858	92497I	9'9775	80.4	十145	+ 23 - 52	+113 -115	+ 32 - 66		+ 3 - 35	
6964	188.21	+1.3140	9'7632	253'44	87.31	9.6121	9'9975	9 9596	9110324	925997	9'9626	96.4			_				$p \\ p$
6965	344'01	I . 3630	9.7657	285'85	92'04	9.2641	9.9981	9.9687	8.9210	915495	9.9709	84.3	_	*****	*****		_		p
6966	115.47	-1.0354 -0.6800	9.7146	68.31	86.45	9 6228	9'9955	9 . 9580	9°1538	9.5962	9.9633	81.1							$p_{_{\rm off}}$
6968	227.02	-0'2244	9'7401	57.9I	84.87	9.6382	9 9898	9 9545	9.3299	9.2480	9'9664	76.6	+ 80	- 24	+134	+- g	-163	. 0	$t^{: : : }$
6970	78.57	+0.2322	9,4619	48'40	83.78	9 6508	9.9825	9 9523	9.4444	9.5447	9.3034	72.7	-152	+ 14	- 83	+ 54	+ 12	- 16 + 45	
697i	155 '96	-o'7198	7019	221'26	83'28	9 6605	9756	9.9489	925129	925072	9'9763	110.1	+126	- 24	-164	6g	5I	— бо	,
6972	213'02	-1 3125 c	7584	16,83	85 40	9 6803	9.9502	9 9434	9.6559	0.1931	9.9946	62.7		_				_	$p \\ p$
6974	282 92	+1 ·5027 6	7246	189 ' 37	87.25	9 6825	9450	9 9428	916750	829496	9.9983	118.4							p p
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0977	75'13	-0'6303 g	9.75I2	181 62	80.20	g ' 686g g	9'9415	9.9412	926860	8n 1958	9'9999	110,0	143	+ 74	- 65	54	- 4	+ x6	t**
69793	308.10	+0.1012 c	7662	174'19	91'78	9 6866	9423	9 9414	9116837	8.7496	9'9993'	118.0	- 14	28	52	2	+114	30	total
6980	112.34	+0.8180	7033	353'2x	92.08	9'6874	9125	9*9413	9.6834	828176	9.8881	QI.I	十177	+ 26	126	+ 65	7I	- <del> -</del> 83	342/2
6981 I	95 . 33	-0.7475	7589	166 68	93.81	9 6828	9.9471	9 9 4 2 7	916676	9.0990	9 9966	118.0	+ 95	20	+154	5 ¹	-150	- 75	
6983	:38 73	-1.3830 c	7207 3	345 00	94.51	9'68rg	9 ' 9484 !	9 9428	9.6624	921476	9'9956	62'3					*******		$\begin{vmatrix} p \\ p \end{vmatrix}$
6985	26.86	+1.1702 g	3.4321	135.03	95.38	9 6754	9.0248	9.9502	924841 926367	9.5243	9'9742	116.5				-			p
6986	98:70	-o 6430 <u>c</u>	7588	311.72	96.33	0.6507	9.0824	9.9515	9 4456	9254.30	0.0212	72.7	- -16a	- 52	04	<b>6</b> 9	- 20	21	t
6987	353'77	+0.4309 c	7047	126 21	95.67	0 6442	9868	9530	923839	9.5664	9 9683	102.1	+ 25	+ 37	+110	48	+·173	+ ro	1.15
6989	265 ' 90	-0'3353 g	7104	115.00	94 23 9	9.6295	9935	9.9564	922339	9'5912	9,0641	100.4	+ 35	8	+ 92	- <del> </del> - 3	+x44	28	2.242
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6993	327 68	+1 ·4757 9	7224	279'10	91'45	9.6037	9.9992	9.0618	8.7656	925991	9.9627	86 4		39	 84	+ 70	+ 2I	— + 55	$p_{\perp}$
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6998	183'57	-0.4144 c	7404	39:34	86 83	9.2120	9 9865	9'9757	9.3903	9:3282	9,9899	75'4	+126	58	-178	- 36	-120	- 19 - 30	r'-t
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7053	101'30	+0.1019	9.7257	146'64	92.87	0.5030	g'g846 a'a855	9:9768 9:9762	914175	9,2592	9.9913	75.0	-167 -105	58	- 10	58	63	9 29	t
7055	153'44	+0.8820	9'7057	x33'95	93.59	9.2180	9.9890	9'9749	923469	9.3879	9 9866	103.3	- - 88	+ 70	- ×47	+ 79	— ба	+ 47	3.58
7056	91.71	+1:3247 -1:3473	9.7622	277:33	91'04	9:5774	9.9996 9.9996	g • g666	8 · 6505	925743	9,9671	87·2			<u> </u>		_		$p \\ p$
7058	313.60	+0.6031	9.7173	90.26	90.04	9.2886	0.0000	9'9646	722055	9.2886	9 9646	30,1		 + 41	- + 71	+ 21	+121	 - - 38	$p_{_{_{\mathbf{J}}}}$
7060	79 9	-0.3765	9'7435	78.84	88.23	9.6064	9.9989	0.0613	8.8508	9.2996	9 9626	85.6	134		- 79	+ 1		16	t**
706x	28.27	+0.0042	9'7140	253.20	87:26	9.6155	9'9974	9 9595	920390	925997	9.9626		86				+ 35 +138	- 6 + 29	rii: tili
7063	30'73	+0.3885 -0.6892	9.7016	241'74	85 41	9 6330	9.9922	9'9557	922731	925871	9'9649	101.4	14 113	+ 13 29	II .	1 -	+ 67		3.
7064 7065	86.36 201.3	-1.4267 -1.1102	9 7504	28.82 33.62	83.32	0.6328	9.9902	9 9475 9 9550	9 3144	9.4449	9.8eez	27.1 62.3		_	_				$\stackrel{p}{p}$
7066	159.0	+x ·5580	9.7274	205.03	83 <b>·</b> 96	9.6723	9.9596	9 9457	9n6147	923558	9 9885	112.0		-	_	_		_	(p)
7068	266'3	-x ·3460	9.7311	25'04	83.02	9.6763	919580	<b>'9</b> *9446	9'6224	9:3473	9,8800	04.5	1- 59	- 69	+103		+x60	_ 22	
7060	318'00	+0.0001	9.7538	197'46	85 25	9.6806	9.9506	9 9434	926544	922088	9'9943	1117.5	+ 7	H 75	+ 52 + 25	+ 52	+ 90	+ 24	. a. I
7071	TO 2 * 77	- - - - - - - - - - - - - - - - - - -	0.7663	180 · 67	87.11	0.6856	0'0443	0.0418	926775	820673	0.0081	118.2	- <del> -</del> 105	- - 32	+168	- I	126	25	t#1
7072	333 6	0.7298 0.6504	9.7047	8.71	87:36	9 6867	9'9435	9'9415	9.6803	8'9242	9.9985	61.3	<b>- 45</b>	18	+ 14	- - 61	II :	+ 75 - 70	. 1
7074	168.47	-1'4022 -1'4130	9'7379	339'06	95'34	9'6764	9'9544	9 9446	0.6388	9n2769	9'9921	03:7	_	_	_			_	p
		+r · 3267				:								_					p
7077	240.60	-1,4383 -0,6292	0.7315	174 59	91'62	9.6832	9.9433	9'9425	926807	8 • 7 ፣ 4 3	9'9994	1118.4			 9	 61	 + 76	 16	2)
7070	87'08	+0.6014	9.7039	144 66	96 78	9.6670	9'9693	9'9472	9 2 5 5 9 5	9'4630	19.800	113.3	180	- - 55	;∥ — 81	+ 57	- 17	1	$r^{*}$
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7082	89.7	-0.1636 +0.7202	9.7471	312.30	96 . 28	9.6515	g g8x8	9'95 x3	9 4523	925406	9.9721	72'4	- 150 ·	27	7 - 96	29	- 53	+ 57	11.
7084	317'2	3 -0.0182 3 -0.0182	3 9 ' 7 0 8 3	271 '01	90'15	9.5904	0000	9 9 6 4 3	7.7995	925903	9'9643	80.6	—	- 47	+149	50	+167 		p
		4733		1	,								1		_				p
7087	307.5	+0.9032 6-0.8558	39.7029	258 . 83	88'49	g 5696	9,9991	9.9679	8256	925624	9 9690	94'	49	- 49	9 + 5¤	81	+163	- 56	1"
7088 7080	203'6 331'8	7 -0'1749	9.7504	75.70	88 14	9 5648	9.9984	9 9685	8'9278 9n1299	9.5529	9 9793 9 9755	98 2	+ 90 - 34	-1- :	5 +156 5 + 28	- 27	一I34 十 95	+ 14 15	1156
7090	46'1	-0 5986	9.7373	64.04	87.14	9.5464	9'9953	9'9713	9 1641	9.2054	9.9765	81.1	g6	4:	3 44	- 10	12	25	1 -t
7091	104'4	7 +0.5681 2 +1.4930	9.7489	233'47	86 73	9'5294	9'9917	9'9736	9,2866	924434	9.9826	72.4	-156	+ 4	4 - 101	+ 19	— 43 —	+ 22	t:   t:   12
7093	142.6	5 — I · 4043	3 9 7 1 1 9	51.64	86.67	9.5293	9.9909	9.9736	9 3054	9'4334	9.9834	77 9					_	=	p
7095	324'1	+1.2257	9.7652	220 ' 62	86 77	9.2150	9.0868	9 9753	92384	9n 342	9.9892	104	+			-		-	Į,
7096	262.5	9-+0.778	2 9 . 7081	3 6	89 63	9'4849	9 9788	9 9 7 8 7	9 4839	8 305	9.9999	72.	+ 25	+ 3	3 + 90	+ 5	5 - <del></del>	+ 69	n He
7008	320 0	7-0.7010	79:7317	349 99	91.01	9'486	9'9794	9 9786	9 478	3 8n 747:	1919993	72.	4 32	1 I	6 + 3	t  — :	2 + 92	1 1 1 1 1	r 37
7099 7100	141.9	7 -0.0389	9 724	336.8	93.50	9 4913	0.0816	9 9777	9 454	5 9n 108	9.996	73	3 +135	5 - 5	9 -13	7 - 5	3 - 68	- 20	5 t
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7118 7119 7120	1782 X 7	2372 202	0 49'8	22 901 193 867 342 660			187.050	6'152 189'016 341'551	0.2136 0.2436	9'7032 9'7533 9'7375	8 · 7072 8 · 7496 8 · 7354	0.5685 0.5413 0.5518	7.6683 7.6732	9'8290 9"7863 0"1523
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7131	1787 VI 15	2373 767 2373 914	15 50.3	299 401 84 337	+2·79	23'463 23'463	15°934 168°489	17 946 168 049	0.7310	9.7165 9.7643	8.7593	0.2310	7.6629	o'1676 g'9886
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7136 7137	1789 V 24	2374 445 2374 623						356'154 188'261				0'5636	7.6761 7.6641	9n1883
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714	2 92'10 3 13'18	3 -1.412 +1.204 3 +0.823 5 -0.749 7 +0.061	0 9 · 765 2 9 · 709	3 233'5' 3 16'9	1 86 . 3 4 88 . 3 0 80 . 3	0 9 . 531 3 9 . 490	7 9 '99 I 2 9 '98 C	6 9 973 3 9 978 8 0 978	33 9 n 288 32 9 · 469 36 9 n 484	34 92446 30 8 974 10 82519	1 9 · 982 6 9 · 998	4 101. 8 107.	7 91 8 91 8 +109	)   3	11 +17	ט ייין י	4 10	.   U	6 t
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7151 7152 7153 7154 7155	1794 VII 26 1794 VIII 25 1795 I 21 1795 VII 16 1796 I 10	2376 512 2376 542 2376 691 2376 867 2377 045	7 36.2 7 36.2		+0.42 +2.92 +1.39	23'461 23'461 23'461	15.490 172.139 354.053	343°436 14'206 174'587 351'725 181'476	0.403 0.4142 0.403	9 7180 9 7073 9 7362 9 7446 9 7095	8.7179 8.7100 8.7352 8.7408 8.7137	0.5573 0.5648 0.5547 0.5419 0.5702	7.6634 7.6657 7.6768 7.6629 7.6772	011302 01648 98484 917223 82363
7156 7157 7158 7159 7160	1796 XII 29 1797 VI 24 1797 XII 18	2377 753	6 4.0 16 28.1 6 37.7	278·368 93'493 266·932	+0.21	23.463 23.463 23.463		1'903 186'791 12'735 192'290 352'791	0'7443 0'6938 0'7329	9 7629 9 6994 9 7609 9 7139 9 7259	8 · 7578 8 · 7062 8 · 7559 8 · 7167 8 · 7244	0.5762 0.5329 0.5678	7.6627 7.6773 7.6627 7.6771 7.6648	9 3768 9 8266 9 9904 0 1208 9 19418
7161 7162 7163 7164 7165	1798 XI 8 1799 V 5 1799 X 28 1800 IV 24 1800 X 18	2378 256	o 12.7 o 31.8	44'453 215'318	-0.87 -4.03 -0.48	23 463 23 464 23 464	358.637 178.492 6.400	168 551 359 183 178 661 5 402 188 693	0'7422 0'6890 0'7421	9 7538 9 7042 9 7639 9 7042 9 7518	8.7076		7.6744 7.6658 7.6732 7.6670 7.6719	9'9180 9"1164 9'1071 9'7871 9"7622
7166 7167 7168 7169 7170	1801 IV 13 1801 IX 8 1801 X 7	2378 964 2379 112	4 23 1 5 38 4 19 57 2	353'609 22'756 165'044 194'060 342'956	0.16 0.24	23'464 23'464 23'464	14.418 154.361 194.800	341.242 12.085 165.099 197.221 350.570	0'7248 0'7346 0'7238	9'7392 9'7253 9'7136 9'7252 9'7603	8·7365 8·7244 8·7148 8·7253 8·7568	0'5567 0'5567	7.6720 7.6683 7.6670 7.6706 7.6732	0,1594 0'1189 0'1660 0,1320 9,8412
7171 7172 7173 7174 7175	1802 VIII 28 1803 II 21 1803 VIII 17 1804 II 11 1804 VIII 5	2379 643 2379 820 2379 998	21 20.0 8 25.4 11 24.9	143'415 321'606	+3.48 +0.99 +3.64	23'464 23'464 23'463	359'918 180'048 7'972	172.208 0.810 178.301 10.308 186.067	o'7088 o'7088	9'7011 9'7618 9'7127 9'7424 9'7387	8.7051 8.7587 8.7137 8.7407 8.7355	0'5611 0'5501	7.6658 7.6744 7.6648 7.6754 7.6640	9.8790 7.8445 7.6568 9.8487 9.8820
7176 7177 7178 7179 7180	1805 I 30 1805 VI 25 1805 VII 26	2380 499 2380 529	6 28.9 6 28.1 6 28.1	280'258 310'550 94'792 122'741 268'763	+3.42 +0.58 +1.51	23'463 23'462 23'462		17.782		9'7045 9'7153 9'7646 9'7604 9'7014	8 · 7095 8 · 7177 8 · 7594 8 · 7554 8 · 7074	0.5664 0.5308 0.5334	7.6773 7.6763 7.6627 7.6633 7.6772	0,1851 0,1659 0,0196 0,1635 9,19422
7181 7182 7183 7184 7185	1806 All 10 1807 VI 6 1807 XI 29	2380 854 2381 031 2381 209 2381 385 2381 563	2 18·2 5 23·9 11 48·5	74 525 246 394	-1.83 -0.21	23'460 23'460 23'459	358'240 185'026 6'138	178 049 356 006 187 429 3 962 194 717	0'7269	9'7215	8 · 7228 8 · 7297 8 · 7464	0'5354 0'5632 0'5494 0'5471 0'5633	7'6768 7'6634 7'6761	9'5050 9"2120 9"6606 9'7305 0"1025
7186 7187 7188 7189 7190	1808 X 19 1808 XI 18 1809 IV 14 1809 X 9 1810 IV 4	2381 740	2 41'6 19 57'2	235'642 24'433 195'591	-3.16 +0.04 -3.16	23'459 23'458 23'458	170.775	13.715 169.306 353.355	0.6906 0.6896 0.7391 0.7071	9.7084	8 · 7115 8 · 7426	0.5367 0.5381 0.5656 0.5458 0.5522	7.672x 7.6753 7.6682 7.6707 7.6695	0,1596 0'0746 9'9420 9,8978 9'0133
7191 7192 7193 7194 7195	1810 IX 28 1811 III 24 1811 IX 17 1812 II 12 1812 III 13	2382 773 2382 921 2382 951	14 19'4 18 52'4 20 16'9 6 33'1	3.062 173.943 323.045 352.573	+1 66 -1 38 +3 66 +2 43	23 458 23 458 23 458 23 458	187 186 7 069 164 054 195 370	7°591 165°552 195°745	0.7306 0.6965 0.7443 0.6947 0.6898	9.7569	8 7536 8 7065 8 7556	0.5604 0.5394 0.5693 0.5412 0.5363	7.6694 7.6708 7.6681 7.6754 7.6722	8n8425 9n7917 9.8322 0.1316 0n1112
7196 7197 7198 7199 7200	1812 VIII 7 1812 IX 5 1813 II 1 1813 VII 27 1814 I 21	2383 127 2383 276 2383 452	8 50'9 14 50'4	163.011 312.189 124.088	+3.49 +1.52	23'458 23'459 23'459	14.776	13'393 174'500 350'925	0.7307 0.7396 0.7159 0.7076 0.7372	9'7347 9'7462	8.7108 8.7339 8.7422	0.5568 0.5649 0.5551 0.5415 0.5706	7.6640 7.6668 7.6762 7.6633 7.6768	0n1526 0'1441 9'8547 9n7786 8'4018
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7152	2'06	-1:3497 +1:4615	9'7094	146.33	92.92	9.5058	9'9846	9.9765	914186	9.2656	9'9925	105.2	-			_		4 B	p $p$ $p$
7154	294'05	+0.012 +0.222 +0.223	9'7467	101.26	91'56	9.2697	9'9990	9.9678	8n8405	9.5620	ე ' ენეი	94.3	+ 10 + 27	- 26	+173 + 65 + 88	- 11	-137 +118 +148	+ 48 - 33 + 3	$t_{\perp}$
		0.5281 0.6208											+125 + 6	+ 13 36	-165 + 91	+ 37 65	- 94 -179		tik 1.
7158 7159	64.09 276.38	+0'9782 -1'3207 -0'8746	9.7629	80°04	88·41 87·23	9'6048 9'6158	9'9991	9'9615 9'9594	8 · 8054 920452	9'5993 9"5995	9 · 9626 9 · 9626	86.0	+157	+ 62	(+114)  -115	(+78)	+ 91	-	p
7161	210'18	-l-n · 8 2 8 n	0'7558	214.82	83:20	0.6650	0.0600	0.0474	0.,5616	0.4566	0'0814	112'4	+120	-1- 70	+159	47	-145	+ 32	t ^{ij}
7162	84'43	-0'1307 -0'1280 -0'6124	9.7004	33'34	83.20	g 6095	9.9071	9.9405	9'5738	9'4454	9 9824	115'2	+124 -141	+ 32	<b>– 83</b>	- 5	16	- I7	$t^{*}$
7165	316.46	-0.5784	9'7539	198'04	85.12	9 6806	9,9210	9 9433	926526	912220	9 9939	117.1	27	8	+ 35	- 50	+129	— бі	•
7167	242'01	-1.4433 +1.3150 +1.4657	9'7274	16.26	85 44	9.68xx	9'9498	9'9432	9.6575	9.1876	9'9948	62'6	i] —	podorno podorno			governe		$p \\ p$
7169	118'71	-1:3552 -0:6937	9.7282	190'19	87.02	9 6825	9 9454	9.9428	926736	829856	9.9980	118.3	3 —	- 7I		- 59	+177	- I6	t
7172	1136'54	+0.4268	0.7030	11330'85	3 95 3	1080'0	10.0520	119 19435	19 045	[ ] Qn 2007	1919925	1 03 3	31 7 354	27	130	- TT	- 70	1 20	9**** t*** 9***
7173	305 30	-0'7058 -0'7620	9 7 1 4 9	152.05	3 06 30	9.0751	0.0623	9 9449	3 0 · 602	9 3754	9 9074	65	5 51	+ 20	+ 6	+ 36	+ 52	+ 65	v-t*
		-1.5313 -1.4653							_	1			_	-		_			$p \\ p$
7178 7179	171'53	+1.0462 1-1.4570 -0.8754	9.7666	135.2	4 93 ° 02 x 96 ° 45	9.6179	9.9968	9.959	9n0839	9 9 5 5 2 5 4	9 9 9 6 2 8 9 9 7 4 2	97'	6		— — +177	85		_ 	$\begin{array}{c} p \\ p \\ r \end{array}$
		+0.3100			1.			1	1			93	4 -141	+ 20	— 66	+ 43	+ 5	  -  14	t:#
7182	250.85	-0.1629 -0.4577 3-0.5376	9 7237	87.4	6 89 · 6	3 9 584	9 . 999	99'965	8.102	2 9 <i>n</i> 5 8 9 . 5 8 4 .	9 9654	80	0 + 46	20	+143 + 100 + 2	_ 3	+154	- 24	r-t
7185	346.24	1 -1 2662	9.7100	75.6	988.1	9.565	5 9 . 998.	4 9 9 9 6 8	8.020	9'553	9 970	84'	8	-		-			l p
7187 7188	221 7	+1'14440 +1'1873 +0'8750	9.765	4 246 2 5 30 0	1 87 · 2 2 87 · 3	7 9 550	8 9 · 996 5 9 · 983	0 9 970 6 9 977	6 9n 131 1 9 431	5 92516 9 9 216	7 9 975 6 9 994	98'	2 1 153	+ 4	4 -129			+ 7	
7189 7190	297 '9; 204 ' 7;	#0:7903   #0:1031	9 747 9 735	4 199°2 0 16'8	88°3	2 9 '492 4 9 '489	2 0 . 080 2 0 . 080	7 9 9 9 7 8 3 9 9 7 8	0 92464 2 9 468	5 9n 029 7 8 972	4 9 '997: 6 9 '998	72'	8 + 94	3: I	+ 56	+ a	2 + 15	+ 2	8 <i>t</i> 3 11 th
7192	3 x . 5	-0.0626	9.759	0 3.7	9 89 6	I 0'486	00.078	7 9 9 9 78	6 9 484	0 8 327	7 9 999	9 72	2 - 99	- 5	6 - 26	5  - 3	6 —' / 9 + 3	7 - 2	o $t$
7194	123.0	+0.6793 +1.3540 -1.2913	9.760	2 315 3	6 93.3	2 9 520	0 9 988	3 9 974	8 9 359	4 9 379	19.987	2 76.	4 -		gc		3	3 7 2	$\begin{bmatrix} p \\ p \end{bmatrix}$
7196	257 7	0 —1 4210 4 +1 393	9.721	5 125 5	I 03.3	0 9 534	09'991	99.972	9 9 2 7 9	8 9 453	5 g 981	7 101	5 -	_			_		$\left  egin{array}{c} p \\ p \end{array} \right $
7198	42 6	0 +0.715; 4 -0.600	7 9 736 6 9 748	3 113.3 3 2023	2 93°1	5 9'535 8 9'550	5 9 999 7 9 996	39.972	8 9 243 6 92122	8 9n 469 19 9 ' 5 1 8	8 9 980 2 9 975	2 79° 0 98°	4 - 10	1 - 2	7 - 4	5 - 1	0 + 9 8 + 8 + 2	8 4	3 7
7200	33 3	4 +0.025	9 710	209 3	5 92 3	4 9 555	291997	3 9 7 9 7 9	∵ 9° 04€	91533	9 973	2 83	'2 — 9		5 - 3	ر – و	.5 T 2		

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		reg. ender	Julian Tag		Welt- Zeit											
7201 7202 7203 7204 7205		VII 17 I 10 VII 6 XII 30 V 27	2384 I	84 14 61 23 38 14	5.6 52.5 53.5	113°973 289°544 103°940 278°117 65°636	+1°41 +1'93 +1'06 +0'66 -0'83	23.459 23.460 23.460	186.890 10.596 194.143	11.088	0'7442 0'6947 0'7319	9.7632 9.6996 9.7599 9.7152 9.7243	8.7584 8.7063 8.7548 8.7179 8.7231	0.2260	7.6629 7.6772 7.6627 7.6773 7.6640	9n8210 9'9572 0n1178
7206 7207 7208 7209 7210	1817	XI 19 V 16 XI 9 V 5 X 29	2384 8 2385 C 2385 I	41 6 18 1 95 7	55.9 52.6 22.7	237°019 54°994 226°344 44°167 215°711	-3.59 -1.00 -4.01 -0.87 -4.04	23.461 23.461 23.462	357.861 178.240 5.686	168*452 358*699 178*521 4*589 188*437	0'5892	9'7548 9'7038 9'7637 9'7050 9'7506	8.7522 8.7071 8.7607 8.7081 8.7476	0.5662 0.5374 0.5662	7.6754 7.6649 7.6743 7.6659 7.6731	9n3126 9'1744
7211 7212 7213 7214 7215	1819 1819 1819 1819	III 25 IV 24 IX 19 X 19 III 14	2385 5 2385 6 2385 7	49 11 97 12 27 3	45'3 46'7 42'0	4.492 33.437 175.712 204.931 353.918	-0'46 -1'52 -3'69	23'462 23'462 23'462	13.805 163.635 194.496	340.867 11.440 165.393 196.781 350.357	0'7236 0'7357 0'7250	9'7270 9'7121 9'7245	8:7379 8:7255 8:7138 8:7241 8:7573	0.5486 0.5542 0.5634 0.5586 0.5376	7.6670	0,1681 0.0992 0.1836 0,1215 9,8574
7216 7217 7218 7219 7220	1821 1821 1822	IX 7 III 4 VIII 27 II 21 VIII 16	2386 2 2386 4 2386 5	29 5 05 15 83 19	5 50.2 5 19.6 5 49.0	164.797 343.382 153.961 332.683 143.447	+0.35	23'461 23'461 23'461	359.669 179.288 7.793	171°373 0°668 177°461 10°154 185°301	0'6917 0'7345 0'7101	9'7009 9'7613 9'7412 9'7403	8 · 7053 8 · 7580 8 · 7149 8 · 7393 8 · 7370	0.5690 0.5383 0.5610 0.5502 0.5453	7.6669 7.6733 7.6657 7.6745 7.6647	9.9167 8.4513 8.8267 9.8402 9.8389
7221 7222 7223 7224 7225	1823 1823 1823	I 12 II 11 VII 8 VIII 6 I 1	2387 C	38 3 85 6 14 13	3 20'4 5 46'1 5 58'4	291.435 321.661 105.239 133.234 279.942	+3.63	23'460 23'460 23'460	15.686 166.738 196.389	344.760 17.570 166.602 195.182 349.917	0'7330 0'6902 0'6934	9'7141	8.7089 8.7566 8.7595 8.7563 8.7078	0.5737 0.5668 0.5308 0.5334 0.5749	7 · 6771 7 · 6755 7 · 6627 7 · 6640 7 · 6773	0.0488 0#1410
7226 7227 7228 7229 7230	1824 1825 1825	VI 26 XII 20 VI 16 XII 9 VI 5	2387 6 2387 7 2387 9	94 12 70 20	39'5 2 24'0 27'2	95 195 268 588 84 978 257 558 74 459	+0.61 -0.51 +0.04 -1.83 -0.49	23 459 23 458 23 458	358 · 174 184 · 175 6 · 057	x86.222	0'7259 0'7216 0'7022	9.7226	8.7504 8.7238 8.7281 8.7476 8.7096	0.5626 0.5500 0.5467	7.6630	9.5977 9.2270 9.5816 9.7234 0.0751
7231 7232 7233 7234 7235	1827 1827	XI 29	2388 3 2388 4 2388 6	73 3 50 15	1 25'3 3 0'7 5 33'7	217.106 246.772 35.096 206.482 24.388	-2.90 -0.56 -3.77	23 457 23 457 23 456	13'979 170'145 350'656	13'590 168'582 353'014	0'6894 0'7383 0'7082	9 7636 9 7097 9 7439	8 · 7 6 x 1 8 · 7 1 2 0	0'5384 0'5641 0'5473		0'0704 9'9696 9n9166
7236 7237 7238 7239 7240	1829 1829 1830	X 9 IV 3 IX 28 II 23 III 24	2389 3 2389 3 2389 5	81 22 359 7	2 24'4 1 55'6 4 51'5	195.677 13.895 184.663 334.123 3.479	+0.80 -2.30 +3.44	23 455 23 455 23 455	186 738 6 491 163 875	185'119 6'903 165'457	o 6957 o 7445 o 6957	9'7574	8 · 7 · 86 8 · 7543 8 · 706 · 1 8 · 7546 8 · 7602	0.5381 0.5704 0.5410	7.6707 7.6695 7.6693 7.6743 7.6709	9n7630 9.7956 0.1374
7241 7242 7243 7244 7245	1830 1831 1831	VIII 18 IX 17 II 12 VIII 7 II 1	2389 2 2389 8 2390 0	713 2 361 13 37 22	2 23 3 7 14 5 2 9 0	144 969 173 665 323 309 134 579 312 146	-1:34 +3:64 +1:37	23'455 23'455 23'455	14 136 171 924 352 390	341 '681 12 '658 174 '372 350 '165 181 '115	0'7387 0'7172 0'7063	9.7090 9.7334 9.7475	8.7118 8.7327 8.7438	0.5652	7.6680 7.6754	0'1244 9'8627 9n8262
7246 7247 7248 7249 7250	1833 1833 1834	I 20 VII 17	2390 5 2390 5 2390 9	69 22 747 2 923 23	2 5 4 7 16 5 3 10 3	124 445 300 709 114 393 289 306 76 109	+1.42	23 · 456 23 · 457 23 · 458	186°794 9°727 194°884	0'471 186'395 11'242 192'042 351'070	0'7440 0'6956 0'7310	9.7000	8 7066 8 7542	0'5756 0'5340 0'5662	1	9n8148 9'9214 0n1151
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Nr.	μ	γ.	log n	G	K	$\sin g$	$\sin k$	$\cos g$	, ,	sin ð'	cos o	N'	gang A	φ	λ   r a	φ	Unterg	ang p	F
7202 7203 7204	27.47 174.80	+0'1636 -0'6622 +0'9062 -1'311	2 9 . 7018 2 9 . 7619 7 9 . 7173	276.64 91.16 264.66	90'94 89'17	9.5767 9.5871 9.5972	9'9997 0'0000 9'9997	9 ' 9667 9 ' 9631 9 ' 9631	8.6066 7n8581 8n5295	9n5742 9 5870 9n5956	9'9671 9'9649 9'9634	87'5 90'4 92'I	+ 14 + -115 - + 66 + 	- 40 - 57	27 - 175 +	- 64 - 88	+ 57   - 57	- 36 - 56	r t** 1)
7206 7207 7208	337 98 285 58 212 54	+0.8410 -0.205 +0.149 -0.543	5 9 · 7568 4 9 · 7658 5 9 · 7678	224.36 42.27 215.01	83.49 83.33 83.25	9.6551 9.6568 9.6668	9.9788 9.9766 9.9691	9'95°3 9'9493 9'9473 9'9465	9n4837 9'5041 9n5613 9'5750	9n5237 9.5134 9n4594 9.4432	9'9743 9'9756 9'9812 9'9826	108'9 70'3 112'3 67'0	+ 25 - + 93 - + 2 -	- 30 <del> </del> - 29 <del> </del> - 10 <del> </del>	- 77 + -149 - - 63 +	- 6 - 7 - 52	+158 ·	+ 7 - 13	t* t* r* t
7212 7213	353'35 17'47	-1.472 +1.256 +1.526 -1.322 -0.720	7 9 729 0 9 714 7 9 726	24'71 175'92	84 ° 03 90 ° 94 85 ° 12	9 · 6755 9 · 6856	9'9579 9'9421	9 9448 9 9418 9 9439	9.6231 9.6848 9.6500	9'3412 8'4738 9n2249	9,9998	64'5 116'9	_	75		   58	- - - - 51		P P P T
7217	264'70 49'77	+0.825 -0.028 +0.067 +0.692 -0.690	3 9 7 7 6 3	348'04	93.20	9 · 6847 9 · 6814	9'9457 9'95'5	9 9 4 3 1	9.6724 9.6506	920504 9 2422 9 92613	9'9972	117.0	+ 27 - -117 - -179 -	- 30 - - 30 -	- 49 - - 121 -	- 14 - 40	+156 + 7 - 69	+ 68	1.16 1130
7222	283 17	2 -1.540 5 +1.455 7 +1.119 8 -1.386 5 -0.882	0 9 7 16 0 9 7 7 66	1 144,30 1 331,30	96 36 94 67	5 9 · 6709 7 9 · 6328	9'962	9'9461 9'9558 2'9'948:	9'000; 3 9n283; 1 9n554	3 9 n 3 9 2 t 2 9 · 5 8 4 2 5 9 · 4 6 2 !	9 9 9 8 0 5 4 9 9 6 5 4 5 9 9 8 0 9	102'0		6 x	- 60	  87	  +158	  46	p p p r
7227 7228	340.87	1 +0 · 396 70 · 168 20 · 381 2 +0 · 528 11 · 188	6 9'724 6 9'732	8 282 6 4 98 6 6 270 8	3 92 °0; 3 91 °38	3 9 · 6089 3 9 · 6029	9 9 ' 9 9 9 6 7 0 ' 0 9 0 0	5 9 · 960 3 9 · 962 5 9 · 964	8 8 9 1 1 1 8 1 7 4 4 4 7 7 2 8	$     \begin{array}{ccccccccccccccccccccccccccccccccc$	9 9 · 962 7 9 · 962	84'9 93'4 89'	+104 9 - 49 5 - 61 7 +179 9 -	- 14 - 17	-175 + 20 6 127	- 33 + 1	+ 83 + 48	- 4	1,-9.16
7232 7233	351'3	8 — 1 · 471 0 + 1 · 176 2 + 0 · 932 8 — 0 · 825 2 + 0 · 156	9 7 7 1 1 4 9 7 1 1	6 258 6 8 42 7	7 88 · 4 4 86 · 7	5 9 5 5 15	29.987	0 9 · 9 6 7 8 9 · 9 7 5	6 8 n 8 3 2 4 g ' 3 6 g 8 D 1 4 2 2	8 9n 503 4 9 359	3 9 · 9 6 8 7 9 · 9 6 8	94	2 — 1 + 34 6 — 143						7*-t*
7237	153.8 3209.3	6 -0'113 1 -0'579 5 +0'622 6 +1'372 8 -1'261	9 759 6 9 703	8 17'1 2 185'8 4 328'5	6 88 3 1 89 4 1 02 8	0 9 490 1 9 484 2 9 505	1 9 983 0 9 979 7 9 980	3 9 · 978 0 9 · 978 7 9 · 976	19.468 $89.481$ $69.429$	98.980 $68n510$ $39n239$	3 9 · 993 8 9 · 998	0 72 8 107 4 74	8 +145 7 + 87 2 -	52	-149	32	87	10	t
724	2 213 3 3 76 9	7 -1 · 488 5 +1 · 33 8 +0 · 72 2 -0 · 67 6 +0 · 03	9 9 7 1 1	5 315 3	7 90'8 0 93'2	0 9 487	5 9 978 8 9 988	9 9 9 9 7 8	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	9 9 3 7 6	7 9 999	6 107°	7 139	201	I 5D	+ 35 - 27 - 15	-103	50	2 2 2 14
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7251 7252 7253 7254 7255	1834 XI 30 1835 V 27 1835 XI 20 1836 V 15 1836 XI 9		13 32'3 10 30'6 14 7'7	65'490 237'429 54'712	-0.82 -3.58 -1.00	23'458 23'458 23'458	357 ° 033 178 ° 051 4 ° 915		-	9.7635	8.7532 8.7666 8.7668 8.7689 8.7466	0.5429 0.5660 0.5381 0.5649 0.5456	7'6762 7'6640 7'6754 7'6649 7'6743	9'9299 924551 9'2186 9'6717 927257
7256 7257 7258 7259 7260	1837 IV 5 1837 V 4 1837 X 29 1838 III 25 1838 IX 18	2392 134 1 2392 312 1 2392 459 2	19 1'8 11 34'1 21 45'8	44'058 215'868 4'812	-0.85 -4.05 +1.52	23'459 23'459 23'459	13'130 194'161 351'150	340 422 10 737 196 408 350 071 170 605	0'7262 0'6916	9'7423 9'7287 9'7230 9'7617 9'7009	8.7391 8.7268 8.7231 8.7578 8.7054	0.5468 0.5526 0.5601 0.5366 0.5698	7.6693 7.6659 7.6731 7.6707 7.6682	0n 1785 0 0766 0n 1127 9n8766 9 9484
7261 7262 7263 7264 7265	1839 III 15 1839 IX 7 1840 III 4 1840 VIII 27 1841 I 22	2393 169 2393 345	22 21'9 4 5'7 6 44'8	164.564 343.700 154.010	-0'53 +2'98 +0'32	23'459 23'459 23'459	7'547 186'987	176'681 9'930		9'7151	8 · 7573 8 · 7159 8 · 7379 8 · 7384 8 · 7084		7.672x 7.6669 7.6733 7.6657 7.6767	8n7449 9'1237 9'8277 9"7939 on 1908
7266 7267 7268 7269 7270	1841 II 21 1841 VII 18 1841 VIII 16 1842 I 11 1842 VII 8	2393 847	14 14 4 21 33 3 16 14 4	115'696 143'762	+1'45 +0'98 +2'06	23'458 23'458 23'458	165'864 195'600 350'681	17'297 165'880 194'524 349'733 176'505			8'7156 8'7596 8'7570 8'7082 8'7492	0'5667 0'5308 0'5334 0'5744 0'5367	7.6745 7.6630 7.6647 7.6771 7.6627	0.1586 0.0757 0n1202 9n9493 9.6745
7271 7272 7273 7274 7275	1842 XII 31 1843 VI 27 1843 XII 21 1844 VI 16 1844 XI 10	2394 556 2394 734	19 19'9 5 9'9 0 25'9	268 ' 748 84 ' 893	+0'64 -0'50 +0'04	23'456 23'455 23'455	183'302 5'998 191'650	355 804 185 655 3 928 192 778 343 282	0'7230 0'7012 0'7415	9'7506 9'7061	8.7250 8.7266 8.7486 8.7088 8.7587	0.5619 0.5508 0.5463 0.5637 0.5386	7.6773 7.6627 7.6771 7.6530 7.6745	9n2384 9n4814 9'7182 0n0446 0n1733
7276 7277 7278 7279 7280	1845 V 6 1845 X 30 1846 IV 25	2395 058 2395 235 2 2395 412	9 57.2	45 696 217 441 35 072	-0'91 -4'07 -0'55	23 ' 454 23 ' 454 23 ' 453	169'442 350'354	13'706 167'793 352'739 175'284 0'358	o'7373 o'7095	9'7637 9'7110 9'7424 9'7364 9'7154	8.7613 8.7129 8.7401 8.7339 8.7175	0.5387 0.5626 0.549x 0.5488 0.5637	7.6767 7.6657 7.6733 7.6669 7.6721	0.0673 9.9982 9.9316 9.3106 9.1796
_	1847 X 9 1848 III 5 1848 IV 3	2396 092	9 7.5 13 18.8 23 1.4	195 453 345 143 14 314	-3'15 +2'90 +0'78	23'453 23'453 23'453	5'987 163'629 194'540	184 690 6 284 165 296 195 156 340 889	0'7447 0'6966 0'6908	9.2006	8.7551 8.7060 8.7537 8.7597 8.7221	0'5368 0'5715 0'5408 0'5352 0'5563	7.6682 7.6707 7.6731 7.6696 7.6659	9n7270 9'7608 0'1446 0n0886 0n1899
7286 7287 7288 7289 7290		2396 447 2396 623 2396 801	1 30'3 5 33'4 6 28'8	184'389 334'376 145'107 323'249 134'942	+3'42 +0'92 +3'64	23'453 23'452	171'739 351'617 171'739		0'7376 0'7186 0'7049 0'7390 0'6905	9'7099 9'7319 9'7489 9'7058 9'7640	8.7127 8.7313 8.7452 8.7114 8.7594	0'5654 0'5556 0'5406 0'5708 0'5318	7.6693 7.6743 7.6649 7.6754 7.6640	o.1058 9.8739 9n8665 8.7071 8.3159
7291 7292 7293 7294 7295	1851 VII 28 1852 I 21 1852 VI 17 1852 XII 11	2397 332 2397 509 2397 657 2397 834	14 41'3 7 26'8 16 47'7 3 32'3	311 844 124 861 300 481 86 551 259 320	+1'55 +2'86 +0'15	23 453 23 454 23 454	8.877 194.010 347.971		0'5957 0'7299 0'7293	9'7004 9'7579 9'7179 9'7212 9'7566	8 · 7 · 7 · 7 · 7 · 8 · 7 · 7 · 7 · 9 · 7 · 2 · 9 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 4 · 2 · 7 · 5 · 7 · 7 · 7 · 7 · 7 · 7 · 7 · 7	0.5750 0.5348 0.5653 0.5552 0.5428	7.6762 7.6633 7.6768 7.6629 7.6768	9n8064 9'8831 0n1118 0n0461 9'9327
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7252	24'75	+0.8510 -0.2852 +0.1624	9'7955	51'72	84.09	9.6471	9 9852	9.9524	9'4086	9.2290	9.9695	74'0	- 73	30	- 22	+ 4	+ 37	I 9	7'''
7254	31'54	+0'4696	9.7082	42'06	83'32	9'6594	9.9765	9'9493	9 5059	9.2119	9.9758	70.3	— 98 <u> </u>	+ 8	37	+ 49	十 52		2*** t
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7257	103'04	-1.2963 -1.2963	9.7308	33'23	83.33	9.6678	9.9672	9'9470	9.5729	9'4423	9.9822	67.1			-	_	=		$\stackrel{r}{p}$
7259	146.83	-0.7527 +0.8886	9.7638	3.45	88.94	9.6859	9'9421	9.9418	9 6849	8.5237	9.9998	61.0	+149	— 78 (+88)	136 	- 57		- 20 + 34	st-
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7262	156'39 236'65	+0.1320	9.7173	168'91	93'28	9 6856 9 6837	9'9459	9'9419	g : 6750	9.0252 9.0482	9.9976	61.8	+ 55	+ 30 + 14	-154 + 114	+ 43	+176	21	1'-1'4
7264	279'2X	-0 6221 -1 551	9 17438	161.06	95.07	9 6806	9.9218	9 9434	926497	7 9 * 24 1 7	9.8833	117.0	+ 14	<u> </u>	+ 72 -	<del>-</del> 34	+129	64	p
7266	342 57	+1.440	9.7150	339 96	95.22	9.6778	9 9533	9 ' 9442	9.6434	92612	9 9927	63.4		phrasent	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				p
7267 7268	35.02 35.02	+1,1306	9.7667	128.87	95 92	9 6460	9 ' 9848 9 ' 9606	9 9526 9 9457	5 gn4138 7 gn6og6	9 · 5548	9.9876	114.8							$p \\ p$
7269 7270	285.72	-0.8898 -+0.4726	9.766	302.0	95 52	9 · 6422 9 · 6344	9.8822	9 953	9°3689 19°294	9 . 5836 2 9 . 5836	9.9622	75'4	- II +100	- 65 + 37			+ 35	- 44 + 15	
7271	105.30	-0.173	9'7263	294 0	93.8	9.6265	9'9945	9 957	9,199	925936	9 9637		-176				43	. 0	
7273	256'59	+0.225 +0.225	9 7527	282'7	92.04	1 9.6085	9.9986	9.000	8.013	3 gn 5 g 98	9.9626	84 .	+ 47	+ 24	-110 +102	+	- 56 +154		
7274 7275	332,10	-1.108; -1.108;	9.7636	237.4	96.48	9 5385	9,993	9.972	9249	924719	9.0800	93.4		-	_	-			p
7276	122.08	+1.162	9.7657	270.8	90'1	9 5903	9,000	9.964	7'739	92590	9 9 9 6 4 3	89.	7 — — 104			_	(—135		$p_{j}$
7278	182,51	+0'995 -0'854: +0'204	9 ' 7445	225'5	2 86.7	1 9.218	9886,6	91975	0 92350	9 9 2 38 38	9.0866	103.	+ 88 -136	- 44	+172	7:	5 — 69 5 — 4	- 67	r-t
7280	300.36	-0.121	9.7176	212'7	87.1	9.501	9 984	9 977	9,419	1 9 250	9 9930						+126	24	r*
7281	274'14	-0.233 +0.233	4 9 7610	30'2	87.3	9 500	9.083	69.977	09.431	0 9 220	9'993	74	+ 28 - 16	- 47 + 52	+ 90	- 2. + 3	+151 +105	16	t
7283	20.20	+1.395 -1.326	9 7586	5 341 8	1 91.8	2 9 4942	9.980	2 9 977	7 9 470	$1 \mid 9n \circ 08 \mid$	9 997	72.	7	_	_		-		$p \\ p$
7285	109 2	-1.248	9 ' 7243	150'3	92.7	3 9 5 5 5	9 9 9 9 9	9,976	5 9 4 4 3 8	39.217	9 994	100.	2 -			-	hall-rever		p
7287	201 2	+1 ·275	0 0 7340	328 4	9 92 7	7 9 501	2 9 984	0 9 977	0 9 425	5 91235	9 9 9 9 9 3 :	5 74	3 + 93	+ 3	 2 +153	+ 4	149	+ 6:	
7288	264 3	-0.735	3 9 75 10	137'6	3 93 2	5 9 5 15	7 9 987	5 9 ' 975 7 0 ' 075	3 9n 372	6 9 357 2 02 376	3   9   9   8   8   9   8   9   9   8   9   9	4 104	0 + 32 6 + 23	- 3:	$\frac{2}{1} + \frac{9}{86}$	5 - I	1 +143	+ 1	7·*
7290	142.10	+0.020	7 9 ' 766	1 125'5	6 93 2	5 9 5 30	8 9.992	0 9 973	4 92277	5 9'449	8 9 982	101,	4 +150	+ 1:	2 -142	, r	li.	1	1
7292	36.83	-0.640 +0.764	9 759	9 114'2	5 92 7	5 9 549	49'995	8 9 9 7 0	8 92 138	69'514	0 9'975	5 98.	4 138	- 4 + 5	7 + 98 3 - 34	4 + 7	$     \begin{array}{r}                                     $		) t**
7293 7294	285 22	3 -1 . 113	79'720	289 I 3 72 5	6 92 · 3	4 9 557 6 9 6 1 6	9'997	39'959	7 9 045	9 9n535 3 9 599	3 9 · 972 3 9 · 962	8 83 82 1	9		-		_	_	p
7295	236.86	+0.856	4 9 758	5 245'3	885.0	9 9 6 2 6	9 994	2 9 957	0 92210	4 92 592	3 9 . 963	9 100	2 + 92			7 + 3		+ 4	
7297	1111.7	-0'369 +0'177	0 0 7652	2 234 7	3 84 4	5 0 642	4 0 ' 087	5 0 ' 053	5 Qn 371	o on 568	8 g · g 68	0 104	71 -107	'  2	3	I I	4:	;   ·	9 1° 4 t*
7298 7299	332.79	1 +0'390 9 -0'516	5 9 ' 7 0 9 S 8 9 ' 7 5 0 S	3 51'4 1 224'9	9 84 ° 0	7 9 647. 2 9 654	3 9 · 985 9 9 · 979	0 9 952 4 9 950	4 9 ' 4 1 1 4 9 n 4 7 8	2 9 558 4 9 527	o 9 · 969 5 9 · 973	7 74' 8 108'	6 - 44	1	o -13	5 - 4	3 +11	1 3	۰ ۳
7300	211.2	+1:133	5 9 ' 732'	7 42'1	9 83.3	7 9:658	9'976	79'949	5 9 503	0 9 511	3 9'975	70'	3						P
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Nr.			T	<u> </u>	777.11	L'	Z	ε	P	Q	$\log p$	$egin{array}{c} \operatorname{log} \ oldsymbol{\Delta} L \end{array}$	$\log q$	u'a	$\log f_a$	$\log \gamma$
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7301 7302 7303 7304 7305	1856 1856 1857	XI 9 IV 5 IX 29 III 25 IX 18	2398 8 2399 0 2399 2 2399 3 2399 5	45 22 99 2	9 ^h 32 ^m 4 5 53'4 3 48'7 2 29'7 5 33'9	15.636	+0.68 -2.43 +1.48	23 457 23 457 23 456	350.677 170.168 358.951	196°100 349'713 169'912 0'171 175'974	0,6011	9 7211 9 7624 9 7602 9 7602 9 7162	8.7219 8.7583 8.7057 8.7566 8.7172	0.5618 0.5354 0.5707 0.5375 0.5610	7.6743 7.6693 7.6695 7.6707 7.6682	0n1059 9n8986 9 9746 8n9536 9 2836
7306 7307 7308 7309 7310	1858 1859 1859	1X 7	2399 9 2400 0 2400 1	30 I 79 08 I	4 15.5 1 4.9 9 11.4	354.652 164.630 313.727 343.722 126.170	-0.53 -3.50 -2.98	23 456 23 456	186°308 343°440	183'938 344'329 16'952	0.7126 0.7094 0.7421 0.7351 0.6899	9 7386 9 7432 9 7024 9 7120 9 7647	8 7367 8 7399 8 7078 8 7145 8 7595	0.5504 0.5449 0.5739 0.5666 0.5312	7.6721 7.6669 7.6761 7.6733 7.6634	9.8102 9n7482 0n1949 0.1521 0.1007
7311 7312 7313 7314 7315	1860	VIII 28 I 23 VII 18 I 11 VII 8	2400 2 2400 4 2400 6 2400 7 2400 9	33 10 1 87	0 17'1 4 20'8 3 27'9	154 339 302 280 116 092 290 968 105 841	+2'97 +1'46 +2'04	23'455 23'455 23'454	350.58x 173.698 358.069	193.913 349.539 175.722 355.718 184.745	0'7414 0'7014 0'7235	9 7625 9 7033 9 7526 9 7254 9 7271	8 · 7577 8 · 7087 8 · 7480 8 · 7260 8 · 7253	0.5336 0.5736 0.5374 0.5610 0.5518	7.6657 7.6767 7.6630 7.6671 7.6627	0n0989 9n9533 9'7397 9n2489 9n3479
7316 7317 7318 7319 7320	1862 1862 1862	VI 27	2401 3 2401 4 2401 4	19 66 r 96	6 54'7	279 954 95 312 239 230 269 139 56 243	+0'64 -3'50 -0'46	23'453 23'453	342'077 13'828	3 939 191 760 343 203 13 747 166 947	0'7000 0'7421 0'6917 0'6889 0'7364	9.7517 9.7654 9.7611 9.7638 9.7124	8 7497 8 7081 8 7583 8 7614 8 7137	0.5458 0.5640 0.5396 0.5389 0.5613	7 6773 7 6627 7 6754 7 6771 7 6648	9'7140 0n0104 0n1779 0'0653 0'0270
7321 7322 7323 7324 7325	1863 1864 1864 1865 1865	XI 11 V 6 X 30 IV 25 X 19	2402 3	98 75 I 52 I	7 59 5 0 13 8 5 28 7 4 13 3 6 28 1	45.694 217.491 35.358	-0'90 -4'08 -0'56	23'452 23'450	177.069 358:061 185.614	352°527 174°624 359°964 184°197 5°747	0'7107 0'7145 0'7338 0'6943 0'7447	9'7408 9'7381 9'7139 9'7597 9'7002	8 · 7390 8 · 7352 8 · 7166 8 · 7557 8 · 7059	0.5356	7.6744 7.6657 7.6733 7.6669 7.6720	9n9430 9'4211 9n2610 9n6826 9'7287
7326 7327 7328 7329 7330	1866 1866 1867	III 16 IV 15 X 8 III 6 VIII 29	2402 7 2402 8 2403 0	83 I	7 3'6	195'181 345'381	+0.01 -3.12 +2.89	23'450 23'450 23'450	194.015 13.079 171.490	165.064 194.754 11.419 173.910 348.791	0'7368	9'7557 9'7629 9'7108 9'7306 9'7502	8 7525 8 7591 8 7136 8 7300 8 7466	0.5407 0.5346 0.5658 0.5558 0.5404	7.6719 7.6682 7.6707 7.6732 7.6658	0°1538 0n0734 0°0894 9°8881 9n9007
7331 7332 7333 7334 7335	1869	II 23 VIII 18 II 11 VIII 7 I 31	2403 5 2403 7 2403 9	40 I	5 11 6 3 54 3 2 8 3	334 300 145 481 322 944 135 357 311 633	+0'90 +1'37	23'450 23'451 23'451	359 464 186 497 8 058	180°564 359°159 185°890 9°796 191°759	о боо5 о 7435 о бо74	g'7060 g'7642 g'700g g'7567 g'71g1	8 7597 8 7070 8 7522	0'5320 0'5743 0'5357	7 · 6648	8.8539 8.6595 9.7950 9.8420 0.1079
7336 7337 7338 7339 7340	1870 1870 1871	VI 28 VII 28 XII 22 VI 18 XII 12	2404 2	72 I 19 I 97	2 19'0 2 29'6	125 115	+0.12 +0.12 +0.12	23'452 23'452 23'453	16.751 169.955 355.260	349°202 19°179 168°413 355°772 178°432	0'7194 0'6950 0'7442	9'7196 9'7331 9'7574 9'7025 9'7628	8 7549	0.5488 0.5425 0.5658	7.6772	010779 01772 99346 916592 92671
7341 7342 7343 7344 7345	1872 1873 1873	VI 6 XI 30 V 26 XI 20 IV 16	2405 1 2405 3 2405 4	28 I 05 83	9 20.0	248 934 65 144 237 931	-0.82 -3.56	23'453 23'453 23'453	11.607 193.694	1.840 188.019 9.173 195.850 349.288	0 7047 0 7196 0 7283	9'7082 9'7468 9'7321 9'7197 9'7631	8 · 7446 8 · 7297 8 · 7210	0'5629 0'5481 0'5496 0'5634	7 · 6761 7 · 6640 7 · 6754	9.4883 9.7048 0.0212 0.1006 9.1006
7346 7347 7348 7349 7350	1875 1875 1876	1X 29	2405 9 2406 1 2406 3	61 1 39 2	2 55 4 0 11 8	185 '962 5 '533	+0.05 -2.42 +1.47	23'454 23'454 23'454	358:484 177:390 6:836 185:698	169 295 359 810 175 348 9 252 183 367	0'5938	9'7011 9'7594 9'7175 9'7374 9'7445	8 · 7557 8 · 7183 8 · 7352	0'5372 0'5610	7.6694	
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7302 7303 7304	269.65 242.39 156.18	+0'9432	9.7645 9.7631 9.7623	11'30 184'41 3'74	86.70 88.64 88.84	9.6835 9.6872 9.6870	9'9456 9'9418 9'9418	9'9424 9'9413 9'9414	9.6725 9.6855 9.6858	9°0306 8″6318 8°5603	9'9975 9'9996 9'9997	21,0 113,0	+ 49 (-157) +141	(- -80) 34	-155 -		- 24 t
7307 7308 7309	32 91 197 26 100 92	+0'6460 -0'5666 -1'5666 -1'4193	9 . 7453 9 . 7045 9 . 7140	168'94 324'91 348'20	93.26 96.72 93.41	9.6849 9.6657 9.6824	9'9452 9'9693 9'9463	9'9421 9'9476 9'9428	926743 9:5598 9:6704	9.0234 9.14589 9.10476	9'9975 9'9813 9'9975	61.8 62.2	100	x x 6	- 9		- 69 r-t - 62 t - p p
7312 7313 7314	183'95 35'18 230'44		9 · 7054 9 · 7547 1 9 · 7276	315 23 129 54 304 89	96.21 96.21	9.6555 9.6479 9.6420	9.979x 9.9843 9.9878	9'9502 9'9522 9'9535	9.4806 9.4221 9.3671	9n5270 9n5702	9.9739 9.9677	71'3 75'5	+ 30 126 57	+ 45 23	(+ 5) (-8 - 31 + +131 - +147 +	56 + 39 -	- 42 r + 16 t + 4 r - 23 r
7317 7318 7319	280 07 100 95 253 53		9 · 7075 9 · 7631 2 9 · 7658	250.05 282.75	92.05 87.57 93.16	9'5576 9'5689	9 9965 9 9977 9 9985	9.9587 9.9697 9.9607	9,1025 9,10636 8,9152	9.5980 9.5349 9.5999	9.9629 9.9625	97 · 9 97 · 1 84 · 9	81/4/1901 88/4/190 91/4/8/0	+ 19	29 +	9 -+ 22 -	+ 37   t   p   p   p   p   p   p   p   p   p
7322 7323 7324	56.77 56.77	-0.2637 -0.1824 -0.4816	9.7402 19.7161 19.7618	55°17 225°83	86.77 86.74 86.75	9.5319	9.9890	9	9 · 2702 9 · 3468 1 9 · 3669	9'4546 9#3841 9'3622	9 9816 9 9869 9 9882	78.8	+110 118 88	+ 4 + 3 - 41	- 58 - - 30 -	80 -+ 173 - 32 113 - 25 -+ 11 - 16 31 - 24 7 -	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
7327 7328 7329	282'97 74'23 323'85	-1.4250 -1.1840 -1.2285 -0.7728	9.7649 9.7129 9.7327	30'52	87 · 24 88 · 17	9'5043 9'49'5	9 · 98 34 9 · 98 06	9 9 9 7 6 6 5 9 9 7 8 6 5 9 9 7 8 8	9 4334 9 4654 2 9 4661	9,2271	9 9937 9 9 9976 9 9 9978	74.0	32		+ 30 +	48 + 95 46 + 33	p p p p p r r t
7333 7334	23 08	-0'523'	9'7588	126 2	93.5	9 5310	0.001	9 975: 7 9 973:	2 9 · 350: 3 9 n 285:	2 9 4460	5 9 · 9823	lor	5 +118	5u	19 -	6 + 25 10 +163 54 + 50 61 - 68	~4 /
7337 7338 7339	344'04 7'23 218'6)	-1.196 +1.504 3 +0.86 5 -0.456 4 -0.185	9 7359 2 9 7594 2 9 7047	256.7	92.83 987.83	9 550 9 609 9 6 617	5 9 1 9 9 5 6 5 9 1 9 9 8 6	5 9 · 970 4 9 · 960 1 0 · 959	8 9n 152 7 8n 93 1 2 9 ' 067	6 9 · 5 · 2 · 2 · 3 · 5 · 5 · 9 · 5 · 9 · 5 · 9 · 5 · 9 · 5 · 9 · 5 · 9 · 5 · 9 · 6 · 6 · 6 · 6 · 6 · 6 · 6 · 6 · 6	6 9 9757 9 9 9626 9 9 9627	98' 95' 7 82'	5 3 44 7 93	- 31	1 143	36 + 41 4 - 163 12 - 178	- 18 <i>1</i>
7342 7343 7344	234 2	5 +0.307 3 -0.506 2 +1.050 6 -1.260 -0.837	7 9 · 7489 7 9 · 7342 7 9 · 7213	235'1 251'6 225'2	7 84 5 6 84 · I 7 83 · 5	2 9 641 1 9 646 7 9 653	5 9 · 987 2 9 · 985 5 9 · 979	99.953 39.952 79.950	7 9n366 7 9 408 8 9n474	1 9n569 5 9 557 8 9n528	9 9 9 9 6 9 7 9 9 9 6 9 9 9 9 6 7	8 104' 7 74' 8 108'	5 —173 1 — 5 —		5 -104 -	41 -156 53 - 13 60 + 40	+ 27 7 - 41 7 - 2 - 30
7347 7348 7349	278.70 16.0	8 +0 244	1 9 761; 0 9 719; 3 9 739;	5 11'5 7 184'2 5 3'9	6 86 · 6 6 88 · 6 6 88 · 7	9 684 8 9 687 8 9 686	7 9 945 3 9 94 1 1 9 942	5 9 9 9 4 2 7 9 9 4 1 0 9 9 4 1	1 9 673 2 92685 6 9 684	2 9 041 7 82616 8 8 584	8 9 · 997 4 9 · 999 9 9 · 999	4 61. 6 119. 6 61.	7 + 22 0 - 77 0 +171	- 3 + 4 +	$     \begin{array}{ccccccccccccccccccccccccccccccccc$	- + 85 + 148 + 46 + 47 - 46 33 - 85	+ 67 r
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			<u>-</u>											
7351 7352 7353 7354 7355	- TYT	2406 841 2406 870 2407 018	8 16.0 8 18.2	313'416	+1.31 +3.49	23	164°184 194°178 350°453	16°535 164'504 193'364 349'313 174'952	0.6899 0.6915 0.410	9.7645 9.7630	8 · 7 · 36 8 · 7594 8 · 7584 8 · 7090 8 · 7466	0.5666 0.5315 0.5339 0.5729 0.5385	7 · 6722 7 · 6641 7 · 6668 7 · 6761 7 · 6634	0 1434 0 1233 0,0782 9,9586 9 7955
7356 7357 7358 7359 7360	1879 VII 19 1880 I 11 1880 VII 7	2407 372 1 2407 550 2407 726 2 2407 904 1 2408 052	9 5.5 22 40.2 13 21.2	116.275 291.129	+1.48 +2.04 +1.16	23'451 23'451 23'451	181'541 5'913 189'828	355.619 183.826 3.956 190.741 343.174	o:7258 o:6990 o:7427	9.7270 9.7253 9.7528 9.7046 9.7604	8·7272 8·7238 8·7506 8·7074 8·7577	0.5599 0.5528 0.5451 0.5644 0.5404	7.6768 7.6629 7.6772 7.6627 7.6763	9n 2630 9n 1533 9 7098 9n 9728 on 1812
7361 7362 7363 7364 7365	1881 V 27 1881 XI 21 1882 V 17	2408 228 2	23 36'2 16 21'2 7 33'7	66 · 744 239 · 546 56 · 262	-0.77 -3.49 -0.97	23 '450 23 '450 23 '449	167.879 349.950 176.344	13.806 166.060 352.370 173.909 359.633	0'7352 0'7118 0'7130	9°7138 9°7394	8.7613 8.7147 8.7379 8.7365 8.7155	0'5390 0'5600 0'5520 0'5457 0'5669	7 · 6773 7 · 6640 7 · 6754 7 · 6648 7 · 6744	0'0637 0'0554 9n9515 9'5155 9n3163
7366 7367 7368 7369 7370	1883 X 30 1884 III 27 1884 IV 25	2409 292 1	23 57'4 5 48'9 14 58'0		-4.08 +1.33 -0.24	23 448 23 448 23 448	5°206 162°926	5 280 164 756 194 277	o 7448 o 6988	9'7001 9'7547 9'7526	8.7562 8.7661 8.7514 8.7584 8.7145	0'5346 0'5734 0'5405 0'5343 0'5660	7·6658 7·6732 7·6706 7·6670 7·6720	9n6272 9'7004 0'1646 0n0553 0'0745
737± 7372 7373 7374 7375	1886 III 5 1886 VIII 29	2409 793 2 2409 971 2 2410 148 1	20 43'4 22 4'4 12 54'I	166.316 345.291 156.065	一0'67 +2'88 +0'19	23 448 23 447 23 447	350.732 128.022	173'572 348'201 180'191 358'575 185'571	0'7022 0'7405 0'6901	9.7515 9.7053 9.7643	8.7286 8.7480 8.7100 8.7602 8.7072	0.5558 0.5404 0.5704 0.5325 0.5733	7.6719 7.6670 7.6732 7.6658 7.6744	9.9054 9.9296 8.9909 9.0319 9.7802
7376 7377 7378 7379 7380	1888 II 11 1888 VII 9 1888 VIII 7	2410 828 2410 857 1	6 16.7	322 '747 107 '400 135 '596	+3.63 +1.24 +1.35	23'448	346°196 15°928	9'117 191'573 348'248 18'339 168'453	0'7319	9.7208	8.7512 8.7220 8.7181 8.7292 8.7559	0.5628 0.5569 0.5500	7.6648 7.6754 7.6627 7.6640 7.6773	9'7994 0n1024 0n1074 0'1571 9'9355
7382 7383 7384	18go VI 17 18go XII 12	2411 536	9 58 3	86'110	-0.25 +0.15 -1.56	23 450	177 759 2 346 185 681	178'470 0'860 187'971	0.2388	9.7625 9.7093 9.7454	8 7601 8 7112 8 7434	0.2382	7.6772 7.6629 7.6768	9n7361 9'2800 9'3487 9n6994 9'9882
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7355	145'2	2 +0.62	44 9	7534	138.88	96.68	9 6594	9'9757	9'9493	925130	9.5047	9.9766	110.1	+118	+ 54	-139	+ 60	- 70	+ 18	
7356	355'5	1 -0.18	32 9	7292	315:12	96150	9 6554	9'9792	9'9502	9.4796	925276	9 9 9 7 3 8	71.3	- 6g	- 27	+ 6	- 31	- - 64	8	٠,
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7370	188.0	7 +1,18	370 9	.4138	211.02	87.20	9.2023	9.0841	9'9769	92 4242	9112423	9.8833	105.6		************	_		-	. *******	p
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7422 7423 7424	• 1906 71907 71907 71908 1908	VII 10 I 3	2417 5 2417 7 2417 9	90 5 67 15 44 21	57'1 16'7 44'2	146 115 292 934 107 197 282 146 96 528	+1.00 +1.00	23'446 23'445 23'446	353'422	17 '535 168 '493 353 '705 178 '525 359 '864	0.7448	9.7589	8.7565 8.7556 8.7599	0'5515 0'5416 0'5660 0'5399 0'5610	7.6627	9.136 9.2896 9.136
7427 7428 7429	†1908 †1909 †1909	VI 17 XII 12 V o	2418 4 2418 5 2418 8	75 23 53 19 01 5	28'8 59'1 33'4	86.082 260.186 47.711	+0.12 -1.26 -0.62	23'447 23'448 23'448	9 928 193 438 348 825	187 · 946 7 · 485 195 · 487 348 · 248 168 · 299	0.7168	9.7357 9.7169 9.7639	8.7325 8.7189 8.7592	0'5470 0'5658 0'5327	7.6772 7.6629 7.6768 7.6657 7.6734	9.951 0.094 9.1975
7432 7433 7434	↓1911 ↓1911 ≠1912 ≱1912 _≠ 1913	X 22 IV 17 X 10	2419 3 2419 5	32 4 10 11 86 13	39 · 8 40 · 7	207 043 27 084 196 880	-3'81 -0'10 -3'23	23 449 23 449 23 449	5.816	182 453	0.4140	9 7200 9 7345 9 747	8 7323 8 7442	0.2202	7.668x 7.6708	9.720 9.720
7437 7438 7439	-1913. 41914	IX 30 II 25 VIII 21	2420 O	41 4 89 0 66 12	55.6 26.9	186 422 335 557	-2 · 45 +3 · 35 +0 · 78	23 449 23 449 23 449	193'016 350'052 171'257	163'277 192'459 348'726 173'494 355'334	0.6902 0.7396 0.7049	9'7635 9'7060 9'7483	8.7594 8.7101 8.7441	0'5350	7.6742	9n974 9'884
7442 7443 7444	+1916 +1916	II 3 VII 30 XII 24	2420 8 2421 0 2421 2	97 16 75 2 22 20	15.2 31.9	313 520 126 566 272 743	+3 47 +1 56 -0 05	23'447 23'447 23'446	5'764 188'017 341'812	182.035 3.942 188.713 343.209 13.901	0'6970 0'7436 0'6934	9'7550 9'7589	8.7523 8.7562 8.7562	0.5554 0.5433 0.5656 0.5417 0.5388	7 6634	9.696 9n886 0n185
7447 7448 7449	#1917  -   1918	XII 14 VI 8	2421 4 2421 5 2421 7	29 3 77 9 53 22	0.6 17.7 3.2	115'859 261'835 77'279	+1'50 -1'38 -0'32	23'446 23'446 23'445	195'979 349'744 174'743	164 · 181 194 · 740 352 · 179 172 · 358 359 · 130	0,7410	9'7069 9'7365 9'7431	8 · 709 I 8 · 7354 8 · 7392	0.5634 0.5544	7 6768	9n962 9.670
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2.11.	٠,-	,		<u>.</u>	<b></b>	$\sin g$	sin k	$\cos g$	cos k	sin δ'	cos o'		<u> </u>	φ	λ	φ	λ	φ	
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		-o.8537											-170	39	120	- 42	- 92	<b>— 6</b> 4	,.
7403	157.31	-1.5250	9.7657	302.00	95'49	9'6412	9.9878	9.9538	9.3687	9115683	9.9680	75 4		_			*****	_	p p
		+1.2112 -0.9076											+ 49	- 55	+162	- 87	- 76	- 5,9	$r \mid r$
7406	44.30	+0.3963	9'7436	78.97	88.21	9 5702	9,9990	9 9677	8.8208	9.5632	9.9688	85 19	-117	+ 18	- 45	+ 45	+ 32		
7408	264 54	0'2262 0'3609 0'4744	9.7636	67.61	87.40	9.5514	9.9964	9 9 9 7 0 6	0,1008	9:5213	9.9746	82.5	1 40	- 27	+ 97	- 2	十135	- 18 - 13 + 17	t*
		-1.2030														-			p
7411	159'49	-1.0820	9.7639 9.750	55.63	86 · 75	9'5347 9'5174	9 · 9924 o · 088 <b>6</b>	9'9729 9'9751	9 · 2676	9'4597	9'9812	78°9		<u> </u>	prosted	-	_		p p
7413	202'61	+0.8428 -0.8988	9.7299	8 ' 92	89.09	9 4862	9'9793	9'9787	9.4804	8.6974	9'9995	72.4	-l- 8o		+150 +101	+ б <u>5</u> - 70	-117 +179	+ 75 82	rili t
7415	262 94	+0.1320	9.4069	355'27	90'48	9 4826	9.9791	9 ' 9789	9.4809	824195	9.9958	72.4			- <del> </del> - 96	+ 6	+×57	+ 25	2***
7417	255'34	-0'1642	9.7043	341'33	91.80	9'4886	9,9809	9.9784	9.4628	910132	9'9977	73'0	+ 31	52	+110	5 43		- 27 - 18	
7418 7419	16.23 202.20	+0.2690	9.7564 9.7242	327'92	92.82	9 · 5002 9 · 5030	9'9831 9'9841	9'9771 9'9771	9n4371	9,2010 9,2445	9 9945	74°3		+ 50 —	- 12	+ 45	+ 55	+ 18 	$\left egin{array}{c} t^{**} \ p \end{array} ight $
		-1.3622												_					P
7422	269.27	- -x : 37×7 - -o : 8644	9,4610	280'88	91'48	9.5708	0,0000	9.9676	8 8 1 5 2	915640	9.9682	86.0	+ 42				+131		
7424	145'46	-0.1360 -0.1360 -0.1360	9.7642	268.80	89 '82	9'5901	0,0000	9.9643	718745	925900	9 9 9 5 4 3	90.2	+154	+ 11	- 50 -145 - 67		85		tife
7427	169.63	-0'4964 -0'8937 -1'2437	9'7378	72'07	87.08	9'6168	919970	9'959 x	9.0678	9'5988	9.9627	82.7	+ 82	- 23 + 50		- 53 + 88		— 32 + 60	
7429	266'61	-0.0424 -1.0637	9.7659	.36'36	83.58	9.6638	9 * 9 7 0 8	9'9481	9'5501	9'4689	9'9803	68'2	(+111)	l	il	_	+156	- 46	
		-0'2309						١.						_ 37	Y 5 5		- 00	<b>+- 11</b>	t
7432	247'01	+0.3249 +0.5256	9'7221	200'15	84.69	g'68or	9'9529	9'9435	926452	9n2663	9'9925	116'7	-⊦ 6x	+ 45	II8	十 II	+178 + 89	8	3.44
7434	27.29	-0'4130 +1'3130	9.7492	192'16	86.45	9.6844	9'9459	9'9422	926716	9n 0627	9'9971	118.3	- 93	+ 4	— 33 —	35	+ 47	- 52 	
7436	133,10	+1'4530	g 7658	163'76	94.44	9.6791	0.0500	9 ' 9438	926565	9.1770	9 995	117.3							p
7437	253.63	-1.0985 -0.9438	9.7655	184'62	88.60	9 6848	9 9426	9 942	9n6830	82 6484	9.9996	118.8	<b>1</b> —	— (—78)		_	_ _ 91	- 43	p
7439 7440		+0.7668															+ 70 + 175	1.	•
7441	161.24	0.0142	9.7241	147'93	96 - 66	9 6699	9.9658	9 . 946	925815	9'4320	9.9835	113'3	+130	+ 23					1474
7442 7443	56 '80 209 '98	-+0:4975 0:7692	9'757I 9'7053	324'87 138'98	96.75	9 6665 9 6599	9 9692 9 9755	9 947	9.5603	9 1 4 6 0 2 2 9 1 5 0 4 6	9 9766	67.7	-122 + 89	+ 7		16	— 10 +179		r
		-1.2337 -1.1492												_		,,,,,,,,,	_	-	p p
7446	18.03	+1:2877	9'7189	101'14	91.78	9'6064	9 . 9989	9'961;	8 1 8 5 4 9	9 ' 5 9 9 4	9 9626	94 5	<b>_</b>		_				p
7448	323'29	-1'5083 -0'9172 +0'4679	9.7386	275'37	90.83	9 5969	9.9997	9 963	8 531	3925953	9 9634	87'9	88		+ 38		II		1414
7450	53.08	-0.5404	9'7122	263.60	89.09	9.5769	9 9997	9.966	5 8n 591	9 5746	9 9670	92'	-1190	1	- 53		+ 15	-	1
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7452 7453 7454	1920 1920	V 29 XI 22 V 18 XI 10 IV 8	2422 28 2422 46	8 13 ^h 12 ^m 3 5 15 19.7 3 6 25.5 9 16 5.4 8 9 5.9	239 280 56 999 227 078	-3 52 -0 95 -4 02	23.444 23.444 23.443	4'703 192'019 12'067	193'134	0'7446 0'6933 0'7337	9.4612 9.6998	8 · 7576 8 · 7061 8 · 7568 8 · 7165 8 · 7260	0'5327 0'5749 0'5337 0'5662 0'5559	7'6640 7'6754 7'6648 7'6744 7'6693	9n4681 9.6562 0n0099 0.0518 9.9487
7456 7457 7458 7459	A1921  1922  1922  41923	X 1 III 28 IX 21	2422 96 2423 14 2423 31 2423 49	4 12 26 1 2 13 3 8 9 4 38 4 6 12 51 0 20 53 2	187 776 7 073 177 410 355 916	-2·56 +1·31 -1·64 +2·18	23'443 23'443 23'442	349 123 178 196 357 470 185 646	347 234 179 213 357 579 184 726	o.6998 o.7419 o.6898 o.7427	9'7042 9'7643 9'7028	8·7504 8·7605 8·7605 8·7078 8·7493	0.5695 0.5337 0.5710	7.6696 7.6707 7.6682 7.6720 7.6670	9n9736 9'2378 9n3326 9n7334 9'7102
7462 7463 7464	71924 V 71924 V	VII 31 III 30 I 24	2423 99 2424 02 2424 19	15 57 7 18 19 42 1 18 8 37 5 15 14 45 6 21 40 3	128 · 277 156 · 679 304 · 128	+3.00 +0.12 +1.22	23 ' 442 23 ' 442 23 ' 443 23 ' 443	344 445 14 411 169 806 352 506	345 354 16 773 168 521 352 680	0.7345 0.7235 0.6928 0.7449		8·7263 8·7573 8·7055	0'5589 0'5532 0'5410	7.6634 7.6658 7.6767 7.6630	0n0866 0n1609 0'1175 9'9386 9n8580
7465 7465 7465	⊁1927 ¥1927	VII 9 I 3 VI 29	2424 7 2424 8 2425 0	30 6 35 4 66 23 6 3 84 20 29 6 51 6 32 6 39 4 13 9	106.944 282.487 96.522	+1.72 +1.11 +0.72	23 444 23 444 23 44 23 44	0°538 185°576 9°957 5 193°356	195'347	0.7317	9'7119 9'7427 9'7376 9'7155	8.7131 8.7342 8.7181	0.5604 0.5510 0.5458 0.5668	7.6627 7.6627 7.6627 7.6772	9.2988 8.7075 9.6937 9.9103 0.0933
7473 7473	1 1928 2 1928 3 1928 4 1929 5 1929	VI 17 XI 12 V 9 XI 1	2425 4 2425 5 2425 7 2425 9	86 13 14 2 15 20 41 3 63 9 35 9 41 6 8 3 17 12 0 6	86.366 229.77 48.126 218.585	+0.18 -3.95 -0.92 -4.08	23'44 23'44 23'44 23'44	5 176 177 6 356 63 6 168 59 77 808	347 645 3 16 349 5 167 912 7 358 290 4 173 967	0.6949 0.7431 0.6968 7.0.7275	9.7597 9.7017 9.7570 9.7212	8.7545 8.7070 8.7528 8.7220	0'5337 0'5733 0'5366 0'5613	7'6745 7'6657 7'6733	0.0032 0.1785 0.0371 9.4631 9.5497
747 747 747 748	6 /1930 7 /1930 8 /1931 9 /1931 0 /1931	X 21 IV 18 IX 12 X 11	2426 2 3 2426 4 2 2426 5 2 2426 6	95 19 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	2 207 776 5 27 04: 8 168 44: 1 197 25	-3.83 -0.10 -0.84 -3.26	23'44 23'44 23'44	6 184.30 6 13.38 6 162.00 6 192.54	3 182 118 3 14 78: 0 162 74: 7 192 11	2 0 7388 2 0 6904 8 0 6897	9 7484 9 708x 9 7634 9 7637	8'7454 8'7109 8'7588 8'7599	0.5657	7.6721 7.6682 7.6671 7.6707	9n5770 0'1013 0'1785 0n0246
748 748 748 748	3 &1933 4 = 1933 5 &1934	VIII 31 II 22 VIII 21 II 12	2425 g 4 2427 g 2427 g 4 2427 g	28 12 44° 06 5 49° 83 0 43°	3 158 16 2 335 47 1 147 71 9 324 64	7 +0.04 4 +3.32 4 +0.78 7 +3.59	23'44 23'44 3 23'44 0 23'44	6 357.56 7 179.05 6 5 62	1 172 82 1 355 12 1 181 18 9 3 88	6 0 7002 6 0 7296 x 0 6962	9 7316 9 7316 9 7566	8 730 8 730 8 753	7 0.555	7 6743	9 9 3 4 5 3 8 · 9 4 6 6 9 · 6 8 5 7
748 748 748 749	7 /1935 8 H1935 9 +1935 0 /1935	VI 3	5 2427 8 3 2427 8 0 2427 9 0 2428 9	660 8 46° 5 21° 337 16 27° 984 19 44° 9 33°	1 283'95 8 313'92 8 98'07 4 126'29	3 +1 2 2 4 2 9 +3 4 2 4 0 · 8 3 5 +1 · 5 2	7 23'44 7 23'44 8 23'44 7 23'44	16 341'76 15 15'26 15 195'08	8 343 24 5 13 91 5 163 22 2 193 74	8 0.694 5 0.689 3 0.731 8 0.740	1 9.404 3 9.423 3 9.423	8 755 5 8 760 3 8 7 8 8 8 709	8 0.238	2 7.6773 5 7.6762 8 7.6622 1 7.6633	0 0 1875 0 0 0578 0 0 1351 0 0 1533
749 749 749 749		VI I VI XII	9 2428 3 2428 8 2428 2 2428	162 17 49 1339 5 15 15 15 15 15 15 15 15 15 15 15 15 1	2 87 72 6 261 81 4 77 60 5 250 37	8 +0:20 0 -1:3 8 -0:2 9 -2:6	5 23 44 9 23 44 9 23 44 2 23 4	14 173 89 13 357 34 13 182 61 12 4 53	06 171.54 17 358.94 16 181.69 16 4.28	7 0'708 1 0'737 7 0'691 1 0'744	7 9'744 1 9'709 9 9'762 4 9'699	7 8 740 0 8 712 9 8 758 7 8 706	0 0 541 9 0 570 0 0 532	8 7.6624 4 7.676 0 7.663 4 7.676	9'7333 9n4004 9n3492 9'6403
749 749 749	6 /1938 97 /1938 8 /1939 99 /1939 90 /1940	XI 2 IV 1 X 1	2 2429 9 2429 2 2429	346 14 0 3225 0 5 373 16 35 5 5 49 20 30 5 727 20 18 5	3 239 03 2 28 72 3 198 60	2 -3.5 0 -0.2 9 -3.3	4 23 4 1 23 4 5 23 4	42   11'80 41   169'7 <i>4</i> 41   348'6 <i>7</i>	55 9:89 17 172:04 77 846:87	6   0 ' 7 3 2  8   0 ' 7 2 5  2   0 ' 6 9 8	5 9 7 5 4 9 7 2 5 6 9 7 5 4	0 8:717 2 8:724 6 8:751	76 0.566 18 0.555 17 0.540	0 7.675	4 0'0434 0 9'9737 9 9n9896

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N	r.	μ	γ	$\log n$	G	K	$\log \sin g$	$\log \sin k$	$\log \cos g$	log cos k	log sinδ'	log cos∂′	N'	bei ⊙ A gang λ	φ	im Mit	φ	bei ( Unterg \(\lambda\)	O gang φ	F
7.7	452 453 454	52'08 274'77 62'14	-0.293 -0.453 -1.023 -1.126 -1.126	0 9 . 7 6 3 2 7 9 . 7 6 3 2	251.00 67.73	87'69 9 87'39 9	9'5553 9'5530	9'9974 9'9965	9'9700 9'9703	9n0409 9'1059	925340 9:5233	9 9730 9 9743 9 0801	96.7 82.2	-ro3 -	- 31 -	- 50 -	+_7	+_4	+ 19 - -	$\frac{r^*}{p}$
7 7 7 7	456 457 458	11.48 15.16 251.78	-0'941 +0'172 -0'215 -0'541 +0'513	9 · 7557 9 9 · 7664 2 0 · 7664	189.56 8.82 176.79	89'01 89'11	9 · 4895 9 · 4836 9 · 4852	9'9790 9'9798 9'9788	9'9783 9'9783 9'9787	9n4828 9'4780 9n4844	8n7310 8.6901 8.2547	9'9994 9'9995 9'9999	72'5 107'8	- 97 - - 76 - + 43 -	- 52 - 8 - 5	- 19 - 17 +106 - 4	- 84 + 13 - 12 - 36	+126 + 47 +173 + 57	- 86 + 27 - 30 - 15	t r* t*
7 7 7	462 463 464	118 °0; 305 °7; 40 °5;	5 -1 · 220 -1 · 448 3 +1 · 310 4 -1 · 0 · 868 5 -0 · 721	3 9 . 7 17 2 7 9 . 7 2 9 8	3 151.63 3 293.39	92.63 92.63	9'5431 9'5028 9'5505	9'9946 9'9828 9'9961	9.9768	9n 1941 9n 4417 5 9: 1243	9.4945 9.1973 9.5176	9 9777 9 9945 9 9750	99.5 81.9 95.6	- 95 +162	- 37	148	- 26	-100		r
7 7 7	467 468 469	165'1 124'8 275'0	+0'199 +0'051 -0'494 -+0'813 -1'239	0 9 7 7 4 0 9 7 7 4 4 4 9 7 7 3 9	93'88 8 269'28 7 82'92	8 90 · 56 8 89 · 89 8 88 · 89	9.5813 9.5893 9.5998	9'9996 9'9999	9 · 9659 9 · 9649 5 9 · 962	8n 3772 5 7n 6526 6 8 · 6535	9 ' 5804 9 n 5893 5 9 ' 5979	9 9660 9 9631 9 9631	90°3	+ 21 +132 +156 - 16	+ 4	165 125	+ 25 - 52	-104 - 46	+ J - 27 + 51	r-t t* p
.	7472 7473	331'1 273'7	6 1 · 0 0 7 3 1 · 5 0 8 1 1 · 0 8 2 0 · 2 9 2 0 · 3 5 4	3 9 . 761 2 9 . 761	6 72 8: 8 217 9: 1 36 5	3 87 21 2 83 24 4 83 24	9.6155 9.6633	9 9973 9 972 8 9 970	3 9 959 3 9 948 8 9 947	5 9 · 0482 2 9 · 5392 8 9 · 5498	2 9 · 5989 2 9 · 4718	9 9 9 5 6 2 7 5 9 9 9 7 8 5 8 9 9 8 6 6	83.0 111.	+ 35	 37	_ _ + 89			- 4	<i>P p t</i> ★ <i>r</i> **
	7477 7478 7479 7480	149'6 191'6 16'8	60 · 47 · 40 · 37 · 3 1 · 50 · 5 · 5 · 5 · 5 · 5 · 5 · 5 · 5 ·	76 9 . 750 33 9 . 765 32 9 . 765	5 200 · 2 1 19 · 8 3 171 · 6 7 192 · 4	7 84 · 68 0 84 · 81 2 92 · 47 9 86 · 40	9.6790 9.6788 9.682	9'953 9'952 9'944 9'946	19'943 99'943 69'942 79'942	6 9n 644; 9 9 645 8 9n 676 8 9n 669	3 9 2 2 5 7 4 1 8 9 9 1 4 1 9 1 9 1 9 1 9 1 9 1 9 1 9 1 9	9 9 9 9 2 8 4 9 9 9 9 8 6 9 9 9 9 7 9	2 118. 2 118. 3 63.	3 4		-155  	- 36  -	— 72   —   —   —		
	7482 7483	8'3	5 -0'969 9 +0'833 4 -0'22 3 +0'08 3 +0'48	24 9 748 24 9 733	7 342 1	9 94 85	0.681	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	7 9 943	19'654	2 9 2 2 7	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	62'	8 — 79 8 + 24	- 39 + 30	- 5 + 94	+ 78 - 24 + 18	+150 -137	+ 28 + 12 - 20 + 52	t*  1
	748 748	7 262 '8 8 60 6	8 -0 '68 3 -1 '54 55 +1 '14 1 +1 '36 72 -1 '42	00 9 . 760 23 9 . 765	2 297 · 5 5 324 · 9	9 94 46 9 96 69	9 630 9 665 6 622	6 9 992 0 9 969 4 9 995	0 9 9 9 5 9 4 9 9 4 7 5 9 9 5 8	8 9 · 559 8 1 9 <i>n</i> 155	8 9n 457 3 9 595	3 9 9 9 9 3 5 9 9 9 9 4	4 67 4 98 4 110	7 — 9 — —						(p) p p
	749 749	2 259 '9 3 173 '	060 · 92 07 +0 · 54 0 · 25 0 · 22 07 +0 · 43	11 9 '74' 14 9 '71	58 101 4 12 275 6	7 91 . 84 34 90 . 81	4 9 606 8 9 597	8 9 998 0 9 999 4 0 000	8 9 · 96	(2 8 n 8 0 7 3 1 8 · 5 5 2 4 5   7 n 7 2 2	9 9 599 5 9n595 3 9 589	4 9 963 4 9 964	6 94° 4 87° 5 90°	0 +135 6 + 16 8 +118 3 +169 5 +139	+ 34 - 15	+101 -173 -131	+ 5 + 3 + 1	B — 10 D — 7 4 — 11	7 — 1 1 — 1 5 + 2	6 t* 1. 2 t* 2 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.
	749 749	7 181 '	34 -0 °95 72 +1 °10 53 +0 °94 41 -0 °97 83 +0 °22	50 9 717 12 9 727	71 250 4 73 35 1	2 87 ' 6   9 87 ' 6   7 87 ' 8	3 9 555 3 9 505	6 9 99 6 9 98	2 9 97 3 9 97 4 9 97	$559^{\circ}409$	97 9°281 78 9n 103	4 9 991 6 9 996	9 74 5 106	8 -167	+ 5 - 6	- 4 - 79 0 -	+ 8	2 + 1 8 + 7 (+ 7 o - 6	6 + 7 2) (-82	$\begin{cases} p \\ r * \\ t \end{cases}$
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	Nr.		T		L'	Z	. &	P	Q	$\log p$	$\log \Delta L$	$\log q$	$u'_a$	$\log f_a$	$\log\gamma$
		Greg. Kalender	Julian. Tag	Welt- Zeit			,								
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	7537 7538 7539 7540	1956 VI 8 1956 XII 2 1957 IV 29 1957 X 23	2435 633 21 2435 810 8 2435 958 23 2436 135 4	30 0 3 12 5 3 54 8	78 ° 026 250 ° 140 39 ° 380	-0.26 -2.66 -0.70	23'439 23'439 23'439	11'720	191.783 9.686	0'7314	9'7597 9'7162	8 7551 8 7186 8 7222	0'5338	7.6633 7.6762 7.6667	9.6277 9n9500 0.0370 0.0007 0n0023
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	7548 7549	1960 IX 20 K1961 II 15 K1961 VIU 11 1962 II 5 1962 VII 31	2437 523 IO 2437 701 G	35'9	320.417 138.508 315.716	+-3.50 1.29 	23'438	359 753 359 753	168:478 350:696	0'6918	9.7610 9.7016	8'7239' 8'7584 8'7056 8'7583 8'7151	0'5394 0'5671 0'5401	7'6752 7'6641	9 3283
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761 761	5 1992 VI 30 7 1992 XII 24 8 1993 V 27 9 1993 XI 13 1994 V 10	2448 981 0 43 2449 129 14 7 3 2449 305 21 34	3 272 463 6 60 528 0 231 522	-0.88	23 435 23 435 23 434	11.544 167.673 347.779	190'298 9'396 169'820 346'220 176'311	0'7292 0'7295 0'6955	9'7574	8 · 7206 8 · 7205	0.2413		9n8743 0'0284 0'0567 0n0192 9'6137
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764 764 764 764 764	12 2004 IV 1 13 2004 X 1 14 2005 IV	8 2453 469 20 3	1'4 29'81 8'3 201'09 2'2 19'09	7 -0:25 9 -3:50 9 +0:43	23 43 23 43 23 43	5 347.87 7 168.29 7 356.08	4 346 125 7 170 721 9 353 648	0'7357	9.7123 9.7405 9.7381	8 · 7140 8 · 7356	0'5632	7.6679 7.6692	0.0161
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7601	7.40006	1.7.069#	A 1 # 0 # 0	4 0	00000		-1-0-0											
7602	36.24	+1:0685 0:9764 1:0857	9'7659	218.39	83.58	9.0822 9.0833	9'9729	9'9486	925347	9n4849	9 9787	III.I	-146 - 52			(+154)	— (—70)	$r_t^p$
7504	100,18		9'7442	187.38	87.78	9 6850 9 6861	9'9434	9'9420	9n 6803	818507	9 ' 9989	118'7	(- 26)(+66)				+ 56	p
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7607	207.65	+o'4163	9.7609	358 35	90,21	g ' 6867	9'9415	9'9414	9.6864	822036	9 ' 9999	60,0	+ 68 + 46 + 86 - 4 + 44 + 1	-146	+ 28	-143		$t^{*}$
7609	89'41	+1.0962 -1.1893	9.7647	350'72	92'74	9 ' 6833	9'9447	9'9425	9'6759	829464	9'9983	61.6			- 28 -	r65 	— <u>5</u> 6	$p \mid p$
									ŀ		,		(+ 74)(-71)					p
7612	223'91	-1-0.7633	9'7514	135.11	96.53	9.6503	9 9822	9'9517	924489	9'5411	9.9721	107'4	+ 24 + 50 + 109 - 30	+142	+ 73 - 38	- 7 -139 -114		$t^{ili}$
7614	105'25	o'0013	9.7663	122'89	95'23	9.6387	9.9893	9'9544	913405	9'5753	g <b>'</b> g <b>6</b> 6g	103'7	-175 + 13 +137 + 11	105	22	- 46	- 13 - 33	$t^{*}$
		0.7487						1			'							t
7617 7618	35.96 35.96	十1'0675 十1'1395	9'7208 9'7229	286 53 72 00	92 · 68	9'6146 9'5585	9'9975	9'9597 9'9696	9'0314	9n5992 9'5394	9'9627	83.8	Passed Passed	5	- 26 -	+ 39	5 x	p p
7619	150.04	-1.0452 -0.4109	9'7594	241 54	86.88	9'5430	9'9945	9.84x8	911991	924932	9.9779	99.6		 81	- + 42		 -+ 32	p rii
7621	28.93	0.3557	9.7653	229 64	86'70	9'5233	0,0003	9'9743	923193	9n4157	9.9847	102'5	- 97 - 8			+ 47	— 32	t
7622 7623	83.74 252.20	0:3345 0:3488	9'70 <b>9</b> 0 9'7 <b>49</b> 6	47'54	86'73	9'5189 9'5189	9'9896 9'9858	9.9748	9'3341	9'3979 9n3025	9,8820	77.1	-137 - 31 + 51 + 34	82	6	- 23 +172	6 + 5	1. Life
7624	159'43	-1.0245	9.7326	34.21	87.06	9 5050	9'9849	9.9762	9'4132	9'2739	9.9922	74'7		\$17mm4		_	_	p p
7626	198'51	+o.8212	9'7644	345 86	91'43	9 ' 49 0 5	9.9796	9.8481	9.4757	8 _n 8990	9.9986	72.2	+ 87 49	+154	7x	-159	+ 83	tik
7628	79'16	-1'0390 +0'2416	9'76r6	332'78	92'49	9.4968	9'9828	9'9775	9'4409	921747	9 9951	73 8	-144 - 2	 		1	+ 30	
7630	275'I5	0'4702	9.7194	319.88	93'08	0,2100 0,2028	9.9869	9.9758	913934	9,3139	0.080e	75.6	+ 87 - I + 8 - 41		- 4 - 41		- 29 - 13	r
7631	344'46	0.20	9'7459	129.20	93,30	9 5246	9'9905	9'9742	913124	9.4221	9 9843	102.3	- 65 + 4I	+ 18	46	+ 87	+ 17	
7033	112.30	-1.2203 -1.2855 +1.2137	9.7667	87.33	89'59	9 5930	9,9999	19 9638	8.2253	9.5926	9'9639	89.0					_	p
7635	83 80	+1.1402	9.7057	260.49	88 49	9 5437	9.9992	9.9618	8n7842	925984	9.9628	93.8		_	_	_	_	p p
7636 7637	0.69	-0.5733	9'7546	76.25	87.78	9'6102	9'9983	9 9607	8 9489	9.5996	9'9627	84 4	- 50 - 37 +176 + 30	+ 1	12	+ 55	- 27	t 1***
7038	170.38	+0.1063	9'7288	65.72	86'04	9 6264	9.9944	9 9573	9'2043	9.5928	9 9639	80.0	+170 + 30 +121 + 1 - 2 - 4	-x77	+ 35	- 70 -105 +142	+ 20	71131
7640	242 83	+0.9920	9.7071	55 52	84 57	9 · 6408	9.9882	9.9539	9.3614	9'5707	9'9677	75 7	- 12 + 60			( <del>- 48</del> )		
7641 7642	165·62 23·80	-0'9607 -1'1373	9.7659	228:15	83.79	9.6501	9'9824	9 9517	924463	925424	9'9719	107.3	+ 84 - 51		1 -	(+ 11)	(70)	t p
7644	128 57	-0.3208	9'7426	13.40	85'71 86'05	9'6819	9 9486	9.9425	926617   0.6658	9n 1559	919955	117.6	+175 - 48	 124	— 16	 63	+ 7	p r-t
7645	340'75	+0.3339	9.7162	187.37	87.76	9 6867	9 9 4 2 9	9 9415	9n6820	818525	9 9989	118.8	- 39 + 48	+ 25	- <del> </del> - 18	+ 83	— ģ	
7047	350.95	0.4027	9'7030	179 53	90'15	0'6882	0'0410	0.0410	026882	7.6643	0.0000	110.5	- 37 - 6 - 60 + 5	+ 23 - 4	+ 29 - 27		+ 51 - 53	ያ# የ
7048 7649	215.99 8.24	-1.1212	9'7543	358.65	90'41	9 6849	9'9420	9 9420	9.6848 9.6793	8n1156	0.0000	118.6					_	$p \\ p$
7650	235'30	-0.9602	9.7314	328.32	96.61	9.6697	9.9655	9*9465	9 5835	914273	9,0839	66.6	(- 73)(-73)			-I.35	- 48	r
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7651 7652		VIII 1 1 26	2454 (		10 ^h 13'	"O I	29°536	+1°56		170°445	168°328 358'252		9.7508 9.7051	8·7464 8·7101	o'5389 o'5725	7:6635 7:6767	9'9212 9:4558
7653 7654 7655	2009 2010	VII 22 I 15 VII 11	2455 2455 2455	035	2 34 7 12	' 2 I	19'441 295'028	+1.59 +2.33 +1.37	23 43	179'138	178'807 3'457	0'6903 0'7432 0'6976	9.7644 9.7008 9.7568	8.7593 8.7071 8.7520	0'5351 0'5351		8.8656 9.5989 9n8297
7656 7657		VI 1	2455 2455		9 3 21 2			十1.10	23'43	166.867	168.952	0.7307	9'7194	8.7216	o'5643 o'5568	7.6638	o'0251 o'0851
7658 7659 7660	2011	VII 1 XI 25 V 20	2455 2455 2456	198	8 54 6 9 23 47	'5 2	242'614	+0'94 -3'30 -0'86	23'43	347'610	198.978 346.137 172.413	0.6945	9.7332 9.7582 9.7020	1	0.2482	)	0n1729 0n0241 g:6868
7661 7662	2013	XI 13 V 10	2456	423	0 29	.8	49 533	-3.30	23.43	182'793	356.281	0'7395	9.7628 9.7681 9.7460	8 · 7601 8 · 7108 8 · 7438		7.6746 7.6657 7.6734	9n5747 9n4251 9:5103
7663 7664 7665	2014	XI 3 IV 29 X 23	2456 2456 2456	777	б 14	. 5	38.867	-4.12 -0.66	23:43	0 101.010	188.273	0.4192	9.7322	8.7303	0.2211	7'6668	929984 0'0364
7666 7667 7668	2015	III 20 IX 13 III 9	2457 2457 2457	279	6 41	5	170'173	1.88 0.98	23'43	0 348'473	168 013 348 072 178 319	0'7444	9.7628 9.7616 9.7588		0'5689	7.6672	9'9768 010430 9'4217
766g	2016	IX I II 26	2457	633	9 3	3'9	159'360	-0.02	23'43	0 356 402	354'351 187'488	0.7314	9'7184	8.7188	0.2282	7.6660	9n5270 9n6577
7673 7673 7673	2018	VIII 21 II 15 VII 13		165	21 5	5 ' 5	327,132	3 +1 43 3 +1 43	23'43	1 192'86	2 583 194 501 344 167	0'7365	9.7098	8.7136	0.2600	7.6753 7.6628	0n0820 0n1328
767	' 1	VIII 11 6		342				5 +1.38	23'43	1 13'520		0.6016					
767 767	7 2019 8 2020	VII 2 XII 26 VI 21	2458 2459	844 022	5 I	1.3	90'35		23:43	1 175 43 2 1 26		0.7213	9.7280 9.7251	8.7283	0'5596	7.6772 7.6629	9.6204
767		XII 14 VI 10	2459	376	10 5	2 8	,	5 -o'rs	23.43		4 10:430	0.7427	9.7044	8 7073	0'5649	7.6633	9'9597
768 768	3 2022	IV 30 X 25	2459 2459	700 878	20 2 10 4	7 · 2 8 · 7	40'47 212'00	z -3 9	23,43	3 347 22 3 167 92	0 191'408 5 345'396 2 170'363	0'7348	9, 7389	8.7149	0'5505	7.6667	0:0310
768 .768	5 2023	IV 20 X 14	2460	232		5'1	201'12	6 -3 5	23.48	175'97	7 353 112	0.7349	9.7125	8.7146	0'5649		9.5788
768 768 768 768	7 2024 8 2025	IV 8 X 2 III 29 IX 21	2460 2460	586 764	ro 5	9°5 8°4	9,00	1 +0:40 5 -2:70 7 +1:10 3 -1:8	23'43	14 183 60 14 12 25	2 183 630 2 183 630	0'7445 0'6913	9'7007	8 · 7055 8 · 7582	0.2364	7 6692 7 6697 7 6706 7 6683	9n5404 0'0162
769	0 2026	II 17	2461	089	12	1.5	328 83	3 -1-3:4	3 23'48	349'25	1 351.630	0'7214	9.7280	8.7278	0.5585	7'6752	919900
769 769 769 769	2 2027 3 2027	VIII 12 VIII 2 VIII 2	2451 2461	443 620	15 5 10	5 ' 6 4 ' 8	317.62	3 +1 · 2 · 8 +3 · 4 · 9 +1 · 5 · 6 +3 · 1 ·	23'4	34 356 86 32 178 28	0 167 589 9 358 026 9 178 106 4 3 24	0 740 3 0 690	9.7045	8.7094	0'5720	5   7 · 6641 5   7 · 6635 7   7 · 6767	9n4756 9'1630
769	5 2028		2461	975	3	1.7	119.85	1 +1.6	23'4	32 186 g6	3 188 77	0 698	9.755	8 7508	0.232	7.6630	9117802
769 769 769	7 2029 8 2029	VI 12 VII 11 XII	2462	300	3 5	1, Q	81.48 109.63	9 -0.0 4 +1.3 4 -2.3	5 23 4 9 23 4	31 192.65 31 199.01	7 168 03 7 198 08 9 346 10	8 0'7326 4 0'720	9.7178	8 717	7 0'557 7 0'549	3 7.6633 4 7.6623 3 7.6763	0,1131
770		VI						1 -0.2	_		3 174'46			_ ,		7.6639	1
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7651 7652	333°83 296'59	+0.8340 -0.2856	9'7528	141°31	96°70	9'6612	9'9733 9'9753	9 9489 9 9489	9n5321 9'5154	9 * 4868 9 2 5 0 4 8	gʻg786 gʻg766	60.8	103 12	+ 68 35	+ 35 + 67		+114 +124	+ 34 + 3	
7553	217'16	+0.3911	9'7665	133.00	96'29	9'6516	9'9816	9'9513	924544	9.5395	9'9723	107.7	+ 71	+ 20	+143	+ 25	-158	- 13	t**
7655	112.04	-0.6757	9.7589	123'13	95 97	9 6387	9.9892	9 9523	9 4147	9:5742	9.8621	103.8	-171	— 26	-116	T 3	+122 - 71		
7656	311'58	十1.0202	0.7221	207.75	04.50	0.6318	0.0032	0.0461	0.2645	05872	0.0640	78.5				_			p
7657	139'54	-X'2165	9.7215	83.20	89.09	9:5777	9'9997	9.9665	8.5923	9'5754	9.9669	87.6		-	-		,		p
7659	278 ' 34	-1'4890	9'7602	254'05	87.96	9.5628	9,9981	g*g68g	829728	925480	9.9711	95'8			_				p p
7650	179,11	+0.4862	9.7042	72'13	87.79	9.5572	9.9976	9.9697	9'0167	9 5385	9'9724	83'6	- -109	+ 21	+179	+ 49	101	+ 33	2***
7661	156'74	-o:3756	9'7649	242'41	87.07	9.5425	919949	9.9719	921858	924957	9.9776	99'3	+133	I2	-158				-10
7663	15.83	-0.3338	9.7481	230'05	86.40	9.5238	9'9904	9'9742	923159	9,4187	9'9845	102'4	71	+ 30	14	+ 2 + 4			
7664 7665	271'59 150'07	-0.0822 -1.0822	9'7343	47'17	86.40 86.40	9 5205	9'9894 9'9856	9 9747	9.3388	9'3971	9,8860	77.0	(+120)	(73) 		_	+138	— 67 —	$\frac{r}{p}$
																:			
7667	284'59	1'1040	9'7037	167.83	91.55	9'4874	919796	9.9785	9114765	8.8317	0.0000	107.5		-		_			p
7668	206.41	+0.2641 -0.3365	9,4600	346'28	91'37	9'4873	9'9799	9.9785	9:4735	828828	9'9987	72.6	- - 88	2 3	+151	+ 12	145 100	+ 33 36	til r
		-0'4547											-114						
7671	95.66	+0'4331	9.7473	141.01	93'08	9.2081	g'g861	0.0761	923947	9.3128	9.9906	104'7	171	+ 39	- 93	+ 38	28	+ 11	t*
7672	129'43	-1.3577	9.4118	350.05	93,18	9.2121	9,0867	9.9756	9,3861	923340	919896	75 6							p p
7674	325.11	+1'1440	9.7650	130,53	93'33	9'5258	9,9903	9'9741	923205	9'4190	9'9845	102.2		-	_				p
7075	203.01	+1'1462	9 7000	272.47	90.30	9.2839	9.9999	9.9054	8.1833	915830	9.9055	89.1		Manage &					p
		-0'6504											160 + 48						
7678	279.54	+0.1123	9.7272	76.32	87.79	9.6100	9'9983	9.9606	8 9465	9 5995	9'9626	84 5	+ 18	+ 1	+ 80	- <del>-</del> 30	+147	+ 11	7*#
7679	64'55 340'65	-0.5301 -0.3114	9.7550	65.64	86.23	9.6215	9'9959	9.9583	9,1401	915964	9.9632	98'6	133 88		66 (165)				
				200176												( 0+)		6.	
7682	130.84	-0'9495 -1'1953	9.7127	30'35	83.21	9,6697	9.9642	9'9464	9.5907	9:4119	9'9850	66.2	- !	52		(	-137		p
7683	349 ° 02	-0'3992	9'7419	21.87	84'19	9.6762	9'9567	9'9446	926285 9.6369	9 29 54	0.0013	63.8	+ 64	- 48	+121	15	-179	+ 3	$\begin{bmatrix} p \\ t \end{bmatrix}$
		+0'3792															29	5	2***
7686	93.95	+0:3395	9.7627	14.02	86.00	9 · 683 r	9 9475	9 ' 9426	9.6662	9.1209	9.9962	62'1	-159	ε	99	+ 30	- 20	+ 47	$t^{:::}$
		-0'3471 												+ 5	-110	- 27	- 37	— 49 —	$\begin{vmatrix} r \\ p \end{vmatrix}$
7689	117107	-1'0607 -0'9772	9'7149	179'34	90.50	9.6867	9.9415	9'9415	926867	7.8038	0,0000	119'1		— (—72	\ <u> </u>	_	- + 99	- 50	p
						,													
7691 7692	85 12 56 30	+0'9016 -0'2989	9'7540	328.48	96 46	9'669g	9'9639	9 9464	925928	9'4074	9'9853	113.0	+113	十 75 30	(+105) - 52	(+85) 35	+ 6	+ 39	
7693	330.01	+0'1455 +0'3861	9'7666	141.81	96.74	9.6628	9.9726	9 9484	925369	9 4849	9.9788	111,3	- 44	+ 28	4 3r	+ 27	+ 91	— I2	$t^{*}$
7695	222 2	-0.2001 -0.6029	9'7577	132 87	96.30	9.6212	9'9814	9.822	9 5132	9.5377	9 9704	107 8	+ 76	- 18	+133	- rg	-179	- 50	
7606	75 579	+1.0207	0'7225	308.44	05'05	0.016469	0.0860	0.082	10:400	Onesa	0.000	7410						-	p
7697	241.30	+1:2975	9'7199	94'86	90'75	9'5961	9 9998	9 9633	814874	9'5947	9 9635	gre	)	_	-		_	-	p
7699	47.87	-1'4160 -1'0652	9 7608	266134	89:46	9 5826	9 9999	9 965	823538	925818	9 9658	gr	<b>1</b> 1 —	=	_	_		_	p
7700	277 47	+0.2660	9.7043	83.42	89.11	9 ' 5769	9.999	9 9666	815826	9'5747	9,3670	87'	+ 4	+ 30	+ 82	+ 57	+164	+ 34	7"
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CL	uo m	Tuliar		Wal	t_	L'	Z	ε	P	Q	$\log p$	$rac{\log}{\Delta L}$	$\log q$	u'a	$\log f_a$	logγ
2030 2031 2031 2032	XI 14	2463 2463	008 185 362	7 10 21 9	5 · 8 9 · 6 4 · 9	60.073 232.297 49.482	-0'87 -3'89 -0'91	23,429 23,429 23,428	182 024 3 439 190 335	180 504 5 754 187 883	0.7388 0.7071 0.7182	9.7092 9.7446 9.7340	8 · 7598 8 · 7114 8 · 7426 8 · 7317	o:5388 o:5630 o:5484 o:5494	7.6755 7.6647 7.6746 7.6657	9n5915 9n2846 9:4831 9n9699
2032	XI. 3	2463	540	5 43	5 . 2	221.362	-4'12	23.428	11.432	13'502	0.4304	9'7177	8.7193	0.2032	7.0734	0.0257
2033 2033 2034 2034 2035	IX 23 III 20	2463 2464 2464	864 042 218	13 33 10 14 16 15	8 · 9 4 · 7 2 · 9	180.848 359.877 169.979	-0.82 -1.82	23'428 23'428 23'428	347'841 176'601 355'730	347.326 178.087 353.617	0.7441 0.6953 0.7299	9'7019	8.7065	o'5355 o'5696 o'5392 o'5584 o'5532	7.6705 7.6684 7.6718 7.6671 7.6731	9.9918 0.0655 9.4662 9.15997 9.16364
2035 2036 2036 2036 2036 2037	II 27 VII 23 VIII 21	2464 2464 2464	751 898 927	4 5 10 1 17 3	3.6 6.6	338 ' 177 121 ' 149 149 ' 237	+-3.50 +-1.63 0.43	23.427 23.428 23.428	192.645 342.981 12.746	194.199 343.453 12.098	o'6916 o'6906 o'6910	9.7466 9.7088 9.7644 9.7635 9.7052	8.7433 8.7127 8.7594 8.7592 8.7104	0'5425 0'5690 0'5311 0'5326 0'5728	7.6659 7.6743 7.6630 7.6650 7.6771	9.5664 0.0757 0.1551 0.0327 0.0616
2037 2038 3 2038 2038 2038 2039	I 5 VII 2 XII 26	2465 2465 2465	429 607 784	13 4 13 3	1.4 1.6	285 307 100 784 274 333	+0.08 +1.03 +1.36	23'429 23'439 23'43	175°379 0°381 183°288	172.983 2.628 181.489	0.7203 0.7273 0.6974	9'7499 9'7293 9'7235 9'7545 9'7038	8 · 7454 8 · 7294 8 · 7224 8 · 7523 8 · 7069	0'5389 0'5587 0'5537 0'5441 0'5651	7.6527 7.6773 7.6527 7.6772 7.6629	9n8622 9.6243 8.5480 9n4538 9.9175
1 2039 2 2040 3 2040 4 2041 5 2041	V 11 XI 4 IV 30	2466 2466 2466	286 463 640	3 2 18 5	7°1 5°6 6°2	51'063 222'970 40'50g	-0.60 -4.11	23 '43 ' 23 '43 ' 23 '43 '	346.510 167.621 354.913	344 606 170 074 352 508	0.4110 0.4134 0.4139	9'7637 9'7152 9'7372 9'7416 9'7110	8.7159 8.7353	0'5501 0'5521 0'5458	7.6656 7.6735 7.6667	0'0428 926567
6 2042 7 2042 8 2043 9 2043 0 2044	X 14 IV 9 X 3	2467 2467 2467	172 349 526	2 19 3	2.7 5.7	19 · 824 19 · 824 189 · 819	-3.49 2.25 2.25	23 43 23 43 23 43	183.100	183.019	0'7444 0'6922 0'7340	9.7003 9.7003	8 · 7055 8 · 7574 8 · 7155	0.2320 0.2320	7.6693 7.6696	9"4752 9"9999 0"0027
2 2045 3 2045 4 2046	VIII 12 II 5	2468 2468 2468	028 205 382	23 5 17 3 23	38 ' 7 50 ' 1	328,71	5 +3.46 5 +1.22 4 +3.48	23'43 23'43 23'43	2 356 68 2 177 46 1 3 88	357'74 ⁶ 3 177 433 3 3 005	0'7410	9.7037 9.7020	8.7088 8.7077 8.7077	0.5725	7.6641	9.3339
7 2047 8 2047 9 2047	VI 23 VII 22 XII 16	2468 2468 2469	885 914 061	10 22 23	34'9 48'4 37'8	91 '92 120 '07 264 '93	8 +0.55 3 +1.62 01.08	23'43 23'43 23'43	0 165'14 0 194'82 0 347'40	0 167'086 4 197'189 8 346'110	0.7331 0.7224 0.6929	9.7165 9.7294 9.7595	8 · 7164 8 · 7272 8 · 7571	0'5578	7.6629 7.6630 7.6769	0'1400 0n1284 0n0293
2049 3 2049 4 2050	V 3 XI 23 V 20	2469 5 2469 5 2469	593 771 947	13 5 20	59 5 34 5 50 5	70.56 243.38 60.04	8 -0.56 2 -3.26 5 -0.86	23'42 23'42 23'42	8 181 20 7 3 27 7 189 60	4 179 595 1 5 614 2 187 145	0.7378 0.7081 0.7166	9.7106 9.7433 9.7358	8.7124 8.7415 8.7331	0'5618	7.6639 7.6755 7.6647	9n0580 9'4623 9n9367
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7802 7803 7804 7805	2076 2076	1 6 VI 1 VII 1 XI 26	2479 456 2479 486	7 4 4	285 952 72 101 100 356 245 086	0.46 1.04	23 426 23 426	191.047 344.928 14.781 167.218	191.514 342.888 13.439 169.672	0'7314 0'7401 0'7163	9'7631 9'7184 9'7341	8.7508 8.7183 8.7100 8.7332	0'5393 0'5574 0'5626 0'5550	7.6638 7.6628 7.6756	0,1444 0,1447 0,0201
7806 7807		V 22	2479 81:	2 37 4		o*8o	23.426	353.480	351°143 176°545	0.7082	9'7450 9'7085	,	o · 5427 o · 5693	7:6646 7:6747	9n7613
7808 *7809 7810	2078 2078	V II XI 4 V I	2480 165 2480 345	10 55 4 16 56 2 10 55 8	51.461 222.675	-0.80	23.426 23.427	174.981 2.098 182.325 10.595	11.82 182.038		g'7628 g'7602 g'7602	8.7582 8.7059 8.7559	o:5333 o:5735 o:5353	7.6656 7.6735 7.6667	9 2528 9 3499 9 9562
7811 7812		X 24 III 21	, -	18 18 9	211.505	-3·97		189 865 348 404	187·865 350·690	0.7317	9.7162 9.7239	8·7177 8·7239	o:5636	7.6713 7.6723	929634 02067
7813 7814 7815		IX 13 III 10 IX 3	2481 02 2481 19	16 24 1	171.810 120.274 161.268	-1·11 +2·47	23 427 23 427	167.474 356.135 175.861	165'697 356'999 176'219	o 6980 o 7422 o 6898	9'7554 9'7028 9'7643	8.7513 8.7076 8.7596	0.2354 0.2354 0.2354	7.6672 7.6661	0'0322 9"5687 9'5355
7816 7817	2082	II 27 VIII 24	2481 73	1 16.6	339 441 151 365	+0.60	_ , .	184 528	2°388 186°598	0'7413	9'7037 9'7517	8.7084	0.2391	7 6741 7 6650	9.5203 9.5971
7818 7819 7820	2083	VII x4	2482 05	23 53 2	328'260 112'769 141'014	+1.21	23.426	11.089 163.341 193.146	8.727 165.134 195.444	0'7234 0'7354 0'7250	9.7257 9.7138 9.7260	8 · 7260 8 · 7142 8 · 7245	0.223	7.6752 7.6629 7.6641	0.0024 0.1008 0.0009
7821 7822 7823	2084	I 7 VII 3 XII 27	2482 23: 2482 416 2482 58	1 37'I	287°338 102°120 276°555	+1,13	23'425	347'297 171'410 355'144	346.179 171.417 356.235		1	8.7052	0'5661	7 · 6772 7 · 6628 7 · 6771	020319 9'9170 926171
7824 7825	2085	VI 22 XII 16	2482 76	3 18.0		+0.22		179'468	177.684 5.459	_	9.2133			7.6630	8 · 7013 9 · 4372
7826 7827 7828	2086 2087	VI II XII 6 V 2	2483 29 2483 44	5 47 5 3 17 50 5		-2'27	23'422	187.994 10.852 166.737	185°549 12°728 166°446		9.7136 9.7644	8.7164 8.7601	0.2622	7.6666	0.0062
7829 7830	2087	VI I X 26	2483 62	11 28.0	213'281	-4'04	23.422	196.693 346.402	195°336 345°559		9.7029	8.7079	0.2337 0.24		On 1504 On 1118
7831 7832 7833 7834	2088	X 14 IV 10	2483 97	4 14 38'3	202 240	3.28 +0.25	23'421	354°146 183°586	185,831	0.7262	9.7237 9.7306	8.7240 8.7296	0'5584 0'5535	7.6692	9n7327 9n5146
7835 7836	2090	III 31	2484 50	3 47 7		+1.02	23'421	191'577	192.856	0.7401	9'7504 9'7064	8.7103	0.5682	7.6697	_
7837 7838 7838	2091 2091		2484 83 2485 00	9 36.4	181 184 329 969 142 498 318 825	+3,43	23'421	167.434 349.187	10.522 165.907 351.538 172.727	0'7380 0'7082		8.7125 8.7415	0'5697 0'5424	7.6684 7.6751 7.6642	
7840 7841		VIII 3	2485 36	9 53 3	307.934	+1.56	23.422		359.836	0.7314	9.7187	8.7187	0.5570		923216
7842 7843 7844	2093 2094 2094	VII 23 I 16 VI 13	2485 71 2485 89 2486 04	7 12 35 6 4 19 4 7 2 0 1 7	121 461 297 161 82 564	+x 66 +2 46 +0 05	23'421 23'422 23'422	5.886 190.992 344.077	6'343 191'565	0:7445 0:6897	9.7022 9.7628 9.7201	8.7058 8.7606 8.7194	0'5659 0'5394 0'5561	7.6631 7.6633	9.7532 9n9679 on1668
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7050	2090	A.I. 15	4400 92	0 35'4	233.678	-3.85	23`424	182'041	181.638	0'7439	9.7004	8.7063	0.2740	7.6746	912933

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780 780	6 221 ·	67	0°577	1 9 .	7471	48*49	83.82	9'6496	9 9826	9 ' 95 17	9 4425	9.5440	9'9716	72.8	+ 95	48	+143	— x7	—16o	- 17	,
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7813	3 6g·	84	+r.022	001	7574	174 '00	01.40	0.6905	9 9410	9 9410	9 0003	8.0944	9'9904 0'0000 9'9993	00.0		40 	•	_	(+ 86) 	(-78) -	p
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7825	159	54	-0.323	9.7	7425 2	79.51	91.21 6	9.6032 c	9,9992	9599	3°7842	9°5993 9°5982	9.0626	90.4	+ 66 +141	8	+131	26	-169 -104	— 15 — 3 + 18	2.181
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7861 7862 7863 7864 7865	2102 I 19 2102 VII 19 2103 I	2488 818 2488 995 3 2489 172 1	2 6.4 7 59.8 7 56.0	151.538 298.544 112.530 287.763 101.890	+2'55 +1'52 +1'56	23'423 23'423 23'423	192'359 347'242 170'486 355'091 178'571	346.220 170.379 356.274	o'7262 o'6910 o'7448 o'6922 o'7346	9'7243 9'7613 9'7601 9'7601	8 · 72 33 8 · 75 88 8 · 70 52 8 · 75 77 8 · 71 52	0'5546 0'5402 0'5661 0'5410 0'5588	7.6650 7.6770 7.6629 7.6772 7.6628	0n0547 0n0331 9'9609 9n6224 9'1293
7866 7867 7868 7869 7870	2104 VI 22 2104 XII 12 2105 V 1	2 2489 703 I 7 2489 881 I 4 2490 029	8 19.2	276.869 91.500 265.708 53.198 81.350	+0.22 -1.05		3'014 187'145 10'744 166'044 195'869		0.7116 0.7124 0.7345 0.6899 0.6935	9'7391 9'7408 9'7122 9'7646 9'7612	8 · 7378 8 · 7373 8 · 7155 8 · 7601 8 · 7564		7.6771 7.6630 7.6768 7.6655 7.6634	9'4303 9n8051 0'0029 0'0702 0n1284
7871 7872 7873 7874 7875	2106 V 2106 X 20 2107 IV 2	3 2490 383 I 5 2490 559 2 3 2490 738	8 10.8 2 26.8 6 17.6	224.230 42.983 213.134 32.529 202.410	-0.77 -4.03 -0.37	23'420 23'418	346'070 174'552 353'768 183'029 1'973	176'404 351'454	0'7422 0'6994 0'7217 0'7219 0'7016	9.7032 9.7545 9.7250 9.7292 9.7515	8.7083 8.7507 8.7254 8.7282 8.7486	0'5384	7.6736 7.6666 7.6724 7.6679 7.6710	0n1216 9.6747 9n7582 9n4428 9.2365
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7891 7892 7893 7893 7895	2115 V 2 2115 XI 1 2116 IV 1	3 2494 016	2 16.7 10 4.8 3 19.6	62'452 233'464	-0'77 -3'86 +0'14	23 42 1	9'155 189'278 347'463	181'312 10'645 187'158 349'660 164'775	0.6955 0.7295 0.7279	9.7586 9.7186 9.7214	8.7540 8.7199 8.7213	0 5351 0 5636 0 5586	7.6756 7.6646 7.6746 7.6690 7.6699	9°8952 9°9349
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7916 7917 7918 7919 7920	2126 2126 2127	X 26 IV 22 X 16 III 13 IX 6	2497 2497	677 854 002	9 15	7 213 316 3 32 430 3 202 801 7 351 984 1 163 629	-0'37 -3'61 +2'39	23'416 23'416 23'416	190.483 9.796 166.919	359'646 191'587 9'804 165'226 350'142	0.7416 0.6896 0.7364	9 7050 9 7641	8.7500 8.7088 8.7608 8.7140 8.7388	0.5672 0.5355 0.5669	7.6724 7.6679 7.6710 7.6728 7.6662	9.0183
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7956 7957 7958 7959 7960	2143 2144 2144	XI 7 V 3	2504 08 2504 26 2504 43	3 I 8.7 9 I7 34.2	224 296 43 076 213 718	-o.4e	23'414 23'413 23'413	1'318 189'823 9'428	184.022 359.424 190.792 9.554 164.785	0'7248 0'6992 0'7424 0'6894 0'7354	9'7262 9'7536 9'7044 9'7642 9'7123	8.7252 8.7509 8.7609 8.7148	o:5538 o:5427 o:5669 o:5361 o:5654	7.6656 7.6735 7.6667 7.6723 7.6716	9,1967 9,0588 9,9723 9,9017 0,0997
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$7984[209 \cdot 27] + 0.8998[217244] = 7.40190 \cdot 12.87 \cdot 00]9 \cdot 6846[9 \cdot 9448[9 \cdot 9422]946758[8898852]0 \cdot 2987[725] = 177 - 17 - 17 - 132 + 20 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6x + 120 - 6$	9 1
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Denkschriften der mathem.-naturw. Cl. L.H. Bd.

## П.

Canon der Mondfinsternisse.

Nr.	Julianischer Kalender	Julian. Tag	Welt- zeit o		albe auer	Mond im Zenith	Nr.	Julianischer Kaleuder	Julian. Tag	Welt-		Halb Dauc	
			zeit est	Part.	Tot.	λ   φ Grade			1 dg	Netr	Grösse	Part.	i λ   φ Grade
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6 7 8 9 10	-1204 IX 23 -1202 II 7 -1202 VIII 3 -1201 I 28 -1201 VII 23	1282 055 1282 242 1282 420	8 25 8 4 o 36 21 ·	9 90 7 89 7 69 4 112 7 112		168 5 120 + 19 87 21 3 + 21 114 23	56 57 58 59 60	1172 VII 2 1172 XII 26 1171 VI 22 1170 XI 5 1169 V 2	1293 345	23 2 8 24 22 18	5 8 4 8 5 6	75 - 70 -	1 +128 - 24 + 18 + 24 125 - 23 - + 20 + 12 7 +168 - 11
11 12 13 14 15		1282 774 1282 950 1283 453 1283 630 1283 807	16 36 6' 1 21 4'	0 71 5 78 3 66 1 106 5 111	36 50	+157 + 22 +114 - 24 - 23 + 18 + 92 - 17 - 71 + 15	61 62 63 64 65		1294 734	13 22 4 4	20.5 12.2 9.3 7.2 2.4	100   1 91   82	
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Nr.	Julianischer	Julian.	Welt-		Ha Da		Mond Zen			Nr.	Julian		Juli		Welt-			lbe uer		id im nith
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	Julianischer	Julian. Welt-		Halli Dau		Mond im Zenith		Nr.	Julianischer	Julian.	Welt-		Hal Daı		Mond im Zenith
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1507 1508 1509	- 225 II 6 - 225 VIII 1	1639 257	12 2 22 24 12 11	1'8 14'3 14'3 14'1 15'1	105 105 104	33 33 31 36	+152 -175 + 26 -177 +132	+ 18 - 20 + 20		1557 1558 1559	- 193 - 192 - 191 - 191	IV 29 X 24 IV 19	1651 1651 1651	049 227 404	5 40	21'9 6'0	112	52 46 —	+ 10 - 90 +116	+ 15 - 13 + 10 - 10 + 7
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1716 1717 1718 1719 1720	y — 92 XI 26 3 — 91 V 23 — 91 XI 16	1687 609 1687 785 1687 963 1688 140	18 6 7 18 45 19 3 20 21	5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	49	- 89 - 22 + 86 + 21 + 76 - 20 - 54 + 18 - 10 - 17	1	1767 1768 1769	prose	61 IV 22 61 X 17 59 III 2 59 VIII 25 58 II 19	1699 067 1699 569 1699 745	2 24 5 14 12 21	5°2 10'5 6'0	94 76	48	-133 - 11 - 41 + 8 - 75 + 8 +175 - 12 + 77 + 12
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1813 1814 1815	- 32 IX 25 - 30 II 10 - 30 VIII 5 - 29 I 30	1709 461 21 14 1709 638 7 31 1710 141 5 45 1710 317 19 3 1710 495 5 23	7'4 8'6 9'7 19'8	83 88 92		+ 41 - 3 	1861 1862 1863 1864 1865	0 1 2 2	VI 24 V 15	1721 244 1721 421 1721 598 1721 923 1722 100	9 34 4 38	17.3 7.0 0.8 1.0 5.5	81 30 33	45 — — —	-132 - 24 +145 + 24 -143 - 24 - 72 - 18 + 12 + 16
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1846 1847 1848 1849 1850	- 9 XII 10 1 - 8 VI 3 1 - 8 XI 28 1	717 612 7 42 718 114 4 49 718 290 23 18 718 468 18 57 718 645 5 51	3'7 8'6 13'2 21'8 14'1	88 102	24 52	-113 - 21 - 73 + 23 + 9 - 22 + 73 + 21 - 90 - 20	1896 1897 1898 1899 1900	22 22 24 24 25	X 28 III 14 IX 6	1729 217 1729 394 1729 897 1730 073 1730 251	7 27 3 51	8·6 5·8 6·5	88 75 78		+ 54 - 15 -117 + 12 - 55 + 4 + 72 - 8 - 53 + 8
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Denkschriften der mathem.-naturw. Cl. LII. Bd.

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3633 3634	1144 I 22	2138 393 2138 570 2138 747 2138 925 2139 101	18 20 12 38 0 48	9°0 20°6 18°8 5°2 2°5	72	51 49 —	+177 - 14 + 89 + 15 +172 - 18 -143 + 18 +111 - 20	3683 3684	1174 V 1	7 2149 31 2149 49 7 2149 67 8 2149 99 0 2150 17	4 23	4'2 2'3 3'2	65	47	-170 - 22 -44 + 23 -65 - 23 -172 - 20 +99 + 19
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3816 3817 3818 3819 3820	1259 V 8 1259 XI 1 1261 III 18	2180 858 2181 035 2181 212 2181 715 2181 891	10 56 20 18 9 54	3.6 6.0 8.6 13.6	103 88 76	50 28	+ 87 + 165 - + 51 + 147 - 171 -	18 16 1	3866 3867 3868 3869 3870	1290 1291	VIII 22 II 14 VIII 11	2192 640	2 8 22 21 14 37	5.6 19.5 21.6		49 52	+ 60 + 7 - 32 - 10 + 28 + 11 + 142 - 13 - 108 + 14
3821 3822 3823 3824 3825	1262 VIII 31 1263 II 24 1263 VIII 20	2182 423	1 42 17 57 18 31	21 6 20 4 6 5 9 3 5 3	78 91	52 50	+104 + - 26 - + 94 + + 83 - +172 +		3871 3872 3873 3874 3875	1293 1294	XII 15 VI 9 XII 4	2193 172 2193 675 2193 851 2194 029 2194 206	2 2 12 29 10 40	4.6 11.1 19.1	110	 49 43	+ 59 - 17 - 30 + 23 +172 - 23 - 161 + 23 - 27 - 23
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4606 4607 4608 4609 4610	1772 IV 17 1772 X 11 1773 IV 7	2368 200 2368 377 2368 554 2368 732 2368 908	16 6 2 17 13 1 8 43	4'4 6' 1'4 11 9'9 11 8'4 88 8'4 88	51 50 3	+109 + 11 +118 - 10 + 98 + 7 -130 - 6 + 89 + 3	4656 4657 4658 4659 4660	1804 VII 22 1805 I 15 1805 VII 11	2379 982 2380 160 2380 337 2380 514 2380 692	17 39 8 41 21 5	10.0 10.0	112	51 43	+ 43 + 19 + 97 - 20 - 128 + 21 + 45 - 22 + 1 + 23
4611 4612 4613 4614 4615	1775 VIII 11 1776 II 4 1776 VII 31	2369 411 2369 588 2369 765 2369 943 2370 119	7 17 1 14 29 2 0 3 1	r . 6 rr:	52	+136 + 13 -108 - 16 +146 + 16 + 1 - 18 +117 + 19	4661 4662 4663 4664 4665	1807 XI 15 1808 V 10 1808 XI 3	2381 193 2381 371 2381 548 2381 725 2381 903	8 10 7 38 8 15	18.4	58 110 110	 49 48 	+107 - 20 -126 + 18 -116 - 17 -128 + 14 - 9 - 14
4617	1778 XII 4 1779 V 30 1779 XI 23	2370 297 2370 799 2370 976 2371 153 2371 330	5 29 4 52 1 19 48 2	1'4 39 6'2 77 5'9 10 0'8 112 1'8 98	7 40	+168 - 21 - 85 + 22 - 74 - 22 + 60 + 20 -166 - 19	4666 4667 4668 4669 4670	1811 IX 2 1812 II 27	2382 582 2382 758 2382 936	6 40 22 45 6 6	10°2 5'3 7'4 20'7 22°2	72 83 112		140 + 11 97 + 4 +- 19 - 8 88 + 9 +- 135 - 12
4621 4622 4623 4624 4625	1782 III 29 1782 IX 21 1783 III 18	2371 508 2372 010 2372 186 2372 364 2372 540	8 28 14 17 21 34 2	7.6 82 7.8 85 3.7 62 1.6 112	52	- 69 + 17 -126 - 3 +144 - 1 + 39 + 1 + 5 - 5	4671 4672 4673 4674 4675	1813 VIII 12 1814 XII 26 1815 VI 21	2383 290 2383 468 2383 969 2384 146 2384 324	2 52 23 10 18 8	8 · 0 4 · 5 6 · 0 12 · 4 20 · 3	67 7 <b>6</b> 100	14 50	-129 + 13 - 42 - 15 + 13 + 23 + 88 - 23 + 165 + 23
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4631 4632 4633 4634 4635	1787 XII 24 1789 V 9 1789 XI 3	2373 929 2374 106 2374 608 2374 786 2374 962	9 29 0 17	9'4 91 3'2 58 3'8 62		+141 - 23 +134 + 23 -143 - 17 - 8 + 14 0 - 14	4682 4683	1820 III 29 1820 IX 22 1822 II 6	2385 711 2385 889 2386 066 2386 568 2386 746	18 44 6 34 5 42	6 4 10 3 4 6	78 94	49	+129 + 4 +80 - 4 -100 - 1 -82 + 16 - 5 - 17
4636 4637 4638 4639 4640	1791 IV 18 1791 X 12 1793 II 25	2375 140 2375 317 2375 494 2375 996 2376 173	16 42 1 24 23 1	9 '0 116 9 '5 9 9 '3 9 5 '9 75 8 '8 8		- 14 + 11 +109 - 11 - 24 + 7 + 18 + 9 +136 - 12	4687 4688 4689	1823 VII 23 1824 I 16 1824 VII 11	2386 922 2387 100 2387 277 2387 454 2387 779	3 32 8 53 4 16	18.2 9.6 1.9		51 47 —	$   \begin{array}{r} +102 + 19 \\ -51 - 20 \\ -131 + 21 \\ -63 - 22 \\ -3 - 22 \end{array} $
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4731 4732 4733 4734 4735	1851 VII 13 1852 I 7 1852 VII 1	2397 495 2397 671	7 21 6 13 15 26	20'2	110	50	- 109 - 92 +129	+ 21 - 22 + 23 - 23 + 23	4781 4782 4783 4784 4785	1881 1883 1883	VI 12 XII 5 IV 22 X 16 IV 10	2408 2408 2409	420 923 100	17 9 11 37 6 54	3,3 1,1	99 35 58	42 0  45	+100 -175 -107	- 23 - 23 - 12 + 9
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482 482 482 482 482	190	VII VI	29 25 4	2417	605 782 462	13 4 1	42 21 30	21.5 8.6 7.6 13.9 16.5	88 84 104	51 	+16 +15 - 6 - 2 -13	8 + 4 - 3 -	18 20 22	4871 4872 4873 4874 4875	1941 1941 1942	IX	5 3	2430 2430	067 243 422	12 0 17 49 0 25	12'1 4'1 0'7 19'0 18'5	65 28 110	7  49 48	- 177 - 93 - 93	+ I3 + 3 - 7 + 7 - II
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4916 4917 4918 4919 4920	1971 VIII 6 1972 I 30 1972 VII 26	2440 993 2441 170 2441 347 2441 525 2442 027	19 44 10 53 7 18	15.6 20.7 12.9 5.9 1.2	112 102 80	39 51 21	- 112 + - 65 - - 160 + - 108 - - 29 +	17		4966 4967 4968 4969 4970	2006 2007	1X 11 <b>1</b> VIII :	7 3 28	2453 2454 2454	986 163 341	12 2 18 53 23 21 10 35 3 27	17.8	49 105 110	35 46 26	+ 76 + 13 158	+ 10 - 6 + 7 - 10 + 11
4922 4923 4924	1974 XI 29 2 1975 V 25 2 1975 XI 18	2442 203 2 2442 381 2442 558 2442 735 2 2442 912	15 16 5 46 22 24	1715	105 109 102	45 23	+ 26 + 128 - 87 + 20 + 62	21 21 19		4971 4972 4973 4974 4975	2008 2009 2010 2010 2011	VI 2	3 I 2 G	2455 2455 2455	197 374 552	21 7 19 25 11 36 8 16 20 11	1 · 0 6 · 4 15 · 2	33 78 106	37 51	+ 69 -174 -125	- 14 + 23 - 23 + 23 - 23
	1978 III 24 1978 IX 16 1979 III 13	2443 238 2443 592 2443 768 2443 946 2444 123	16 25 19 3 21 10	16 0	109	41	- 64 - + x x 5 - + 73 - + 45 + - x 64 -	3		4977 4978 4979	2011 2012 2013 2014 2014	VI IV a IV a	4 25 5	2456 2456 2456	083 408 763	14 31 11 3 20 10 7 48 10 52	4.8 0.3 15.4	70 18 105	28  38 31	-166 + 57 -117	+ 23 - 22 - 13 - 9 4
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4937 4938 4939	1985 X 28 1986 IV 24 1986 X 17	2445 190 2446 367 2446 545 2446 721 2447 076	17 43 12 44 19 10	12.0	102 105 10 <b>6</b>	35 21 34 37	+ 60 + 90 + 168 + 67 + 63 +	13 13 10		4986 4987 4988 4989 4990	2019 2021 2021	VII 1	26	2458 2459 2459	681 361 538	5 13 21 32 11 20 9 3 4 11	12.3 11.0	86 100 99	34 	+ 39 -171 -139	+ 20 - 21 - 21 + 19 - 19
4942 4943 4944	1989 VIII 17	2447 578 2447 756 2447 032	15 37 3 4	15 '4 10 '2	106 110 102	38 49 23	-166 -129 -145 -164 -149	11 14 14		4993 4994	2022 2023 2024 2025 2025	IX i	28 18 14	2460 2460 2460	246 572 749	10 59 20 14 2 47 6 58 18 11	1.1	43 35 104	42  31 42	+ 53 - 43	+ 16 + 13 - 2 + 3 - 5
4947 4948 4949	1992 VI 15 1992 XII 9 1993 VI 4	2448 612 2448 789 2448 966 2449 143 2449 321	4 57 23 43	15°2	87 105 110		-159 - 74 - 74 + 3 +165 - 99	- 23 - 23 - 22		4997 4998	2028 2028	VIII : VII	28 12 6	2461 2461 2461	281 783 959	11 36 4 10 4 16 18 20 16 50	0 8 4 6	97 30 68	31  -  -  -  -	- 62 - 62 + 86	+ 7 - 10 + 22 - 22 + 23
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5006 5007 5008 5009 5010	2033 2034 2035	IV 14 X 8 IX 28 VIII 19 II 11	2463 2464 2464	879 234 559	10 2 1	52 43 9		108 23 40	24 42 — 39	- 43 - 1	5 + 6		5056 5057 5058 5059 5060	2068 2068 2069	XI V	7 2. 9 2. 6 2.	175 85 176 55 176 65 176 87	9 5 5 11	47	9.8 11.5 12.3 16.2	100	 12 42 47	— 80 十ェク9 — r 38	7 + 13
5011 5012 5013 5014 5015	2036 2037 2037 2039 2039	VIII 7 I 31 VII 27 VI 6 XI 30	2465 2465 2465	090 267 946	14 4 18	2 11 51	17.6 14.6 10.0 10.5	93 95	46 34 —	+ 153 - 63 + 72	1 — 17 3 — 17 7 — 19 7 — 23		5061 5062 5063 5064 5065	2072 2072 2073	VIII 2	4 24 8 24 2 24	78 o8	6 I 5	22 I	2 1 15 0 13 9 15 2	104 106	36 30 37 25	+132 +120 -107	+ 10 + 6 + 11 5 - 14
5016 5017 5018 5019 5020	2040 2040 2041 2041 2043	V 26 X1 18 V 16 XI 8 III 25	2466 2466 2466	477 656 832	0	1 44 32	18.3 17.1 0.3 2.3 13.3	109 31 49	48 44  25	+ 73 13	7 — 21 + 19 2 — 19 2 + 16	5	5066 5067 5068 5069 5070	2075 2076 2076	VI 2: XII 2: VI 1: XII 1: VI	2 24 7 24 0 24	79 29 79 47 79 64	4 8 2 2 8 11	36 20	7'4 11'0 21'7 17'5 3'9	95 112 110	52 46	-134 - 39 -174	+ 23 + 23 + 23
5021 5022 5023 5024 5025	2043 2044 2044 2045 2046	III 3	2467	588 866 043	19 11 7	38 22 41	15.0 14.7 12.7 0.2 0.8	105 101 15	36 35 19	68 171 112	7		5071 5072 5073 5074 5075	2079 2079 2080	XI 20 IV 10 X 10 IV 20	6   24 0   24 4   24	80 50 80 68 80 85	5 5 2 17 9 11	5 27 21	3.3 13.0 16.5 15.3	97 102 108	 22 42 37	一 76 十 95	+ 2x - xo + 7 - 6 + 2
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5036 5037 5038 5039 5040	2054 A 2055 2055 T	II 22 VIII 18 II 11 VIII 7 VI 17	2471 2471 2471	498 675 852	9 22 10	20 42 50	15.3 15.7 14.9 9.1	107 106 98	37 39 36 	139 161	+ 11 - 14 + 14 - 17 - 23		5086 5087 5088 5089 5090	2088 2090 2090	V 5 X 30 III 15 IX 8	24 5 24 3 24	84 66	2 1 23 8 22	56 43 50	1.7 2.6 14.4 12.5 15.6	52 105 100		- 48 + 6 + 17	- 16 - 13 - 6 - 6
5041 5042 5043 5044 5045	2057 2058 2058 2058 2059 2059	XII 11 VI 6 XI 30 V 27 XI 19	2472 2473 2473	886 063 241	3 7	11 13 54	11'2 20'1 17'3 2'5 2'8	111 100 51	50 45 —	+ 72 - 51 - 119	+ 23 - 23 + 21 + 21 + 19		5091 5092 5093 5094 5095	2093 2094 2094	VIII 29 VII 8 I 1 VI 28 XII 21	3 24 24 3 24	85 70 85 87 86 05	2 17 9 16	20 56 56	15.0 5.9 10.8 22.0	75 95	52	+101 +107 -148	- 9 - 22 + 23 - 23 + 23
5046 5047 5048 5049 5050	2061 2061 2062 2062 2063	IV 4 IX 29 III 25 IX 18 III 14	2474 2474 2474	097 274 451	9 3 3 3 18 3	36 30 31	12'4 14'0 15'4 14'2 0'8	104 106 104	14 31 38 32	+ 33 - 147 - 51 + 81 + 122	+ 2 - 2 - 2		5096 5097 5098 5099 5100	2095 2095 2097 2097 2098	VI 17 XII 11 IV 26 X 21 IV 15	24	86 58 87 09 87 26	3 6 5 12 3 1	11 14 29	5.6 3.2 10.2 12.3	58 94 100		94 25	- 23 + 23 - 13 + 11 - 10
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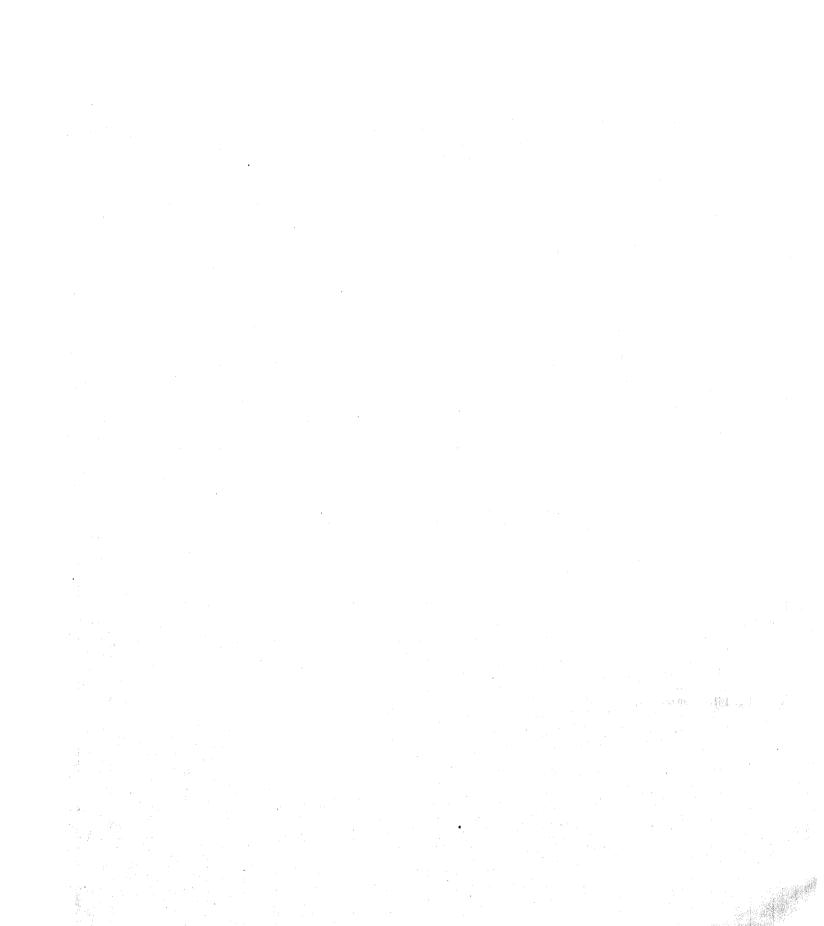
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5101 5102 5103 5104 5105	2099 IV 5 2101 II 14 2101 VIII 9	2487 622 2487 799 2488 479 2488 655 2488 833	8 28 2 47 8 22	16*3 2*1 14*2 16*1 14*3	47 104 107	32	-142 -126 - 38 -124 -105	- 6 + 13 - 16		5151 5152 5153 5154 5155	2133 2134 2134	X.1 12	2500 2500 2500	438 615 793	0 27	10'9 20'1	96 111	50 46	+ 90 -152 - 11	- 19 + 17 - 17 + 14
5106 5107 5108 5109 5110	2104 VI 8 2104 XII 2 2105 V 28	2489 010 2489 689 2489 866 2490 043 2490 220	19 35 4 58 22 20	12.9 8.0 11.7 19.4 18.8	86   - 98   - 110   2		- 5 + 66 - 77 - 22 - 47	+ 22 21		5159	2137 2137 2138	VIII 30	2501 2501 2502	649 825	19 10 23 19	1.6 13.2 13.3 15.0	102 103 106	24 25 36 40	+ 76 + 10 + 17	+ II - 5 - 9 - 13
5112 5113 5114	2106 XI 11 27 2 2108 III 27 2 2108 IX 20 2	2491 254	11 18 8 4	3'1 2'9 13'9 1 11'2 16'2 1	55 - 104 3 97 -		- 13 - -174 - -120 - - 87 -	- 17 - 3		5163	2140 2141 2141	VI 30 XII 23 VI 19 XII 13 VI 8	2503 2503 2503	036 214 391	22 24 11 29 14 5	4'6 11'2 20'9 19'1 6'5	97 112 110	51 49	+ 24 -172 +147	- 23 + 23 - 23 + 23 - 23
5117 5118 5119	2110 VIII 29 2 2111 VII 21 2 2112 I 14 2	2491 962 1	6 33 0 49 1 4 1	16.5 0.8 4.3 10.6 20.4	30 - 66 - 95 -		-115 - -112 - - 11 - - 14 - -102 -	- 9 - 21 - 22		5166 5167 5168 5169 5170	2144 2144 2145	XII 3 IV 18 X 11 IV 7 IX 30	2504 2504 2504	248 424 602	0 17 19 54 16 44	3.2 8.7 12.8 10.1	001 89	10  46 49		- 7
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5132 5133 5134	ALZO TILL 9 2	495 418 1 495 595 496 275	5 11 1 7 56 1 2 22	4.4 10 6.4 7	95 34 95 33 78	3	124 136 118 35 154	· 13 · 16 · 23		5181 5182 5183 5184 5185	2152 2153 2153	V 18 XI 12 V 8 XI 1 III 19	2507 2507 2507	378 555 732	7 30 8 18 8 7 8 31 3 7	5 5 2 5	73 51	51 47 —	123 132	- 19 + 17 - 17 + 14 - 1
5136 5137 5138 5139 5140	2123 XII 3 2 2124 V 28 2124 XI 21 2	496 629 496 806 496 983 497 160 1 497 662 1	5 21 1 5 45 0 43	4'8 2	70 -	9	76 83 87 61 117	· 22 · 21 · 20		5188 5189	2156 2156 2157	IX 11 III 7 VIII 30 II 24 VIII 20	2508 2508 2508	589 765 2	6 52 3 12 6 14	15 6 1	21	39 45 —	100 + 12	+ 10
5141 5142 5143 5144 5145	2127 III 28 2 2127 IX 20 2 2128 IX 9 2	497 839 r 498 017 498 193 r 498 548 498 873	8 35 I 4 49 I	9.9 6 6.7 10 8 1 11 2.2 4	08 43 10 42 48 —	+	166 + 127 - 136 - 2 -	3 1 6			2159 2159 2159	VII 11 I 4 VI 30 XII 24 VI 18	2509 2509 2509	622 799 1 976 2	7 13 7 54 2 53	2'4 11'2 18'8 19'3	97	49	+124 -107 + 92 + 17 + 74	+ 23 - 23 + 23
5146 5147 5148 5149 5150	2130 VII 21 2 2131 I 13 2 2131 VII 10 2	4499 050 4499 228 4499 404 1 4499 582 1 4499 758 2	0 33 1 2 46 1 1 43	R'7 Y	10 48 10 42 90 —	3   <del>-</del> 7   +	134 + 7 + 171 + 175 +	- 21 - 22 - 22		5197 5198 5199	2162	XII 13 IV 29 X 23 IV 19 X 12	2510 2511 2511	833 010 188	8 9 3 18	18.81	96 85 10	49 50	-123	+ 23 - 14 + 11 - 11 + 7
	),							5			10-10-A. (			3						

## Fehlerverzeichniss.

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Pag. 7, Nr. 108, Columne F: statt r-t*, lies r*.
     9, " 165,
                           μ: ist die nach dem Decimalpunkte stehende 8 lädirt.
 "
                           log sin k: statt 9.9777, lies 9.9778.
     9,
             194,

    ∴ Aufgang: statt - | -, lies (o) | (-66).

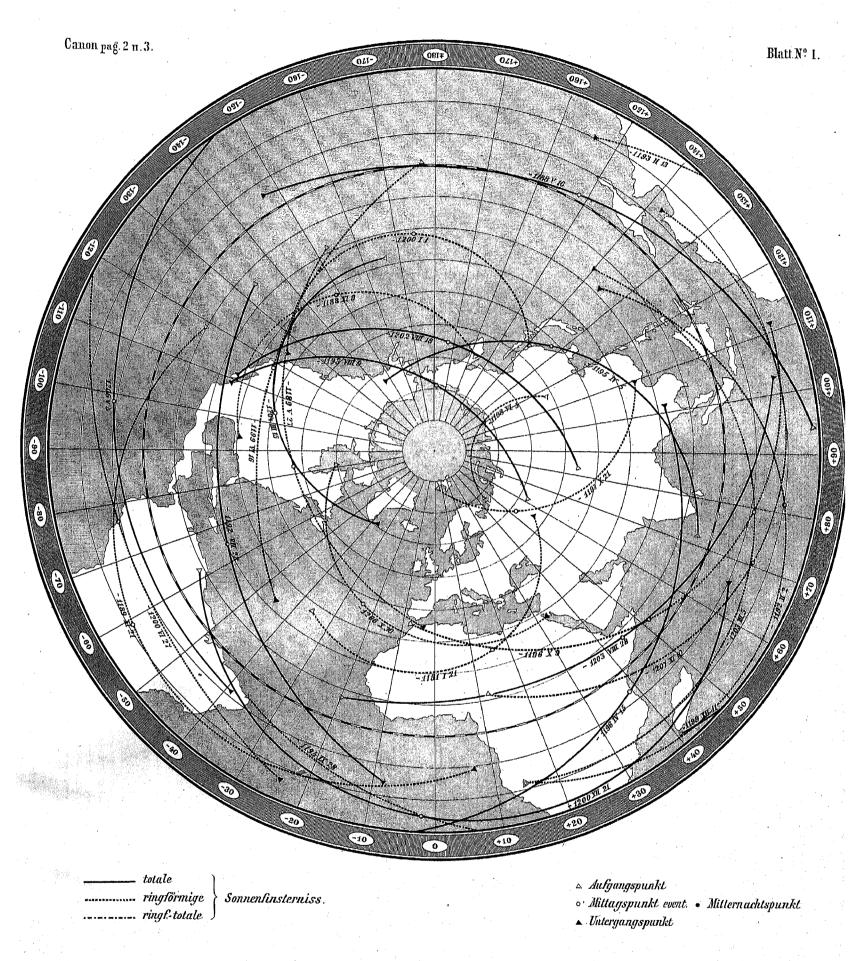
    18, "
            260,
                           ⊙Untergang: statt -|-, lies -4|-55.
                           F: statt p, lies (r).
     17,
                           \odot Aufgang: statt -|-, lies (-76)|(+66).
            399,
                           ⊙Untergang: statt -|-, lies -93|+58.
                           F: statt p, lies (r).
     18,
                           \log f_a: statt 7.67.8, lies 7.6778.
            429,
                           ⊙ Aufgang: statt -|-, lies -72|-64.
     19, "
             415,
                           ⊙ Untergang: statt -|-, lies (-80)|(-80).
                           \bar{F}: statt p, lies (r).
    21, " 491,
                           F: statt r-t, lies r.
    23, "
            532,
                           F: statt r-t, lies r.
 "
    23, "
                           \bigcirc Aufgang: statt -|-, lies +ro|+63.
            548,
                           ⊙Untergang: statt - | -, lies (+37)|(+77).
                           F: statt p, lies (r).
    33, , 762,
                           \log \sin g: ist die letzte 3 undeutlich.
    55, " 1302,
                           K: statt 86°20, lies 86°21.
    60, " 1472,
                           Weltzeit: ist die 3 in 34 1 lädirt.
    79, " 1945,
                           F: ist in t* das t lädirt.
                           log sin ô': ist die 4 dem Decimalpunkte folgend undeutlich.
    87, , 2138,
 , 129, , 3172,
                           \odot Aufgang: ist (-81) theilweise undeutlich.
 , 185, , 3324,
                           F: statt r^*, lies r-t^*.
   139, im Kopf: statt Centraliät, lies Centralität.
   151, Nr. 3710,
                  Columne K: statt 96 . 18, lies 96 . 81.
   161, " 3972,
                           μ: ist die letzte r undeutlich.
 , 163, , 4020,
                           F: statt r, lies r*.
 , 163, , 4045,
                           F: statt t*, lies r*.
                           F: statt t*, lies t.
   175,
         " 4327,
   187, " 4612,
                           G: statt 168.65, lies 168.64.
                           log sin g: statt 9.6864, lies 9.6862.
                           log cos k: statt 9,6752, lies 9,6750.
   197, " 4884,
                           G: ist die dem Decimalpunkte folgende 8 undentlie .
                           log sin k: ist in 9.9883 die zweite 8 lädirt,
   205, "5079,
   265, , 6568,
                           \log\cos\delta': ist die vorletzte Ziffer 8 lädirt.
   266,
         " 6616,
                           Julian. Tag: ist die letzte 5 lädirt.
   281,
        " 6992,
                           G: statt 246°41, lies 246°40.
   828,
        ,, 822,
                           Julian. Tag: statt 1467 701, lies 1476 701.
   342, " 1792,
                           λ: statt +156, lies -156.
   355, " 3012,
                           Julian. Tag: statt 199. 420, lies 1991 420.
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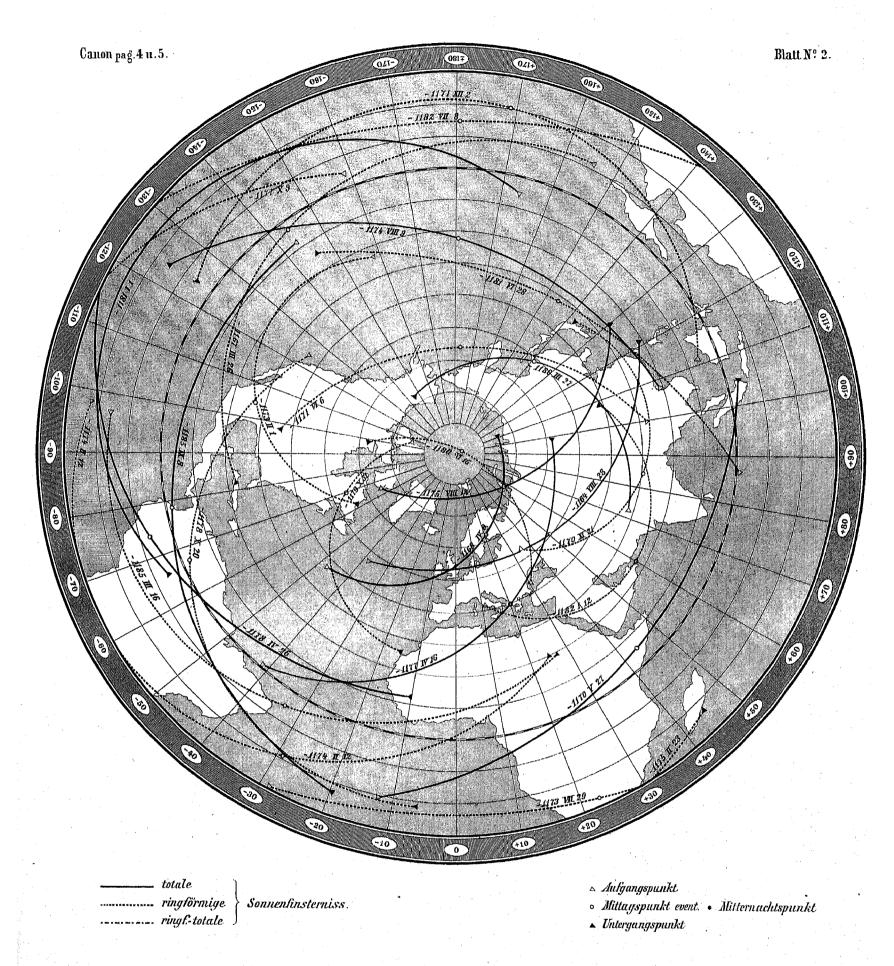
## Ш.

Iconographie zum Canon der Sonnenfinsternisse.



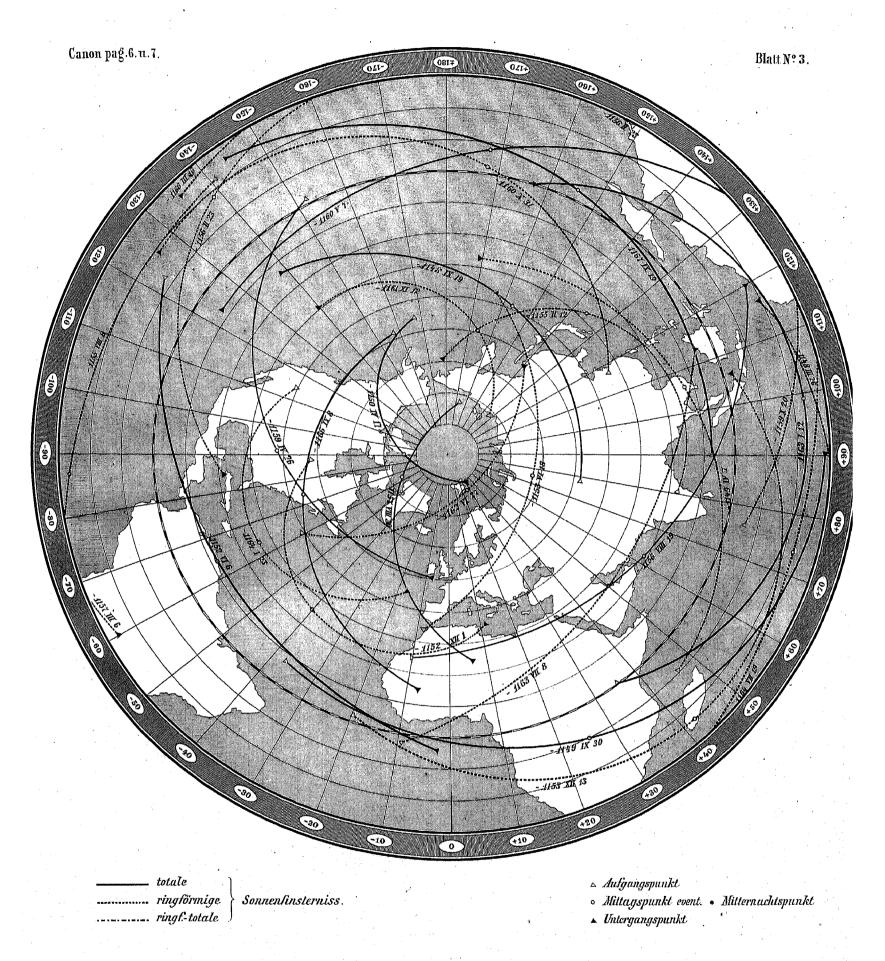


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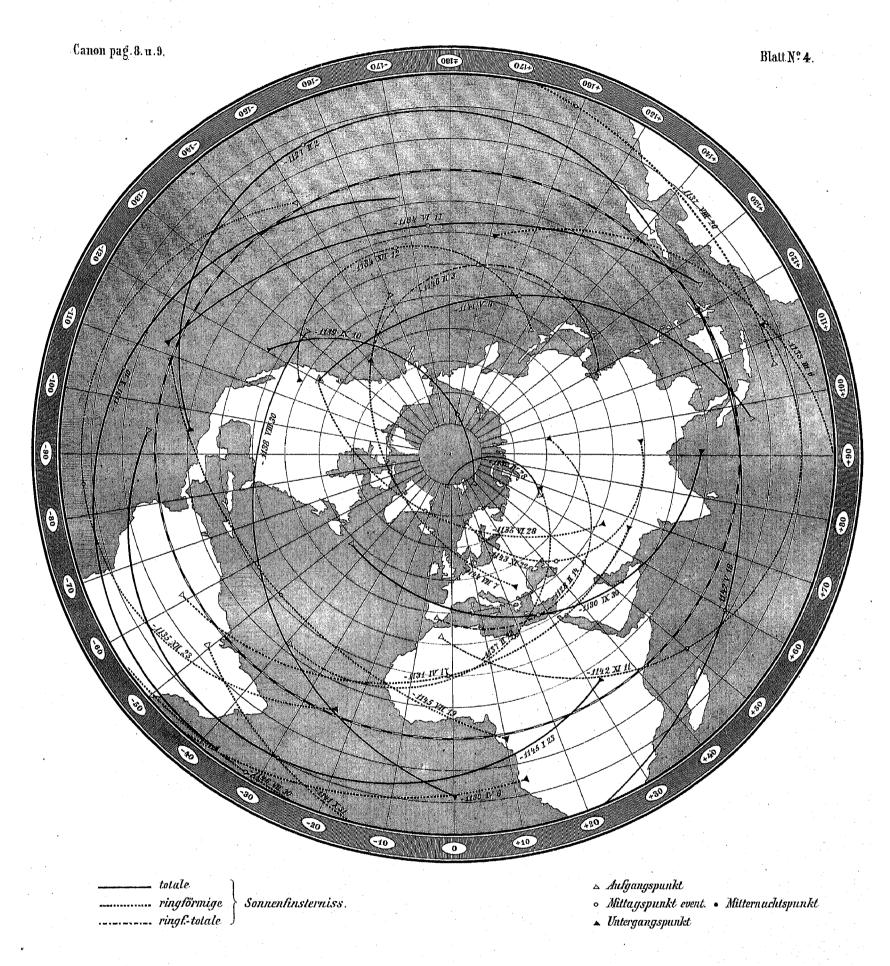
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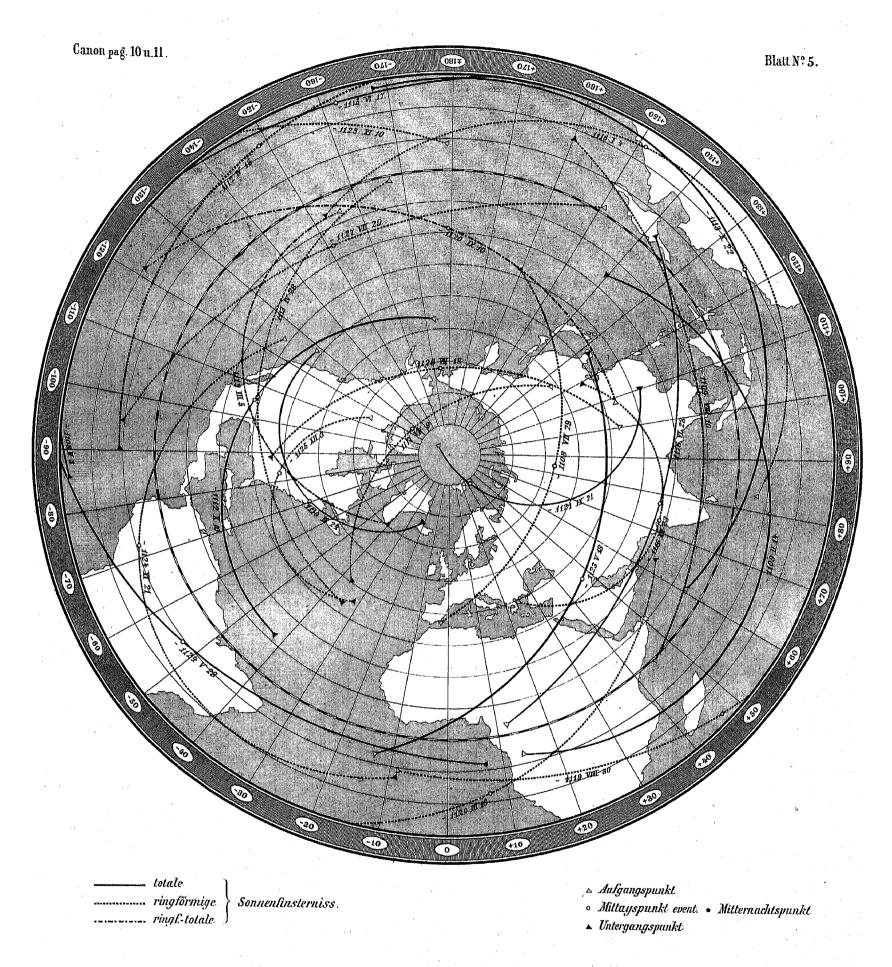
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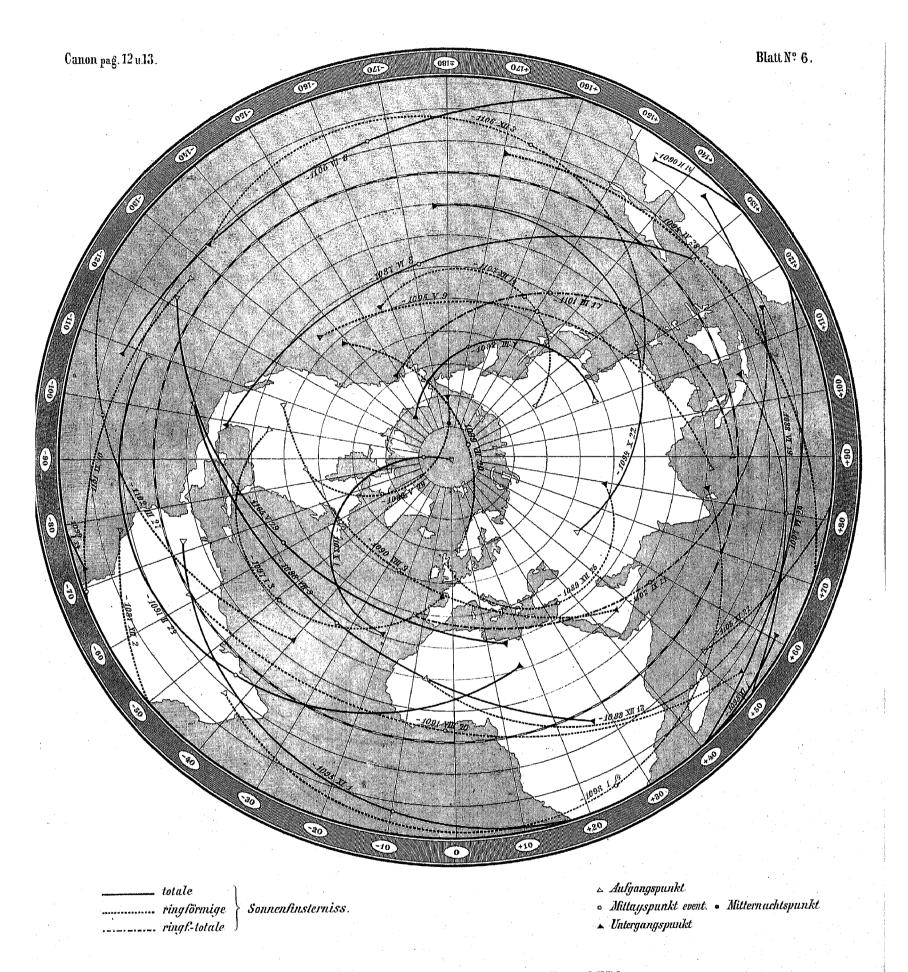
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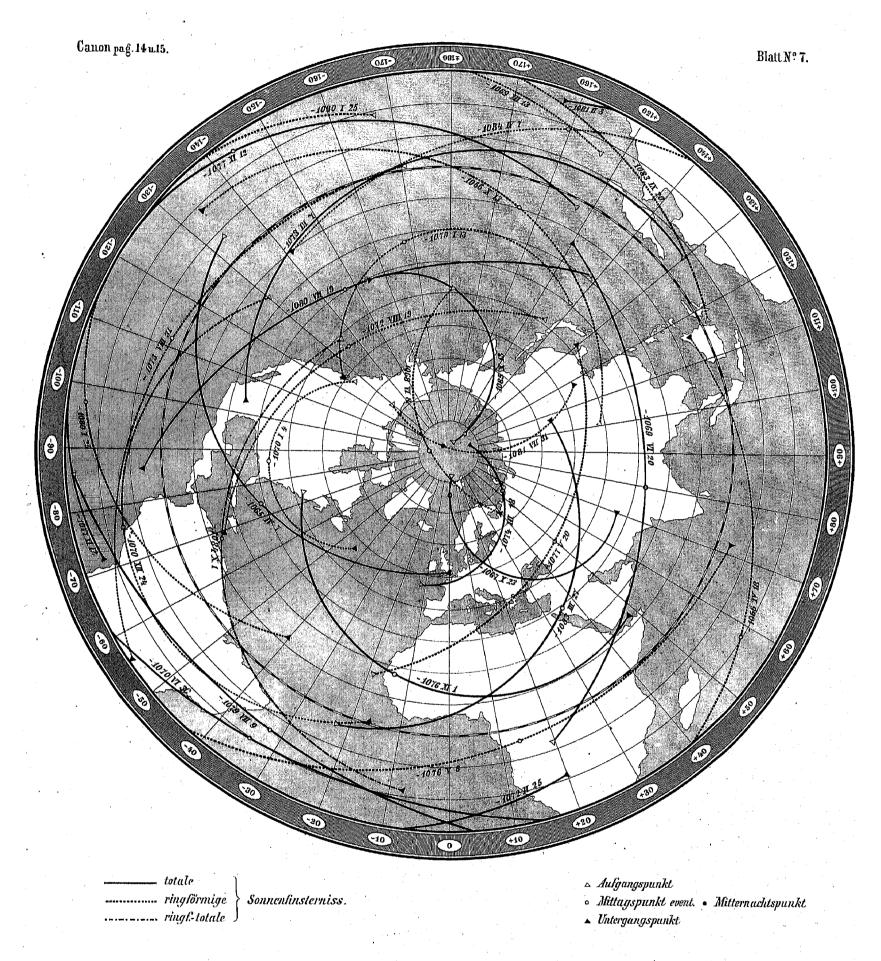
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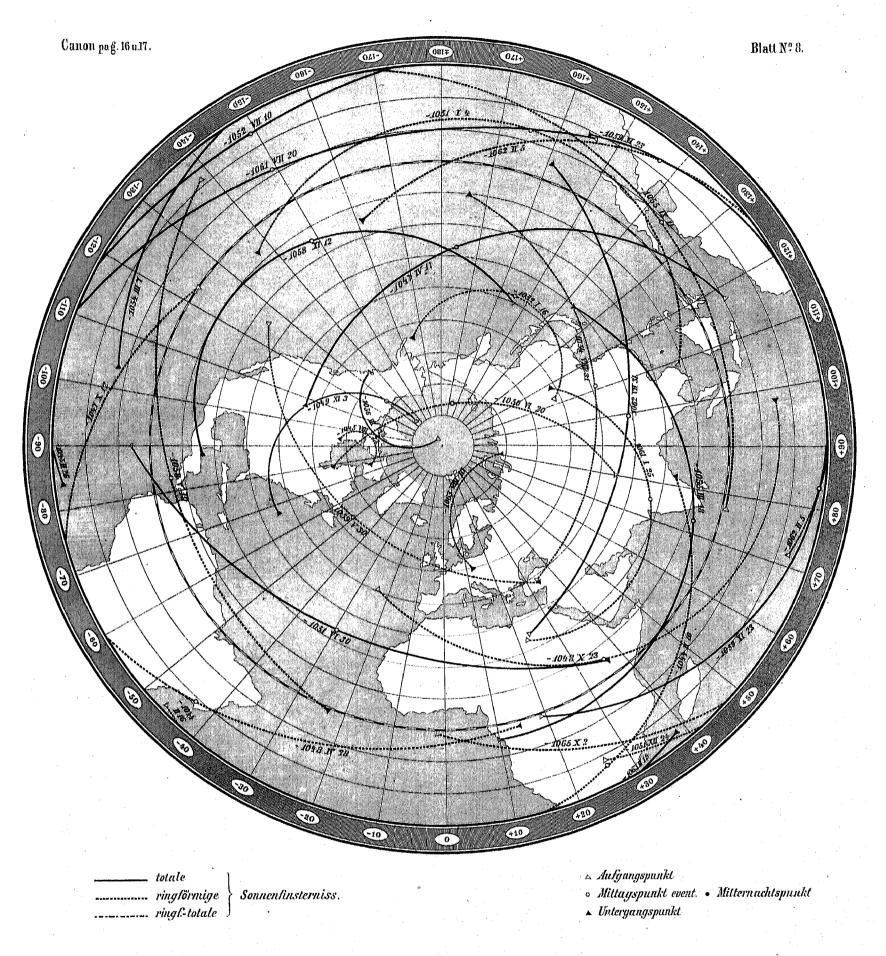
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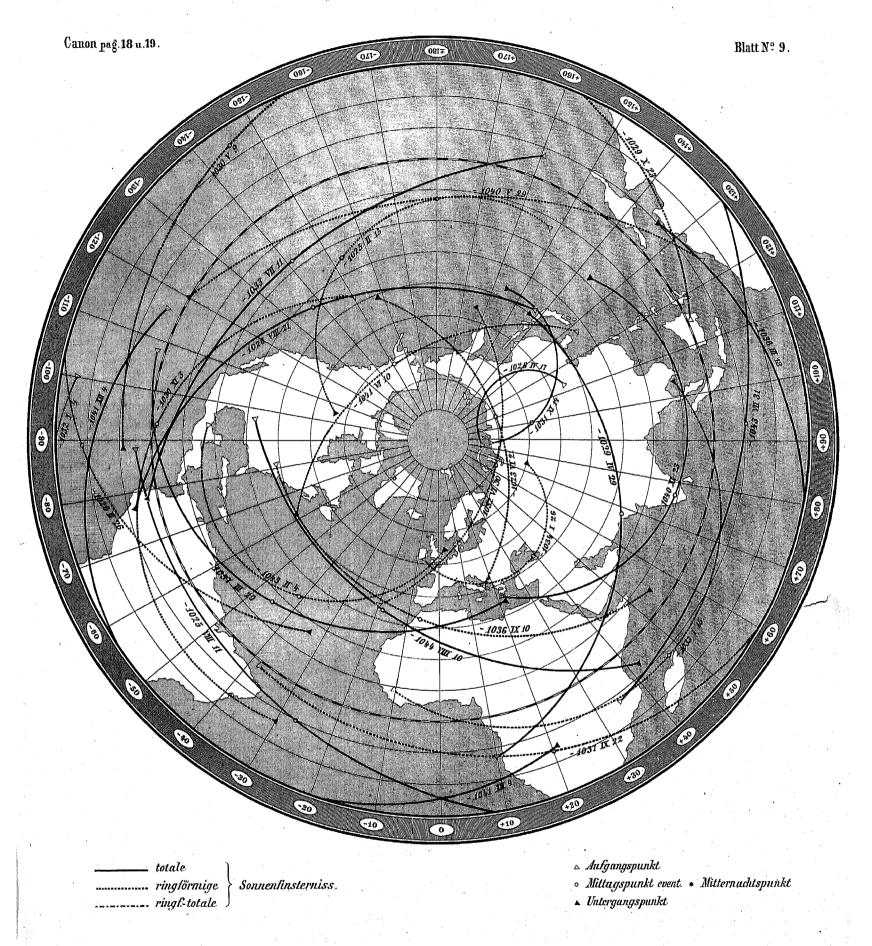


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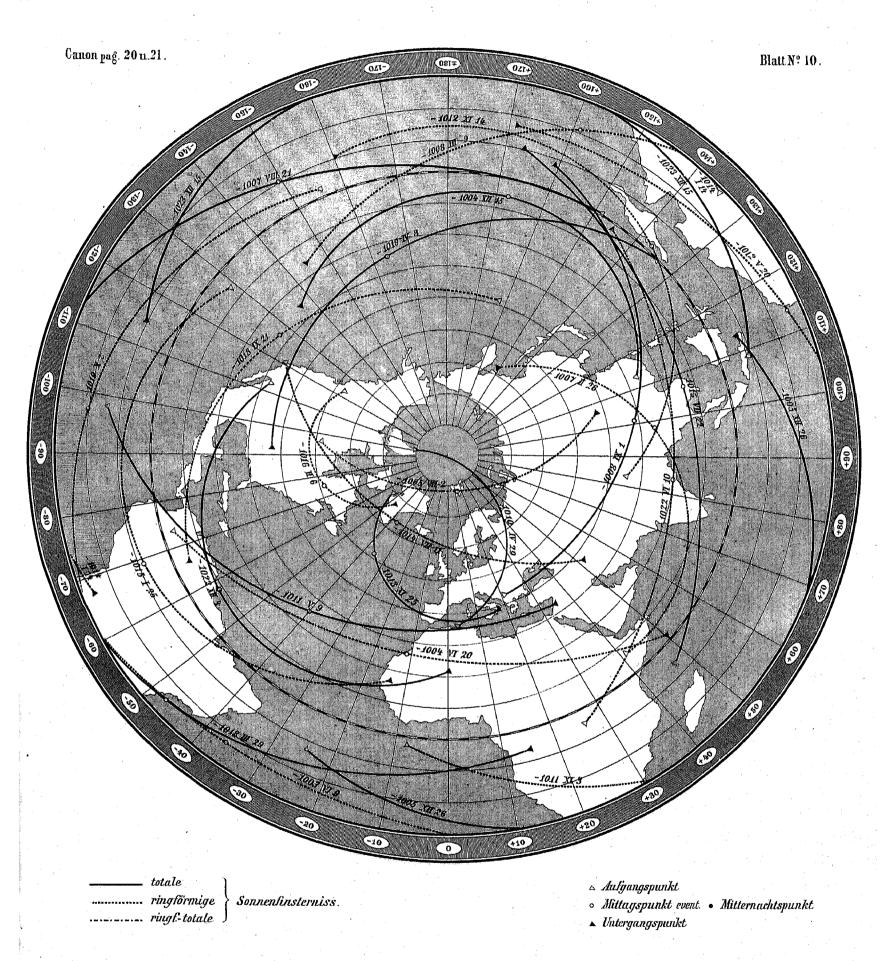
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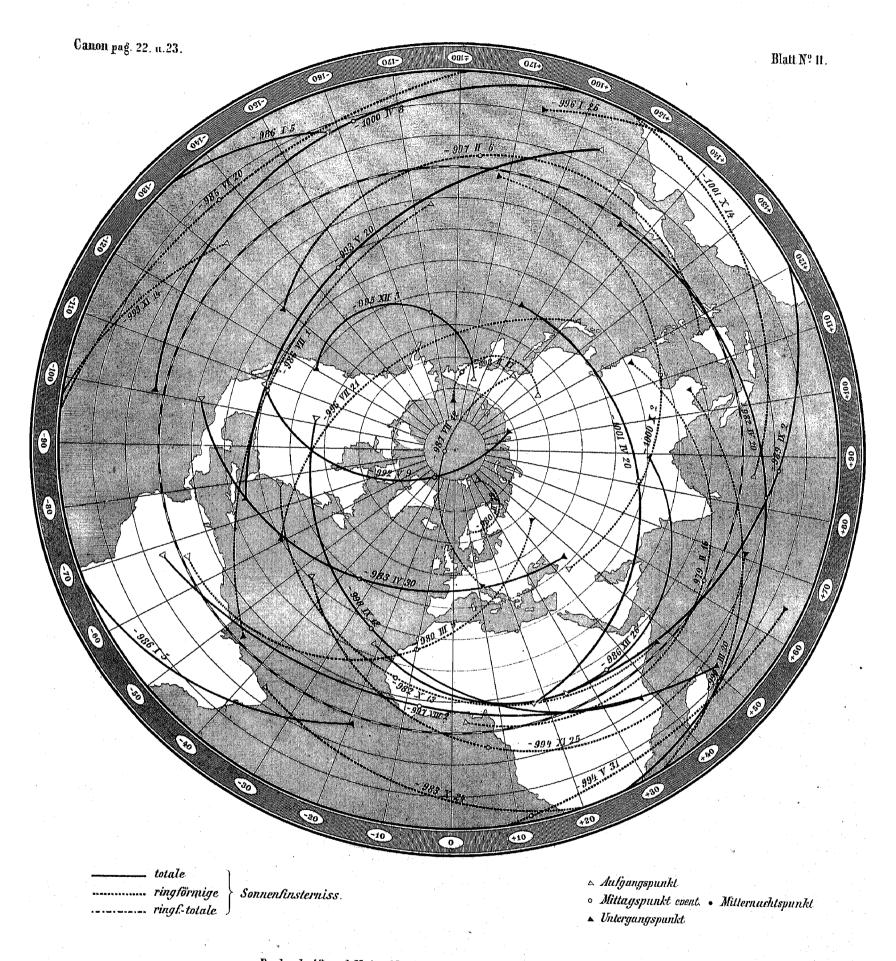


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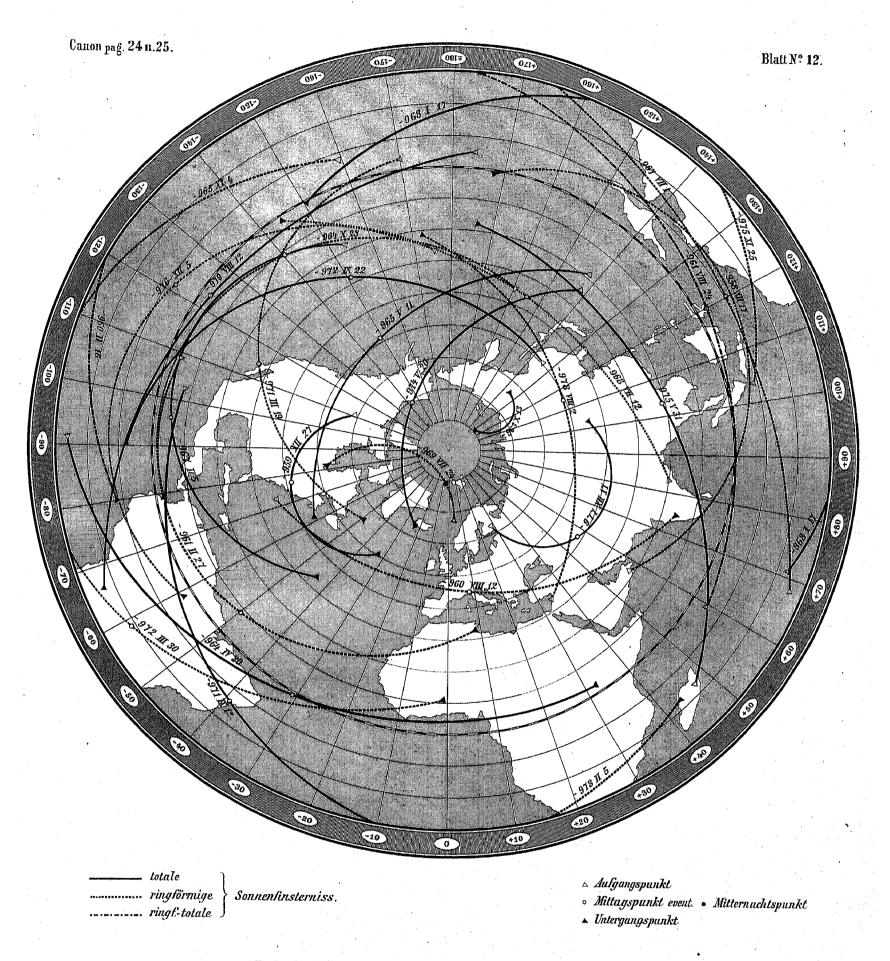
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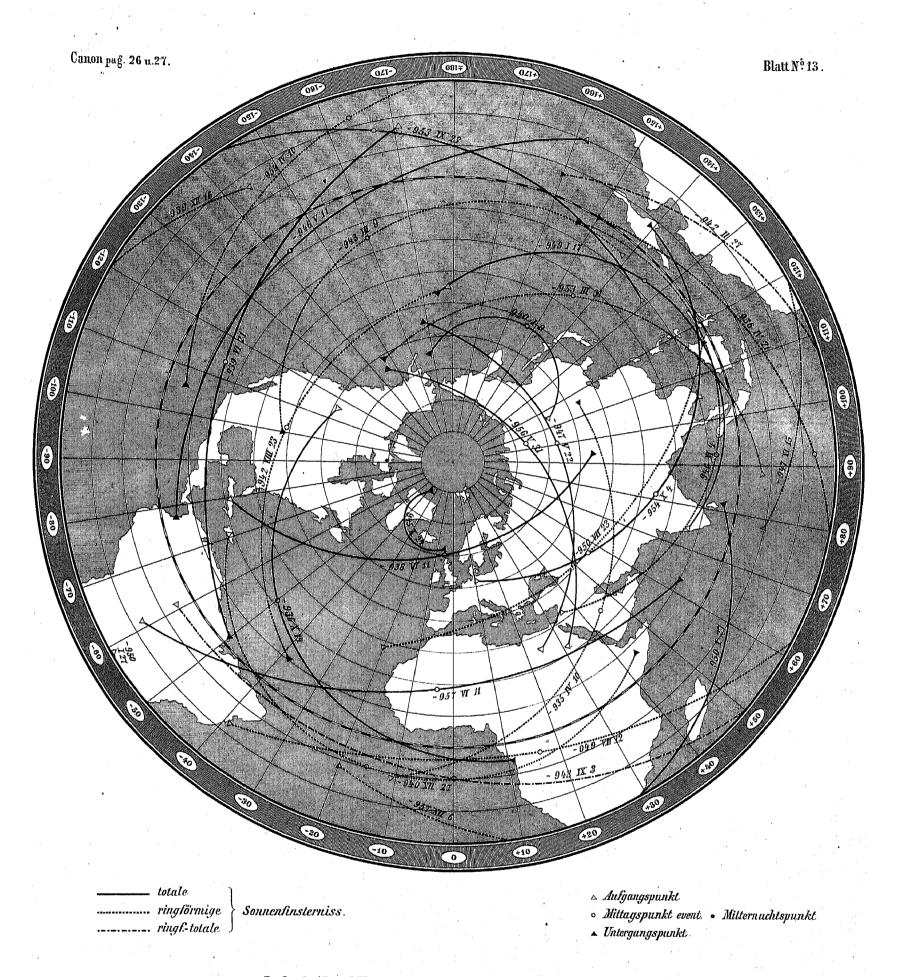
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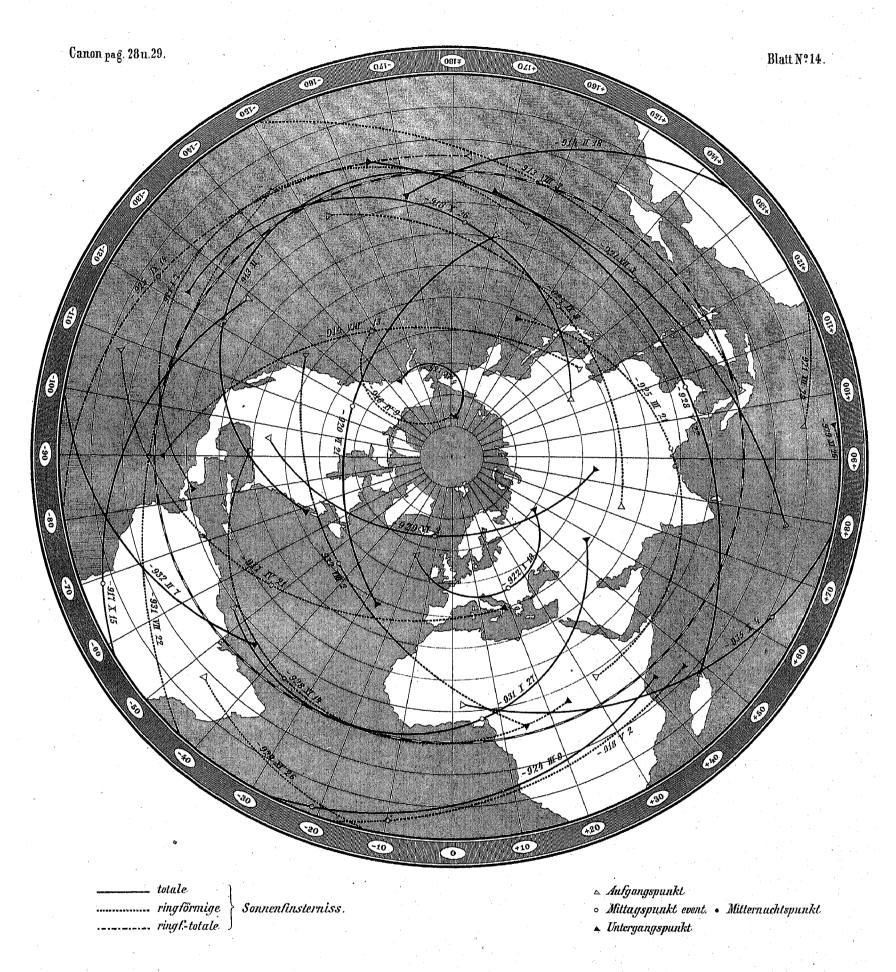


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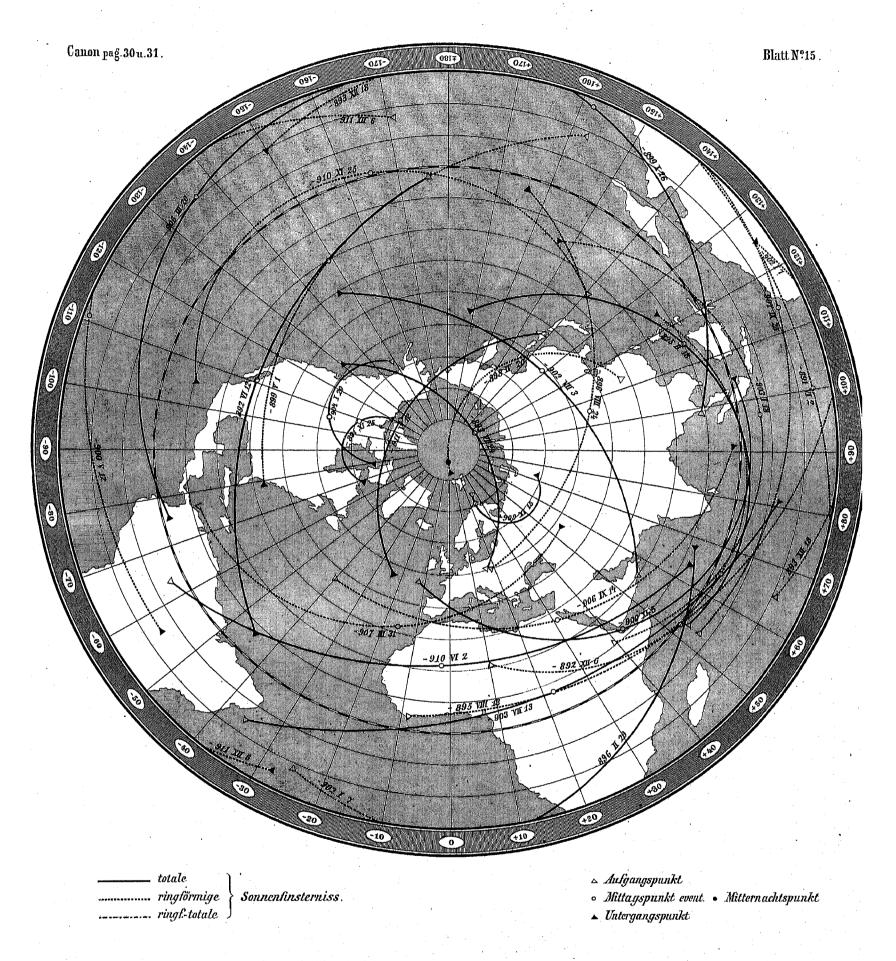


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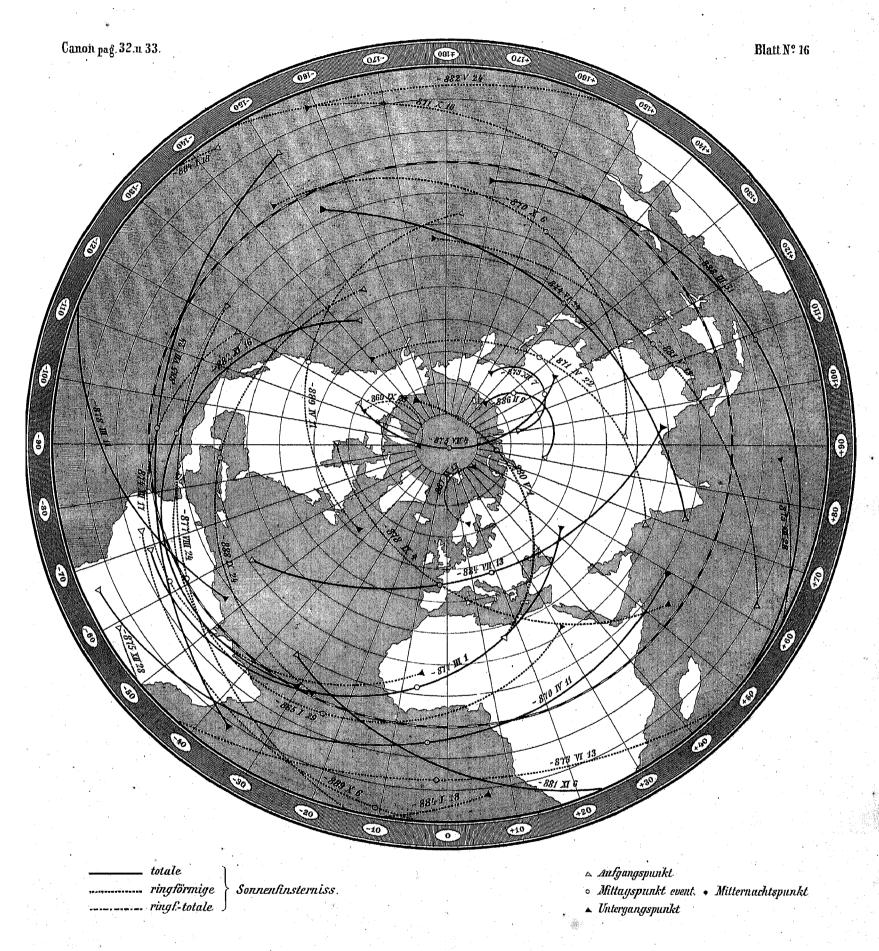
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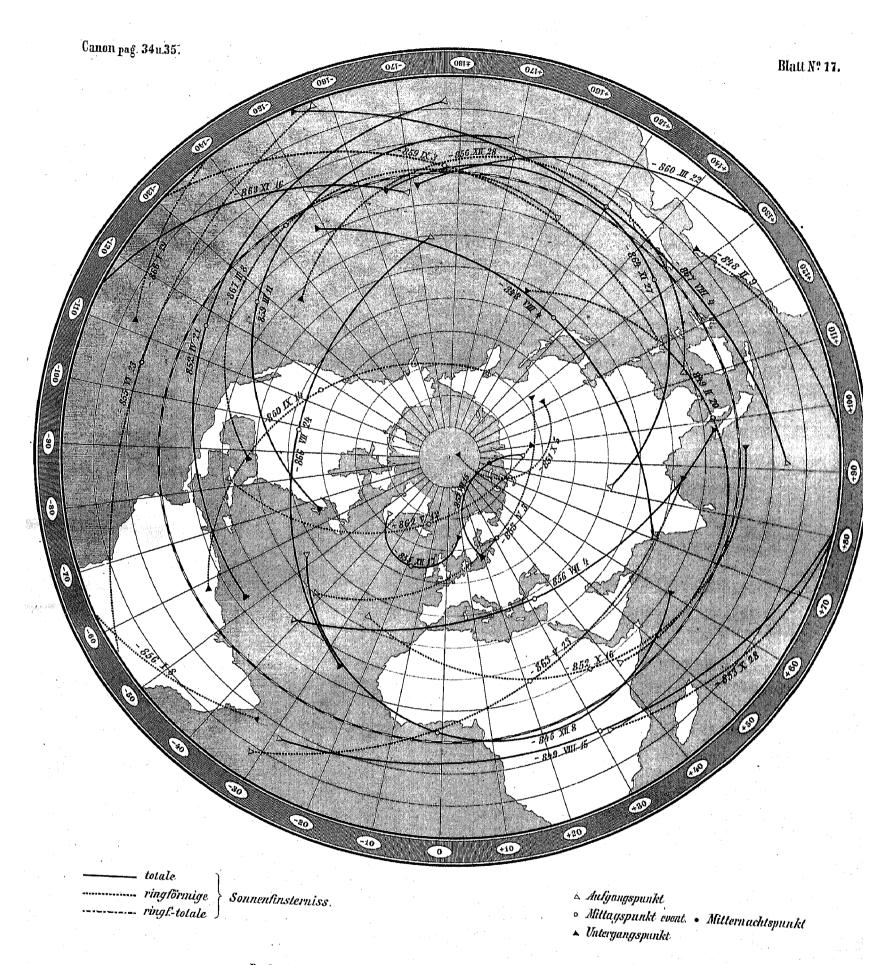


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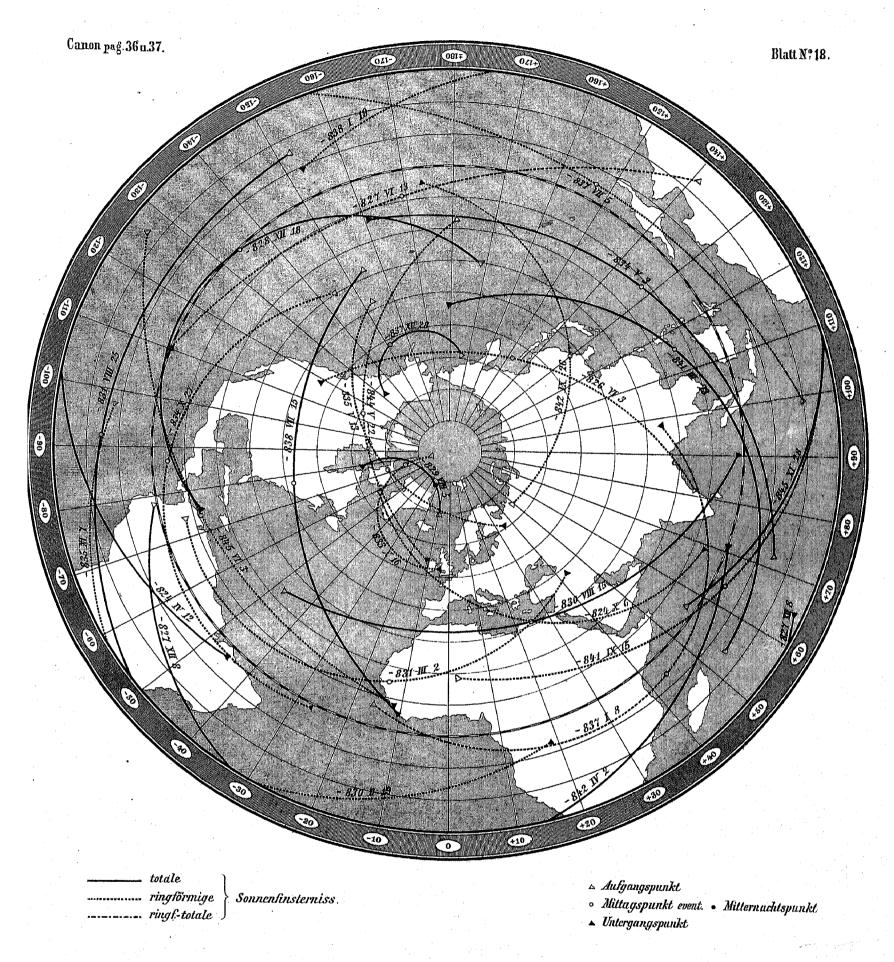


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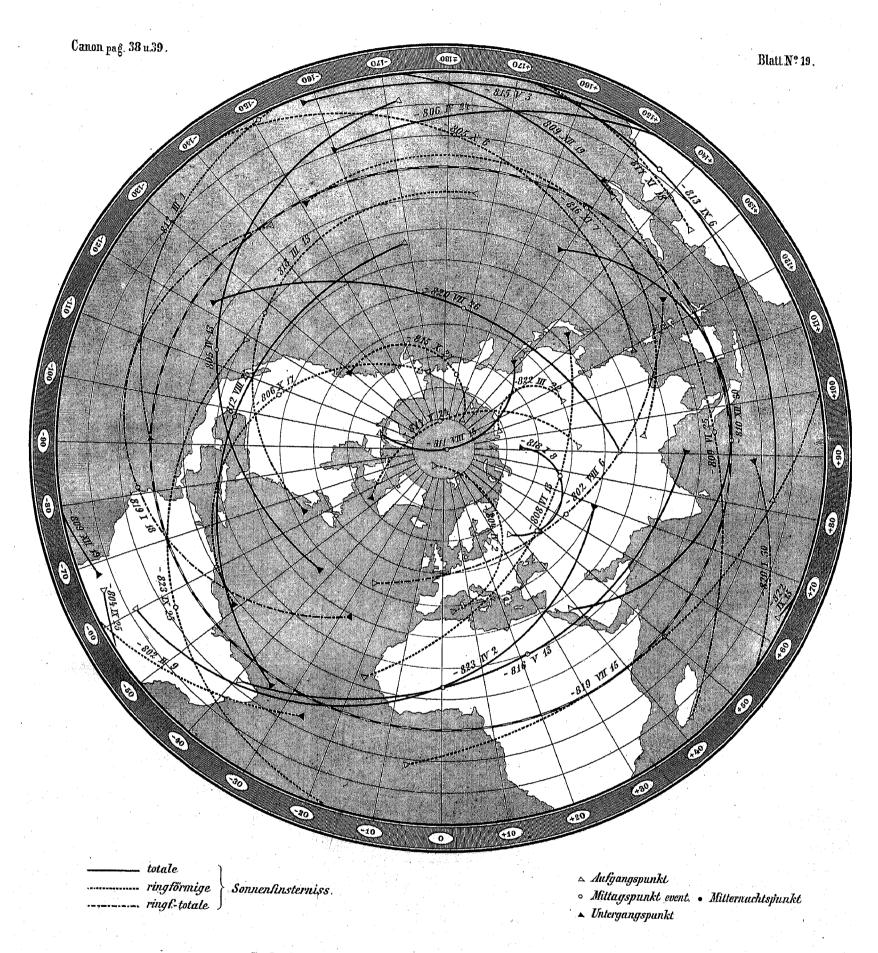
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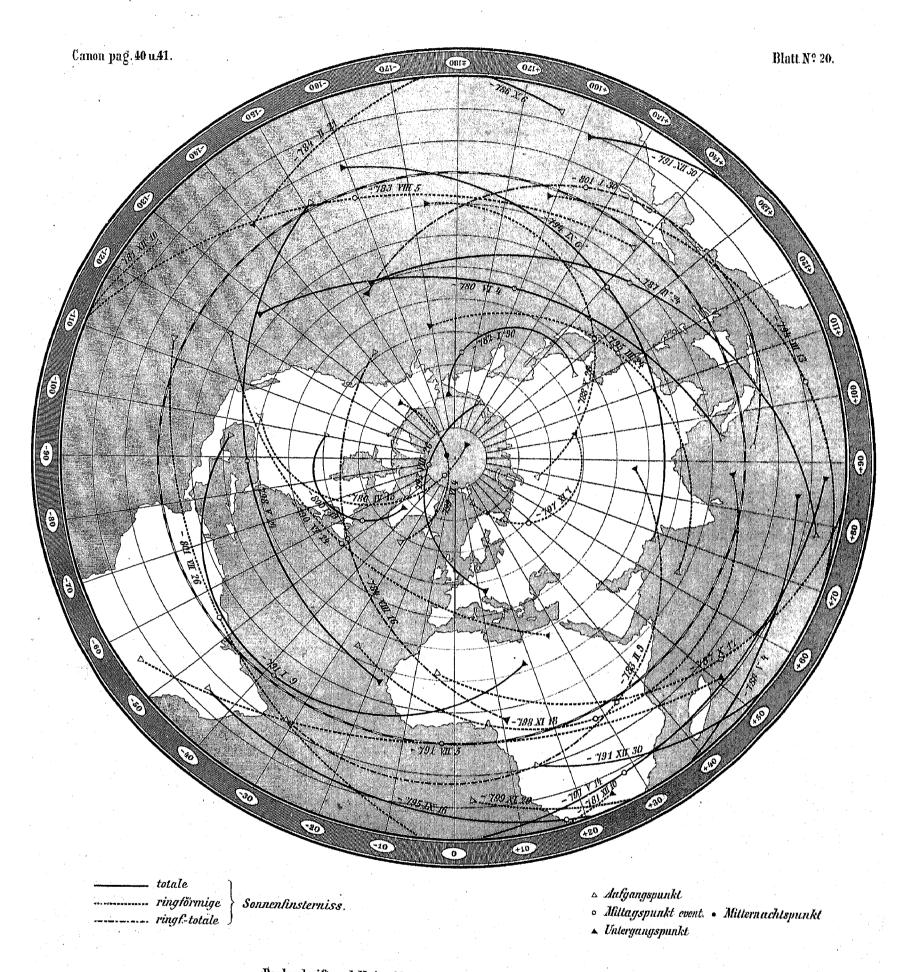
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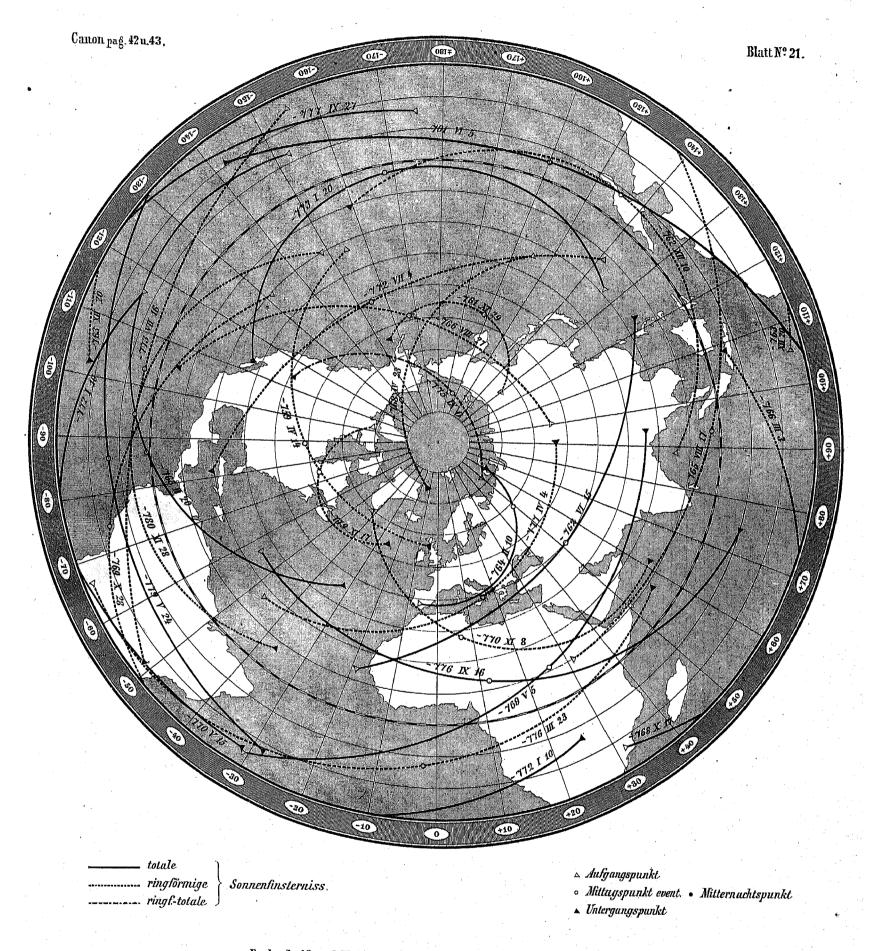
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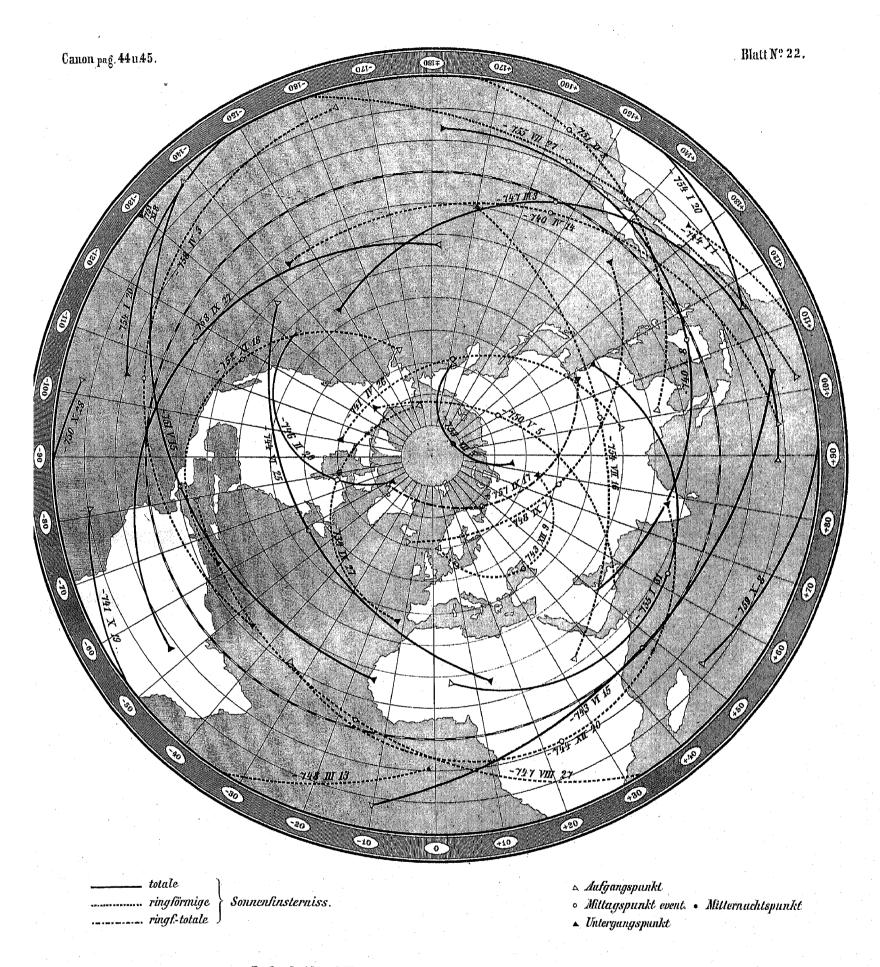
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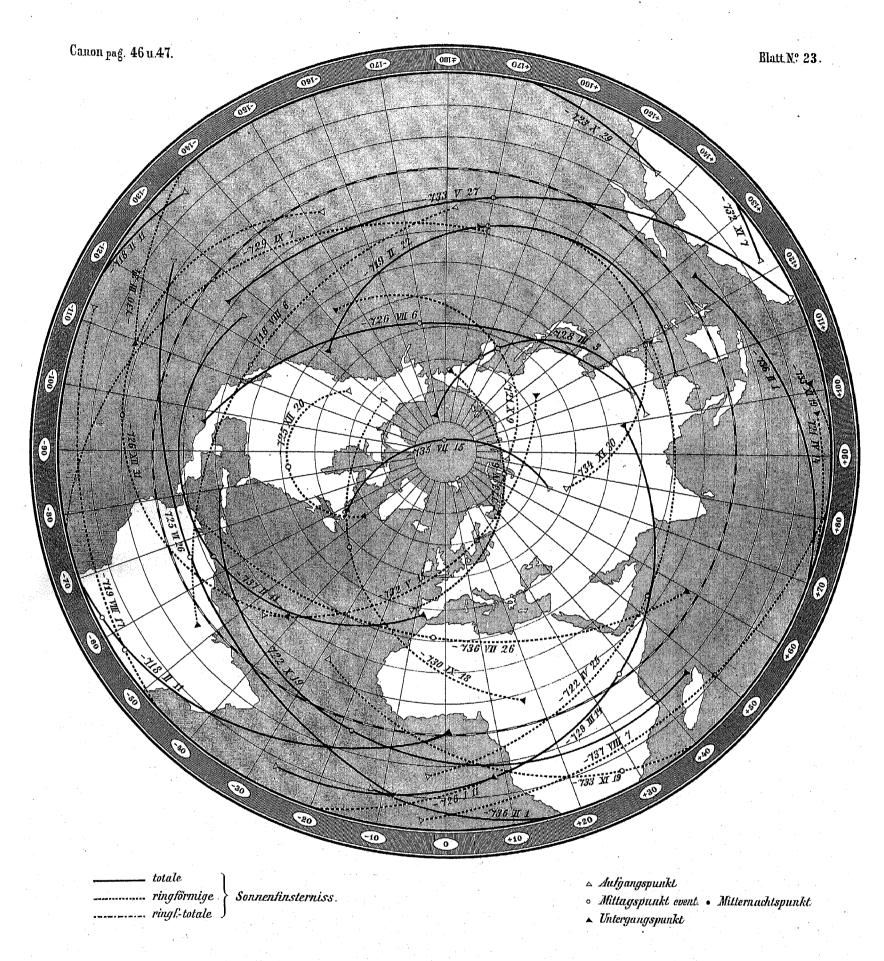
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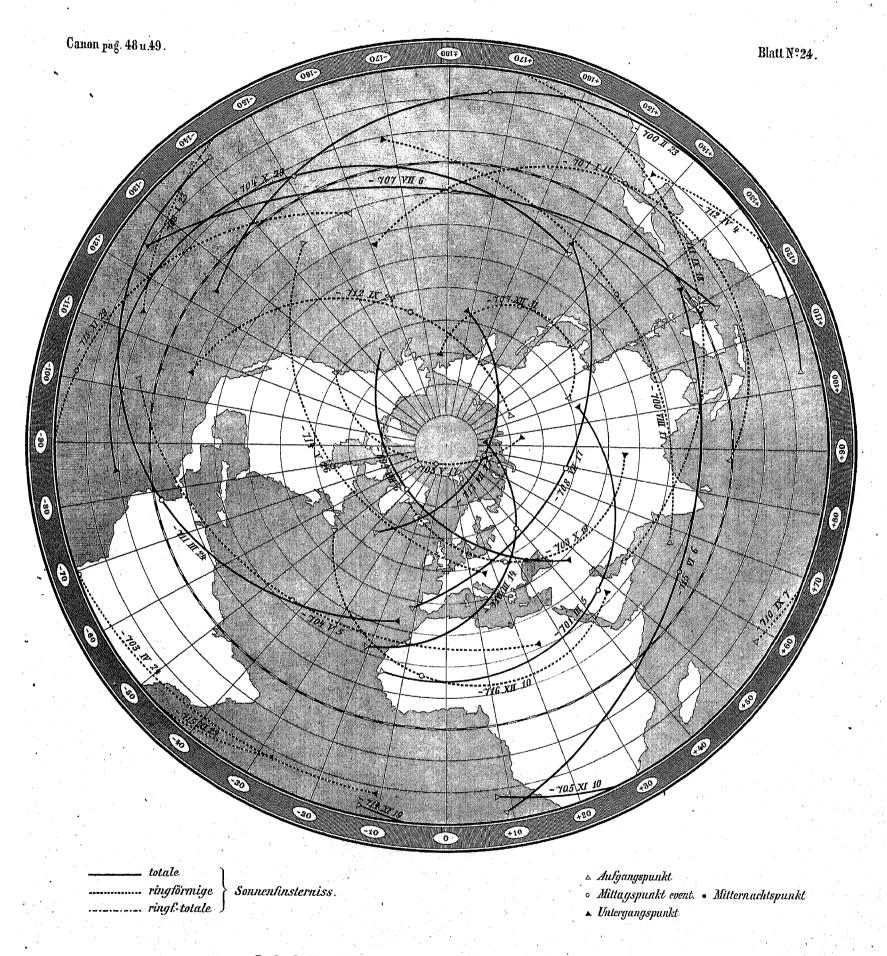


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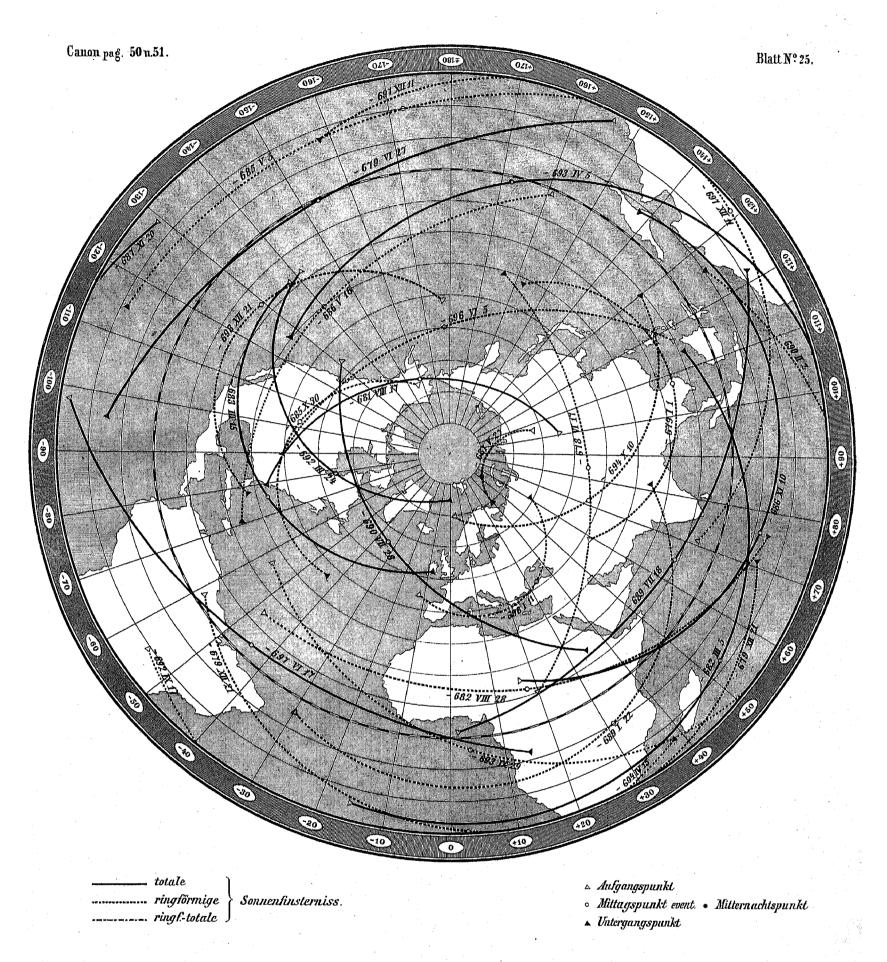


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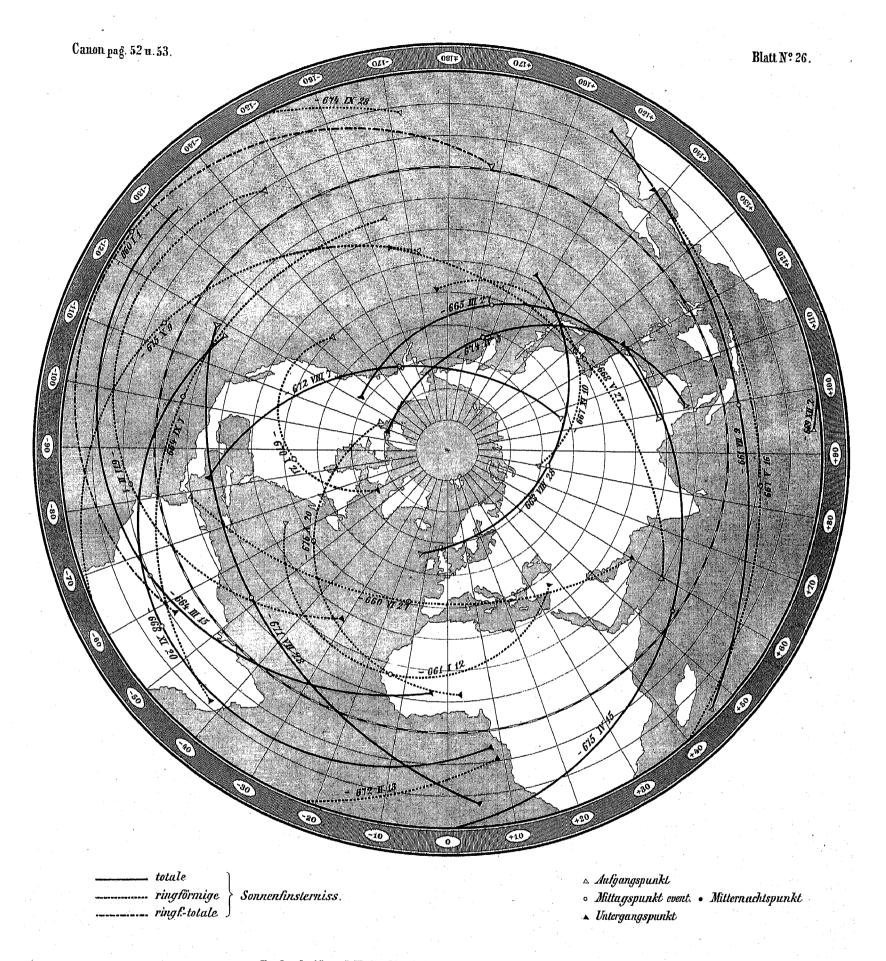
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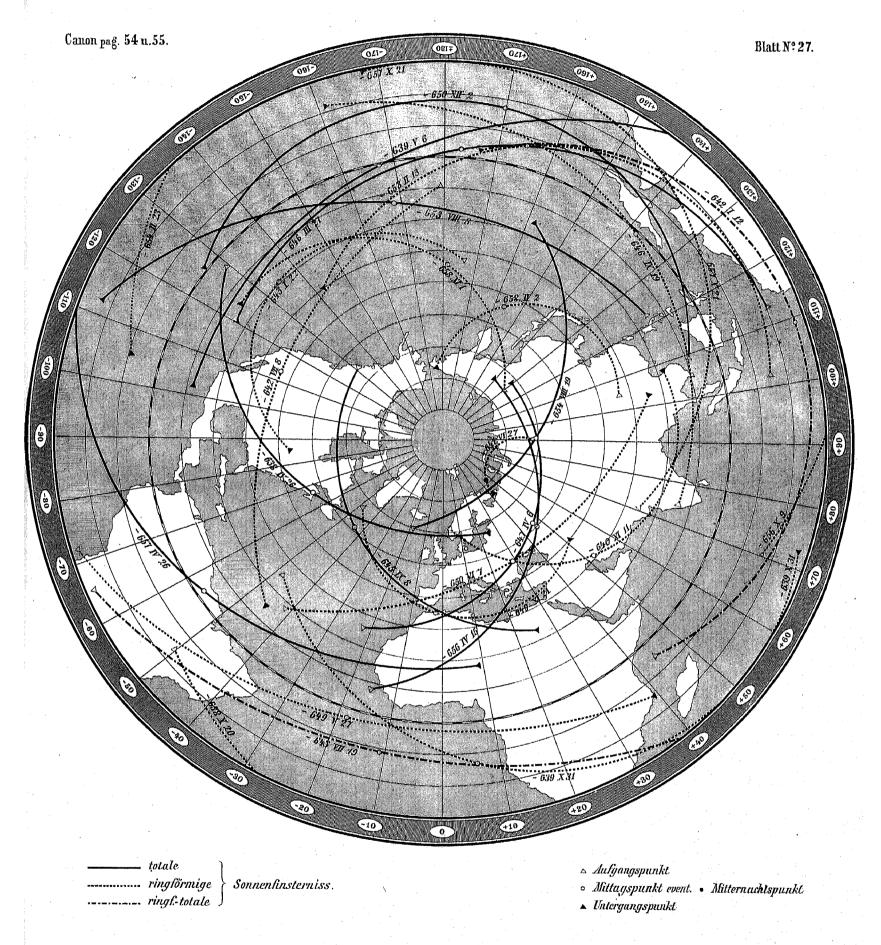
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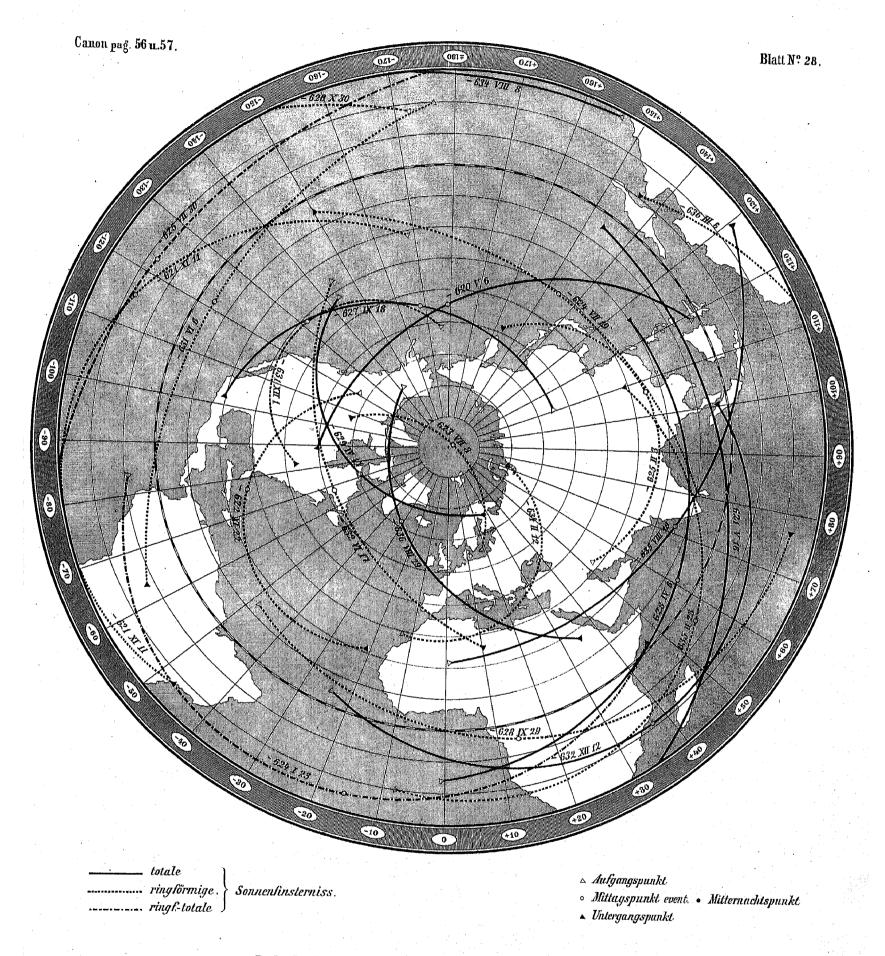
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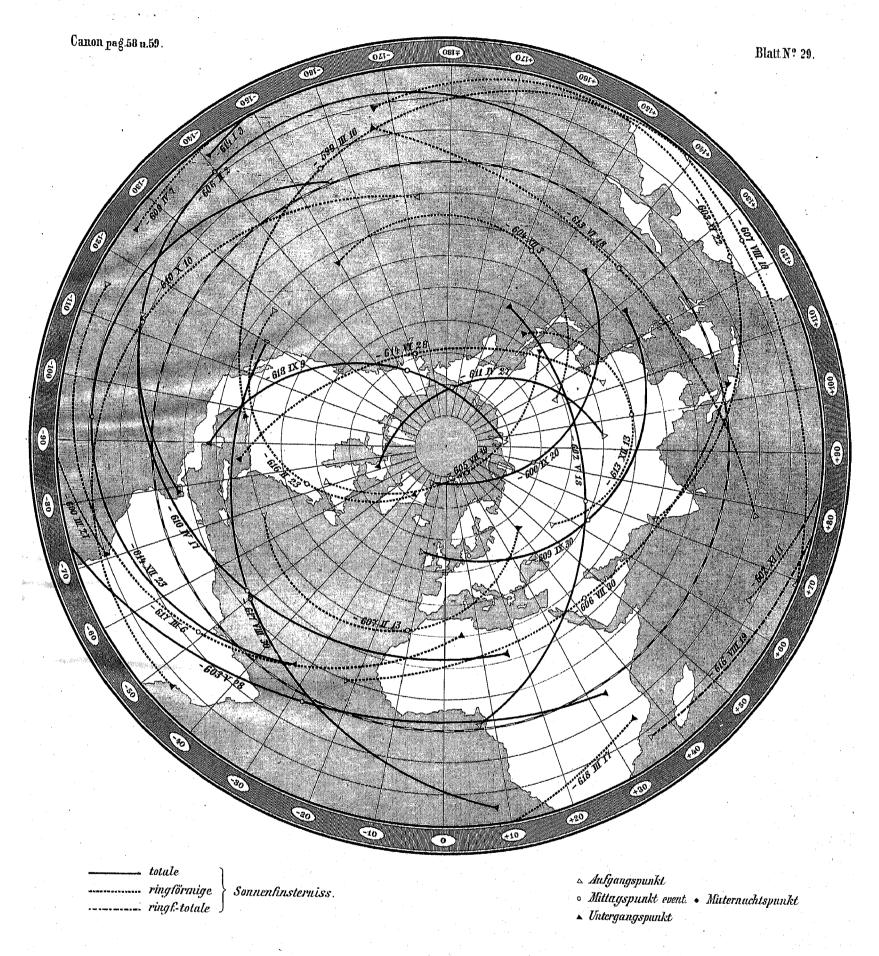


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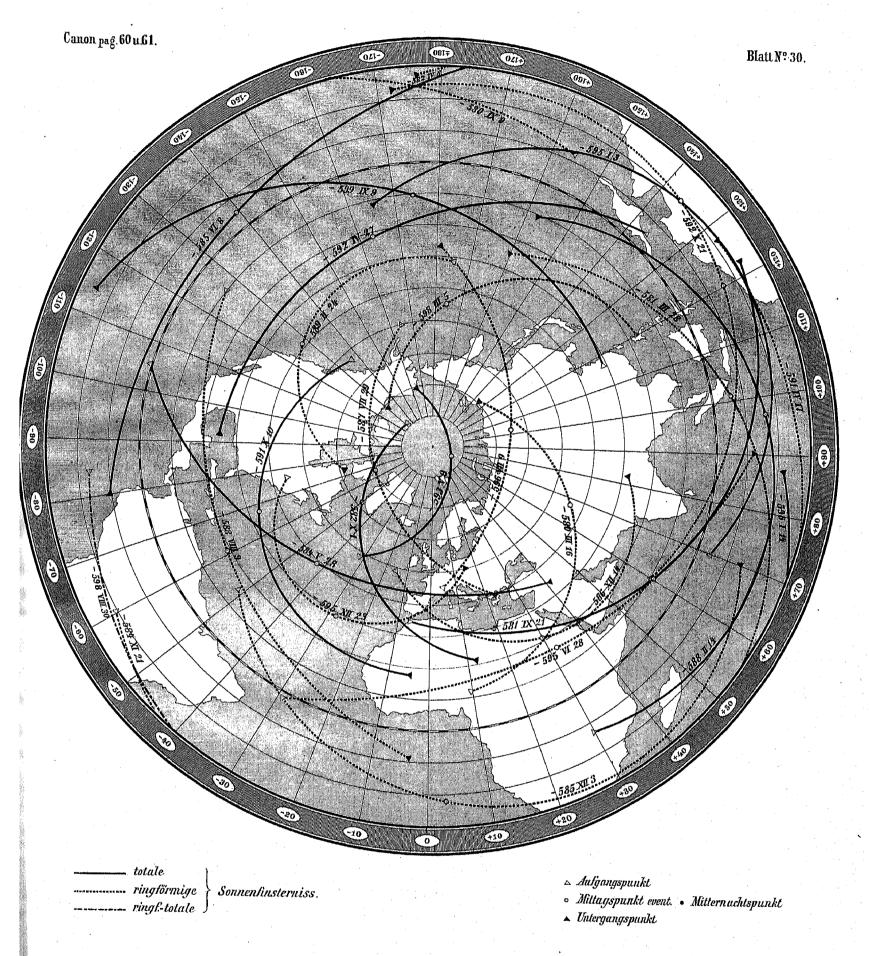
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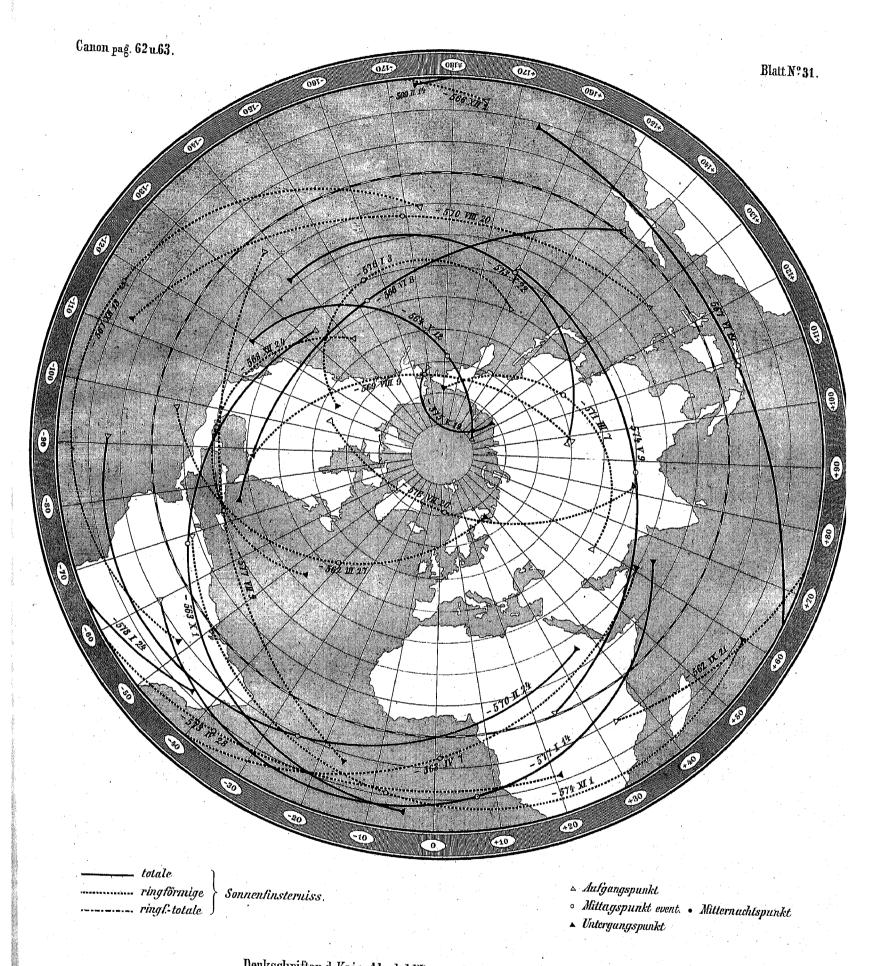
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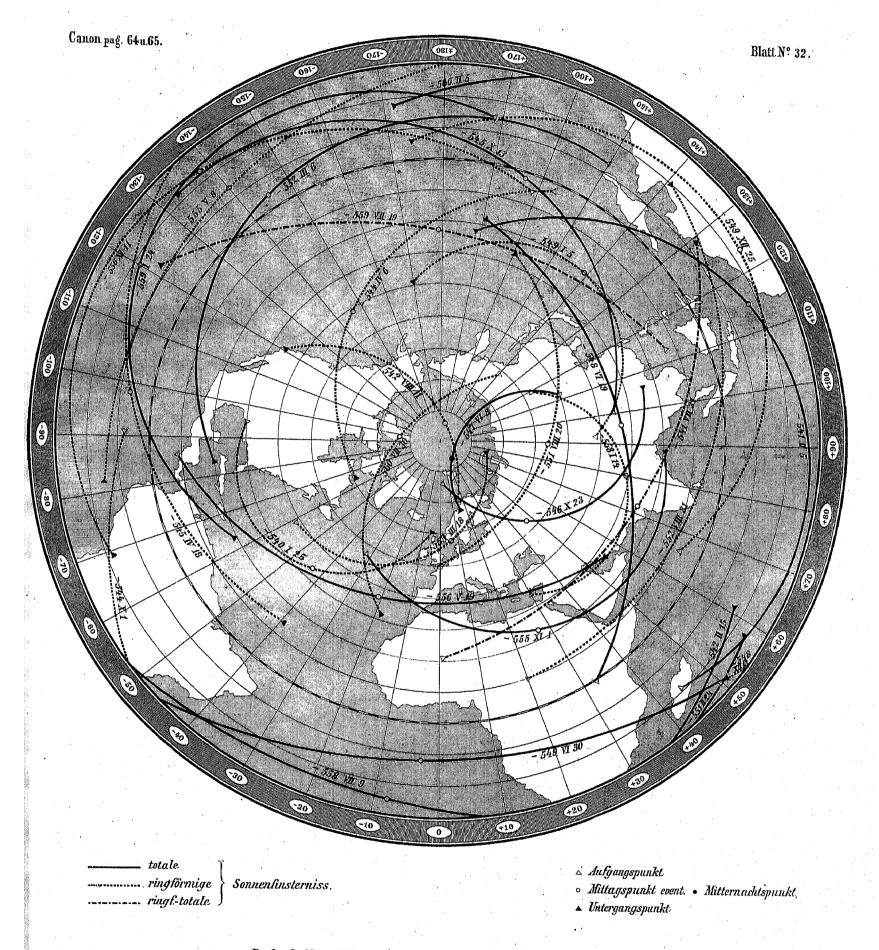


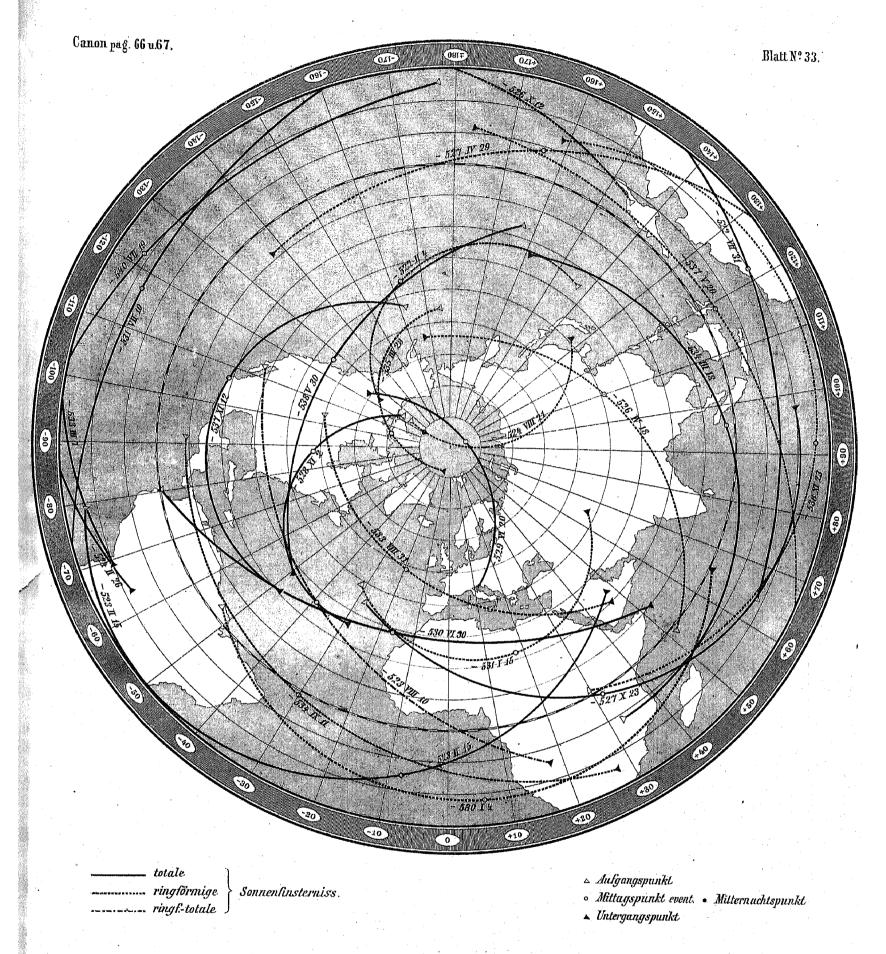
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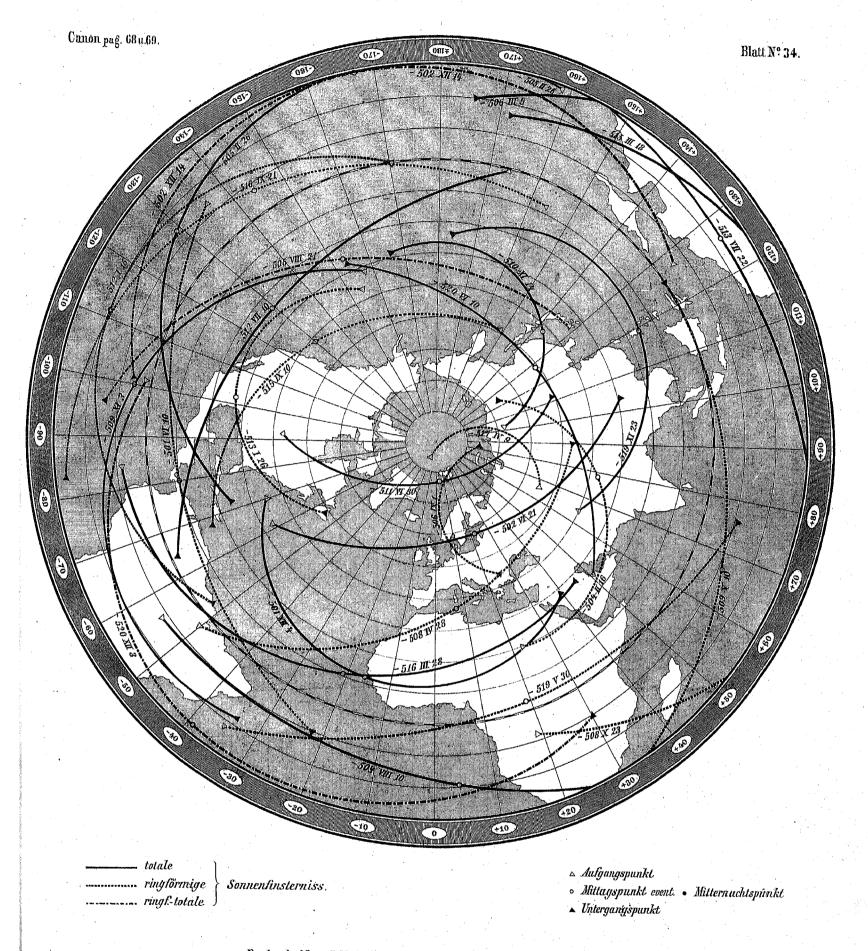
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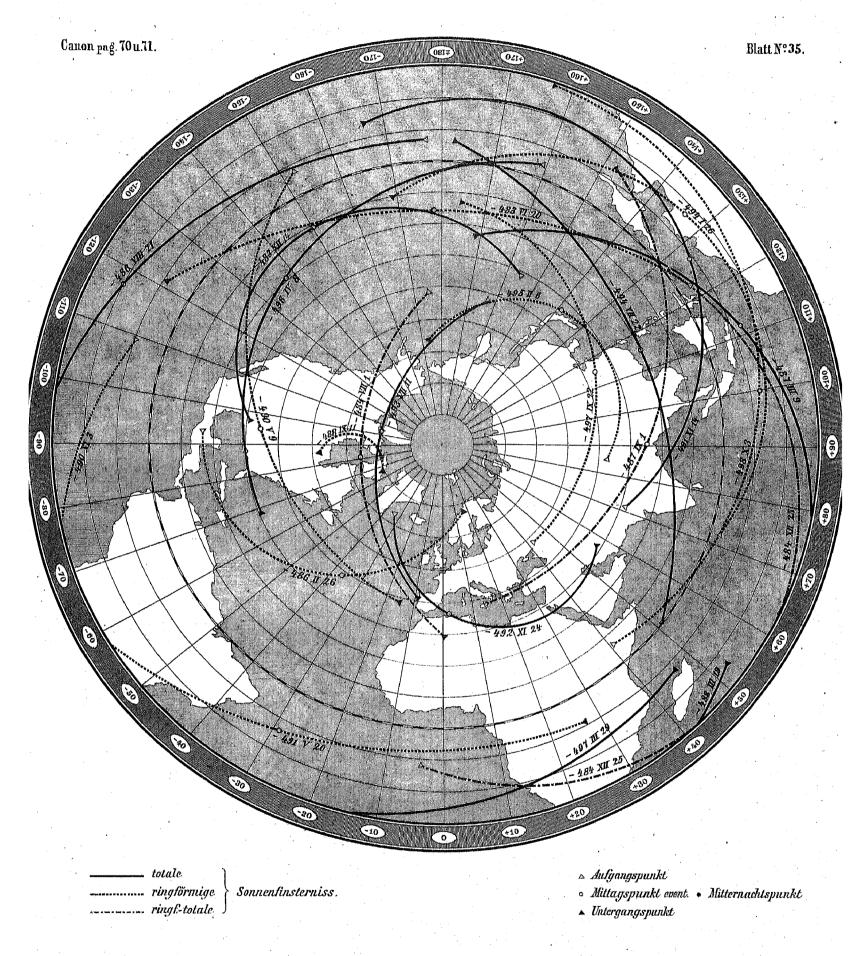
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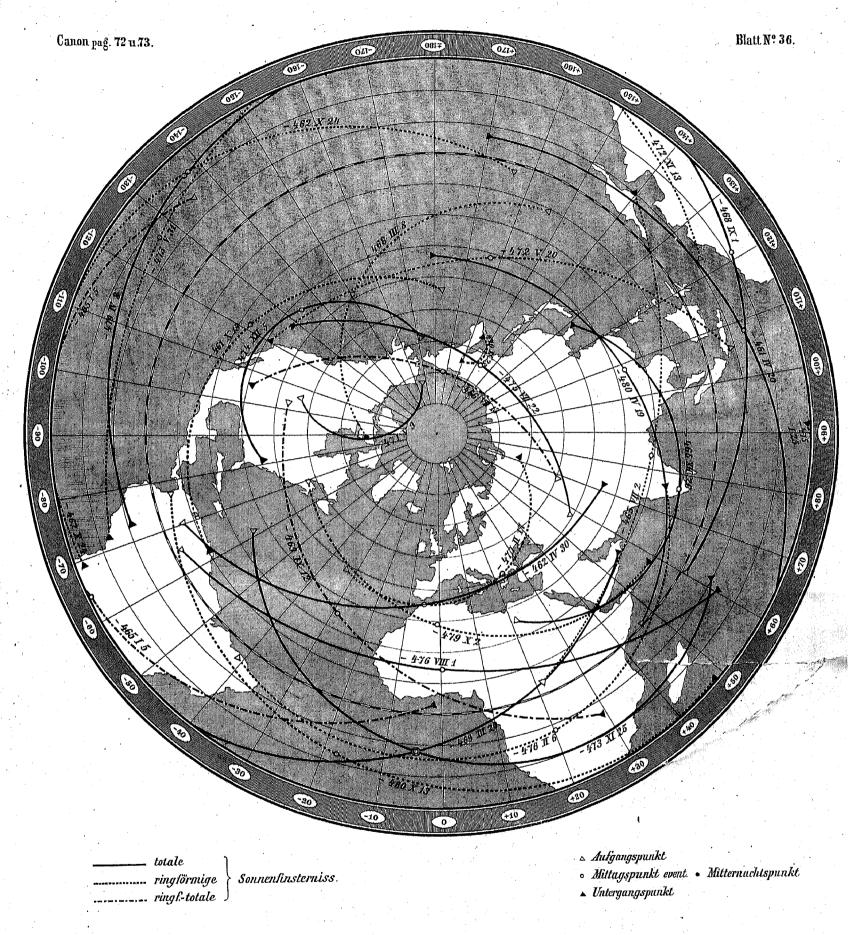


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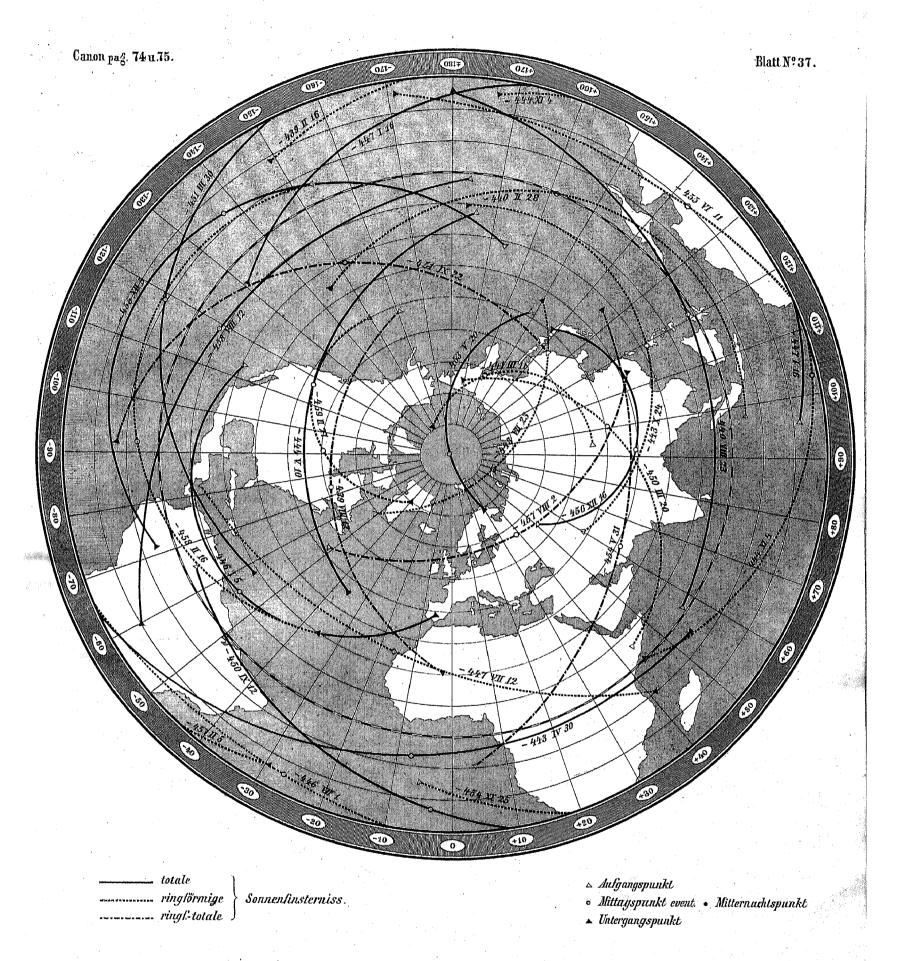


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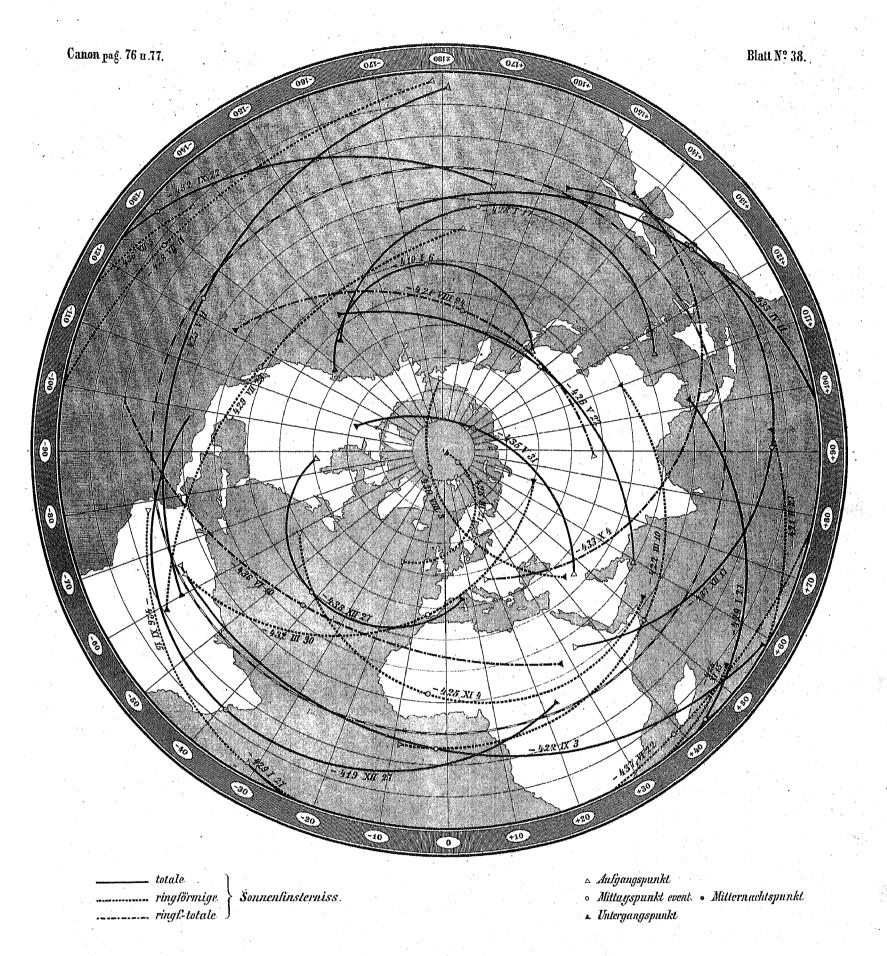


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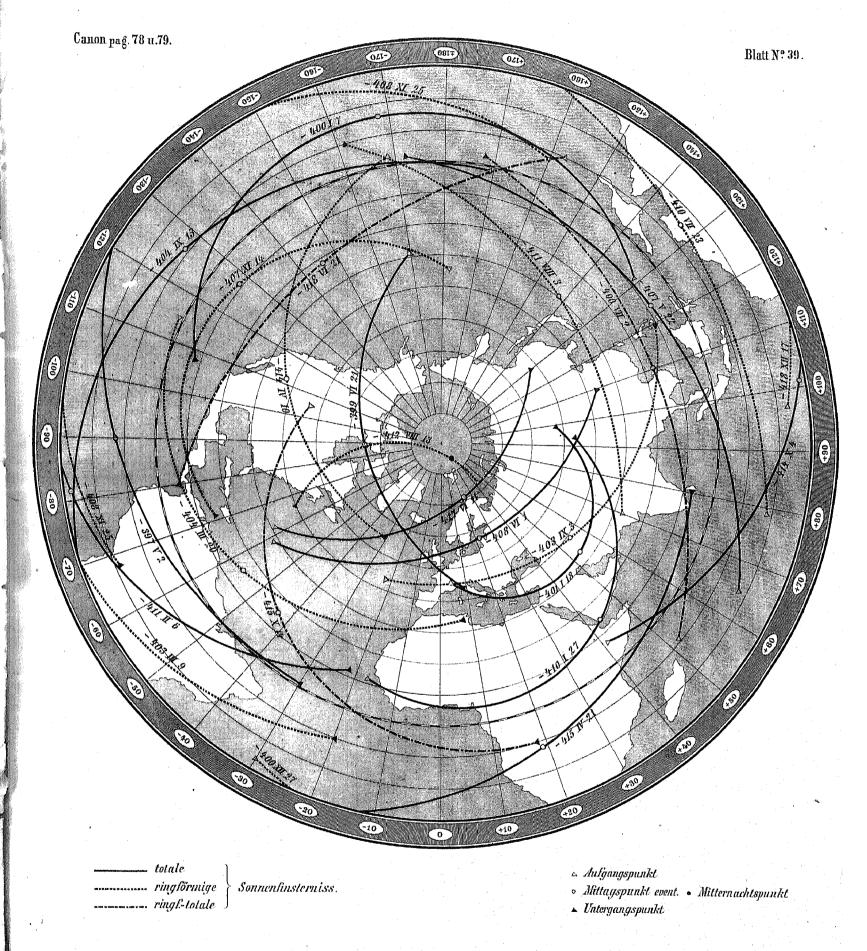


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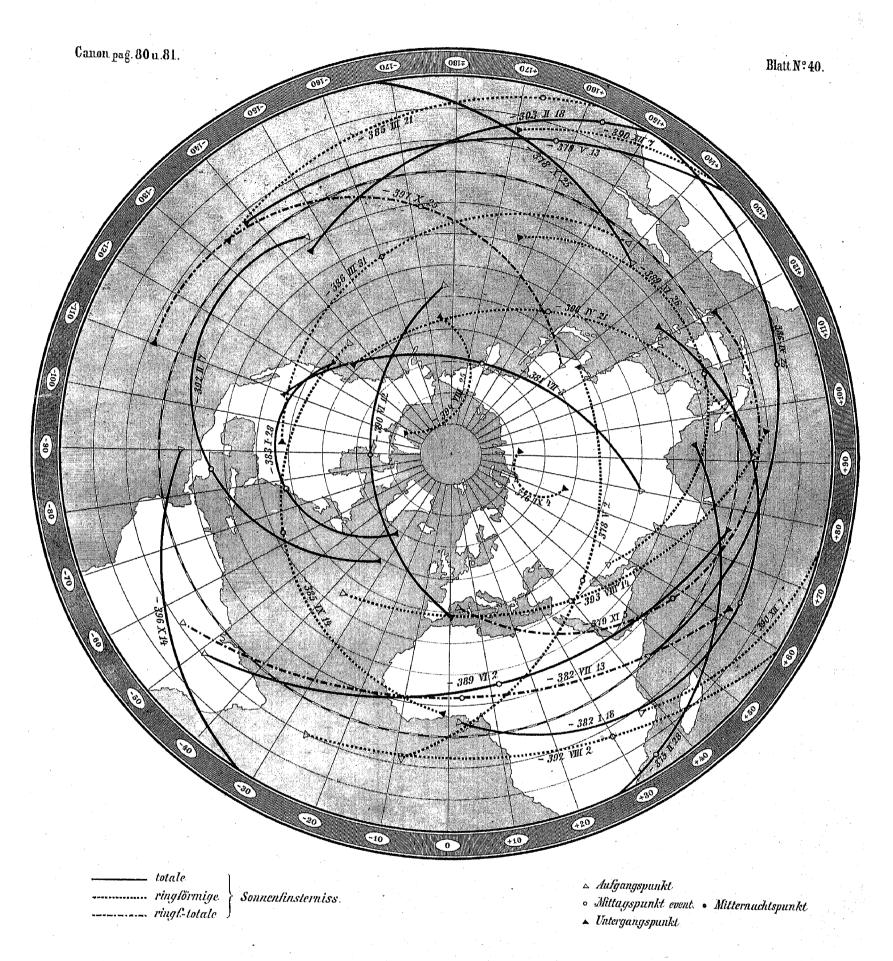


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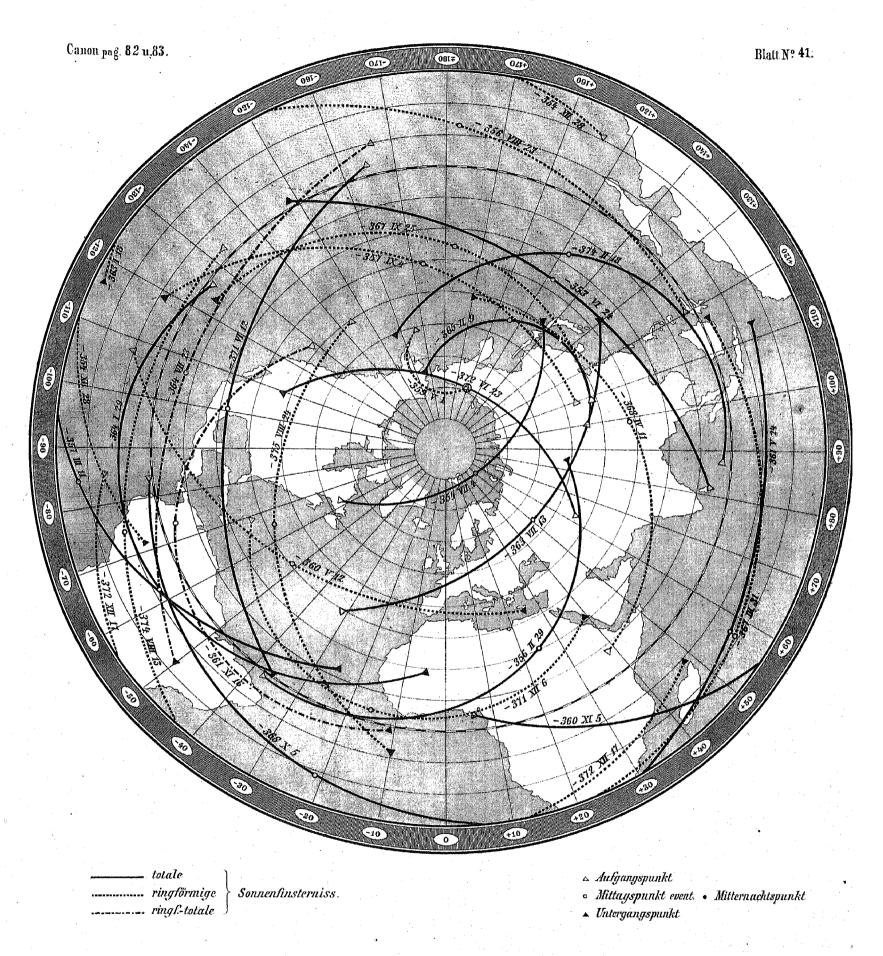


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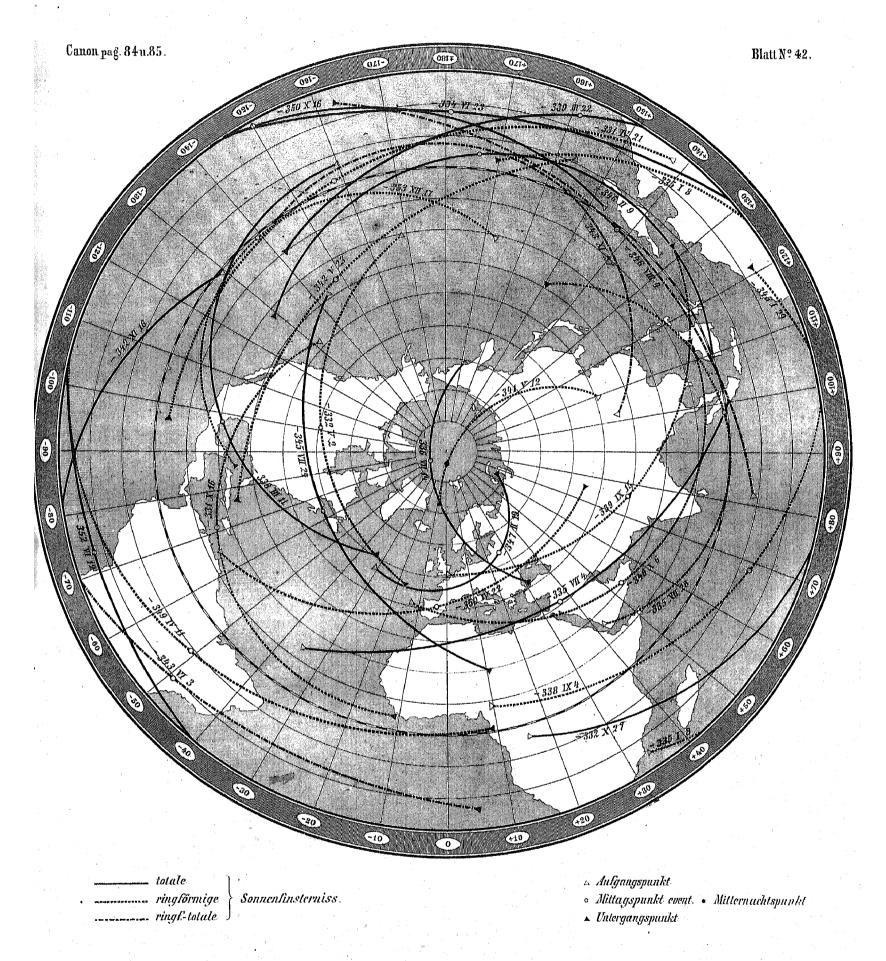
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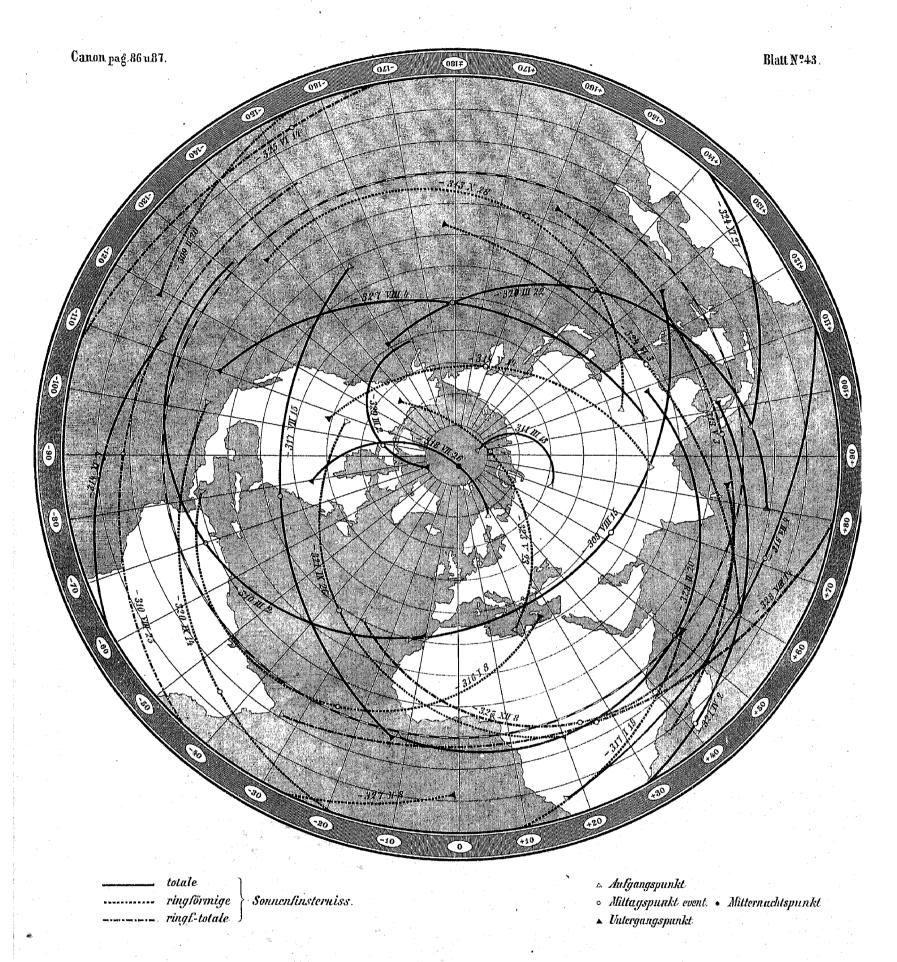


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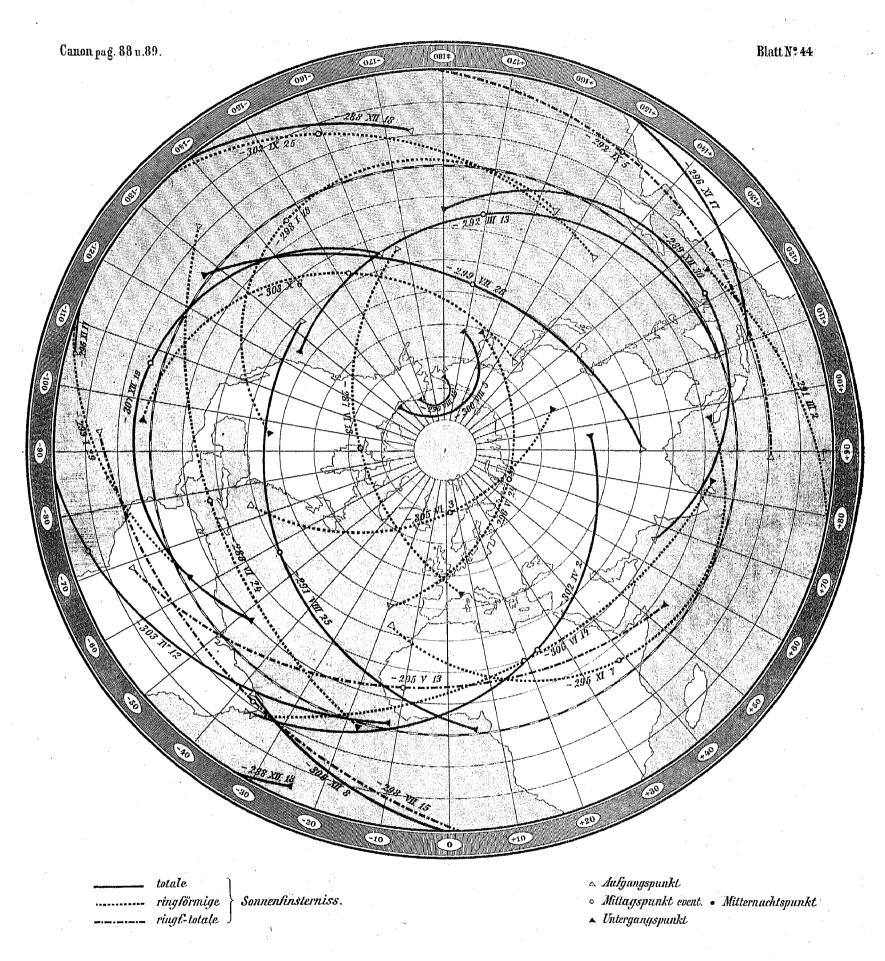


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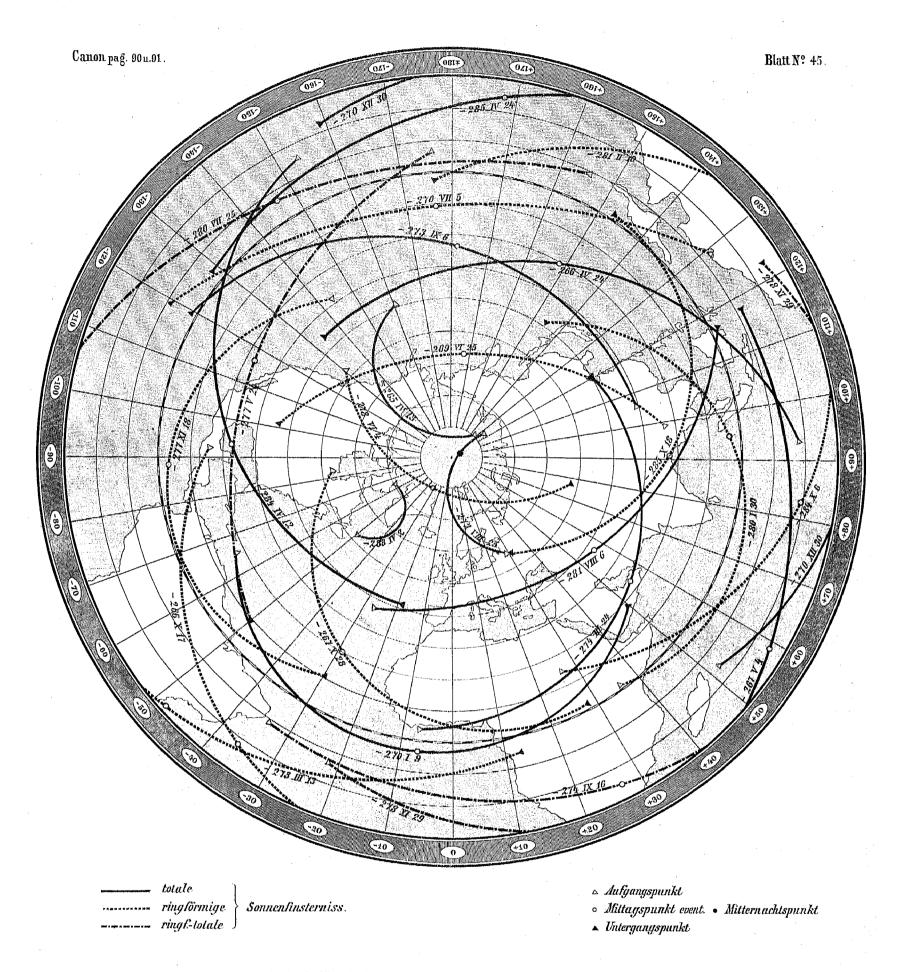
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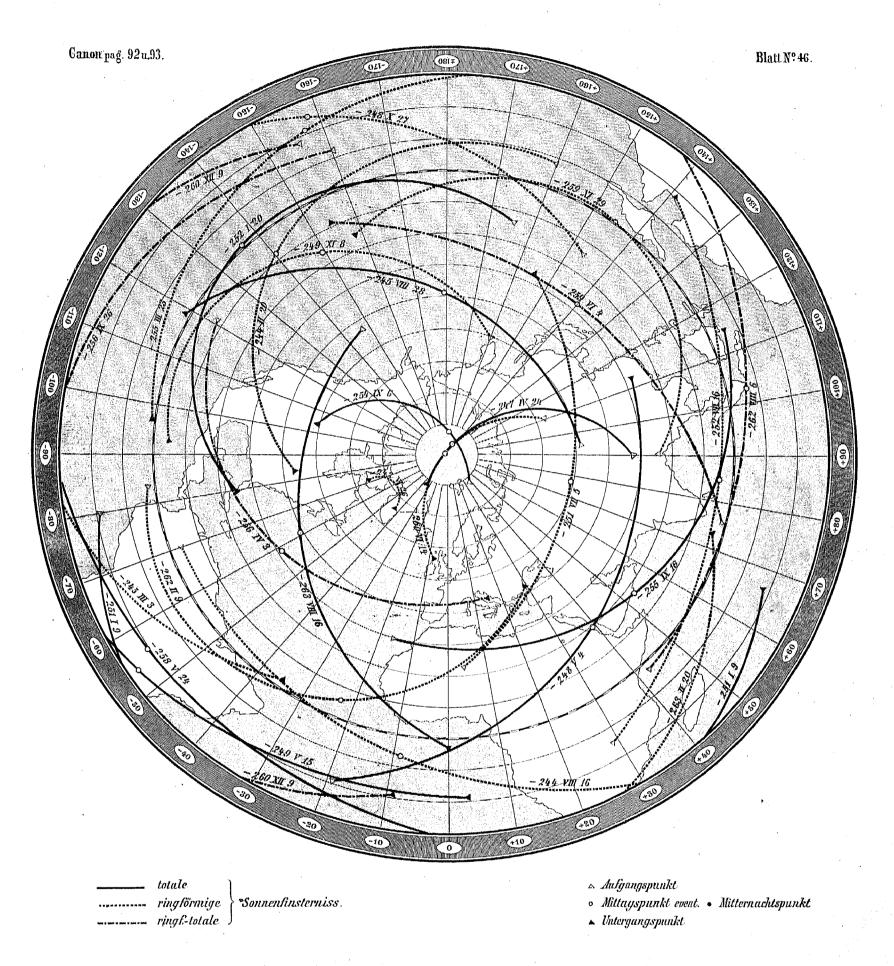
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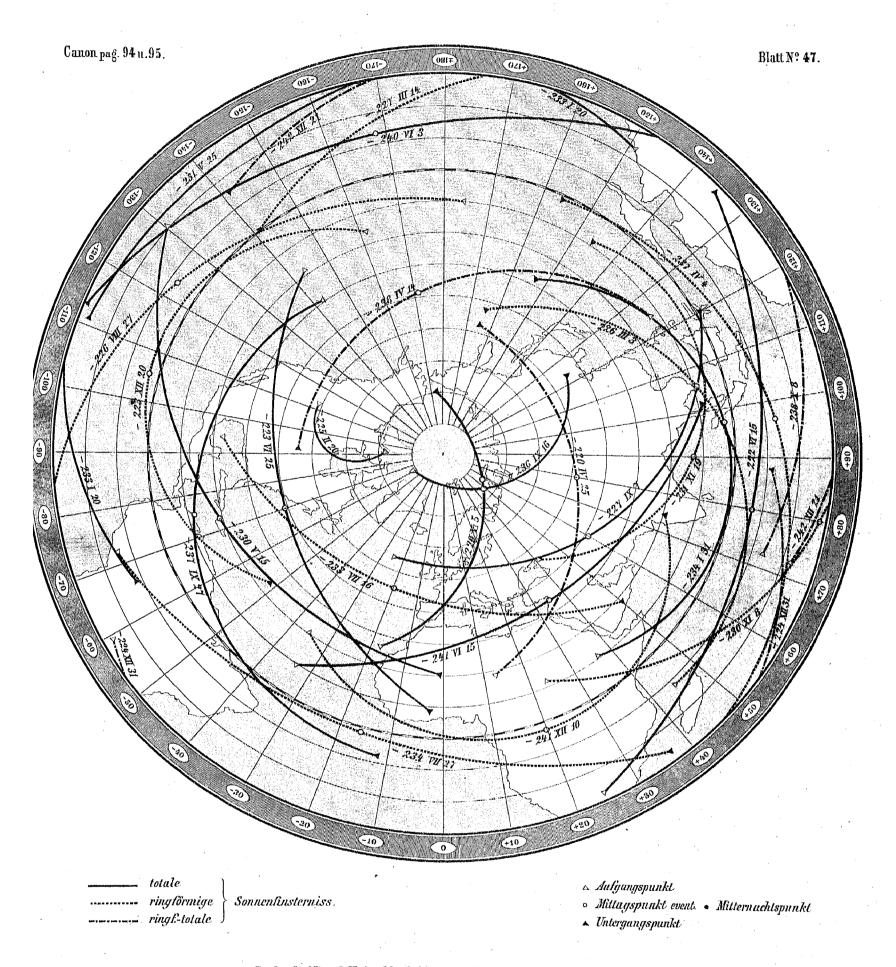
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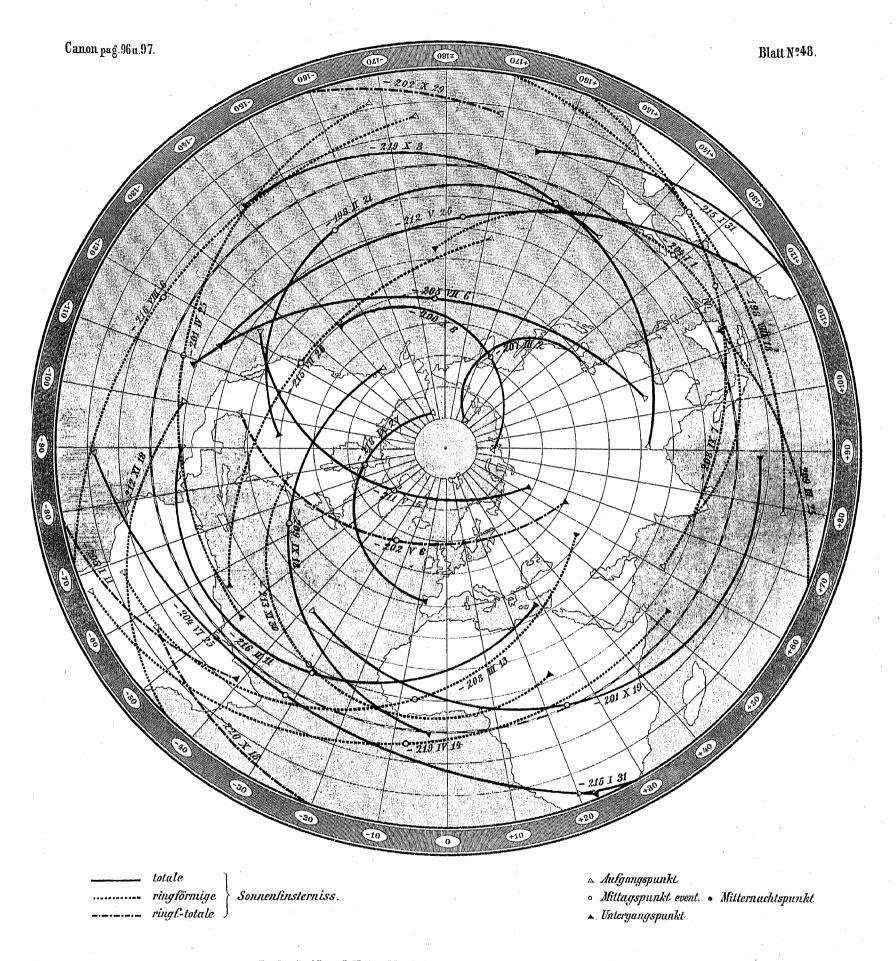
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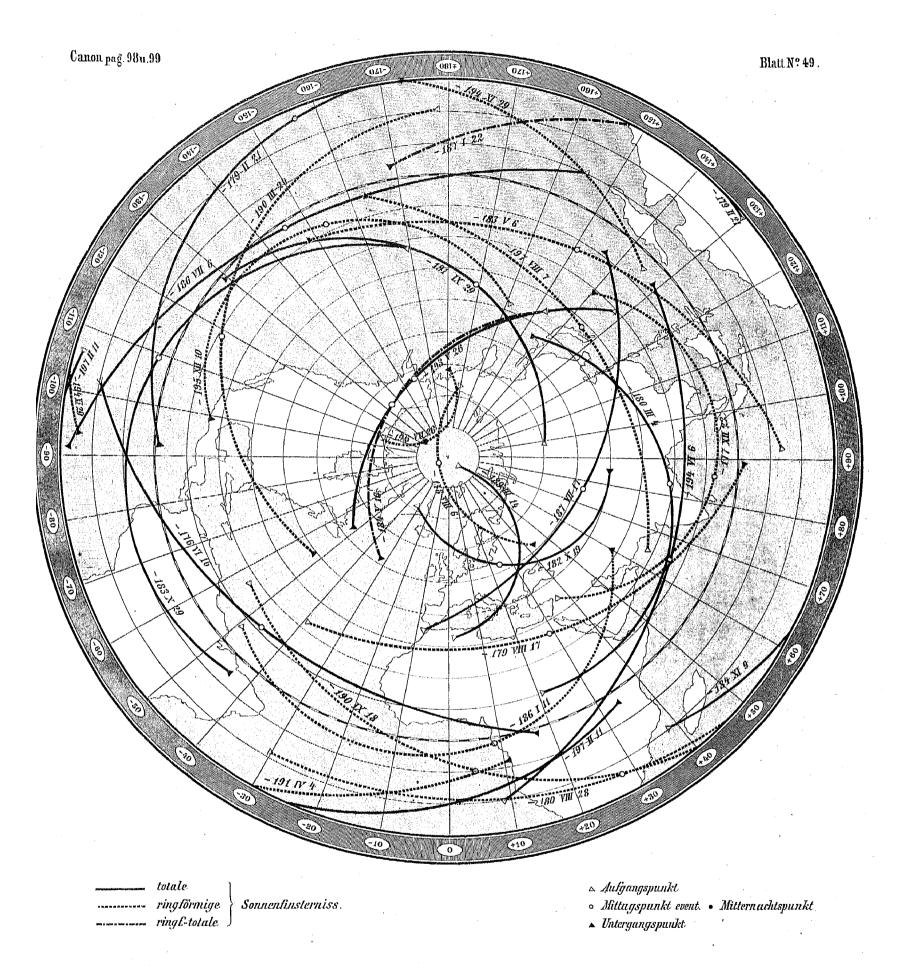
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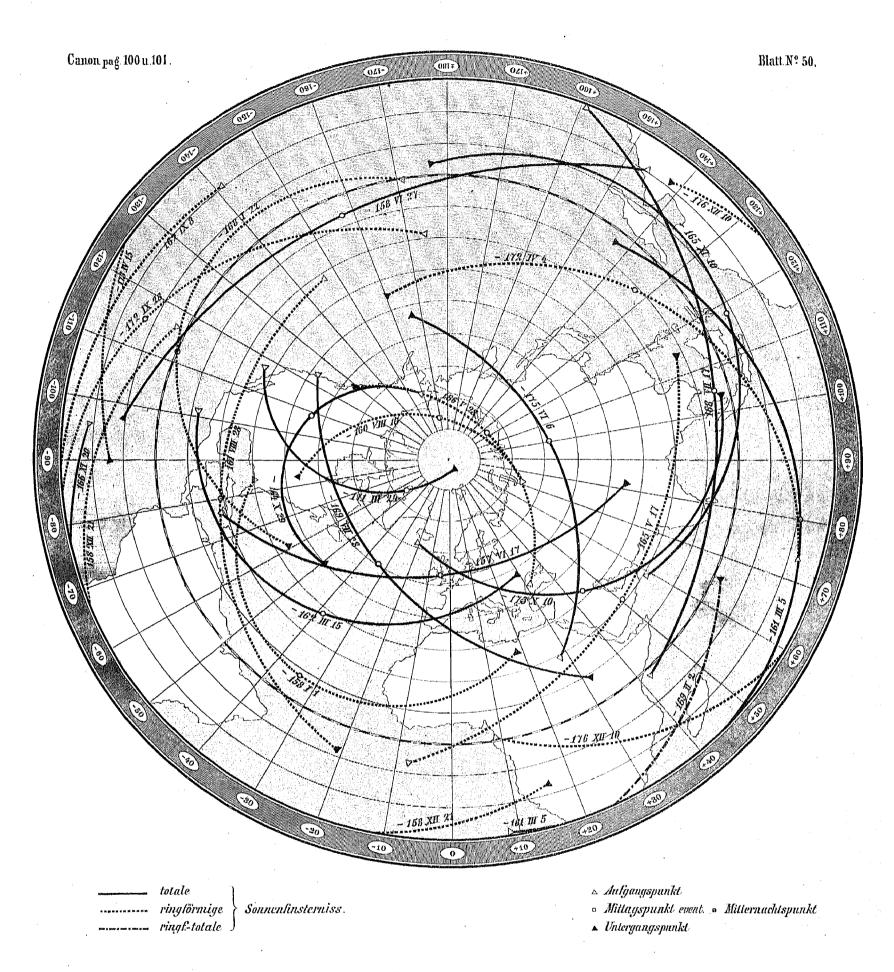
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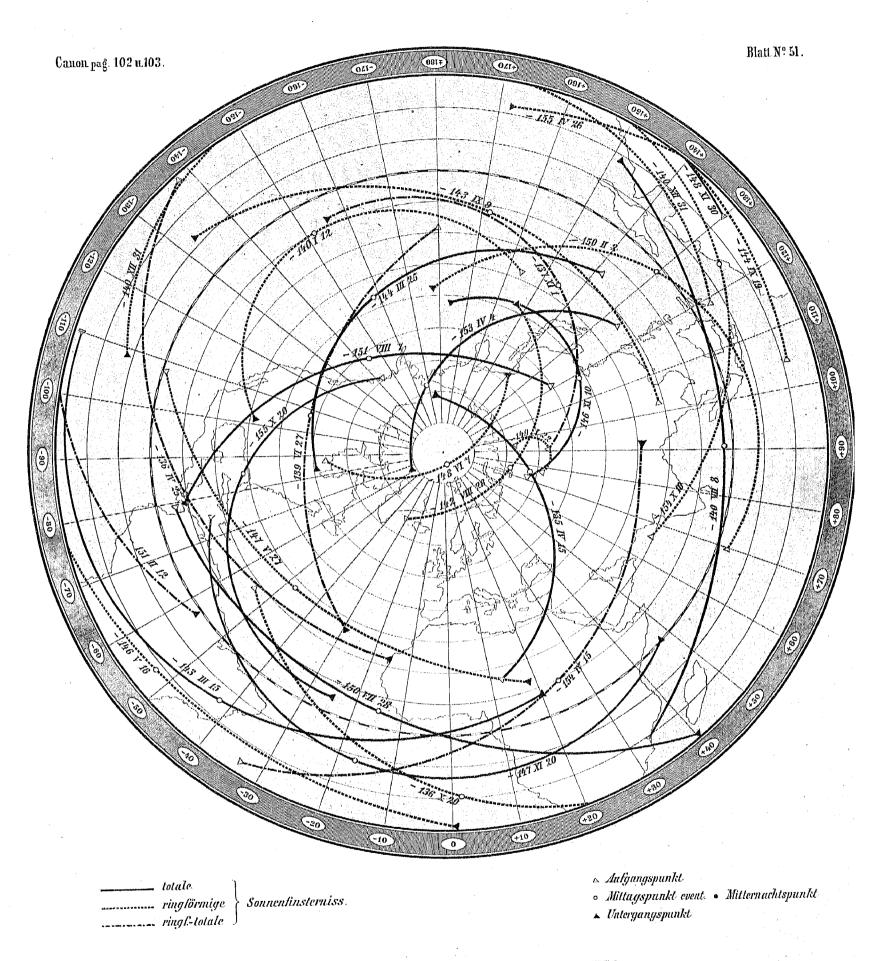
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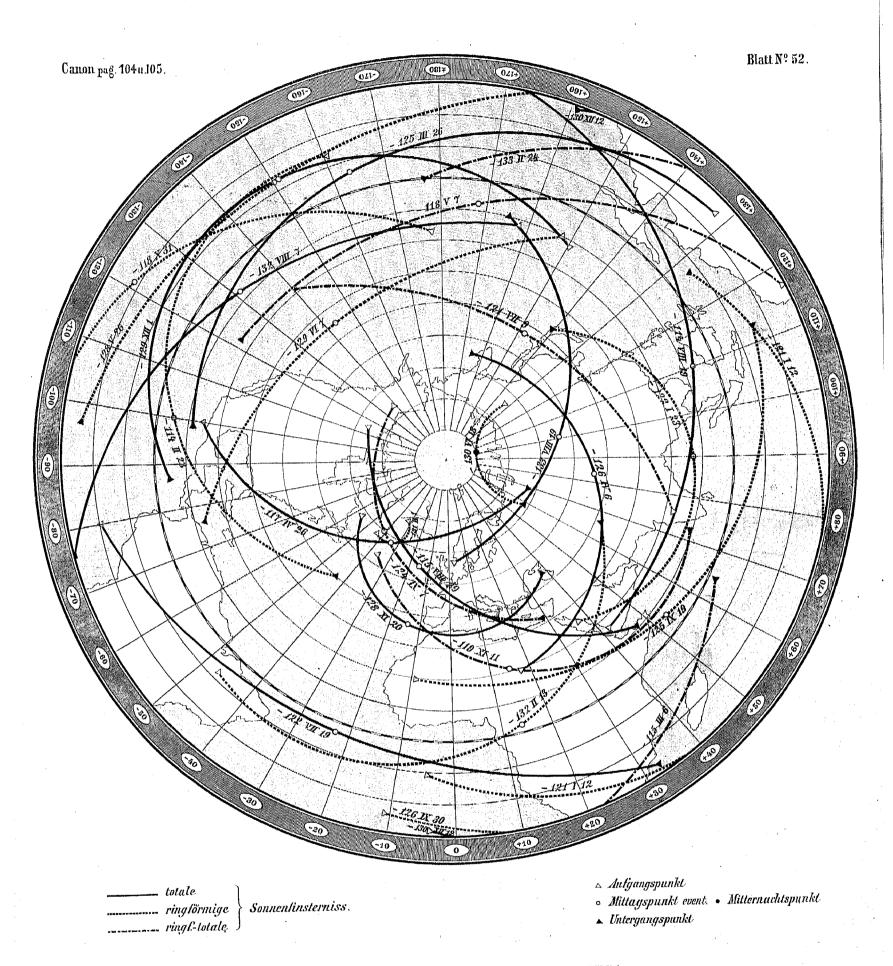


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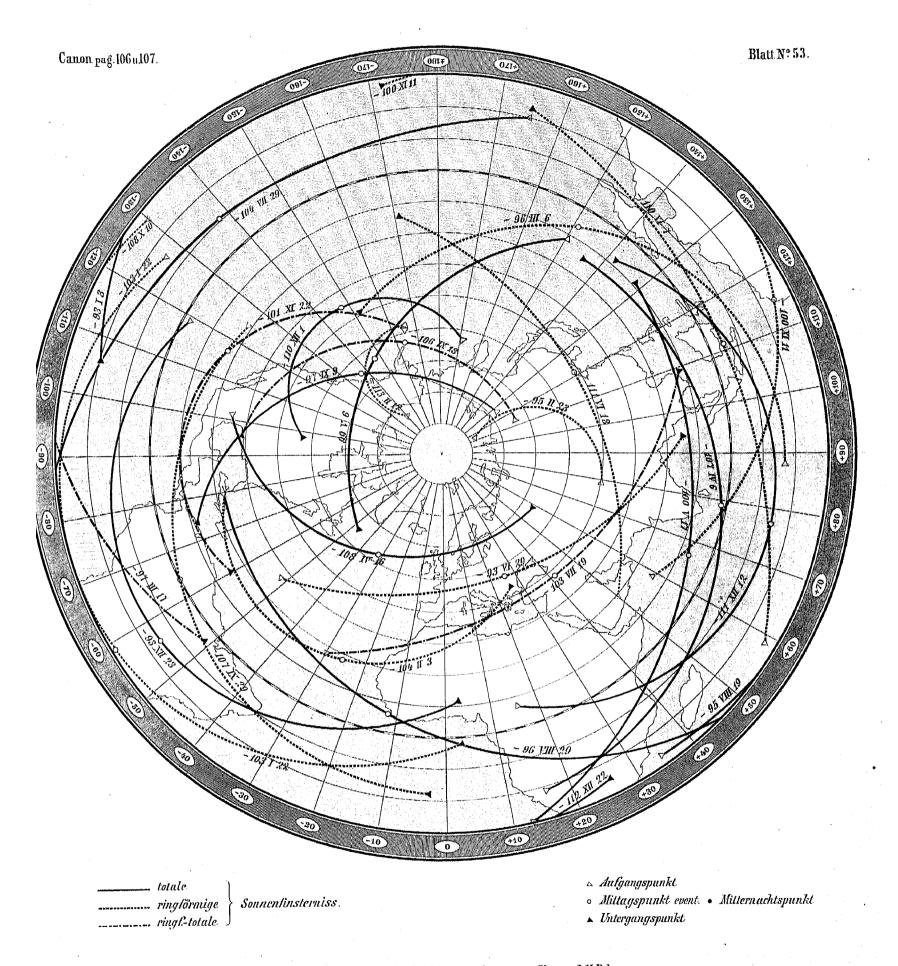


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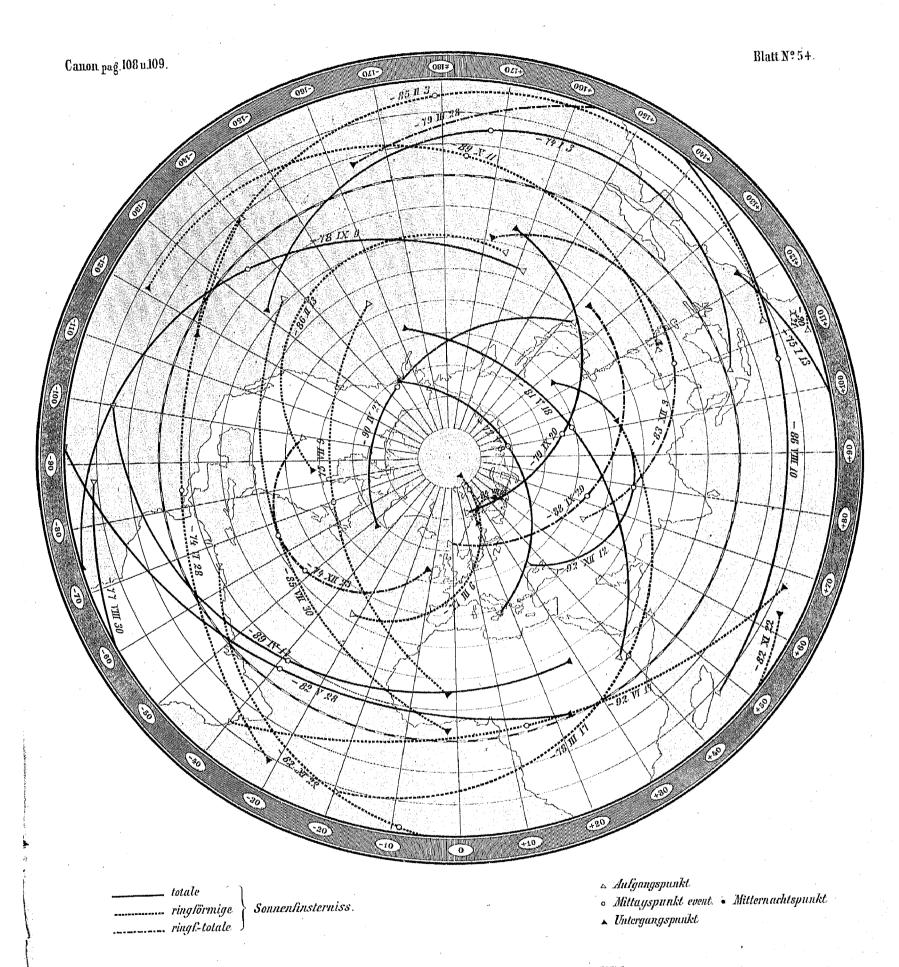


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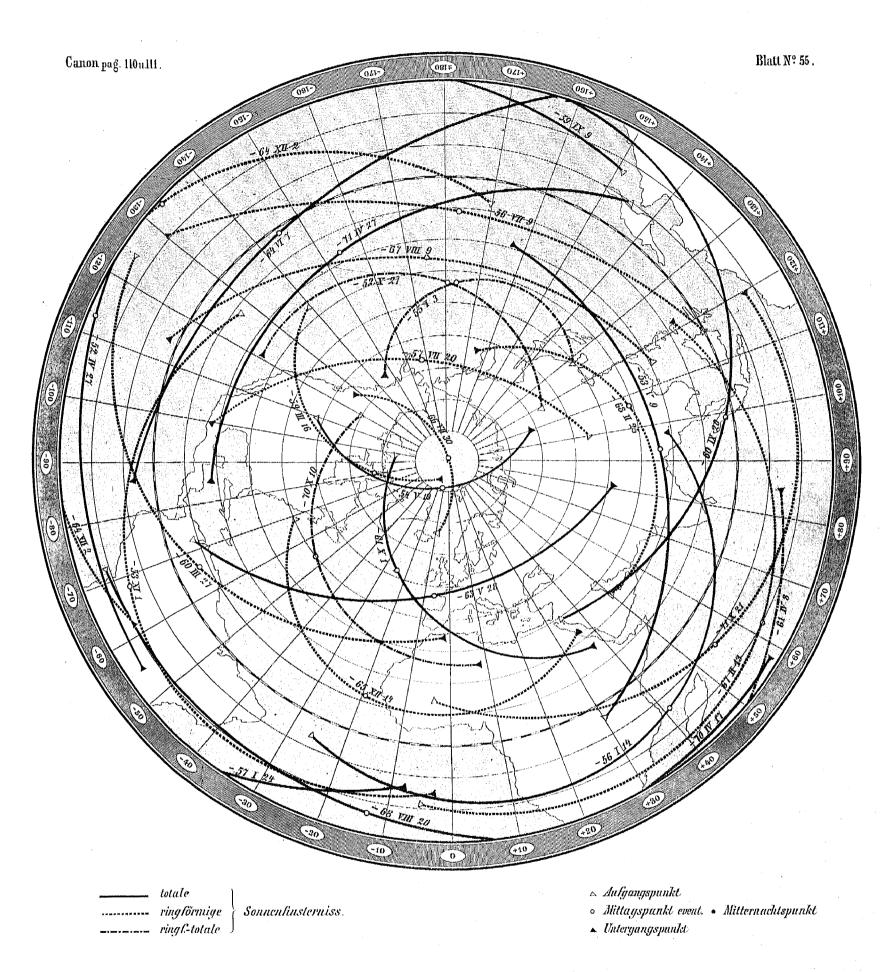
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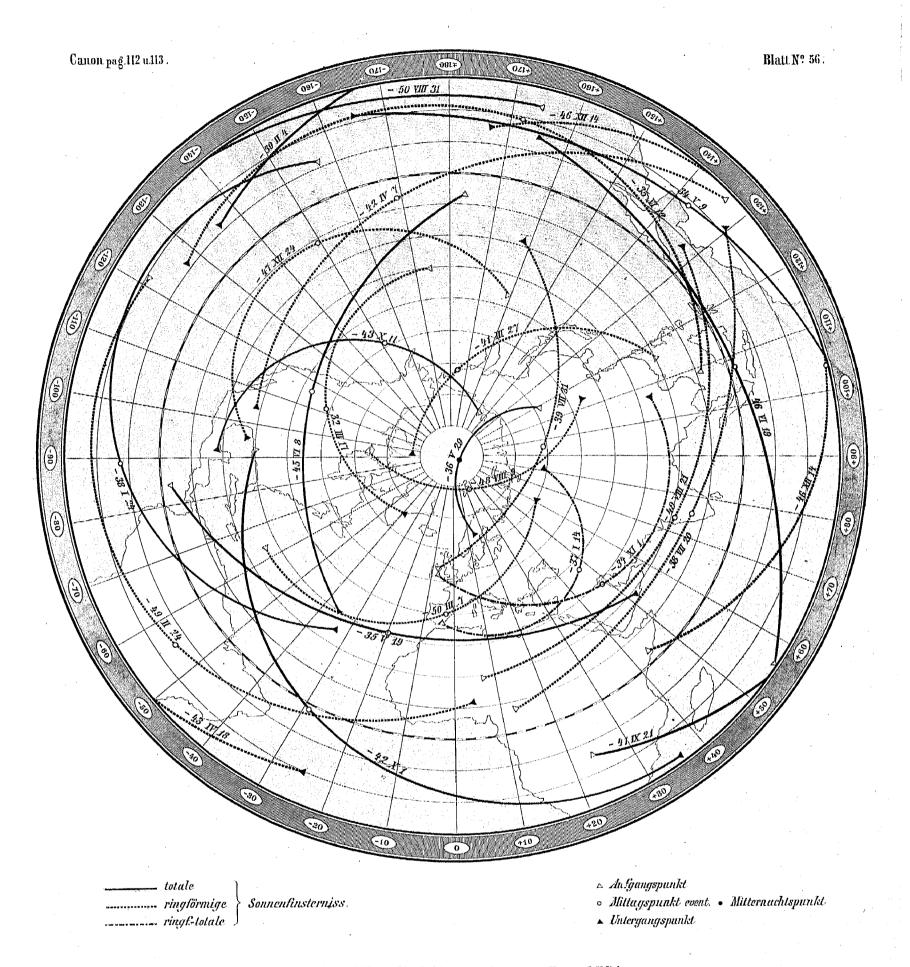
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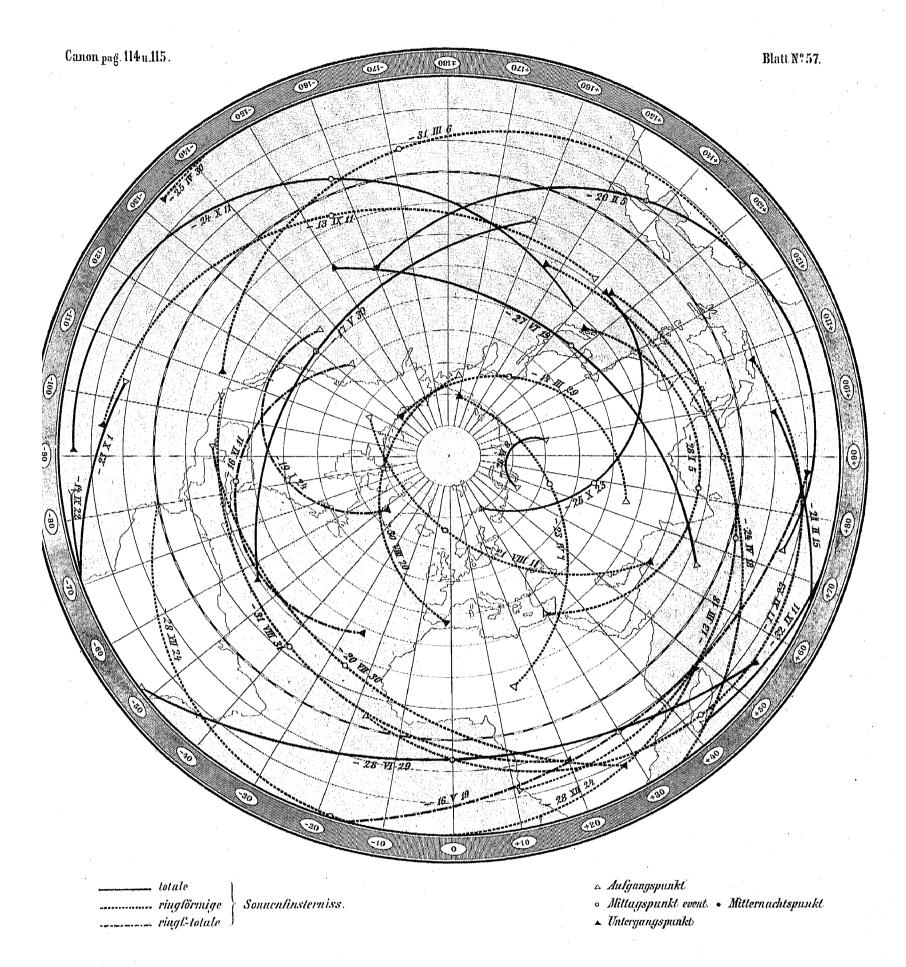
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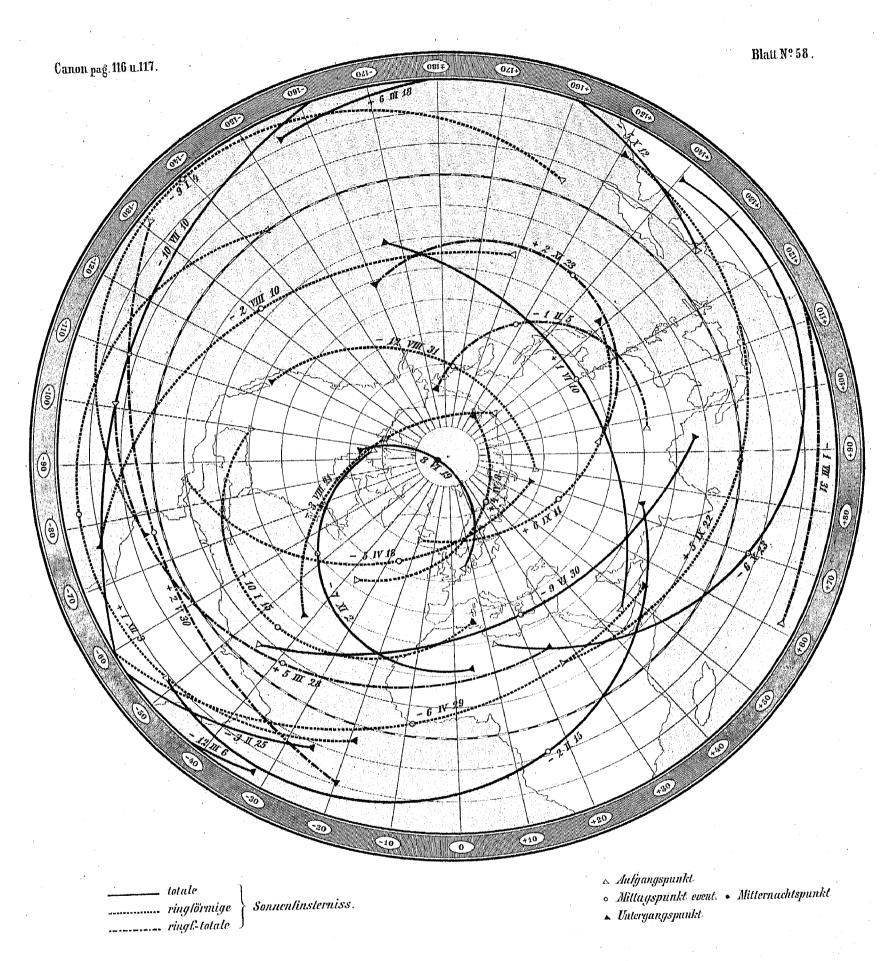
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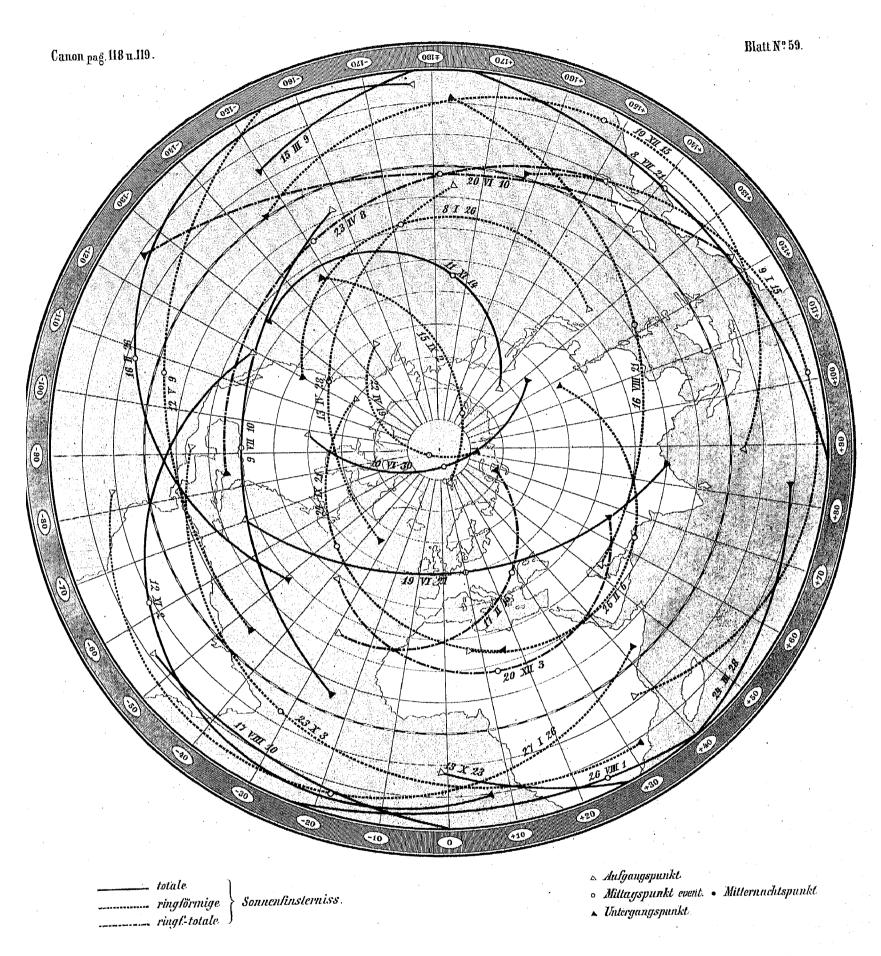
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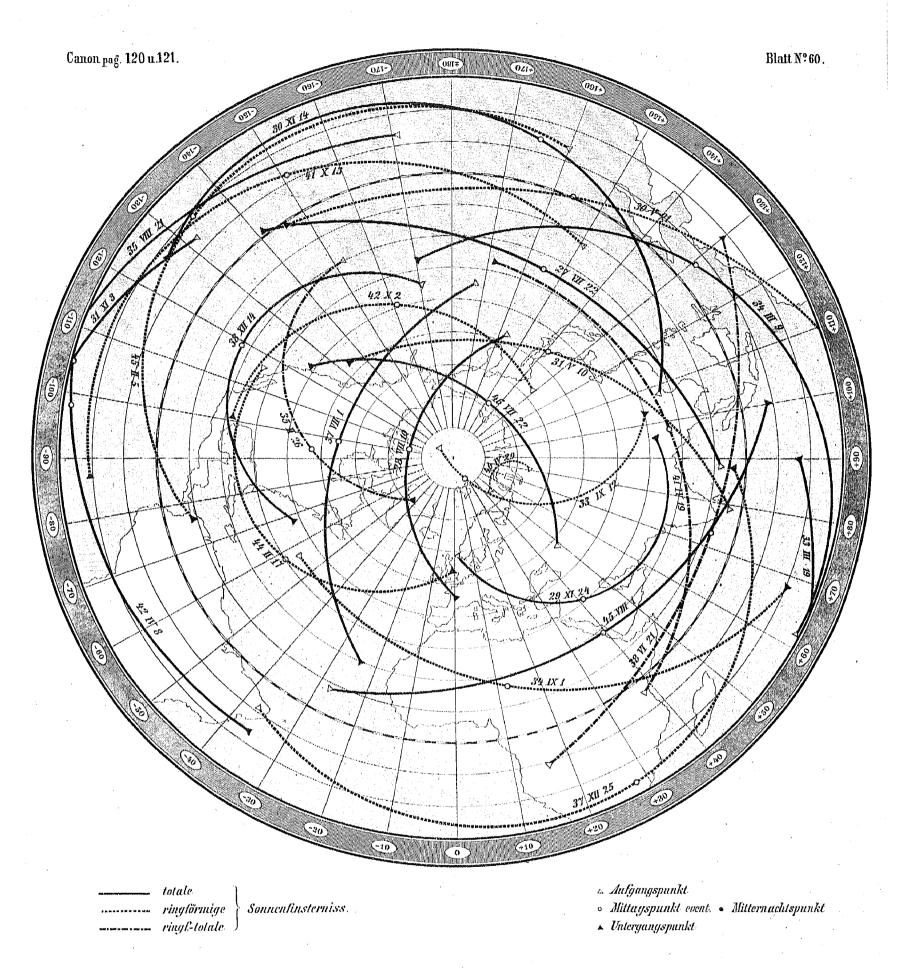
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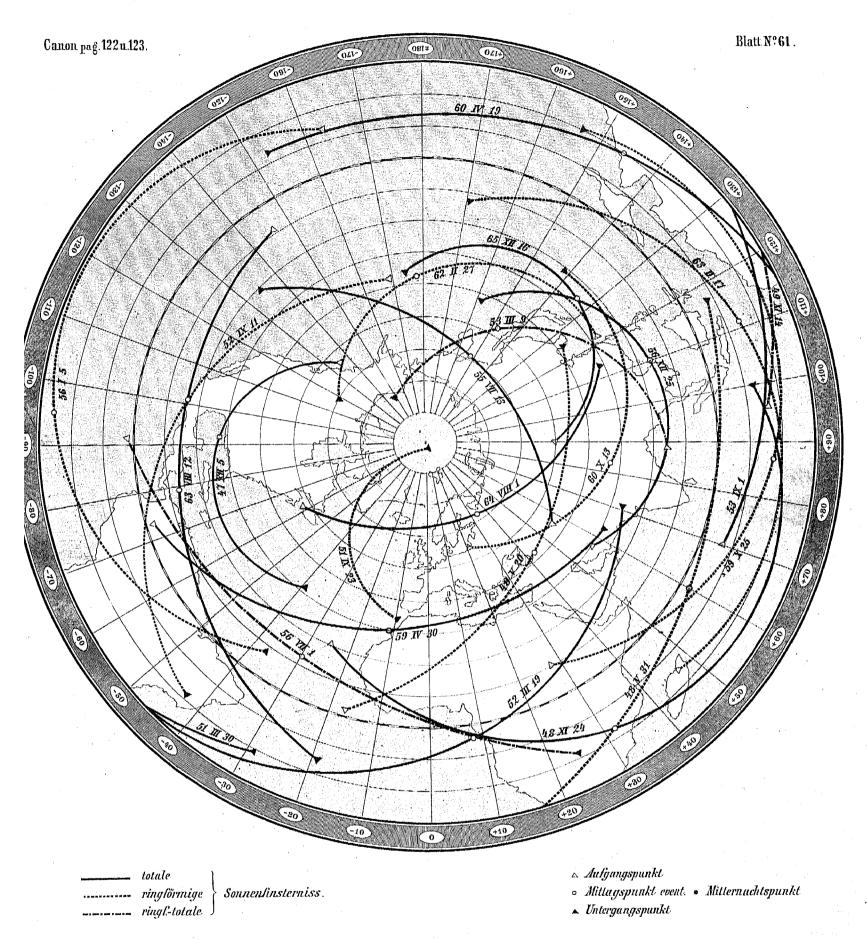


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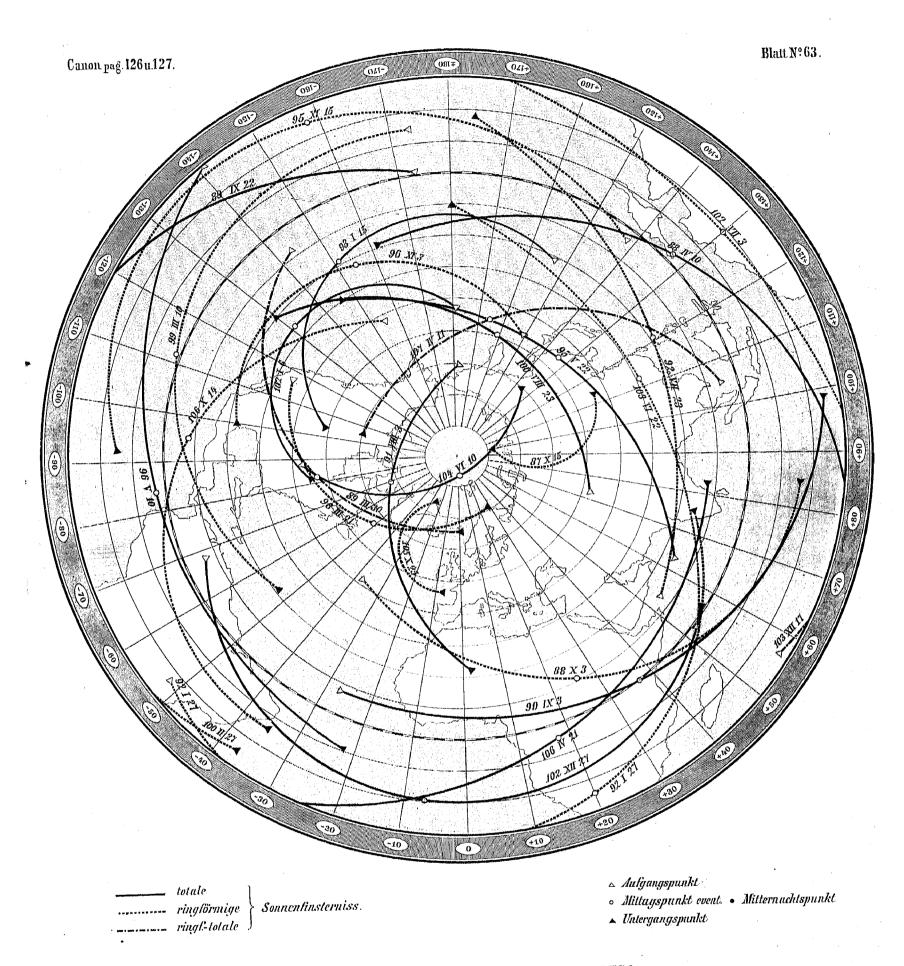


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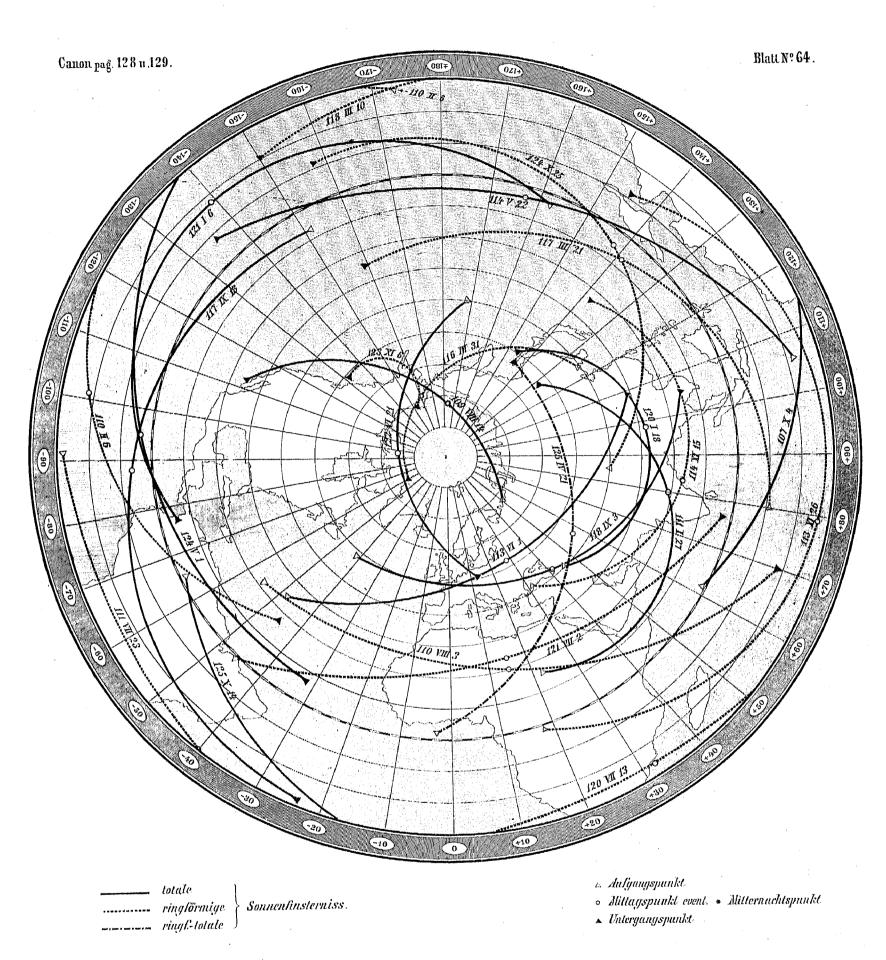
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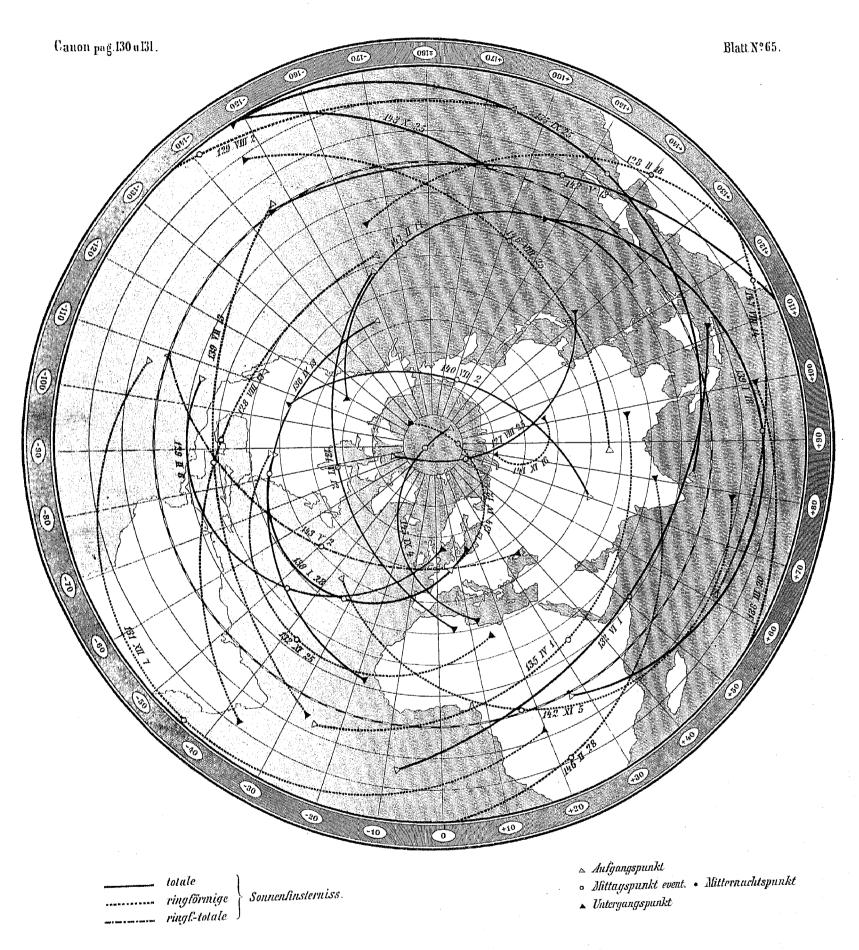


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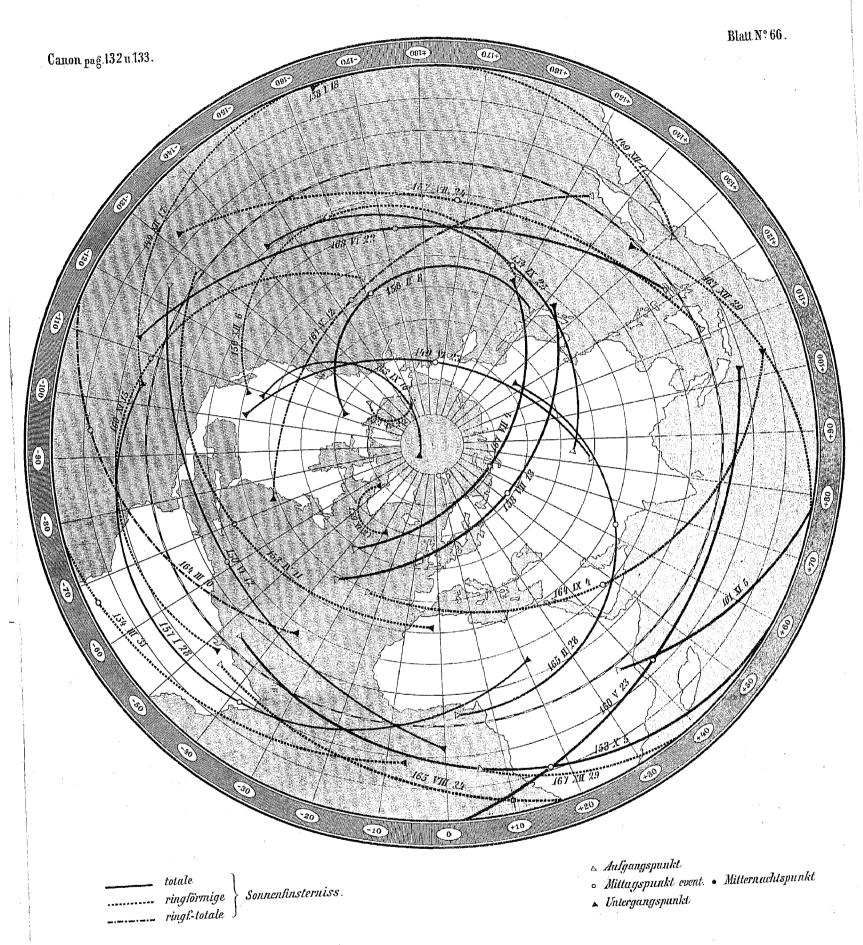


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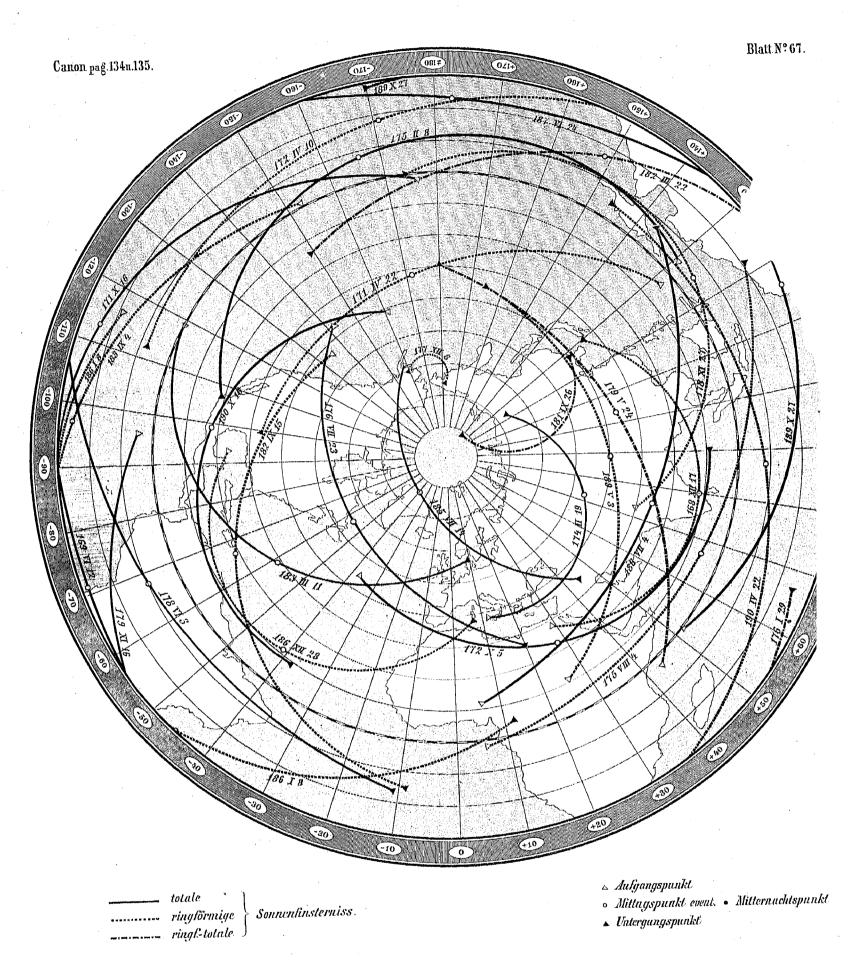


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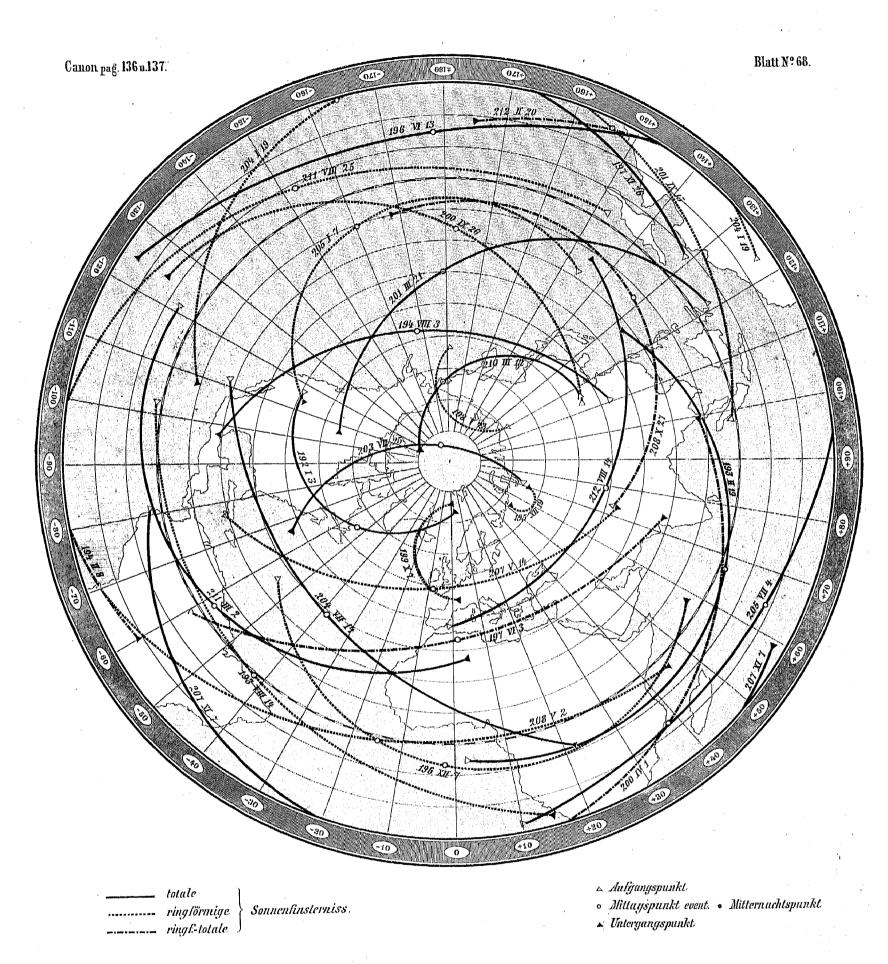
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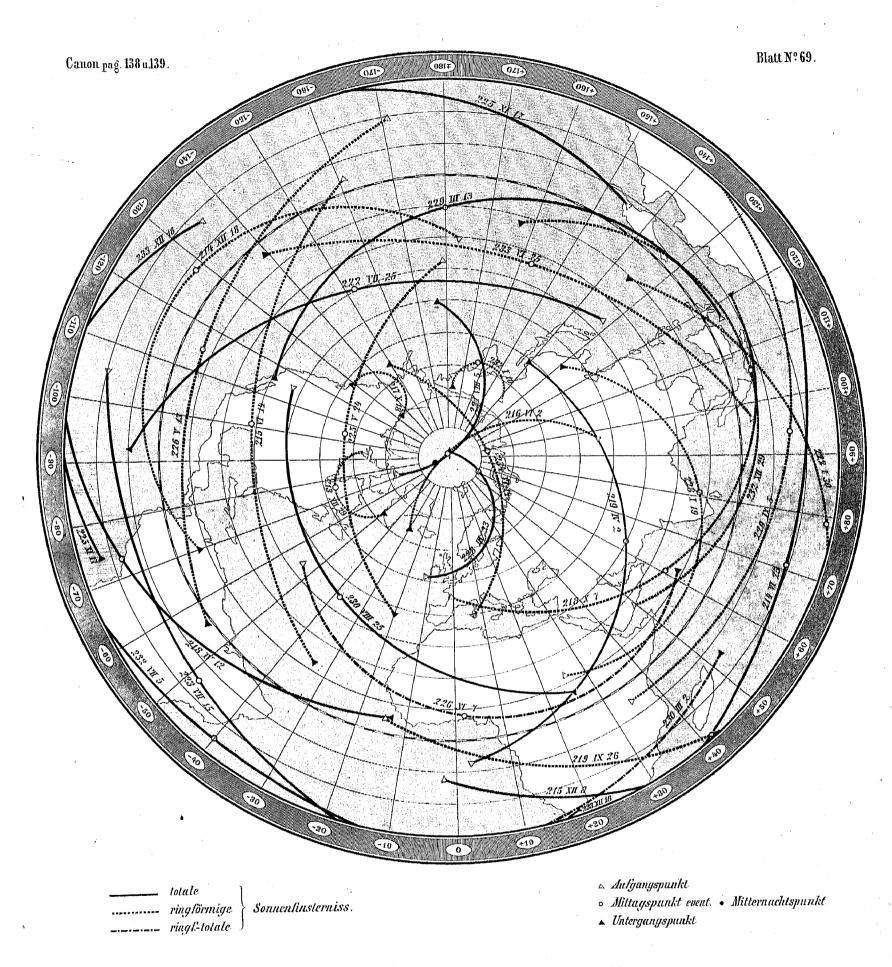
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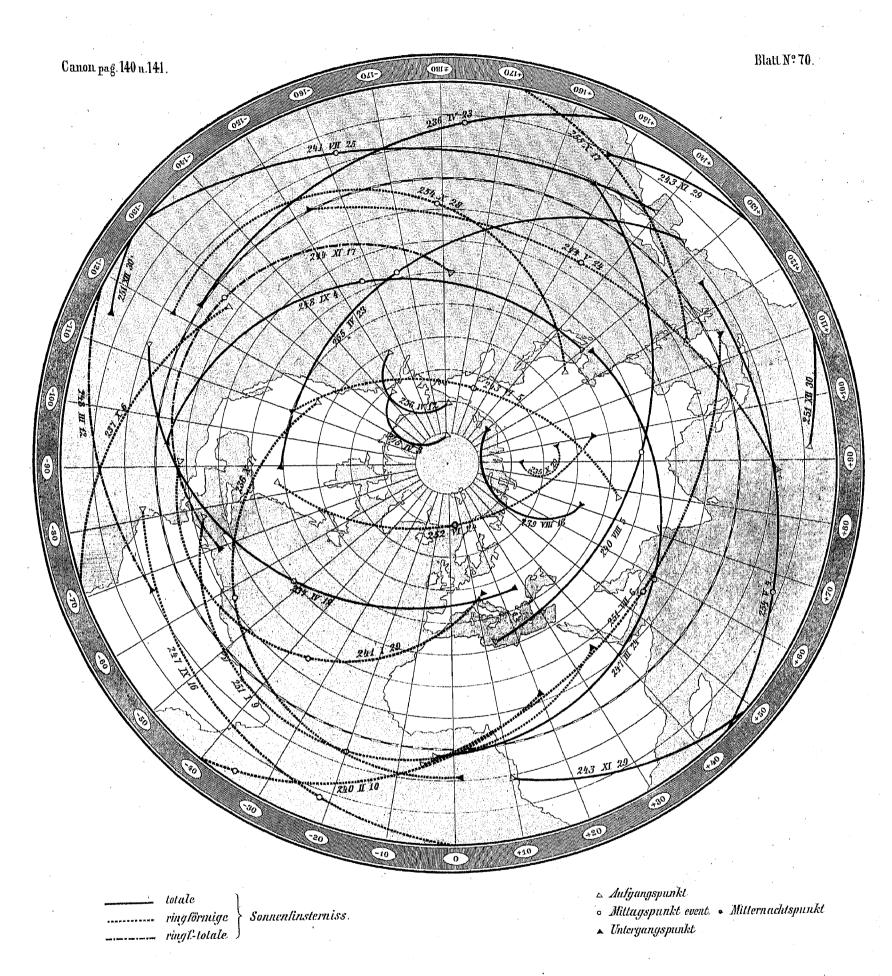


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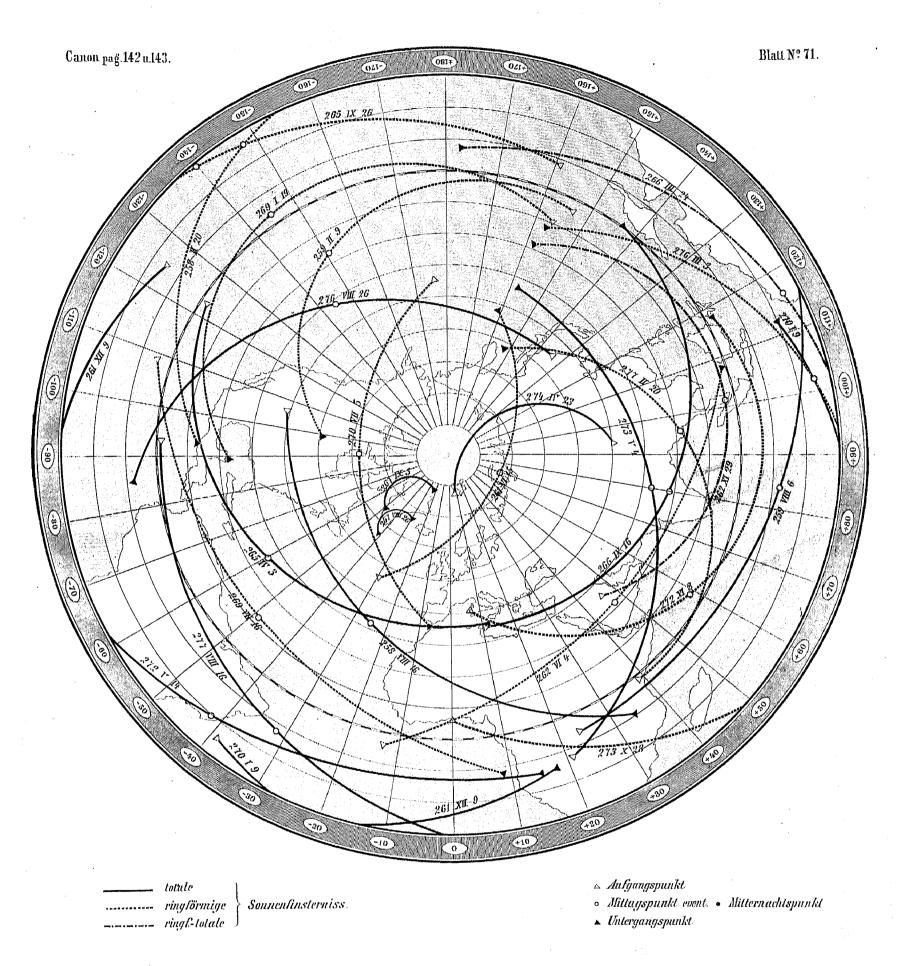


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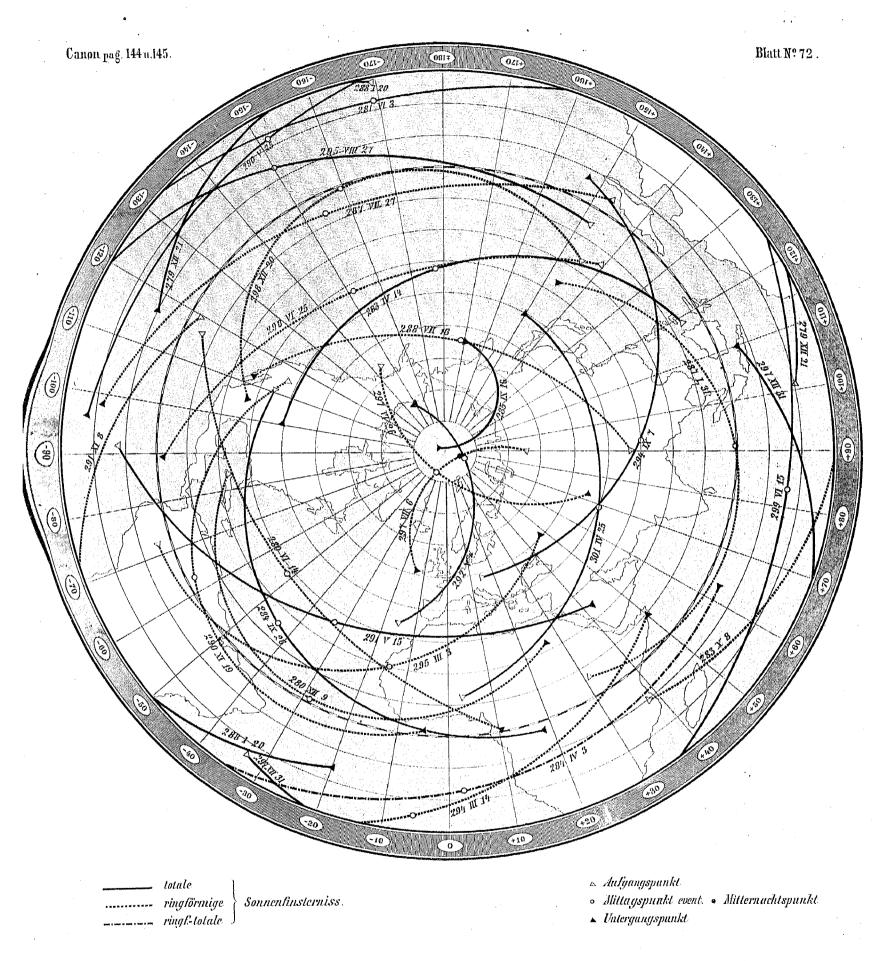


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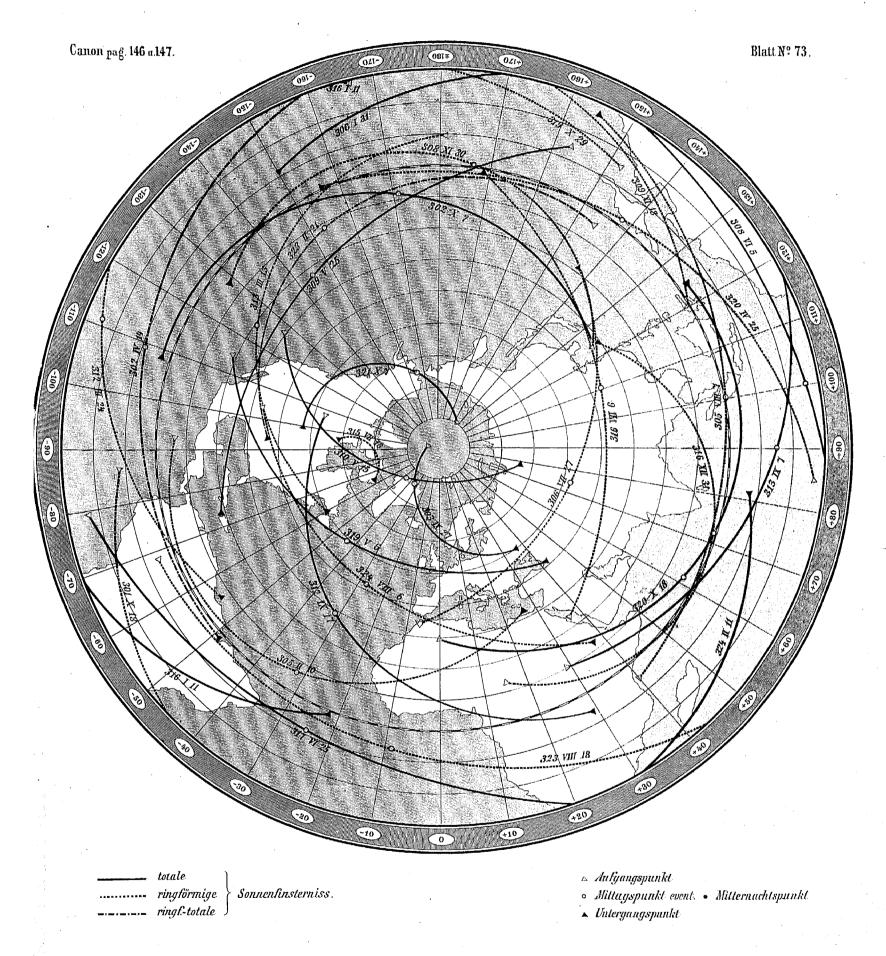
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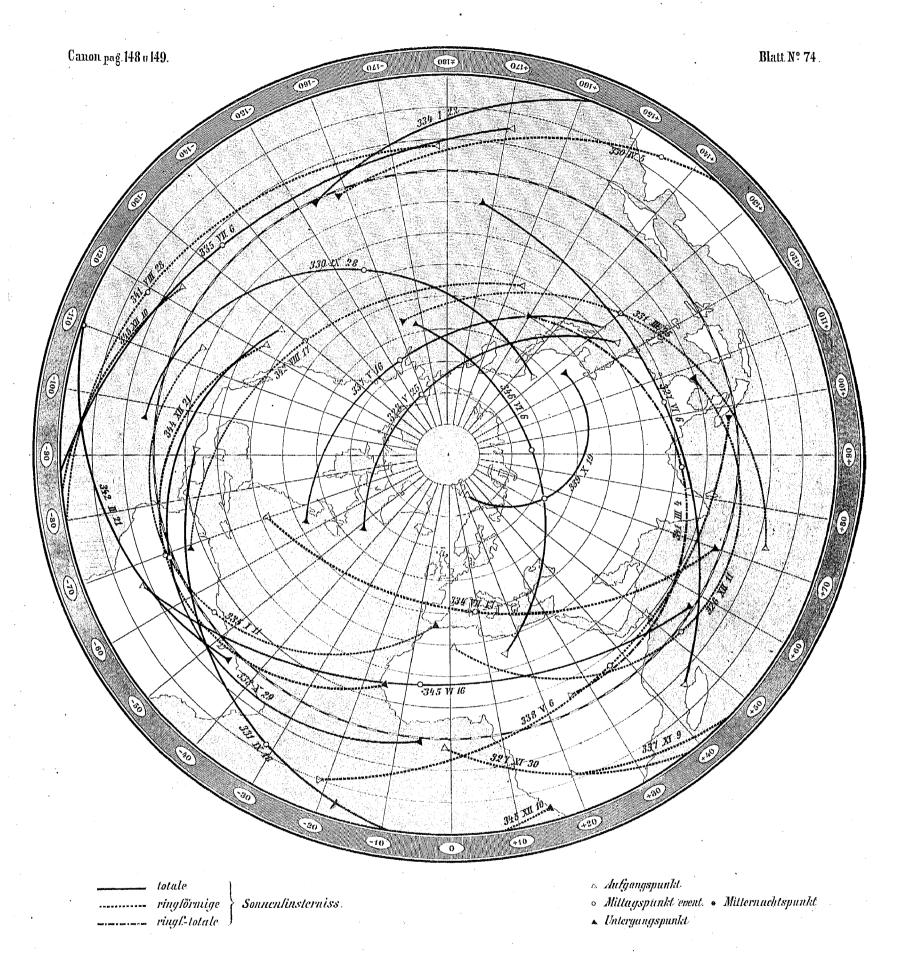
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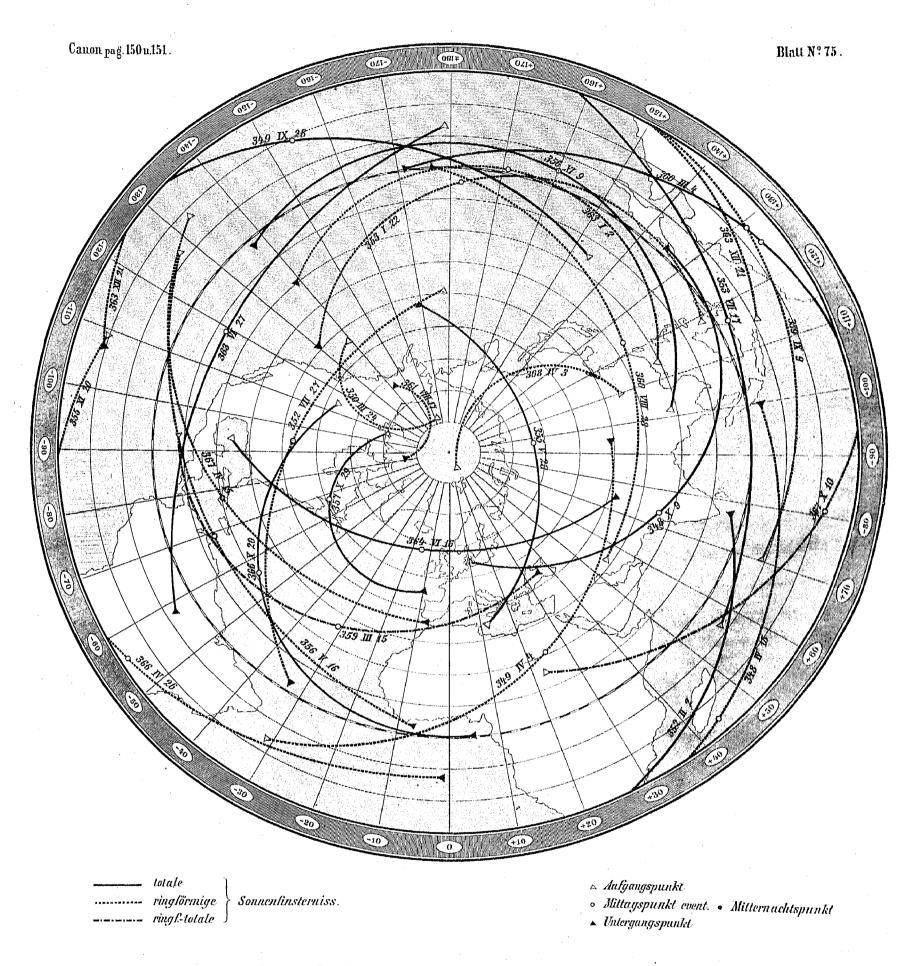
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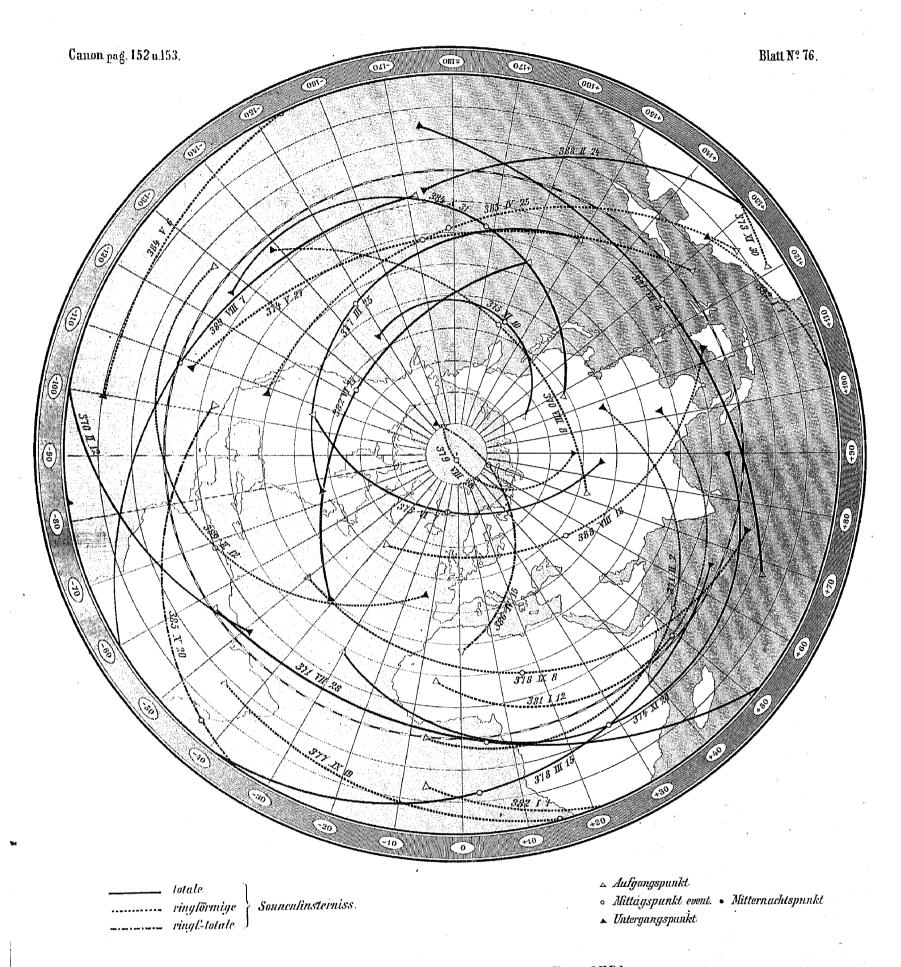


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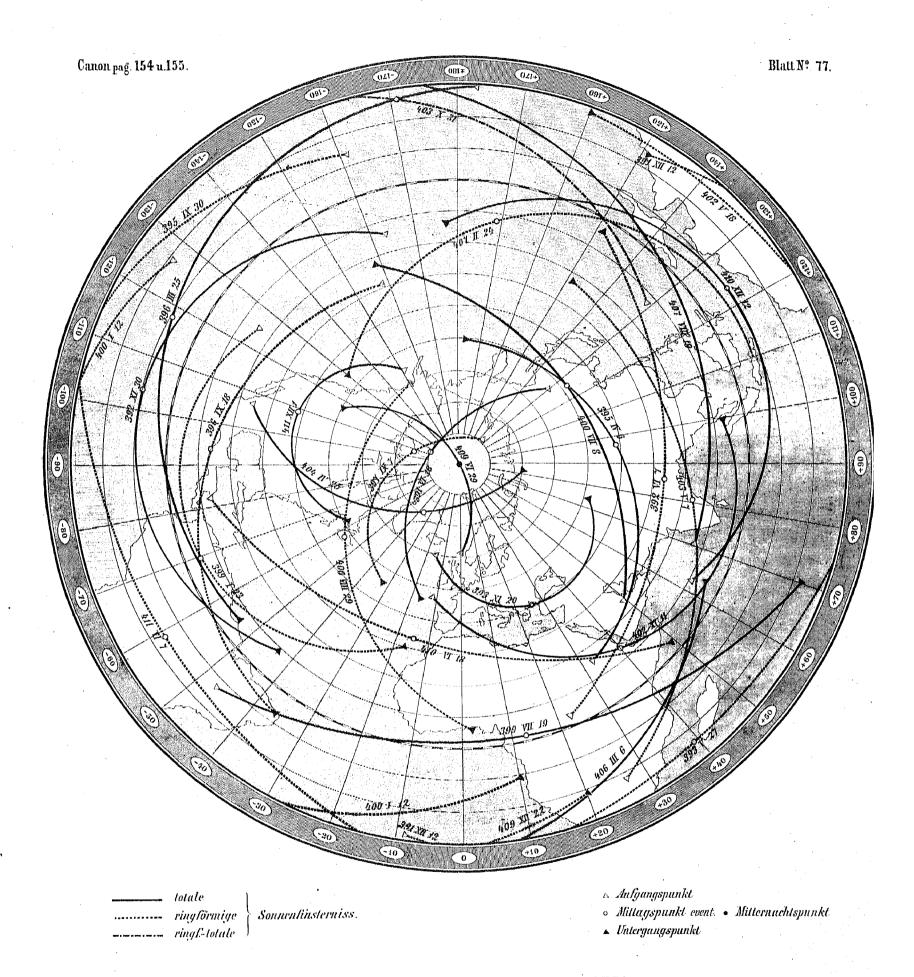


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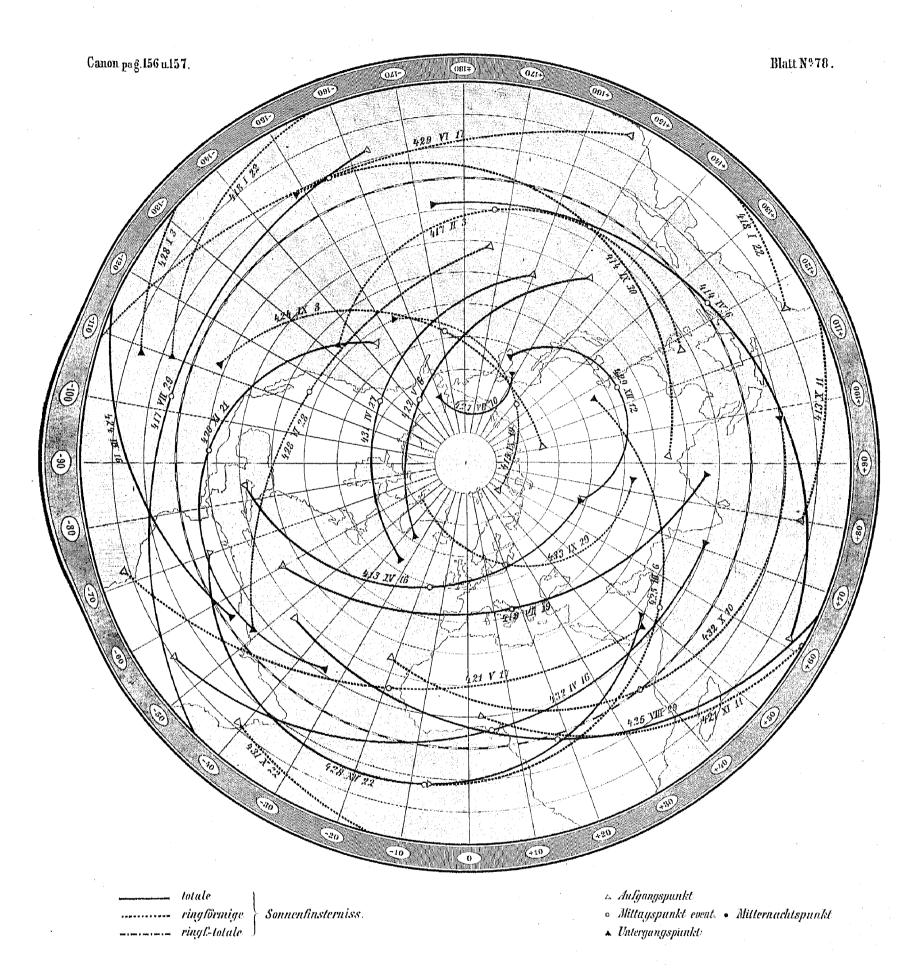
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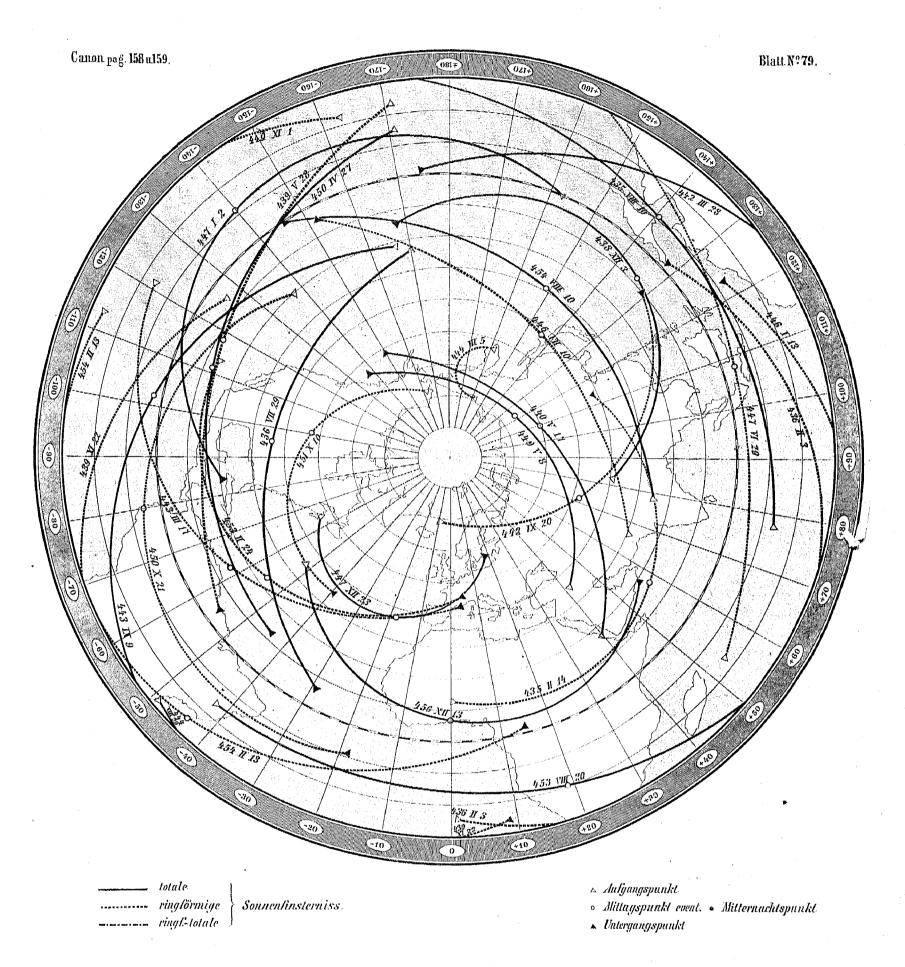


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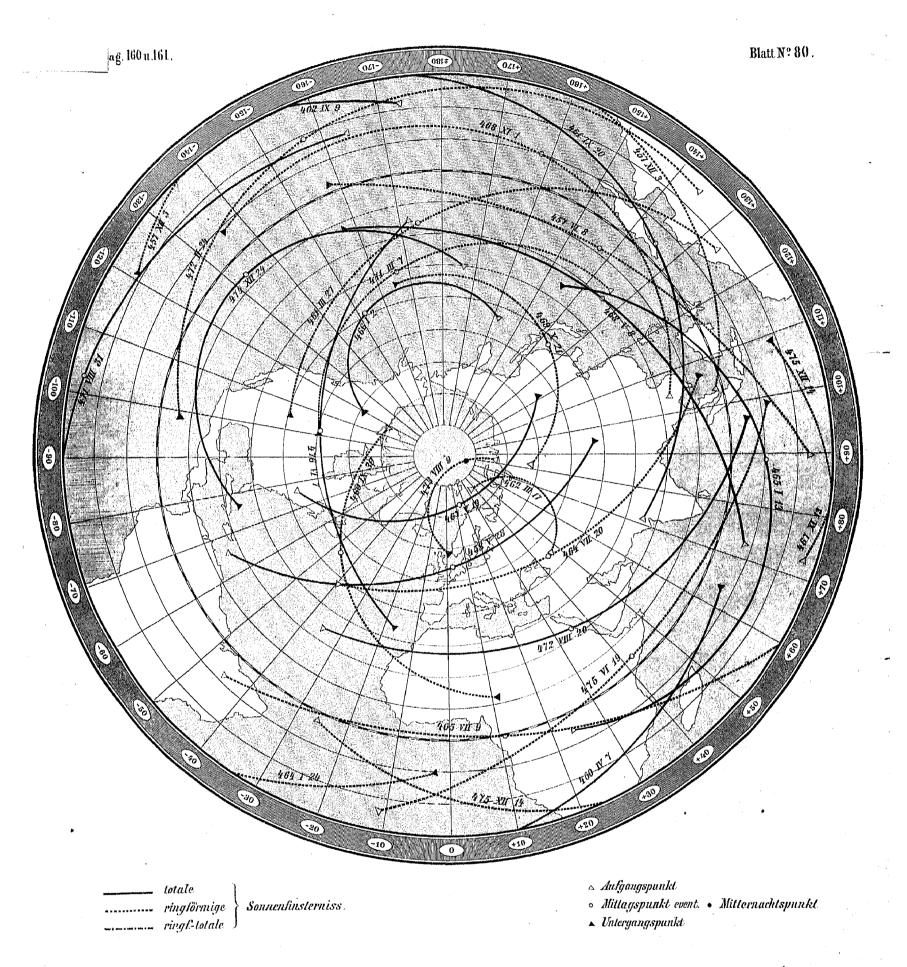


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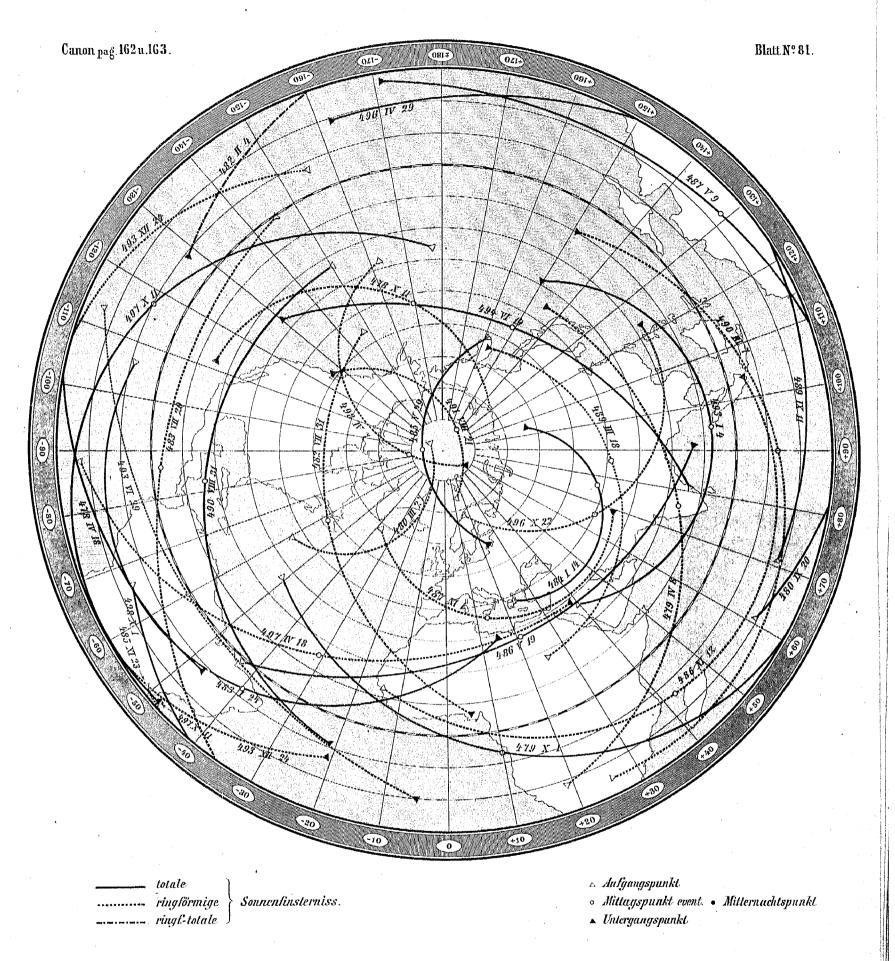


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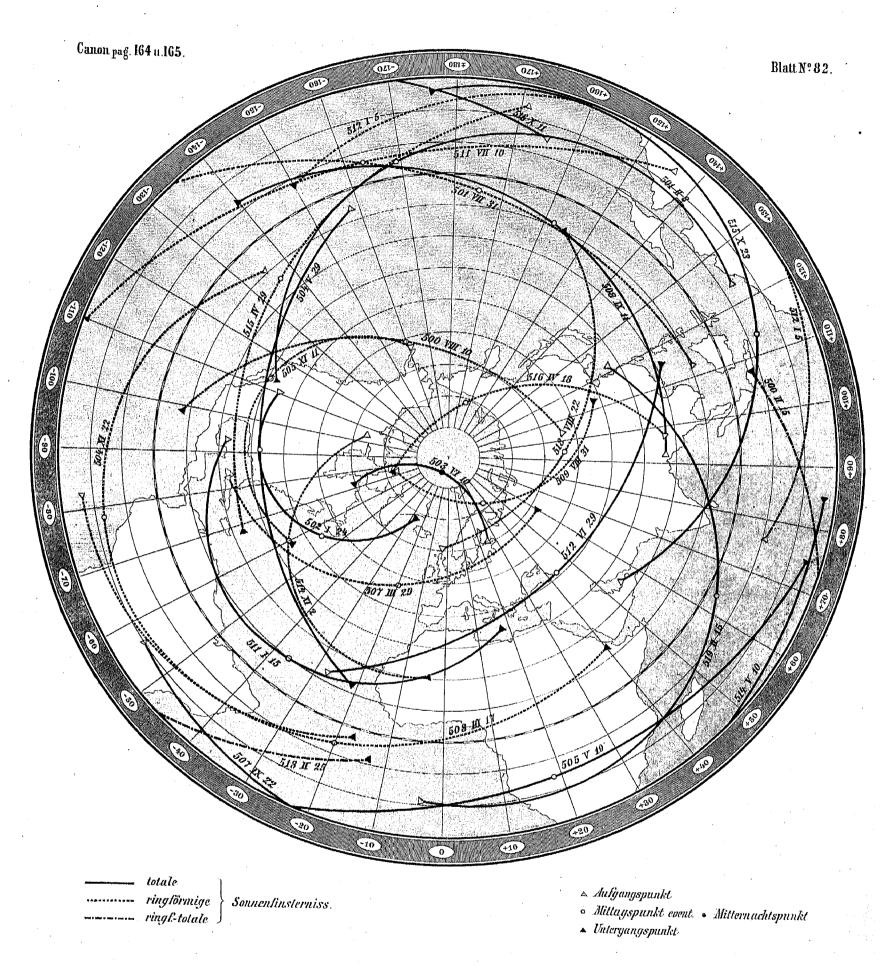
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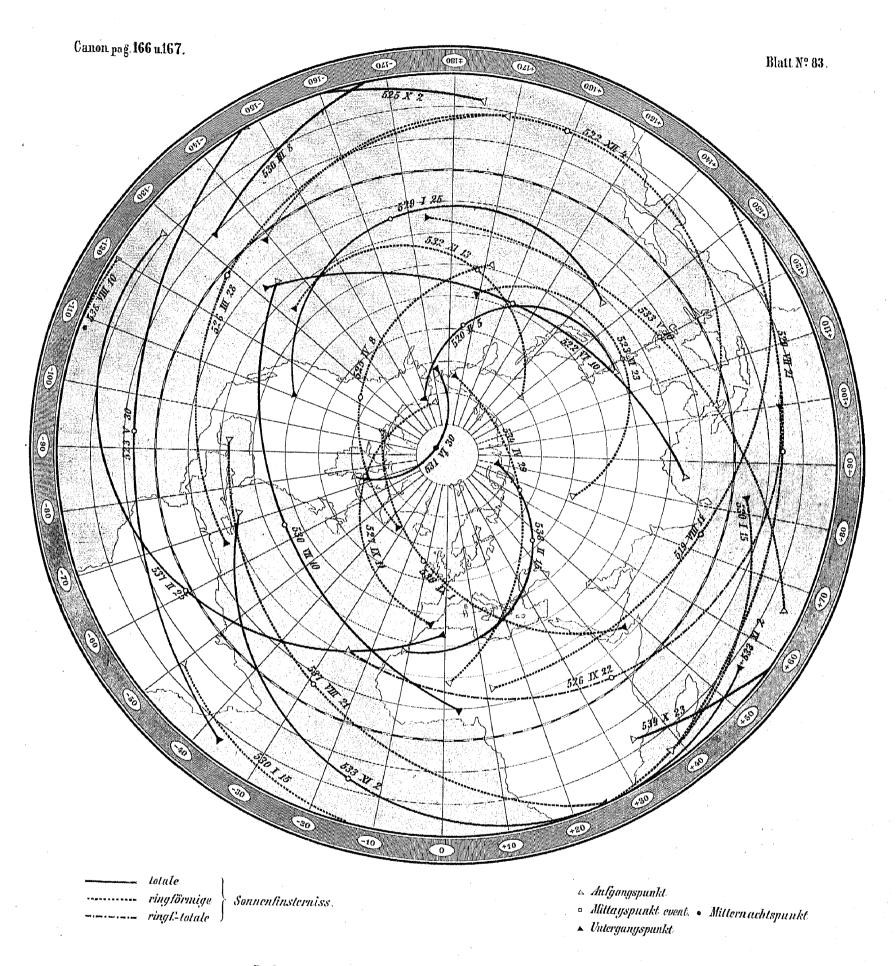
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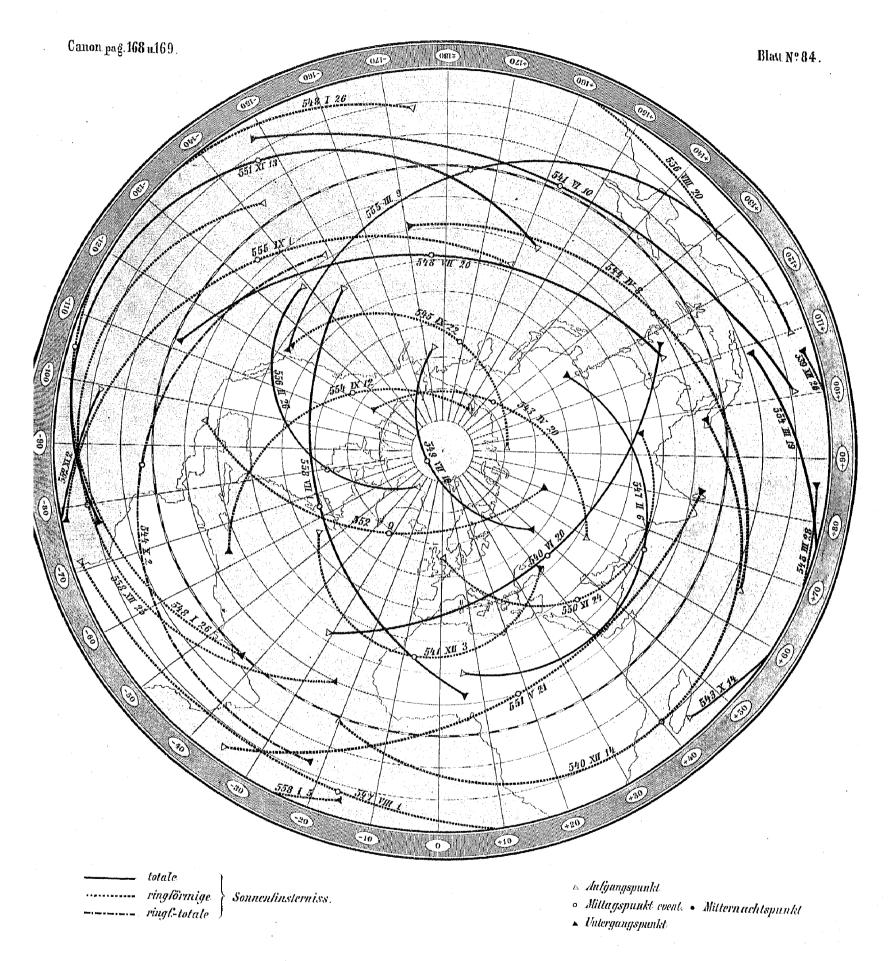
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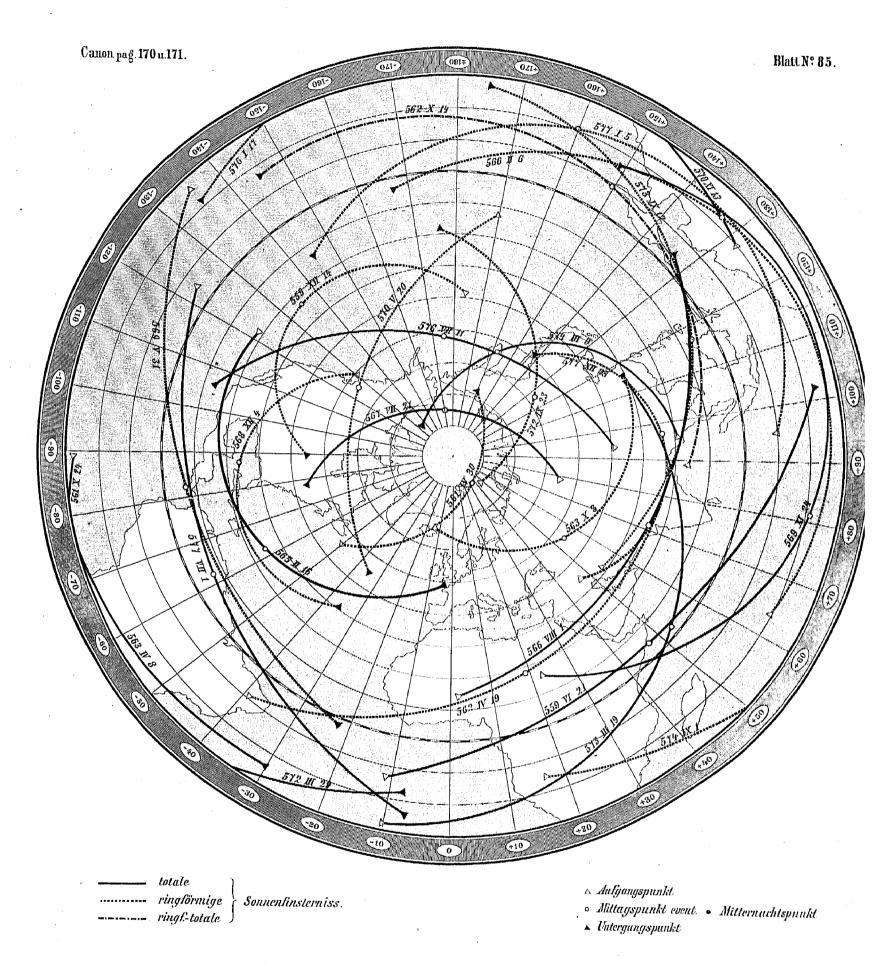


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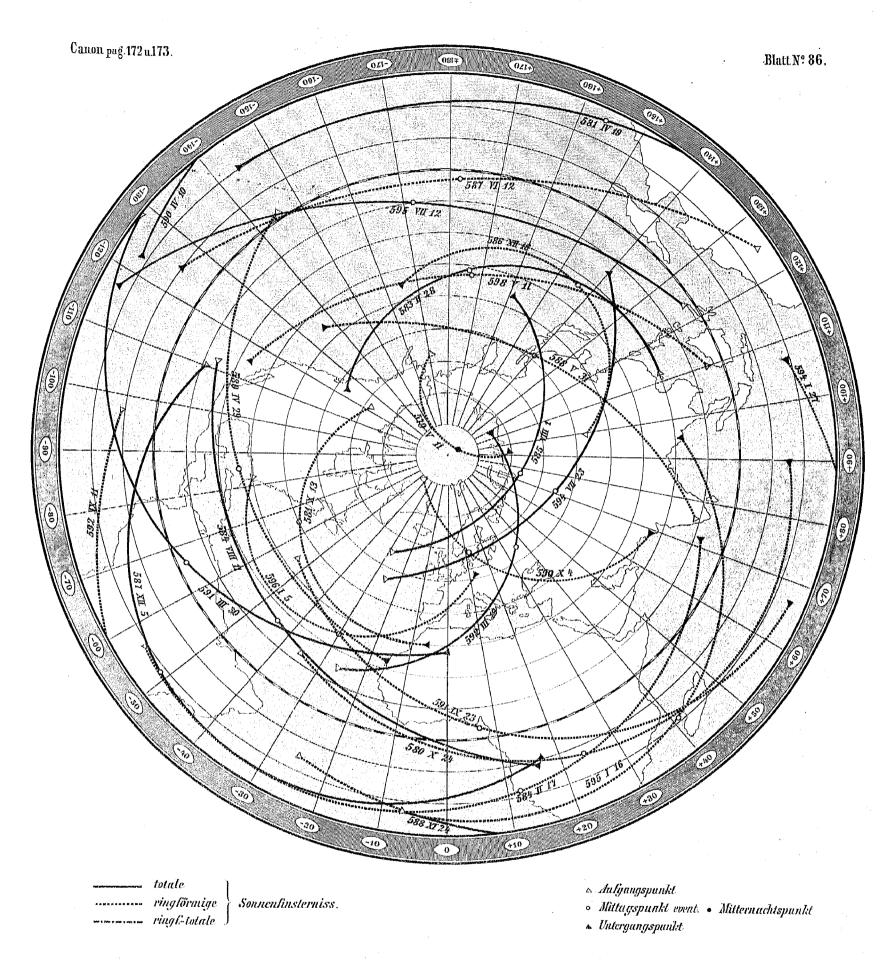
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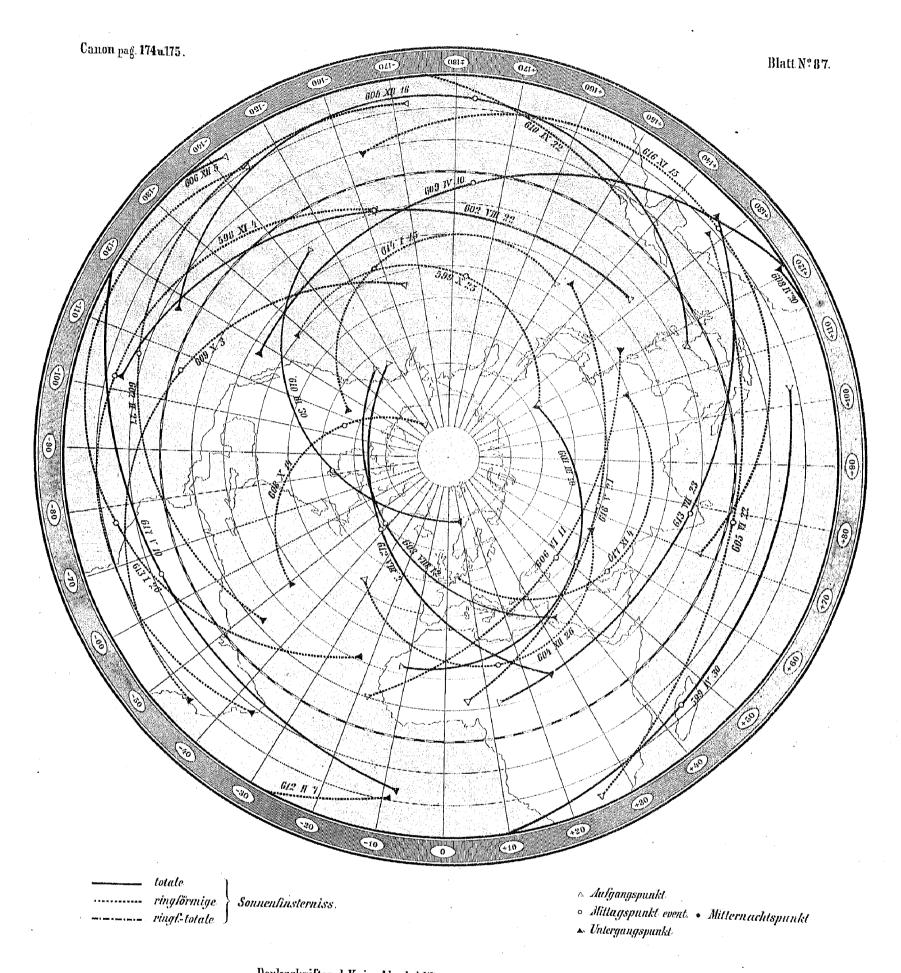
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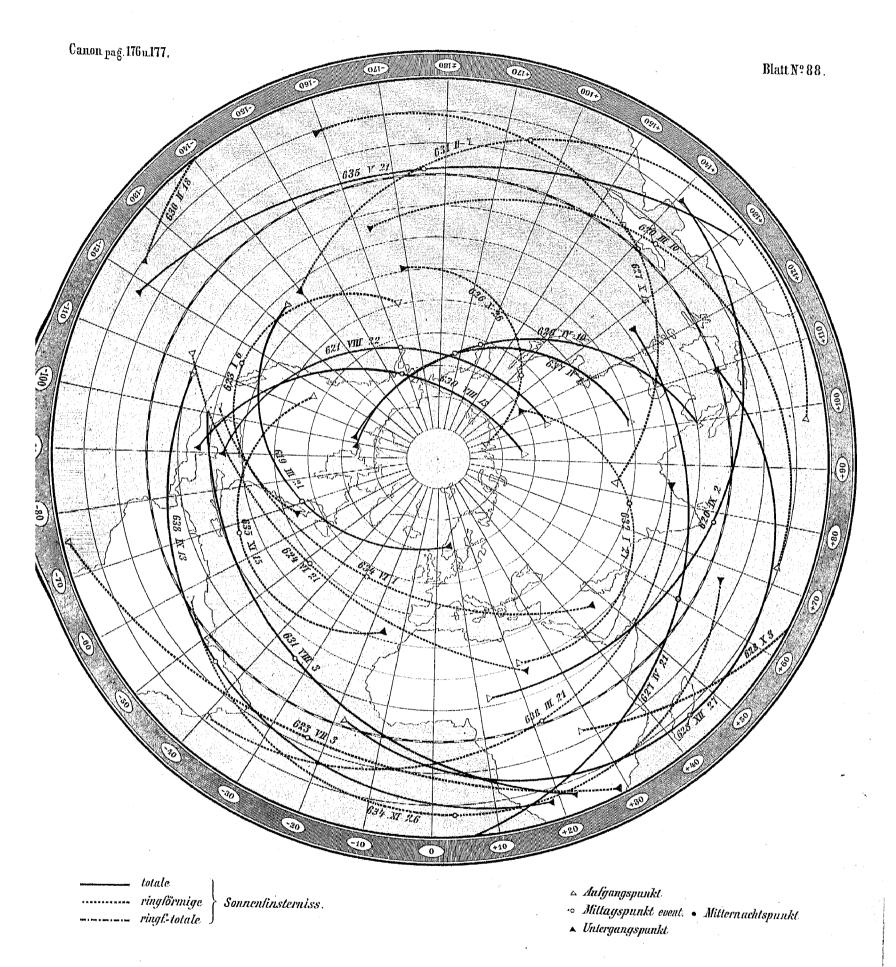


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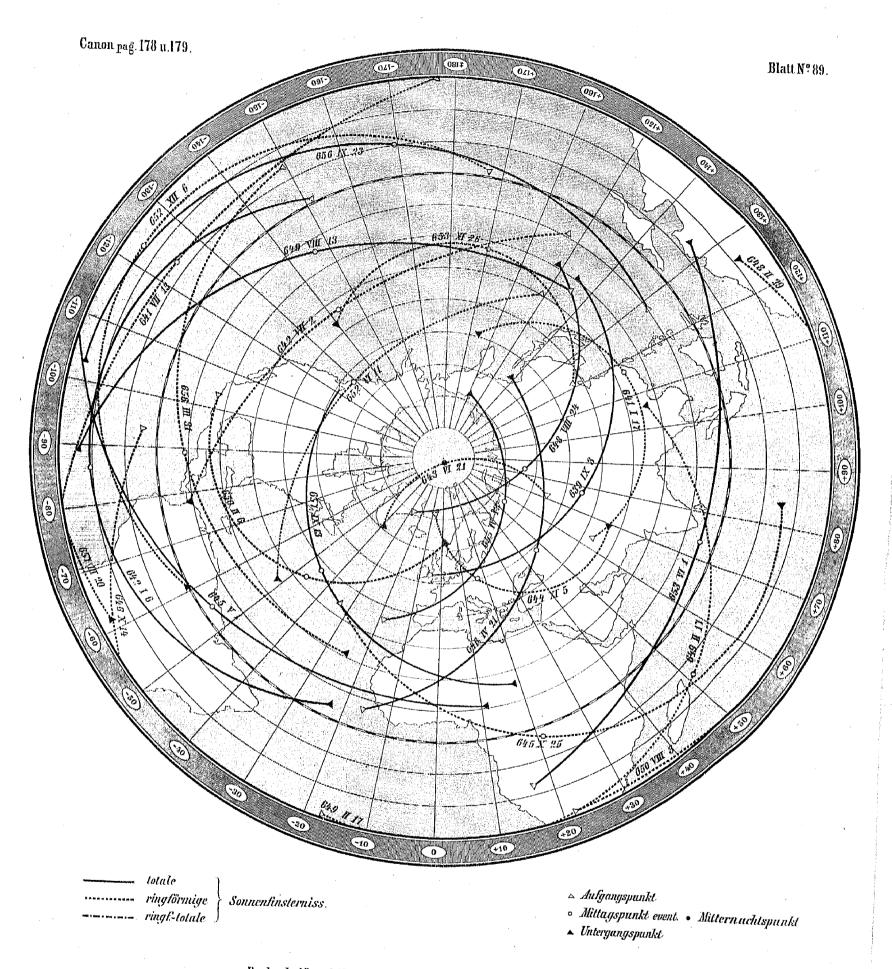
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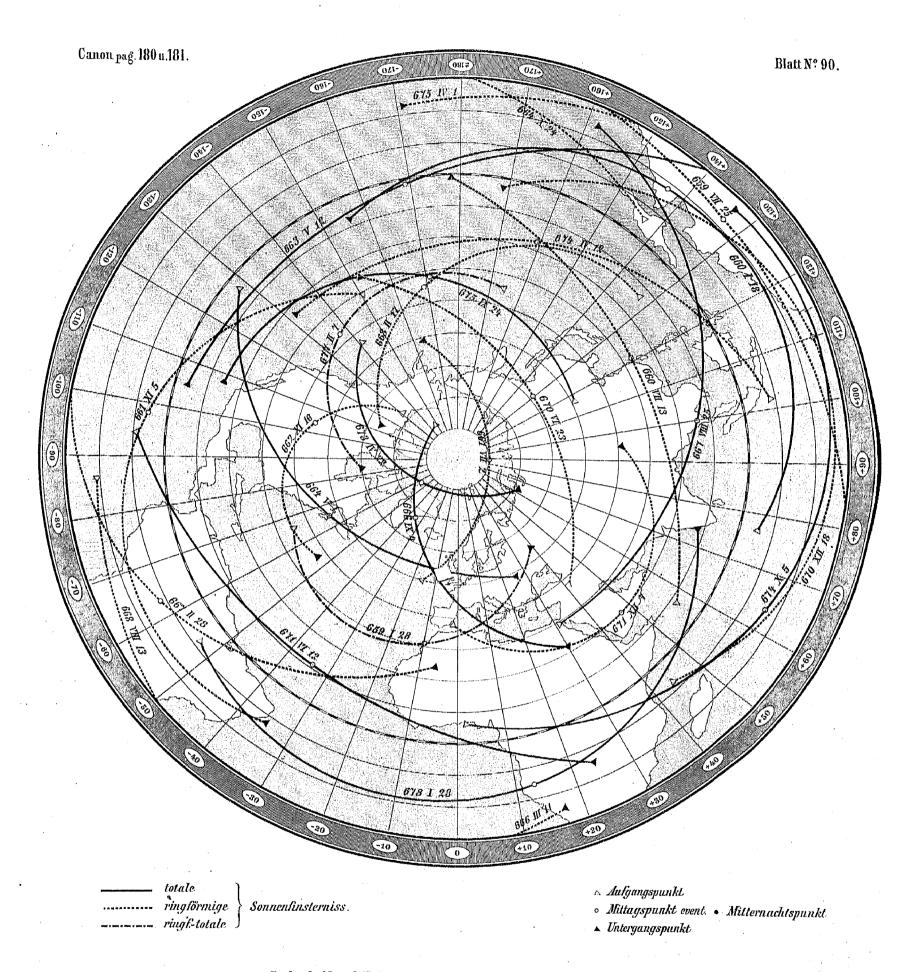
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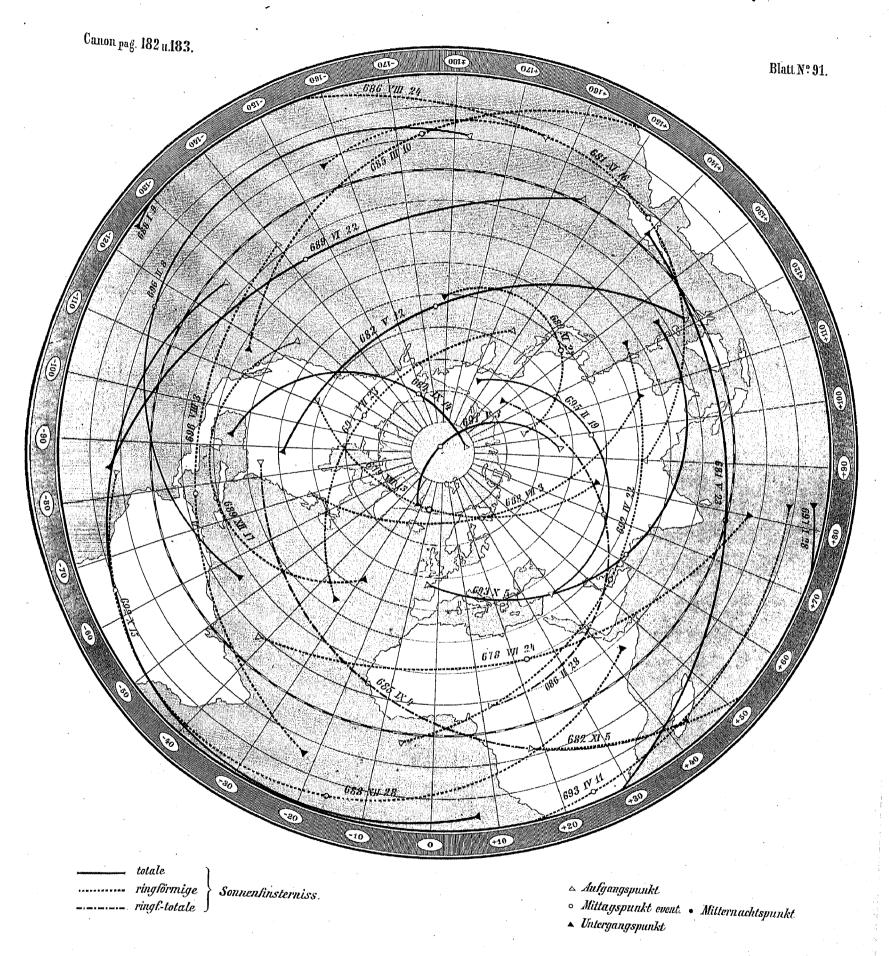
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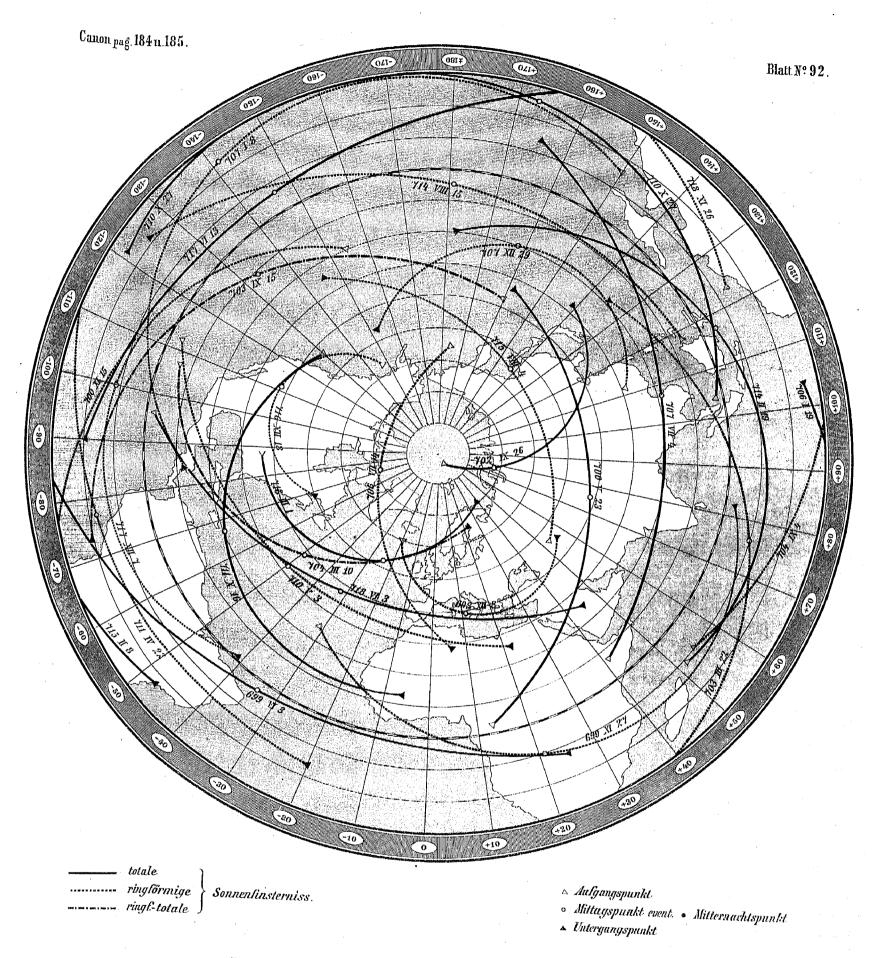
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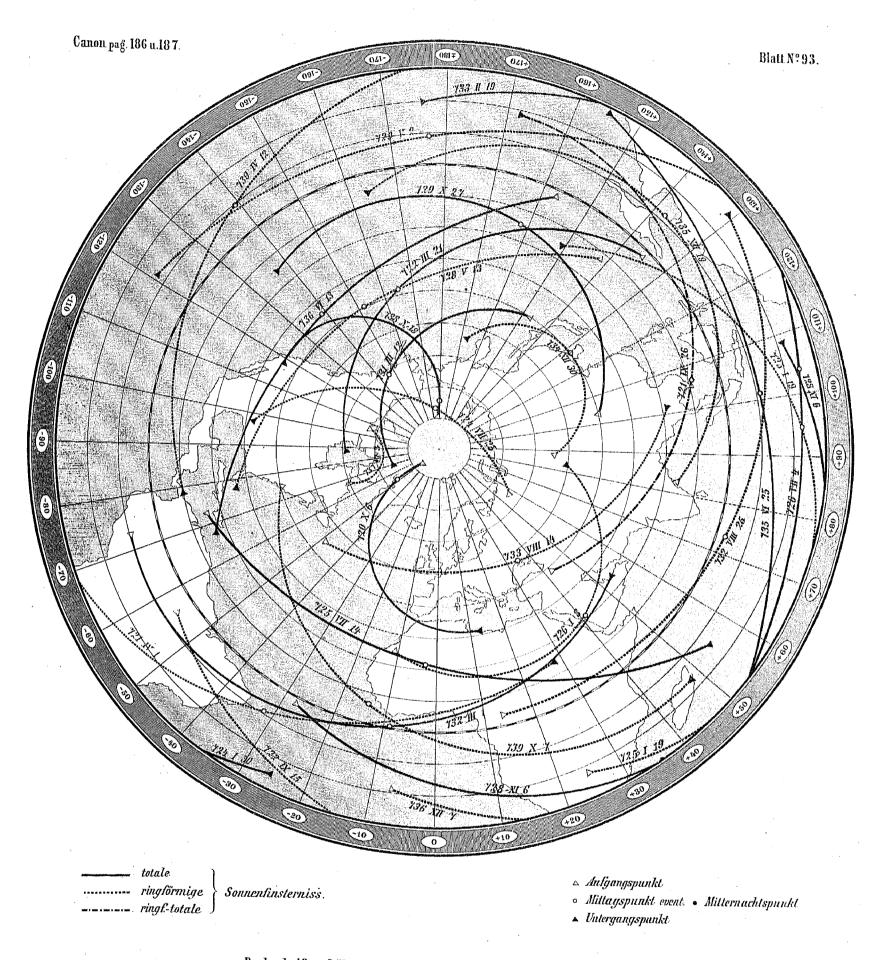
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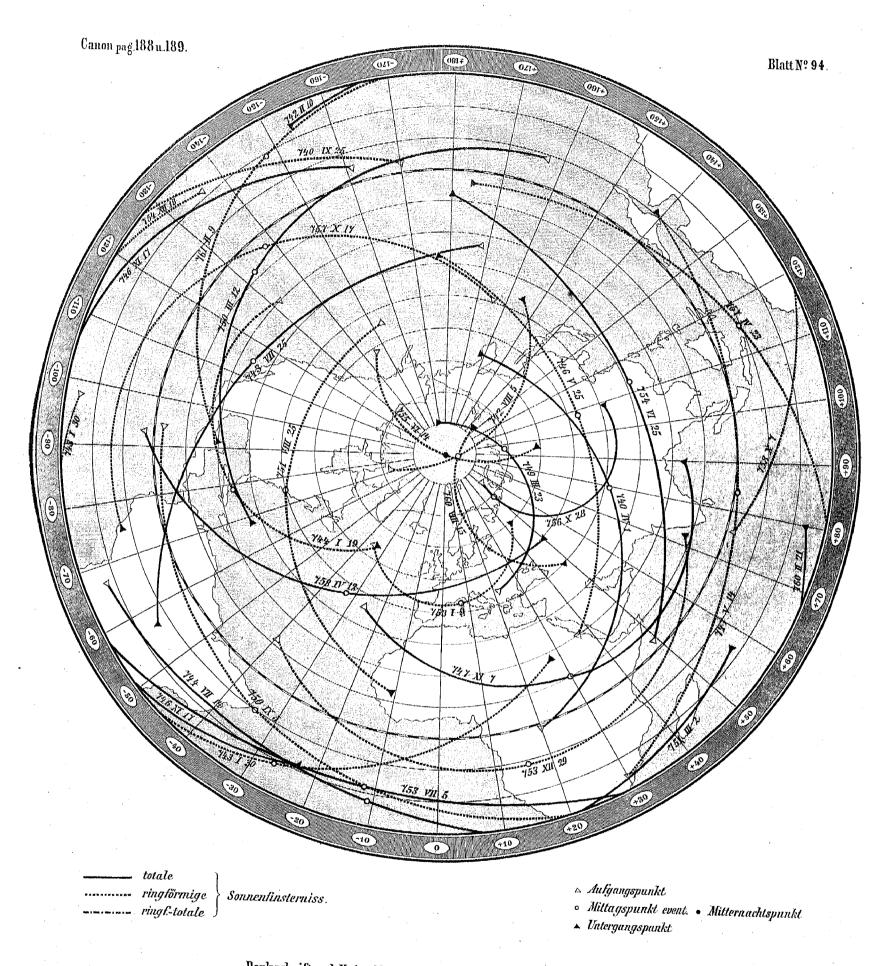
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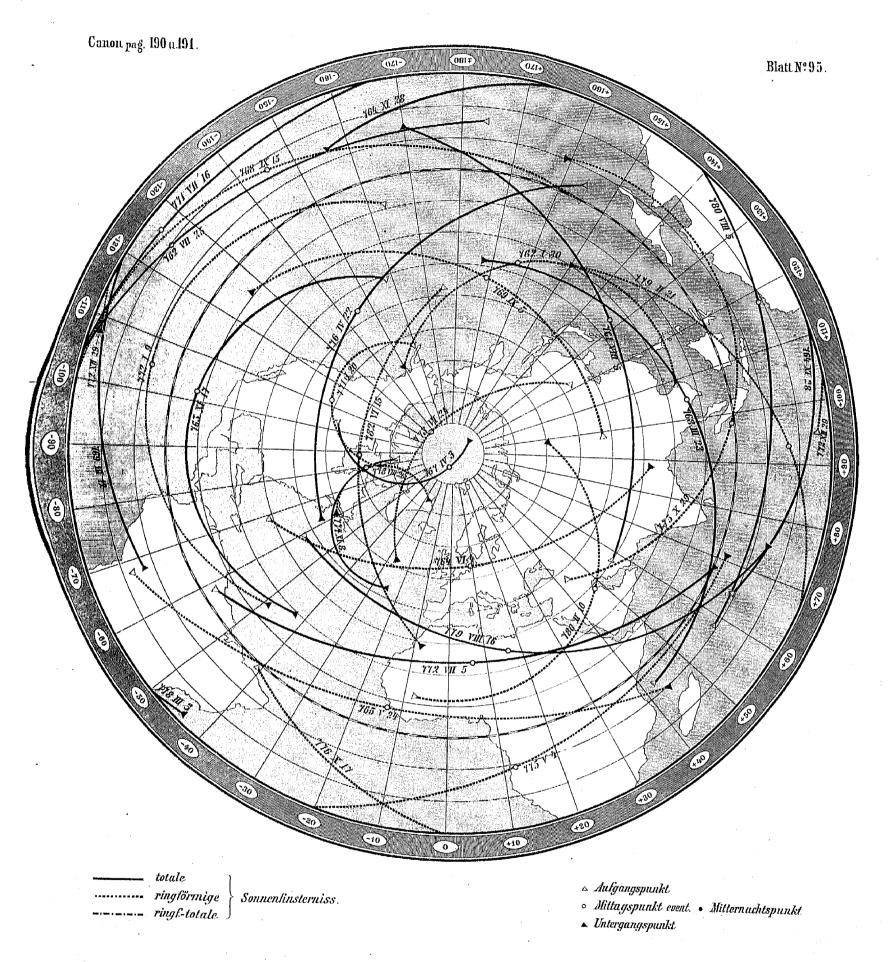
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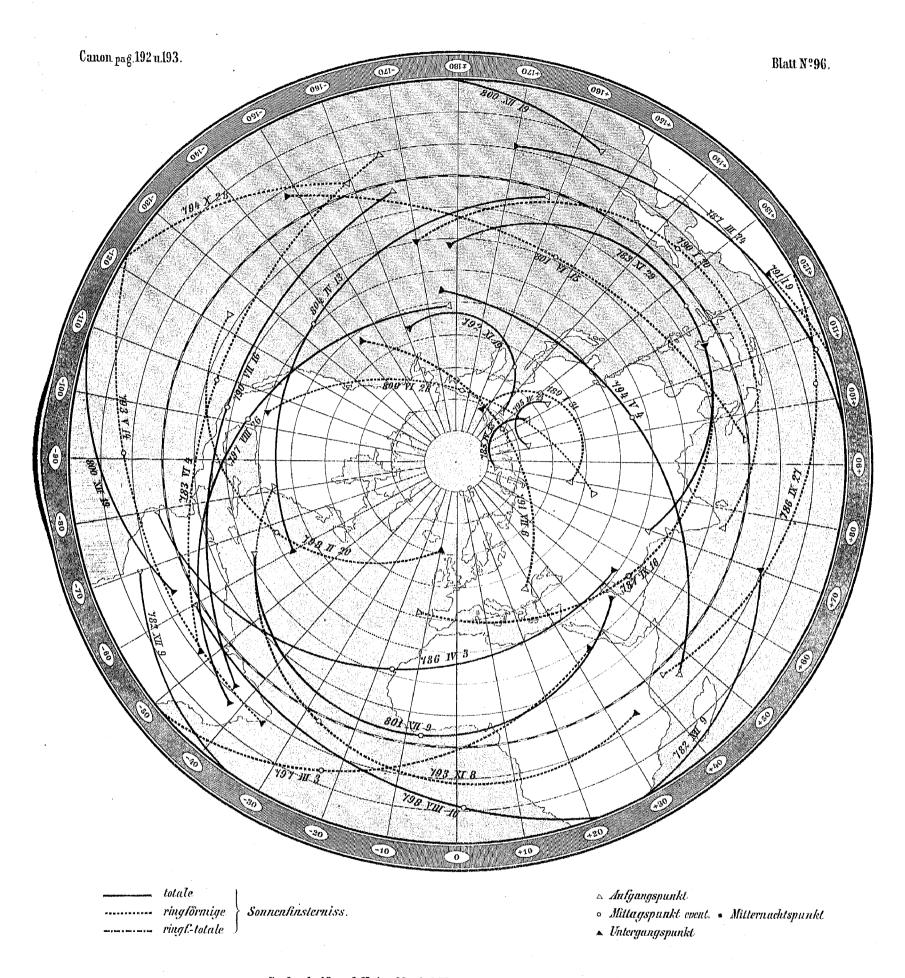
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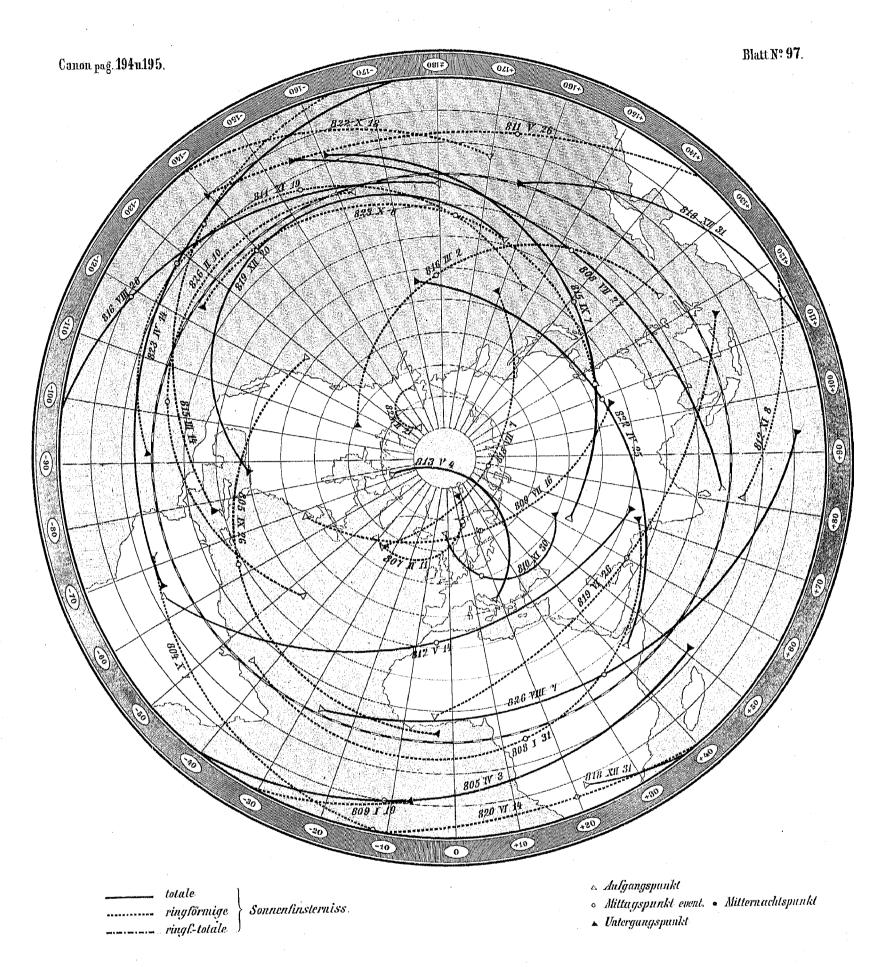


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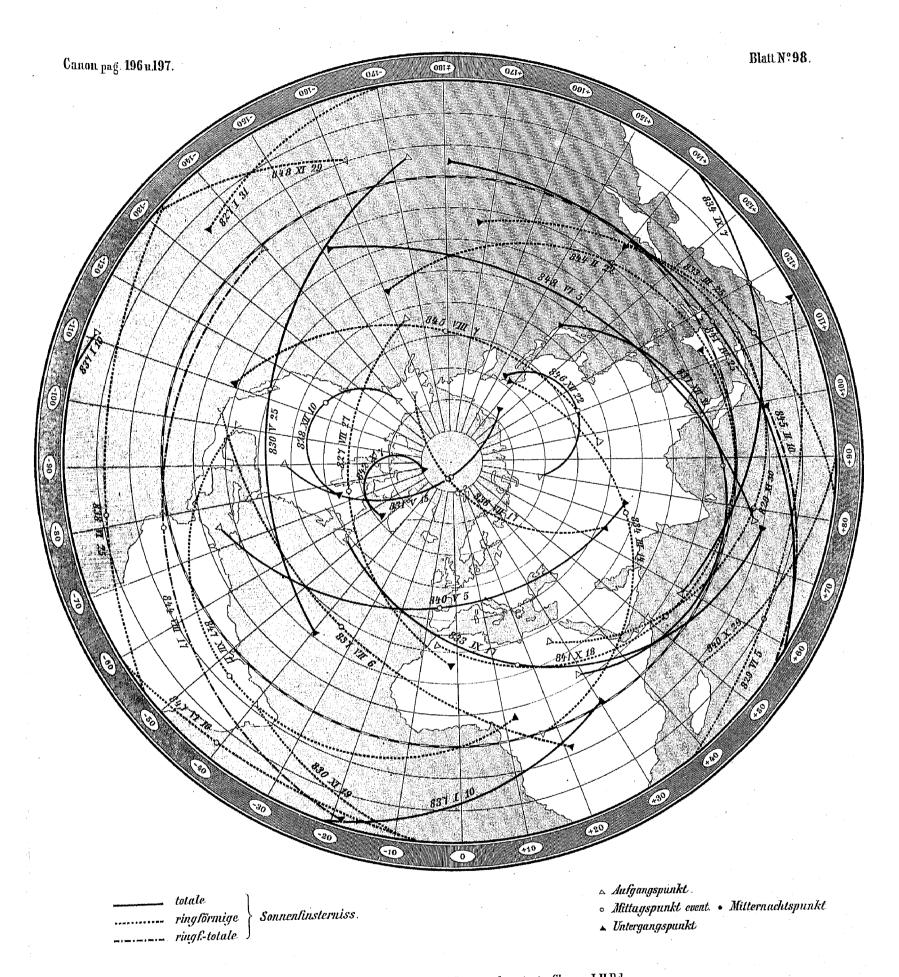
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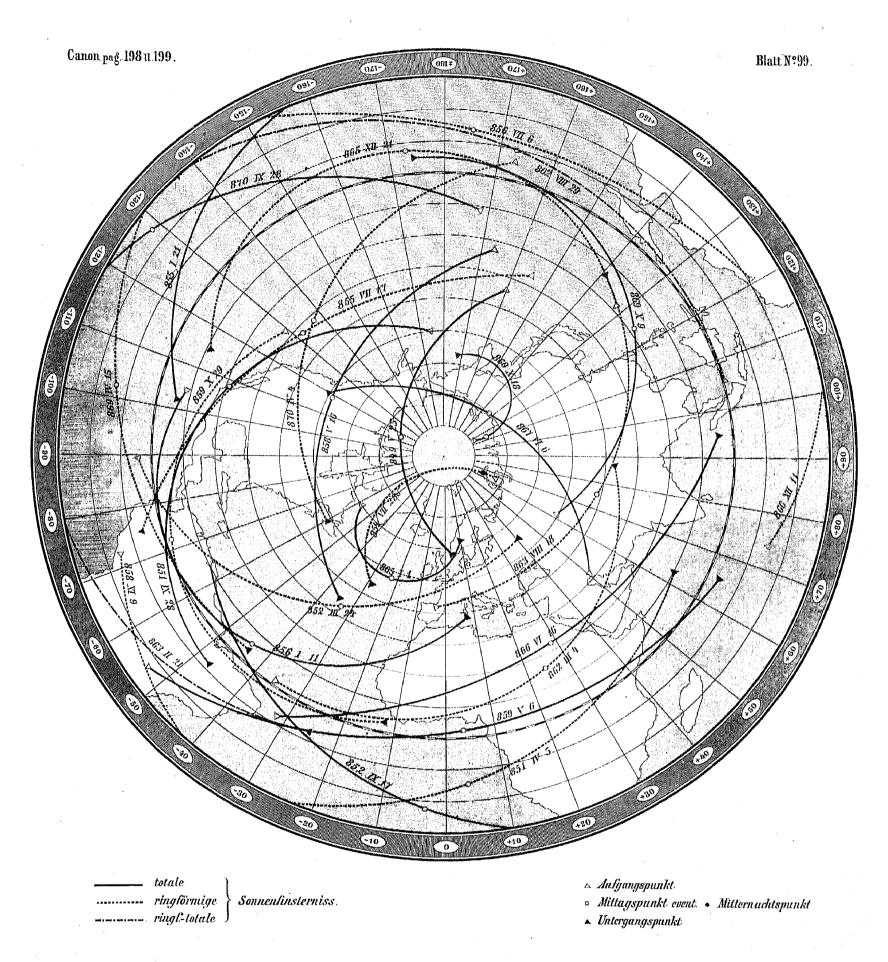
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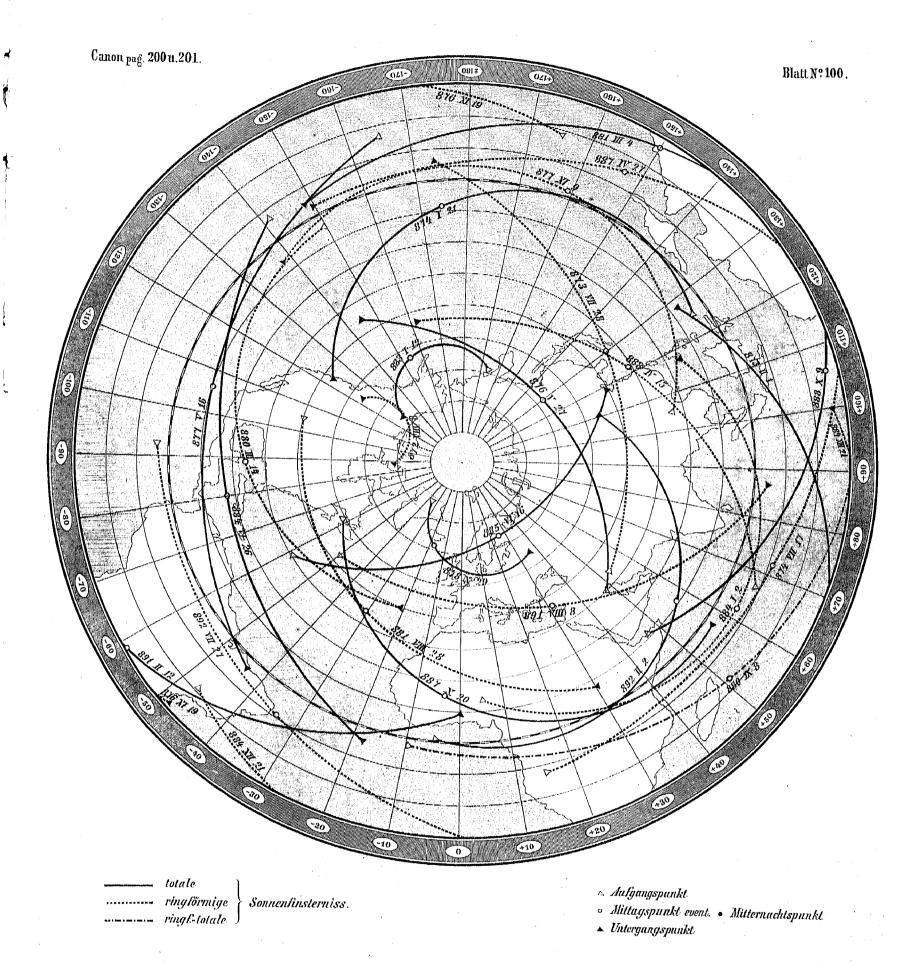
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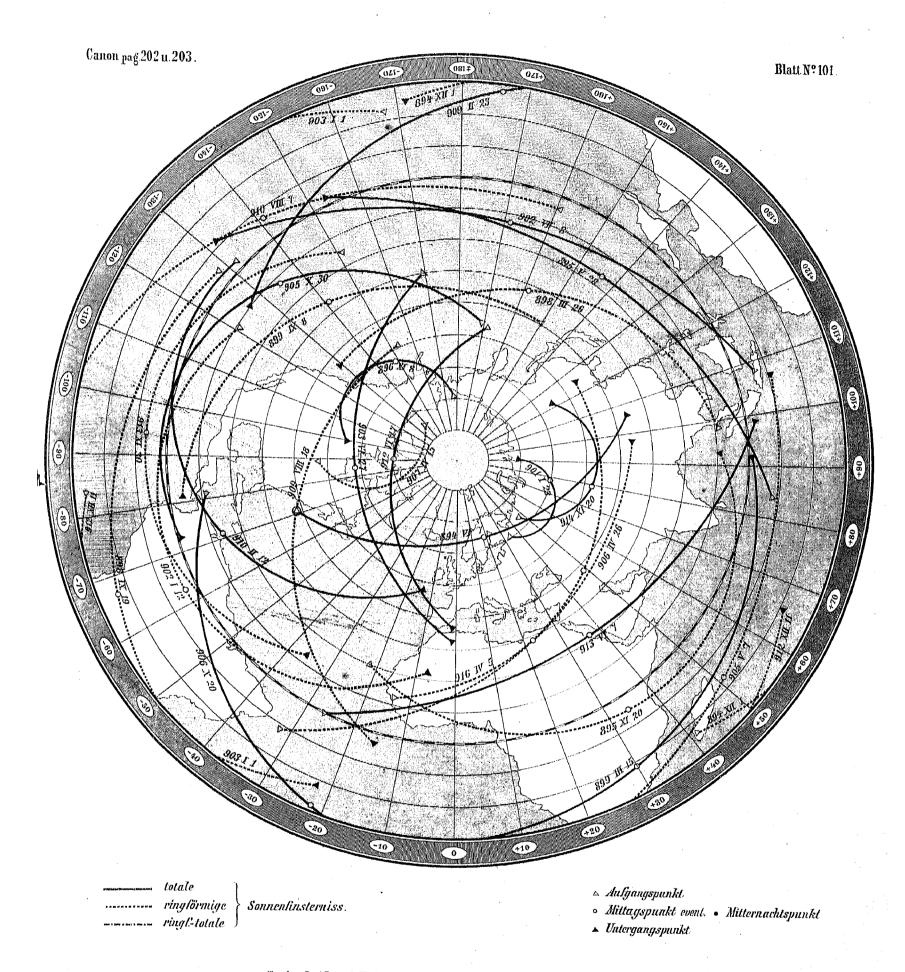


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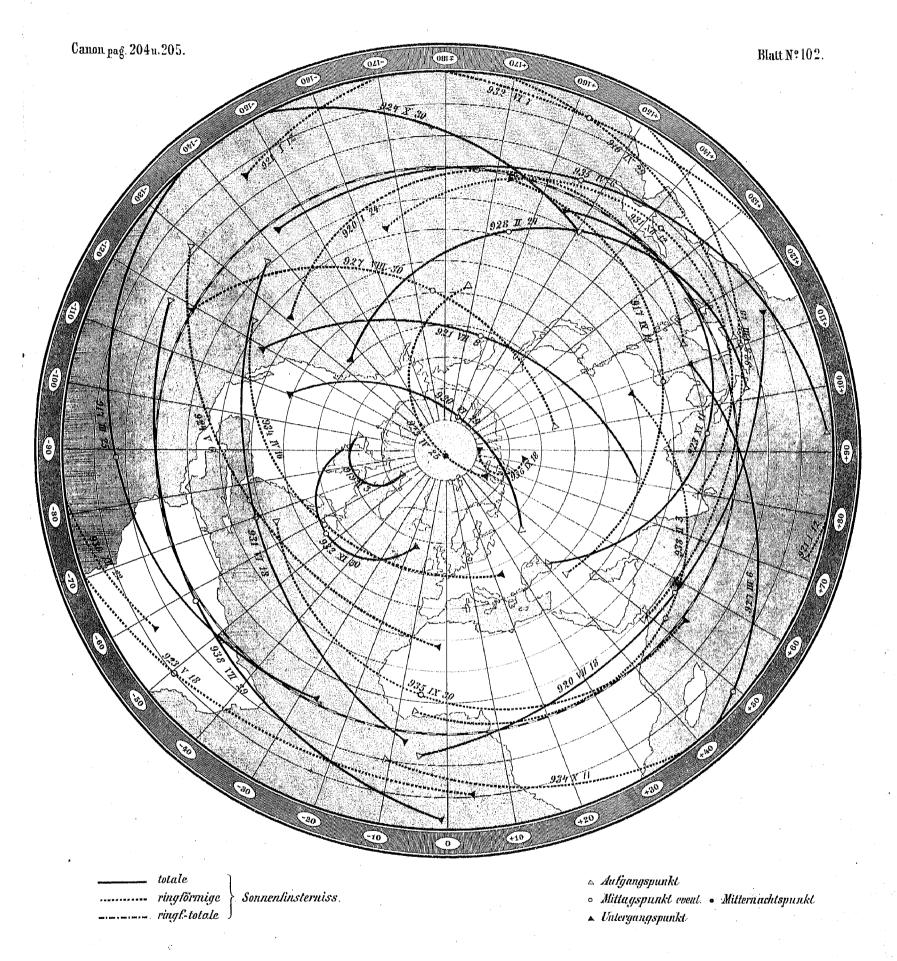
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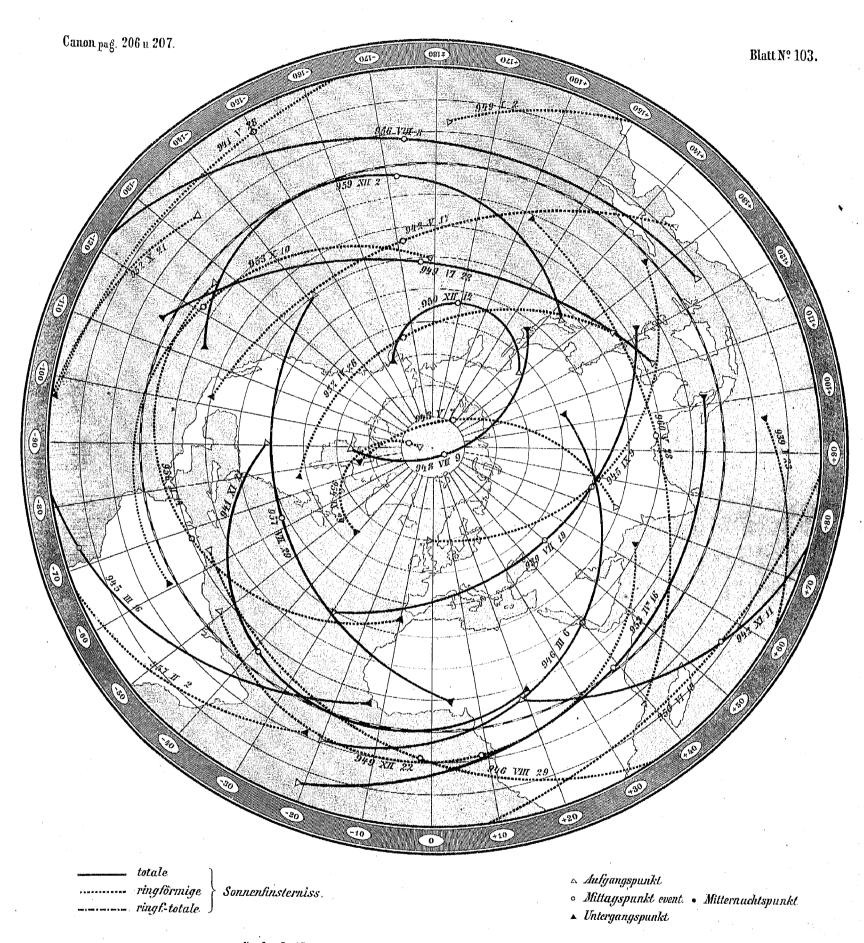


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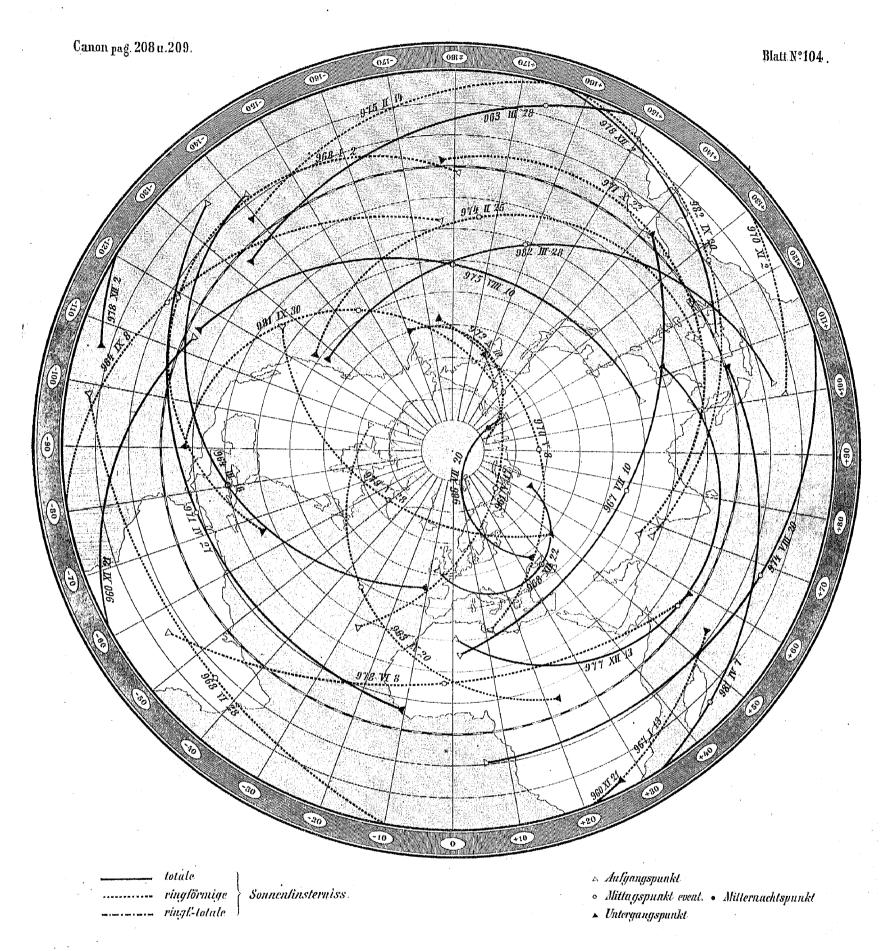
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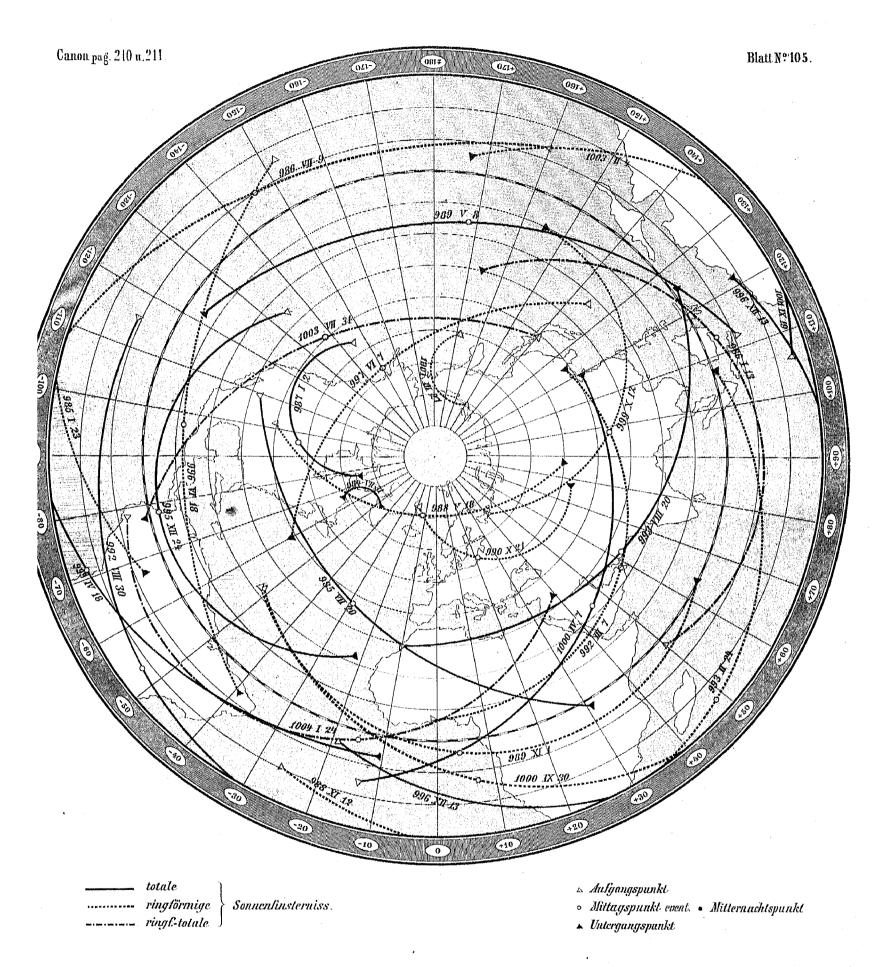
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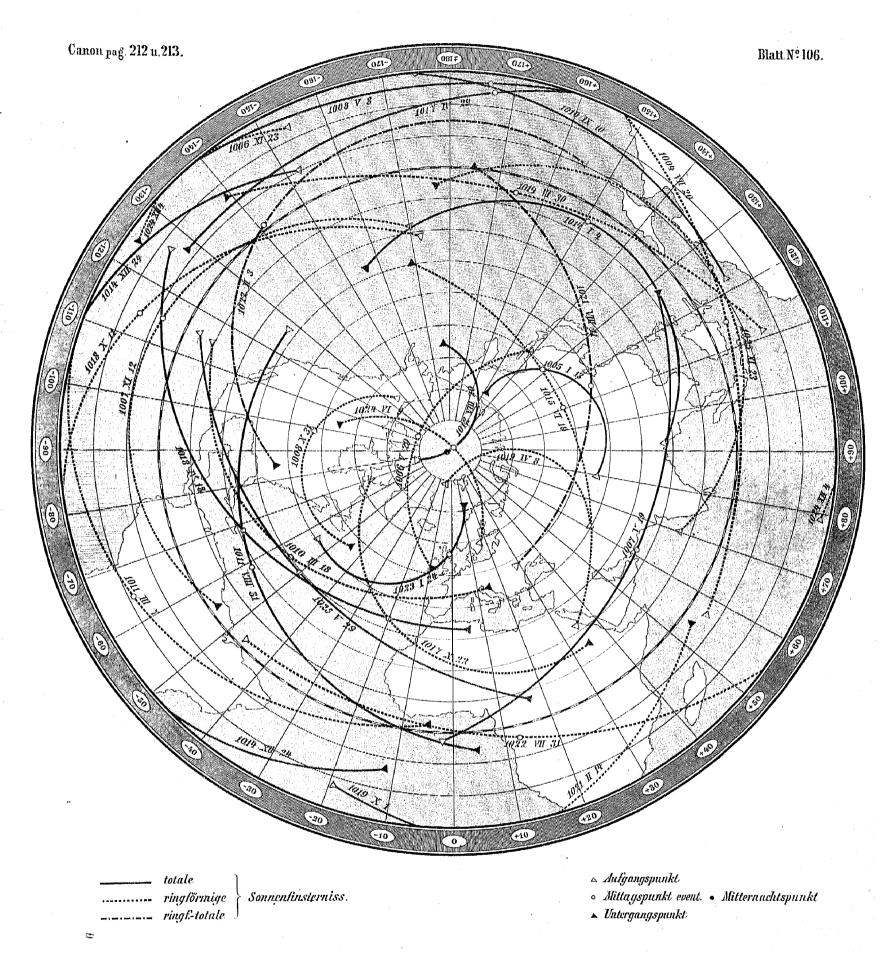
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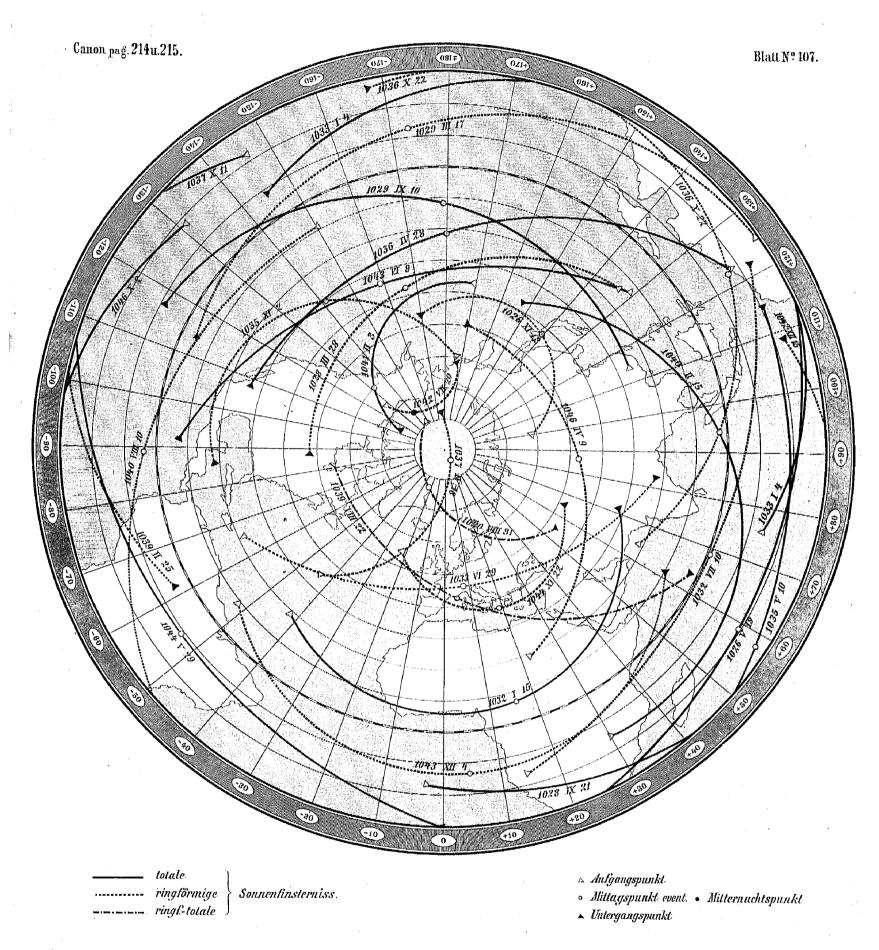


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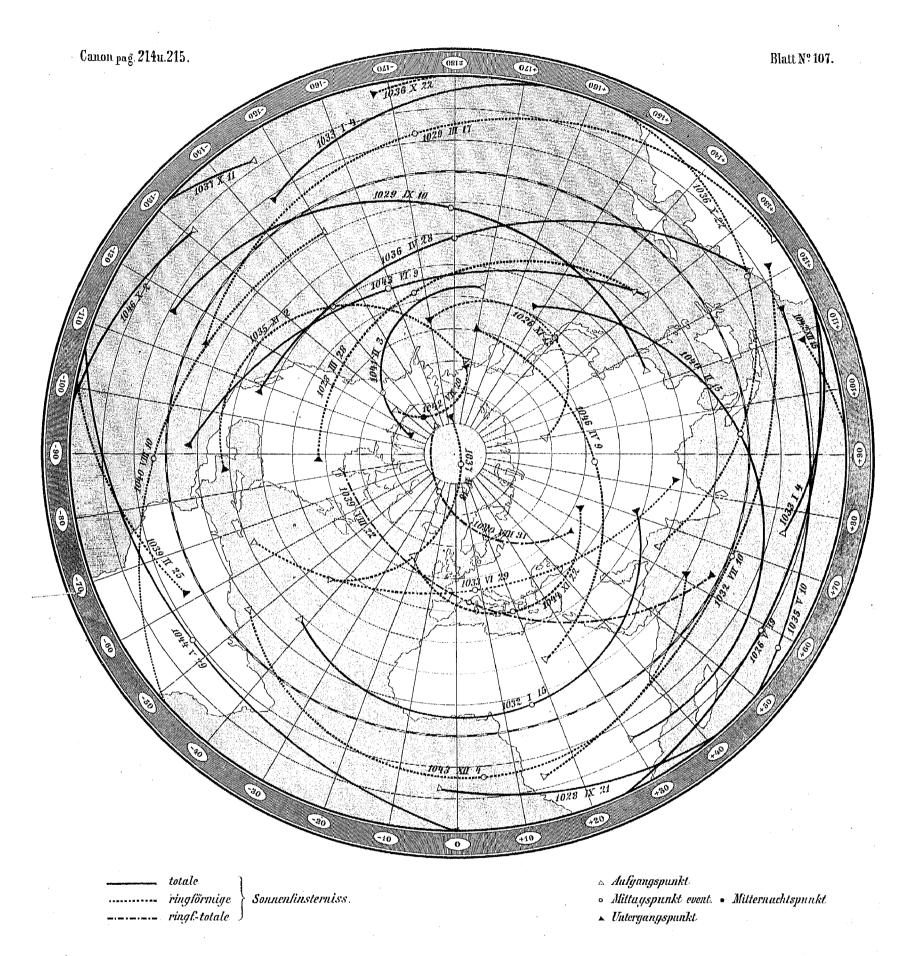
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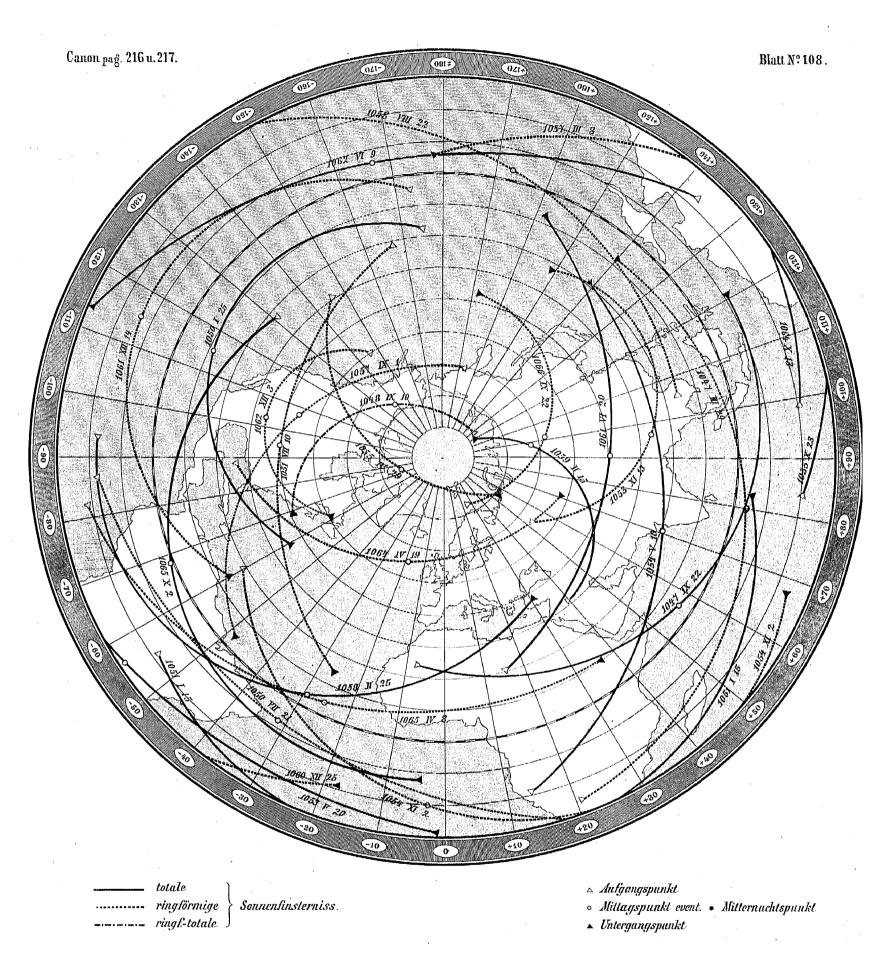
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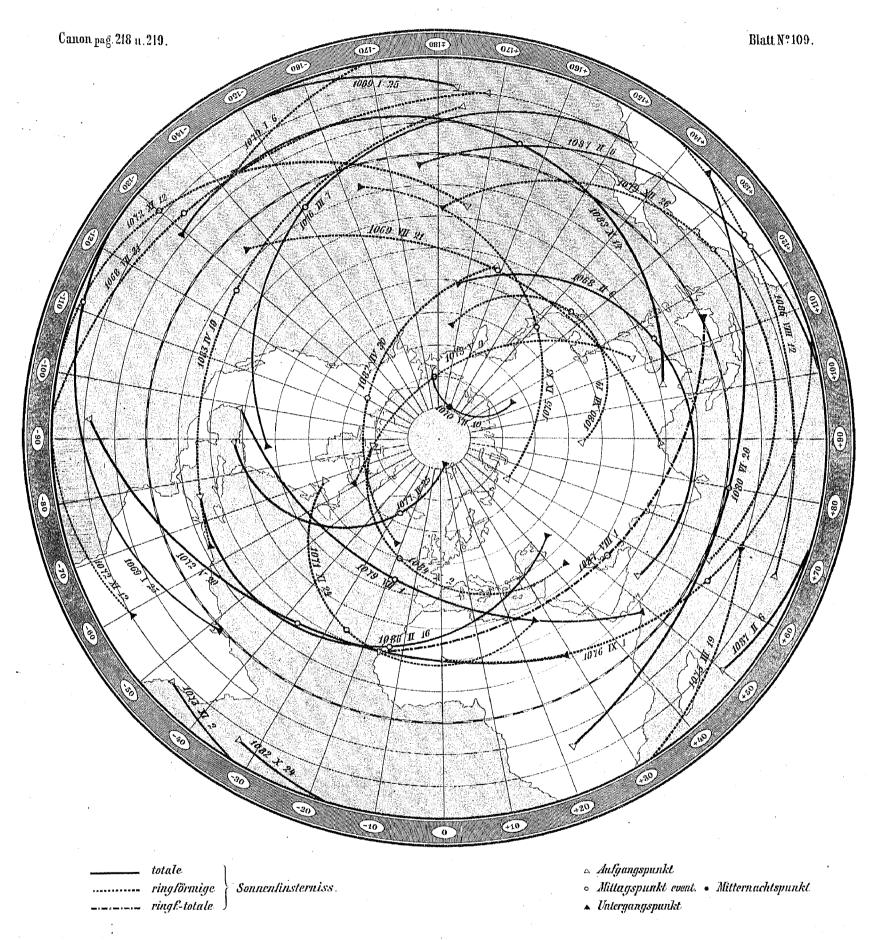
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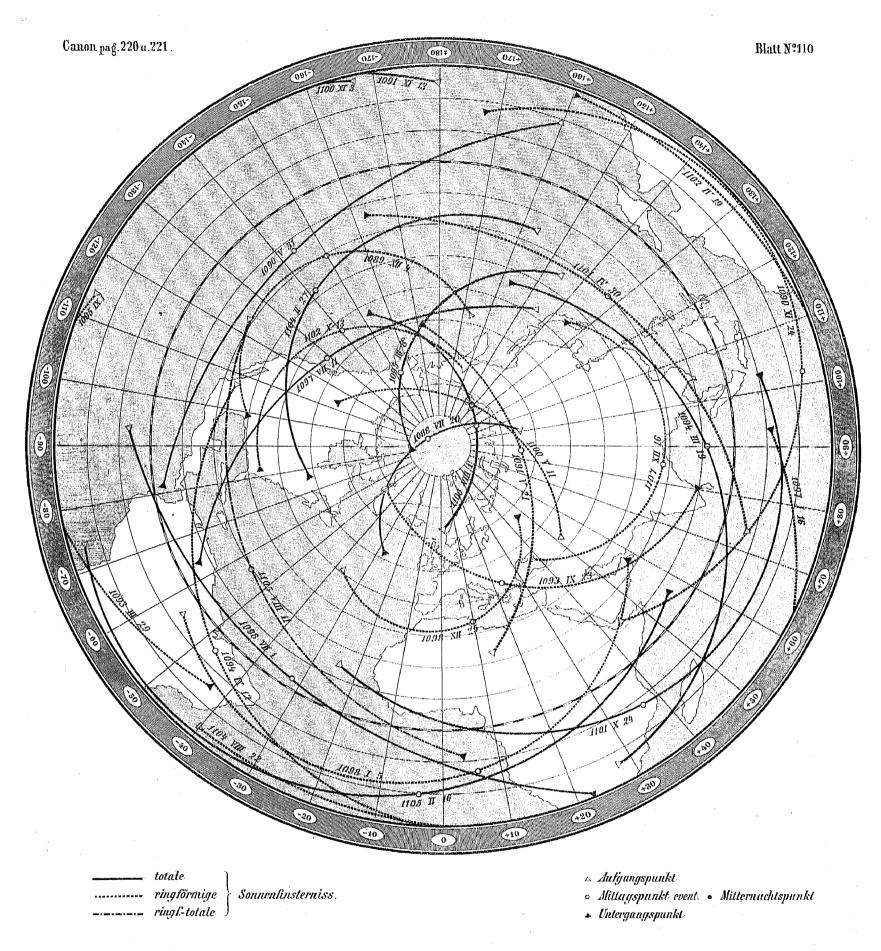
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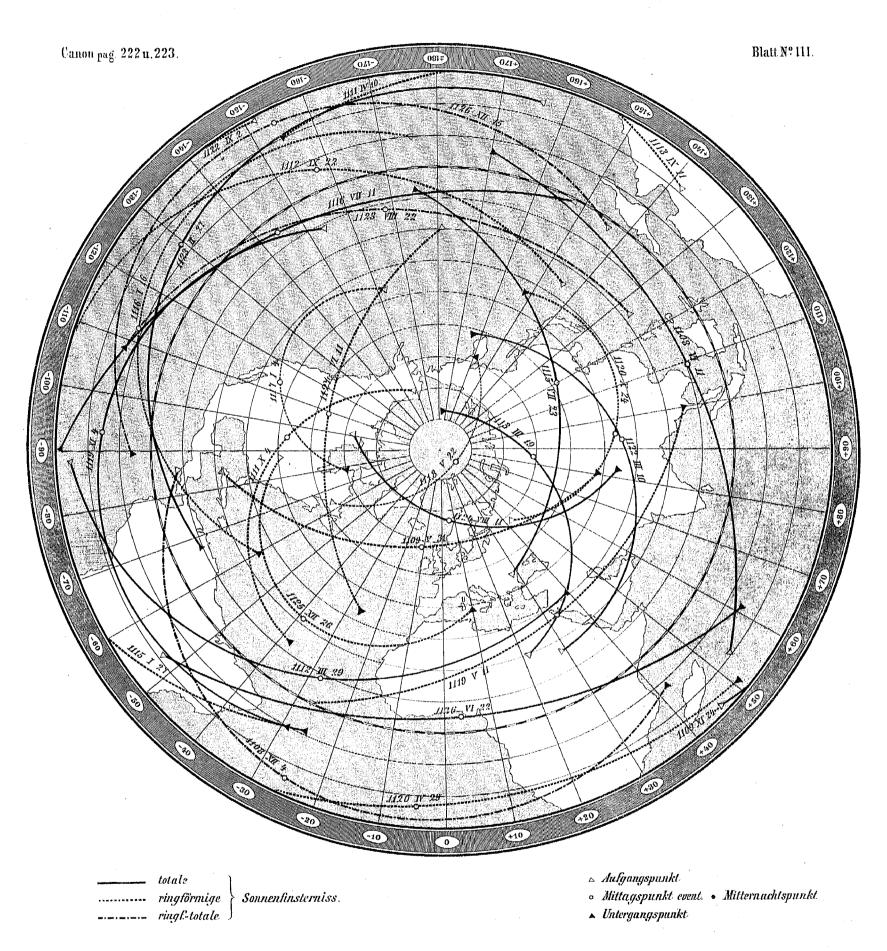
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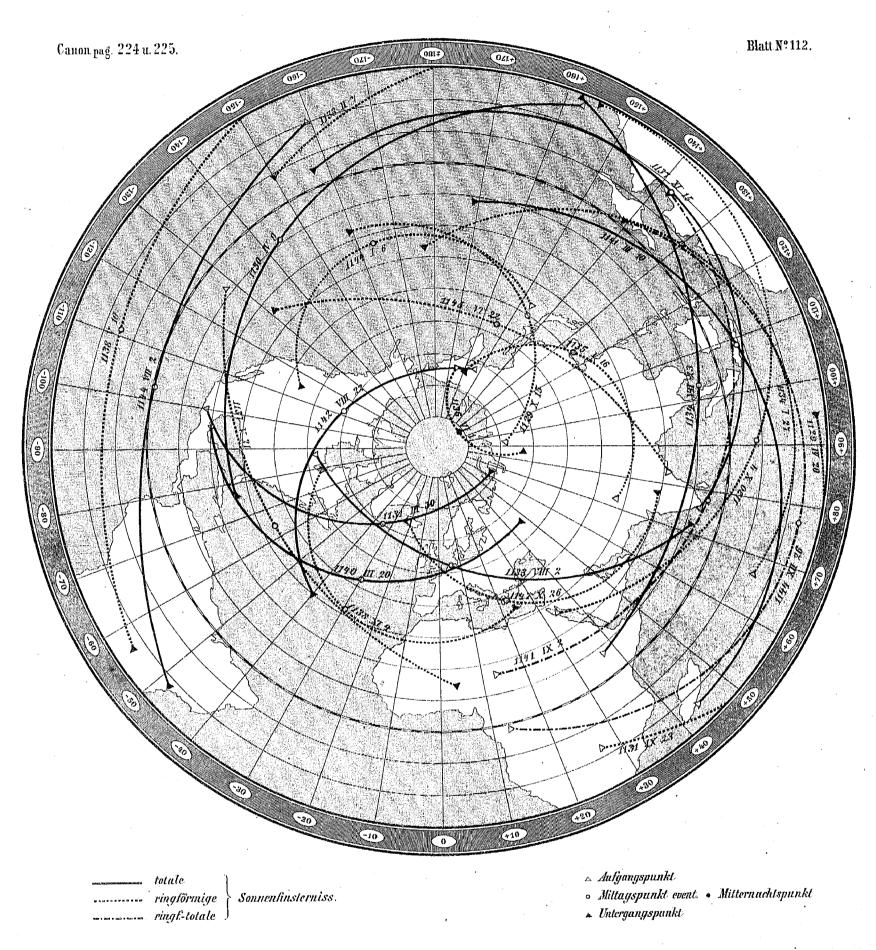
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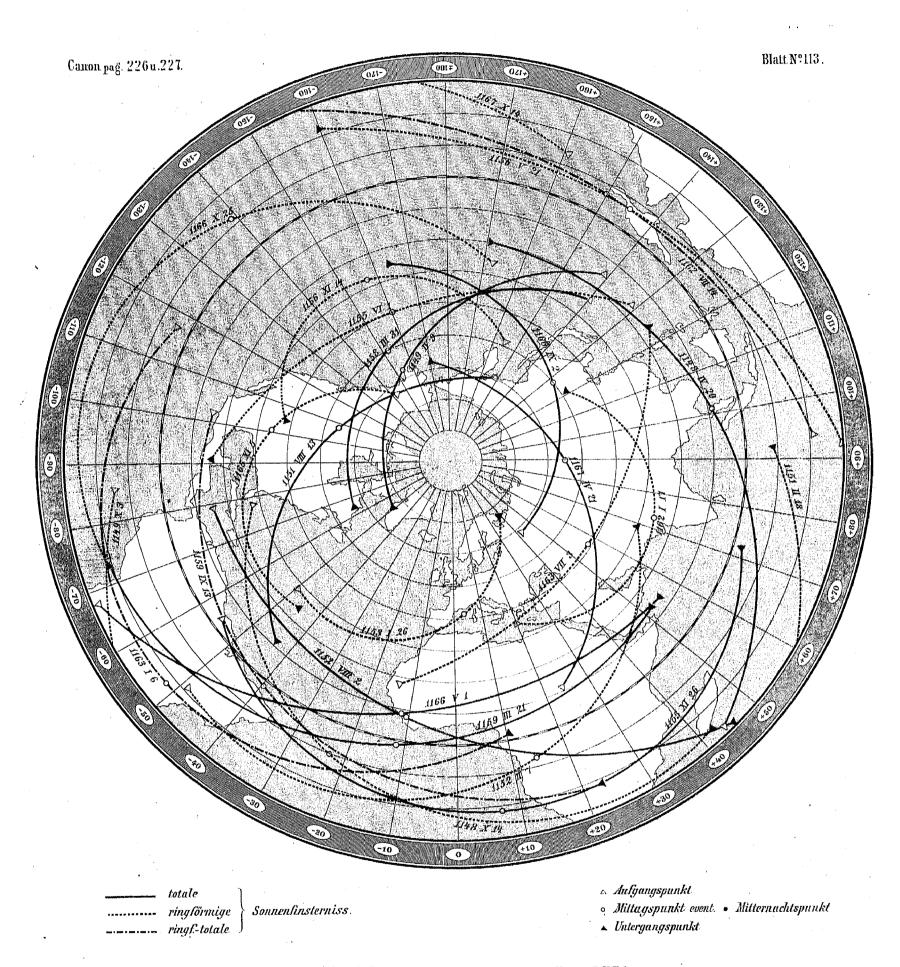


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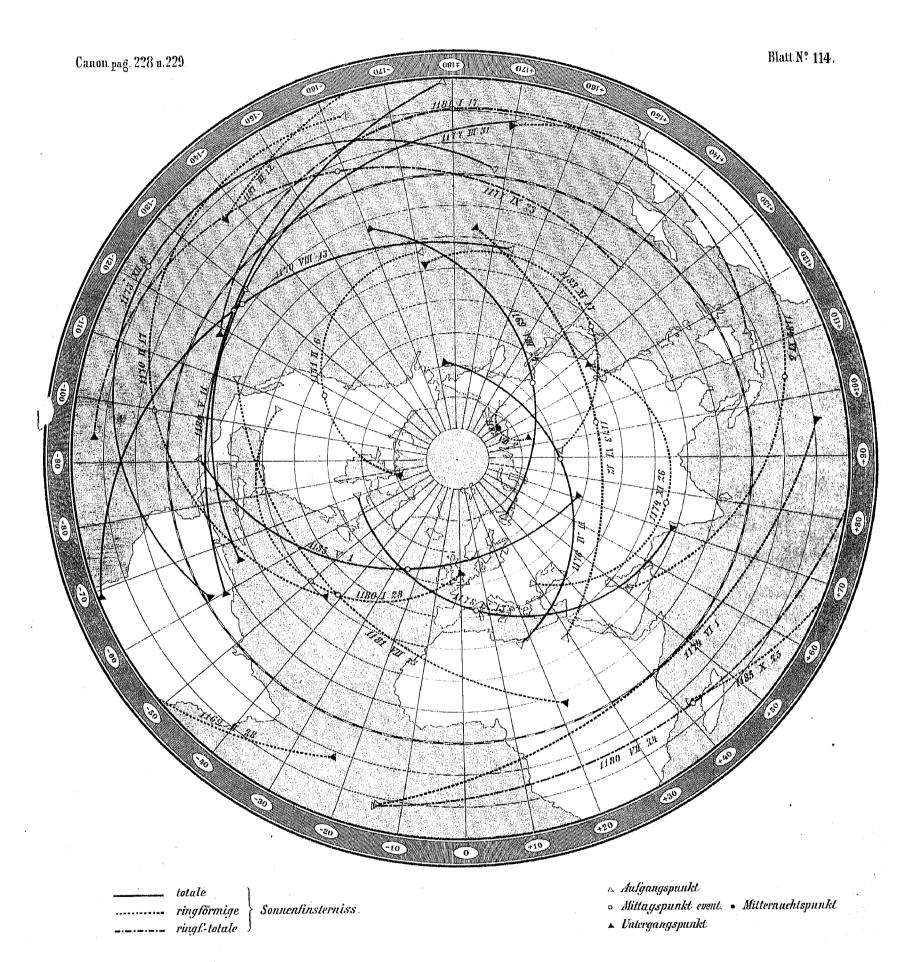


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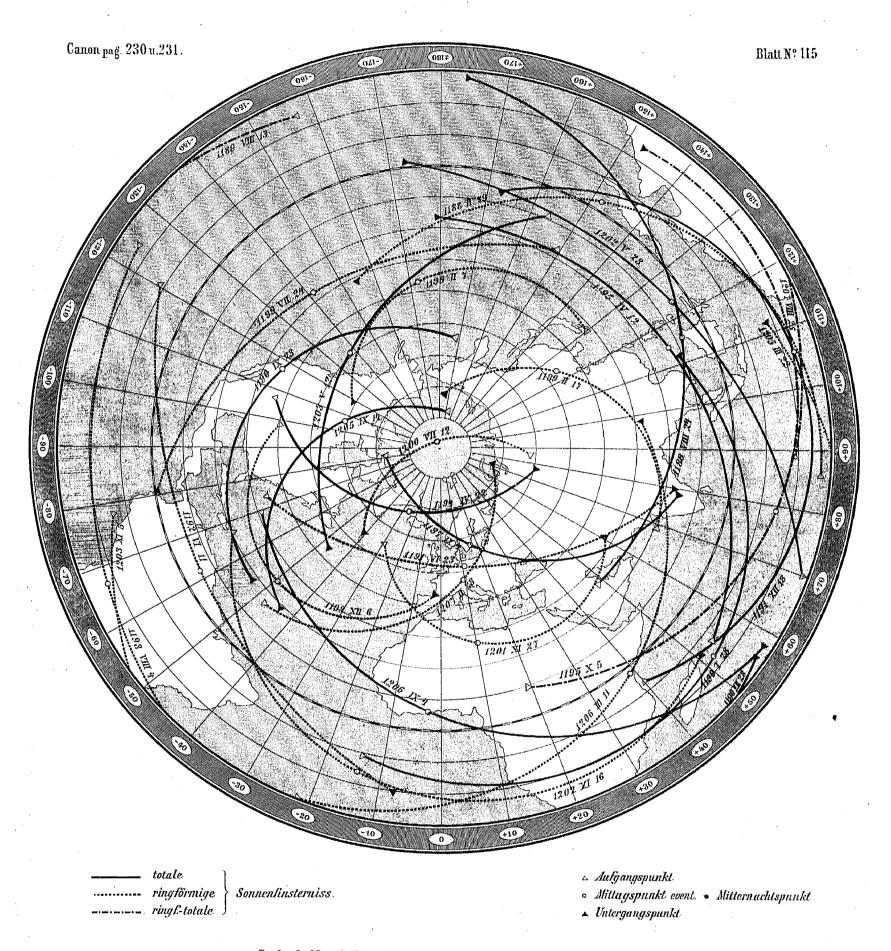
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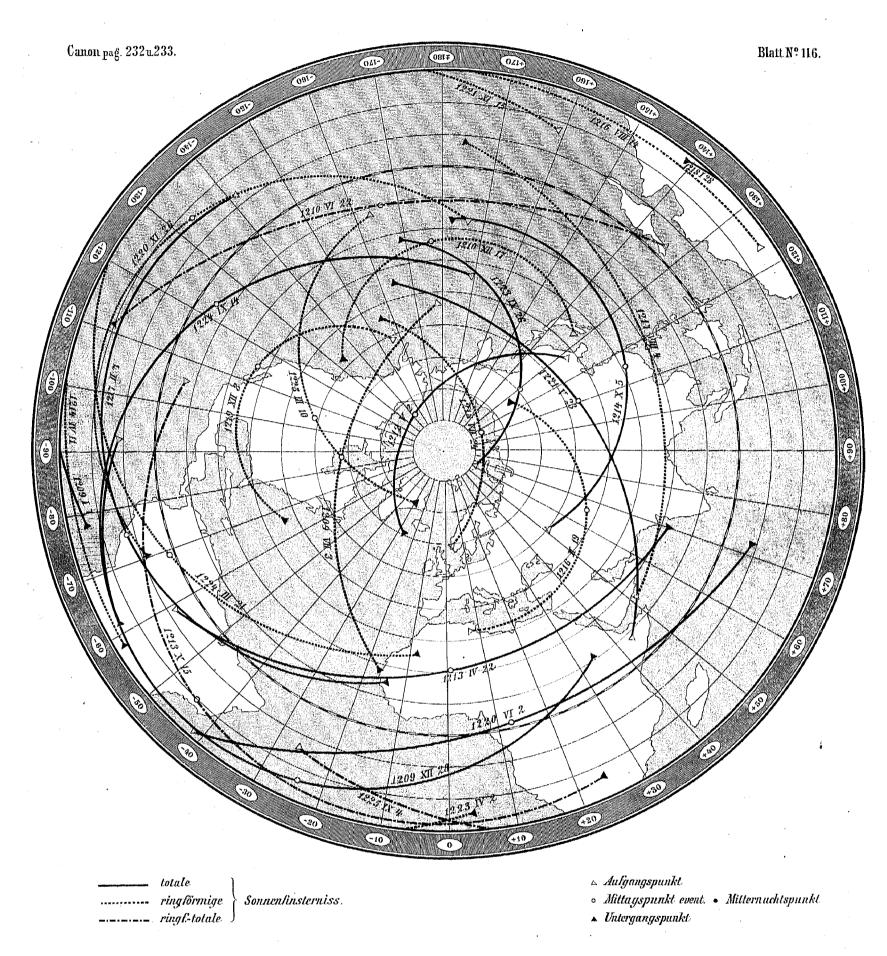


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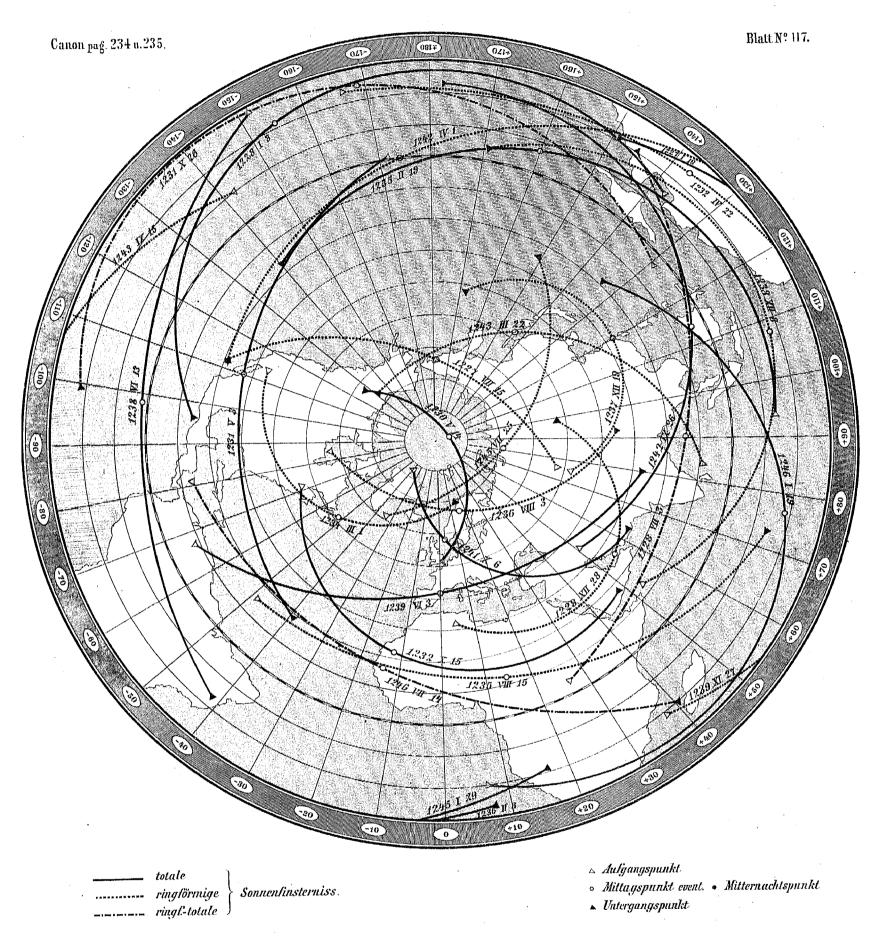
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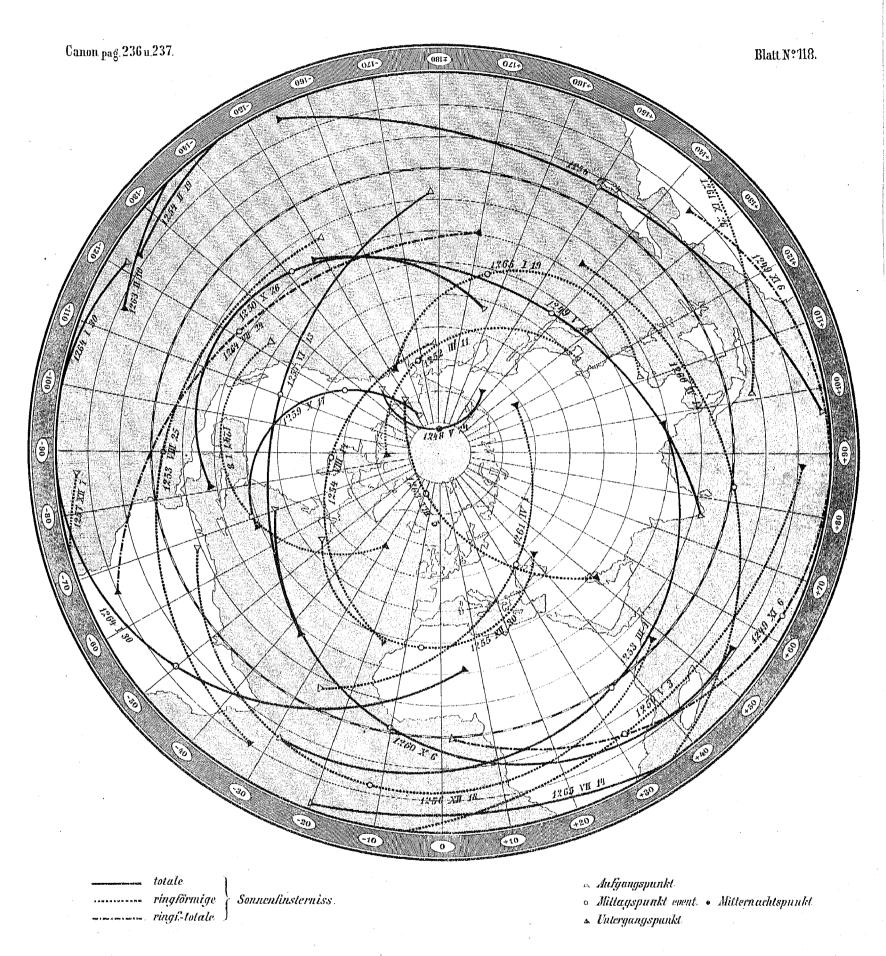


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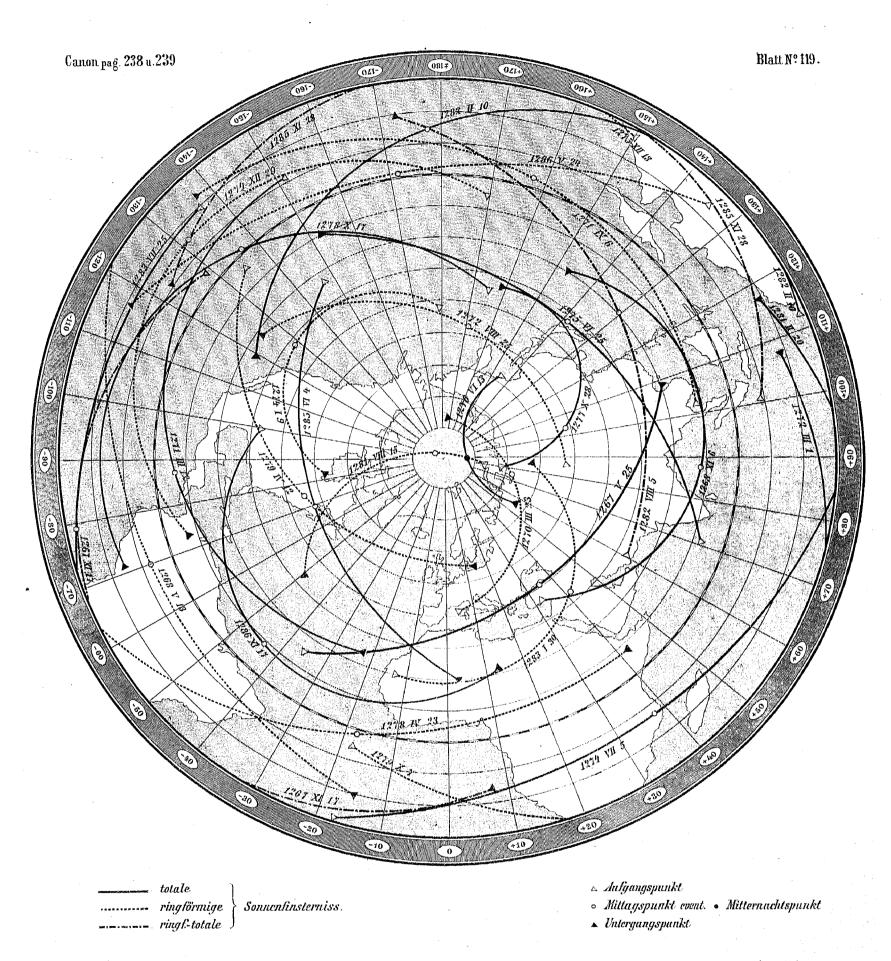


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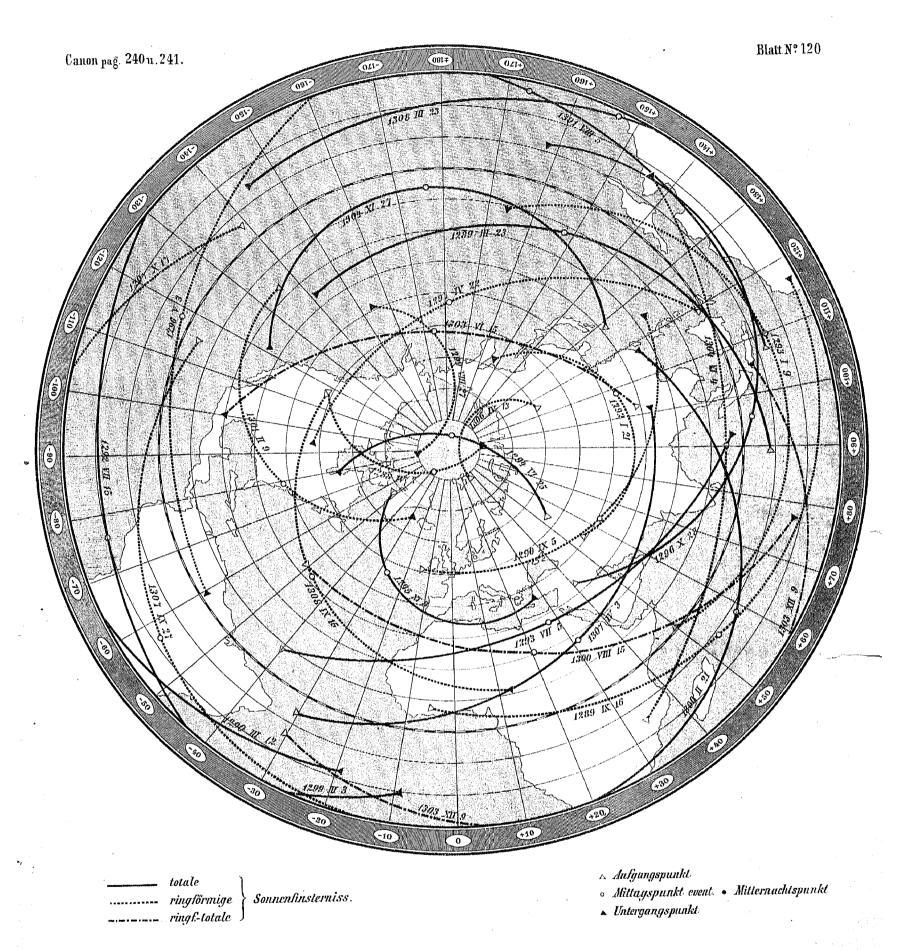


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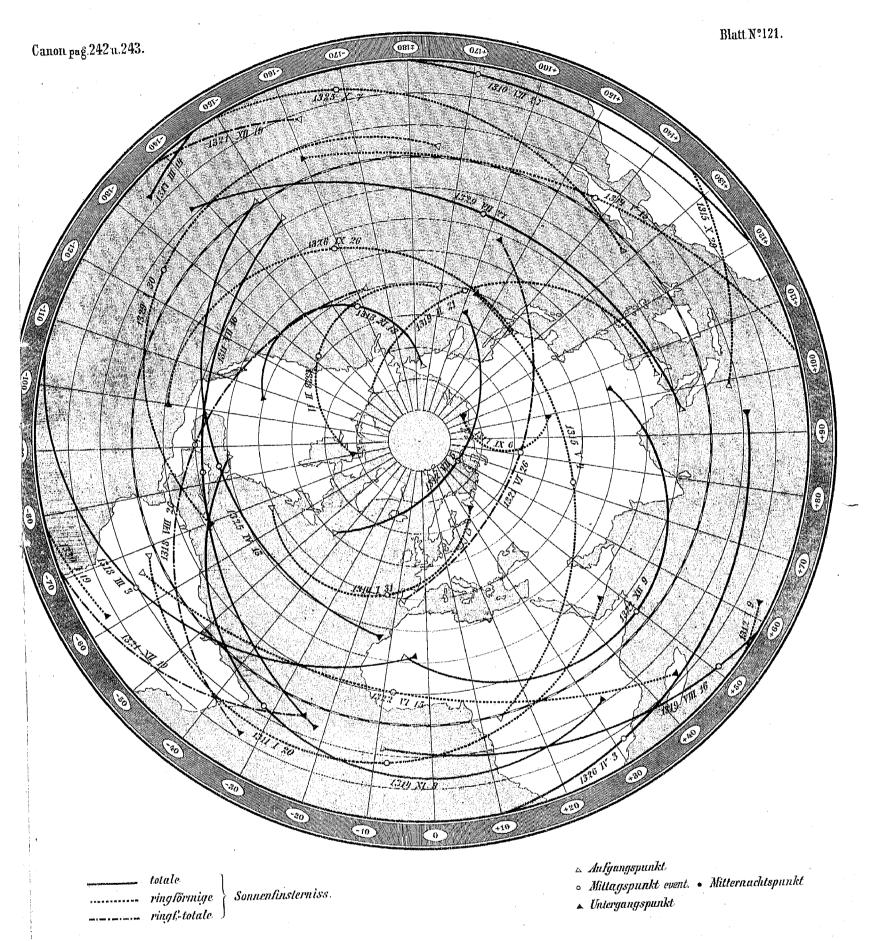
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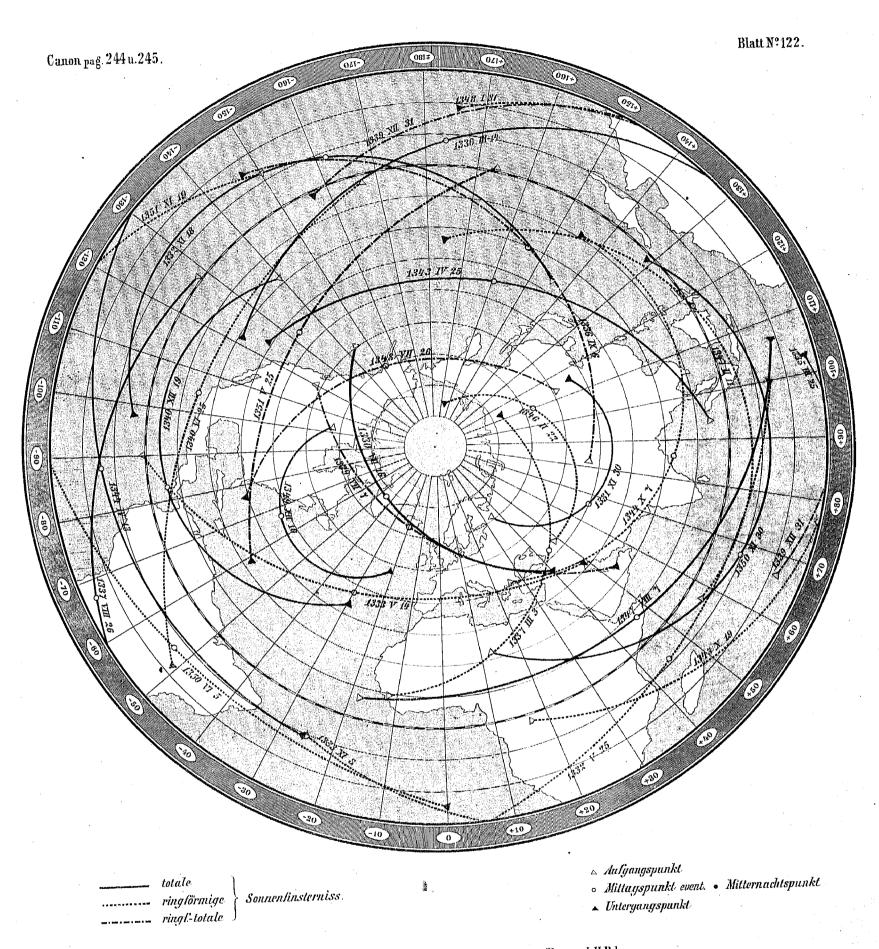
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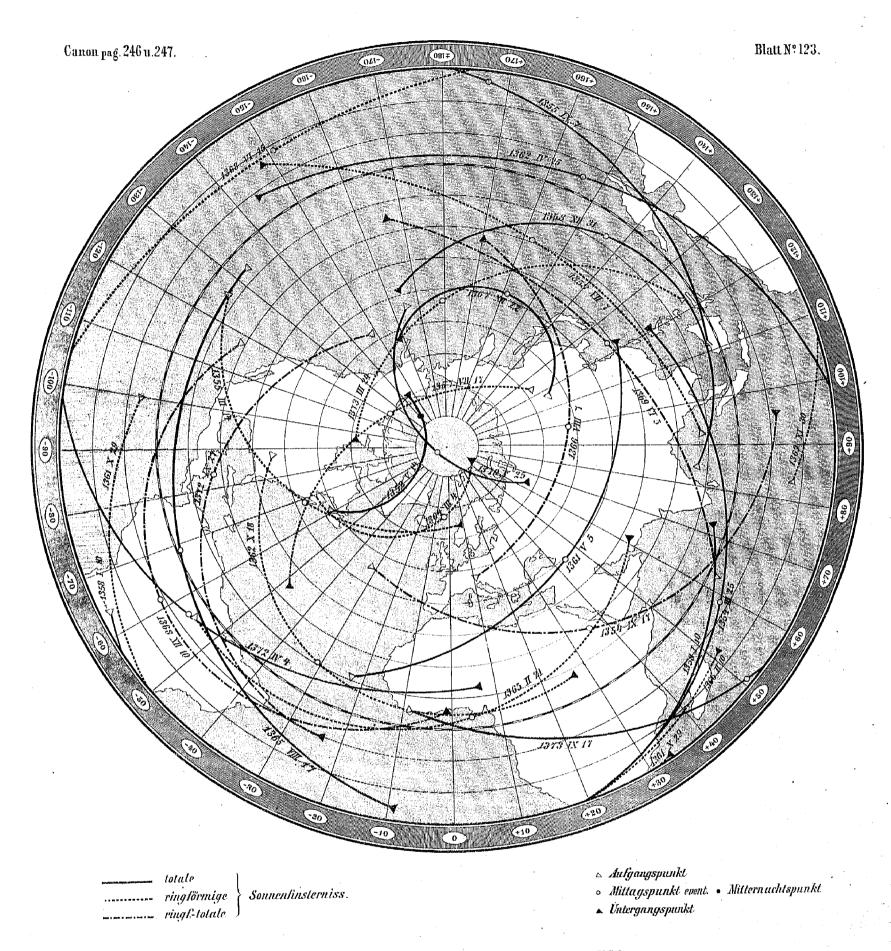


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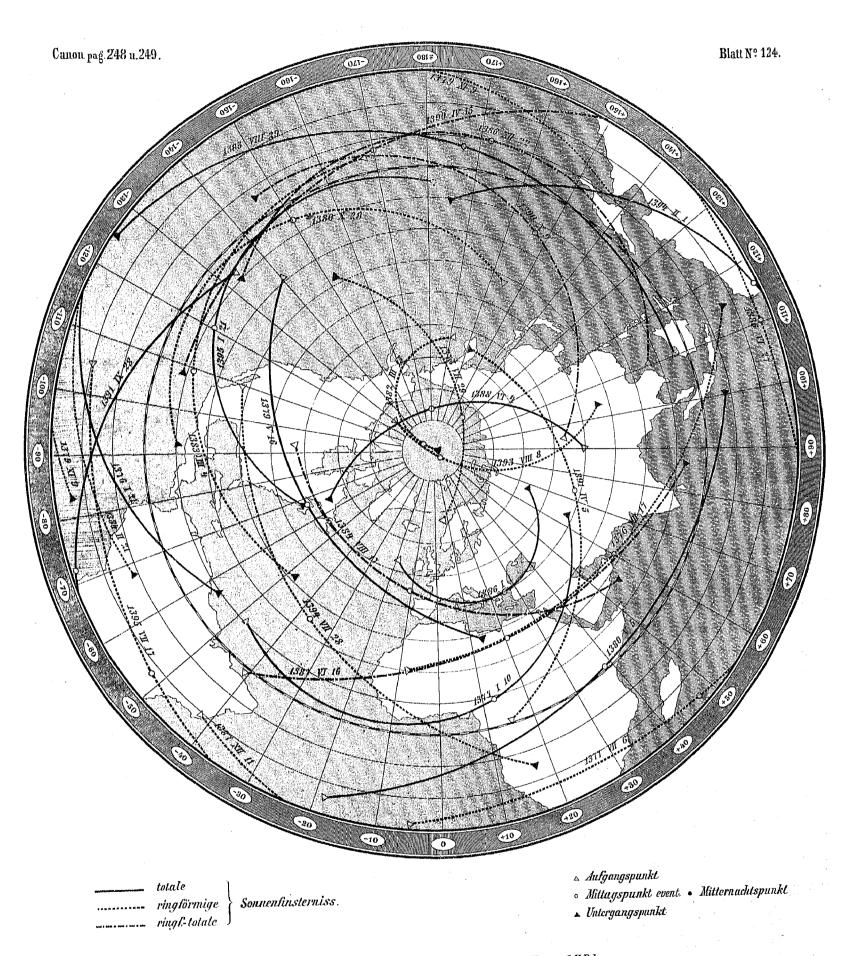


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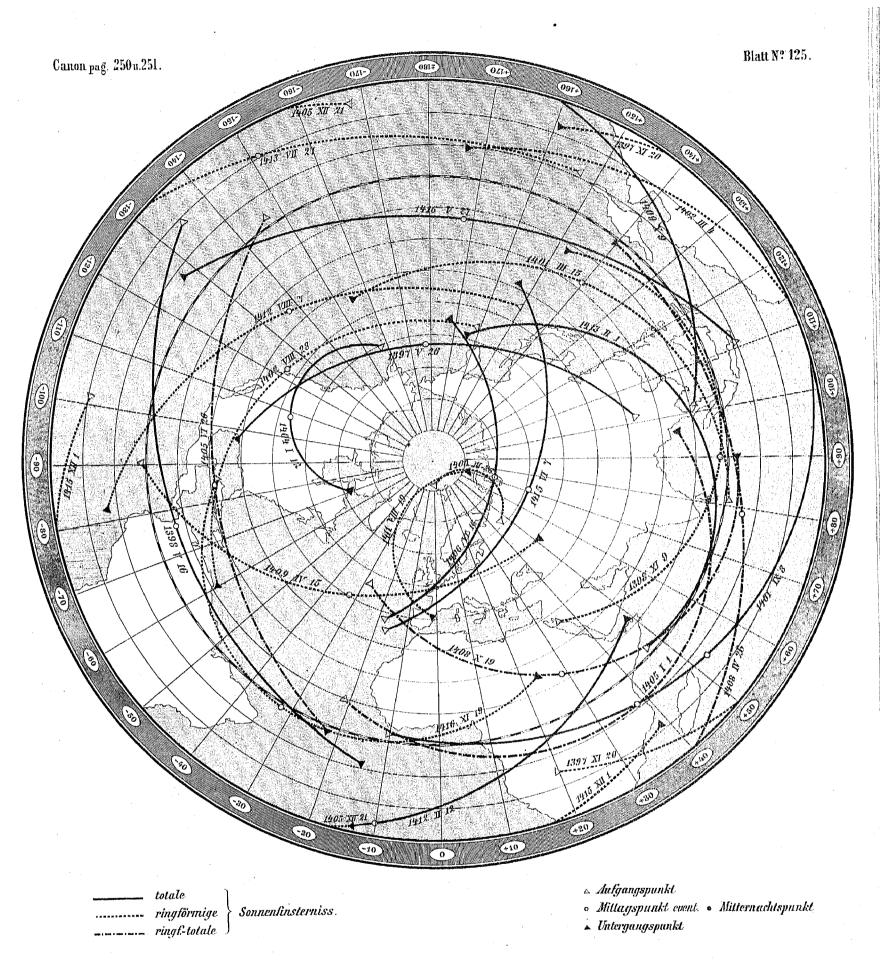


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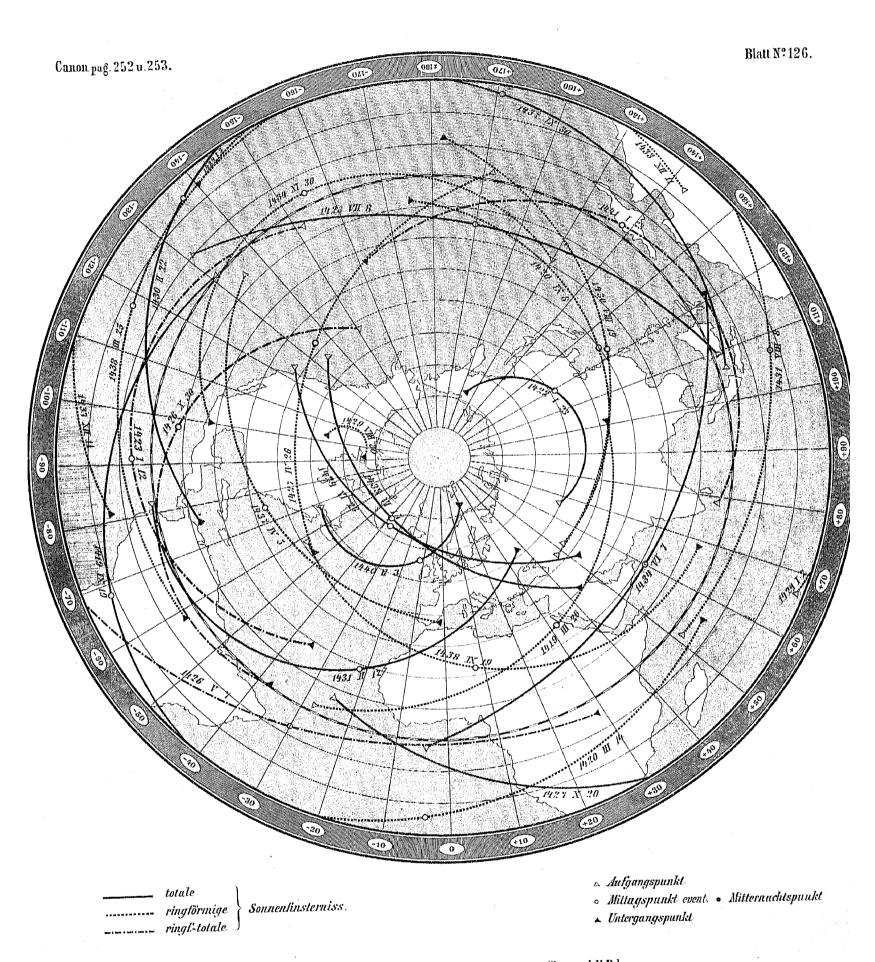


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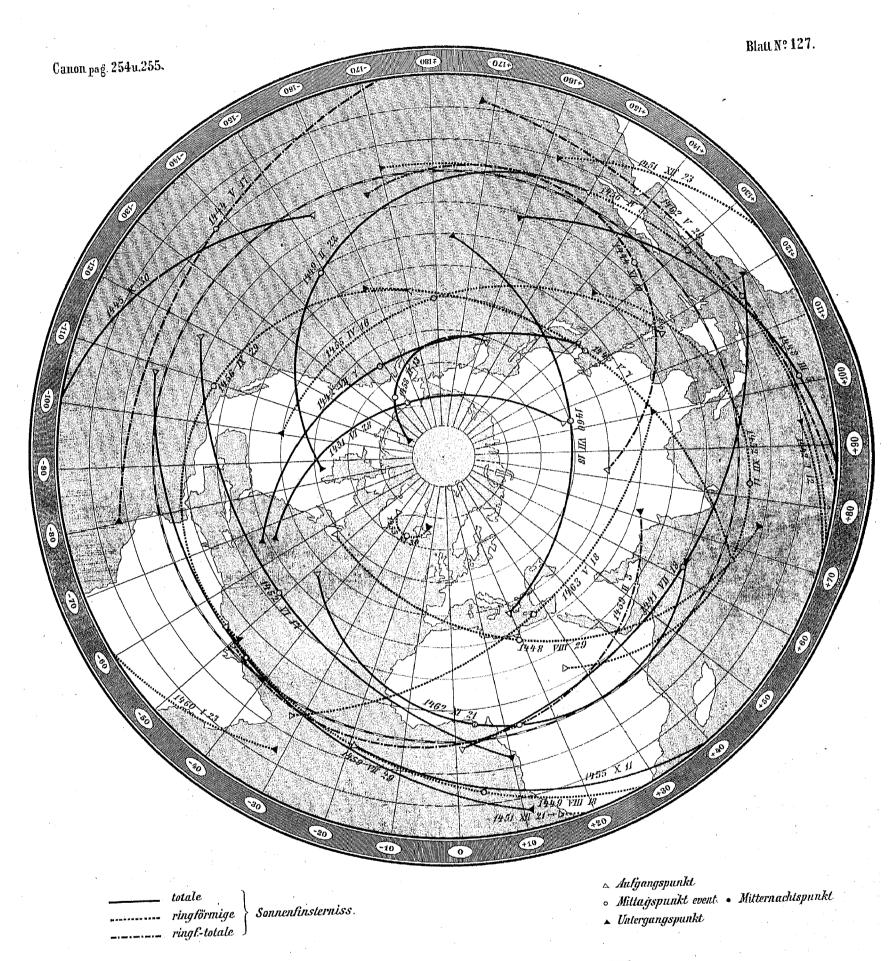
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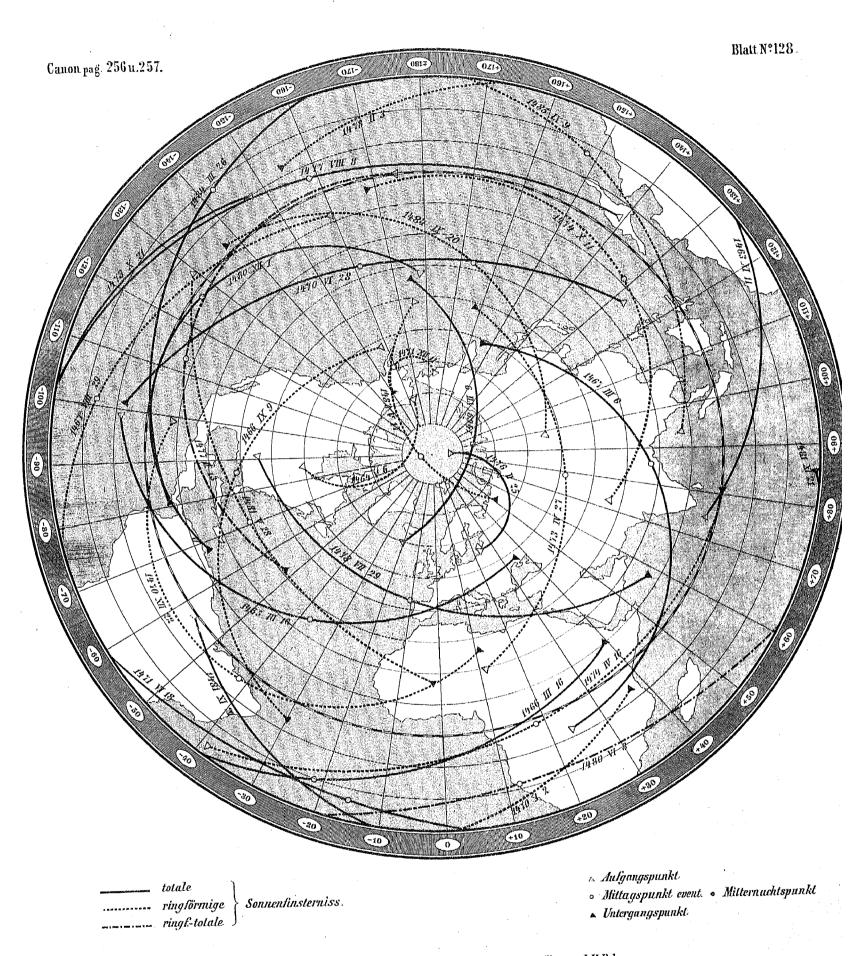
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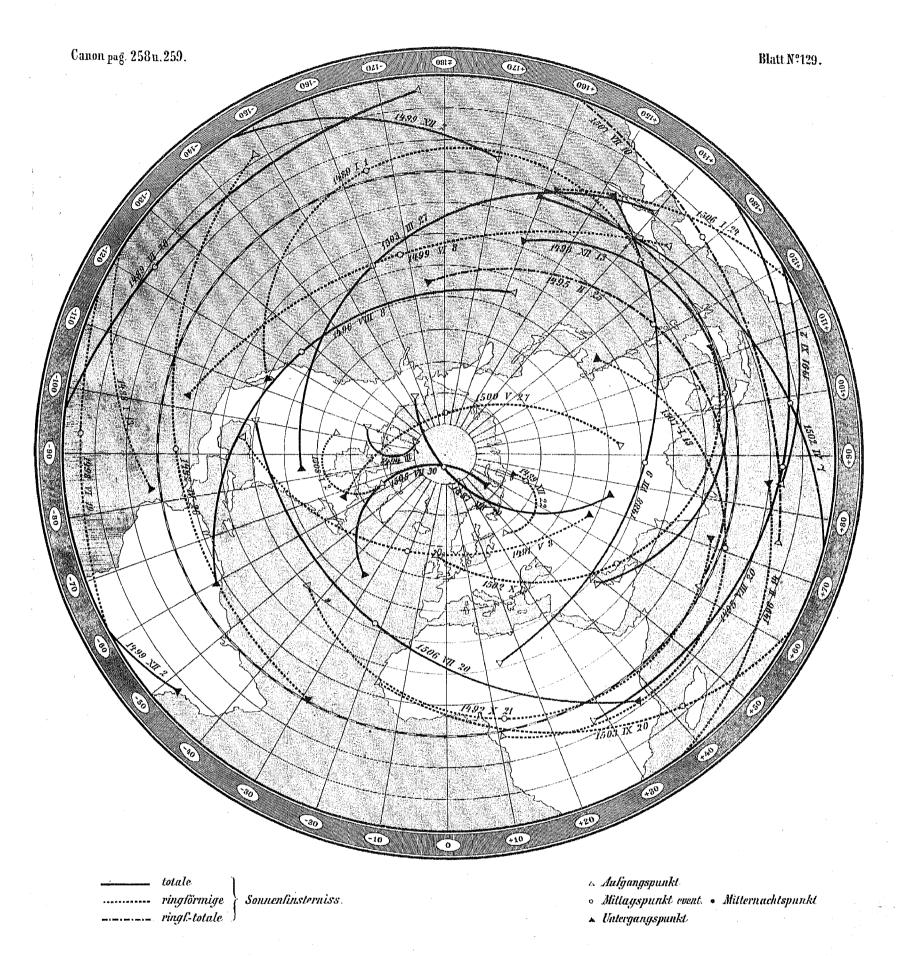


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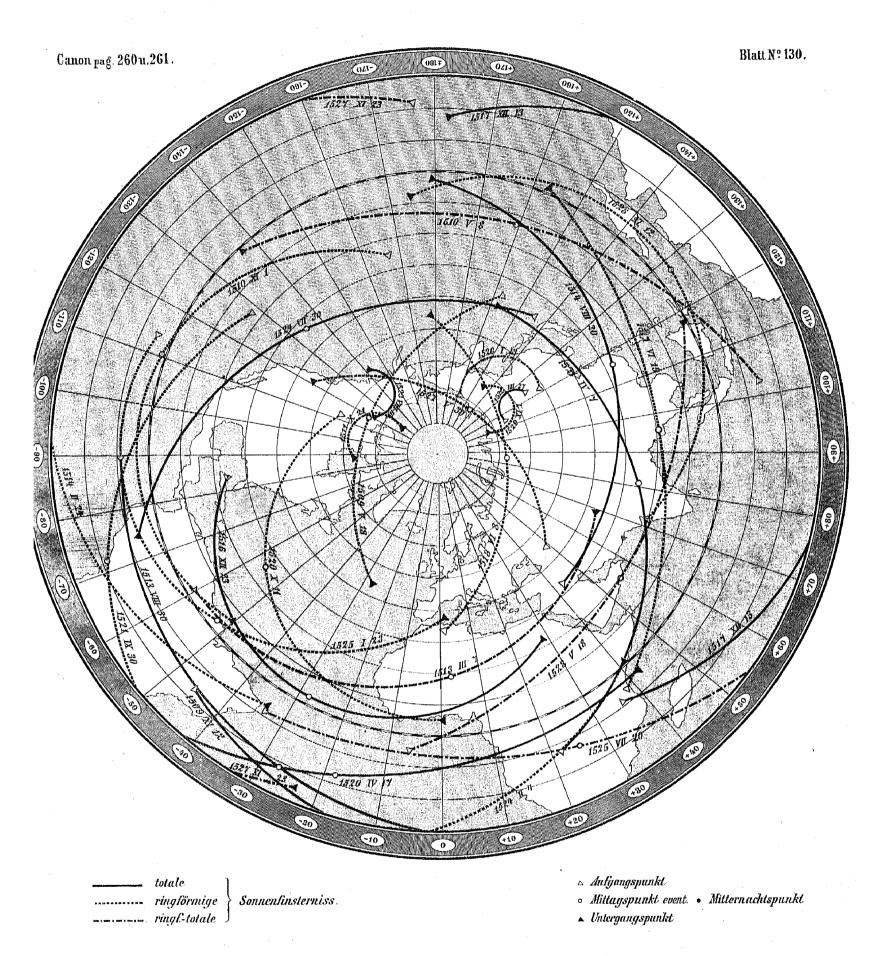


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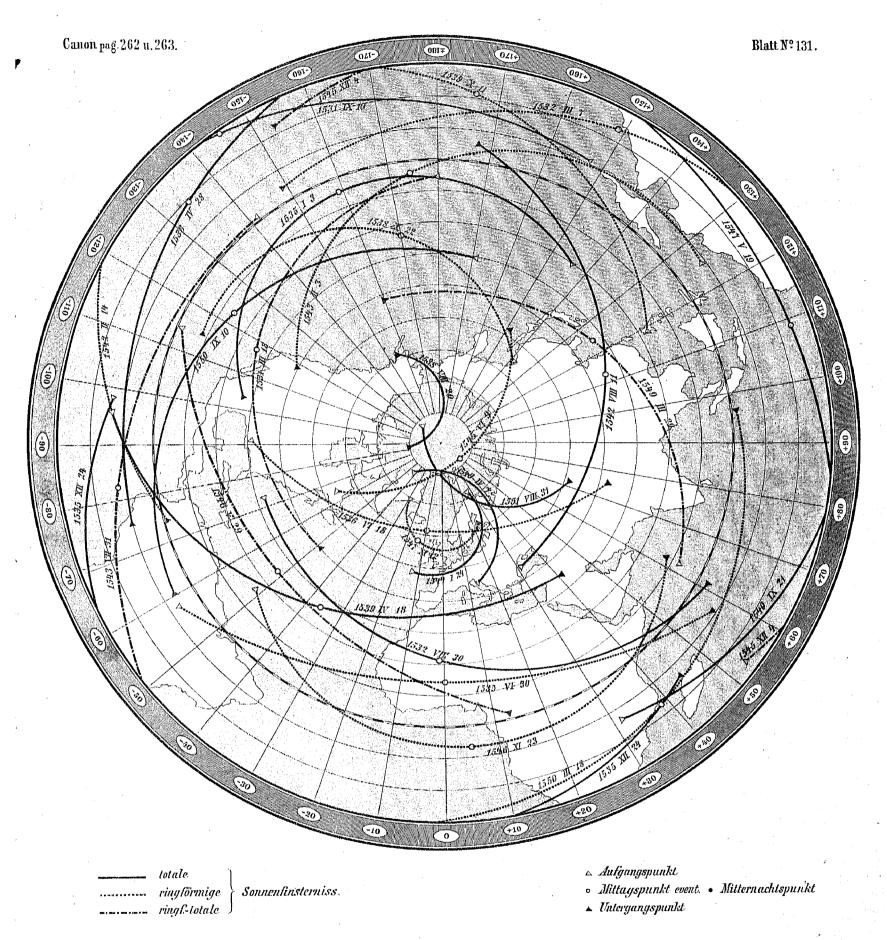


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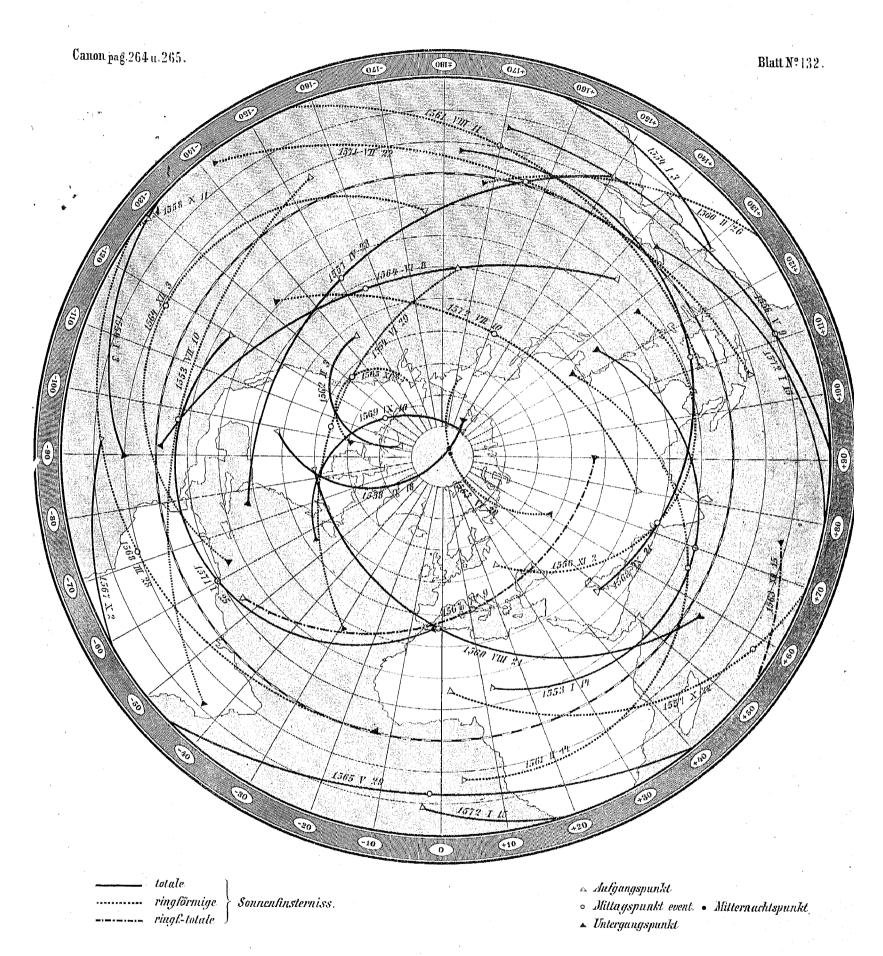
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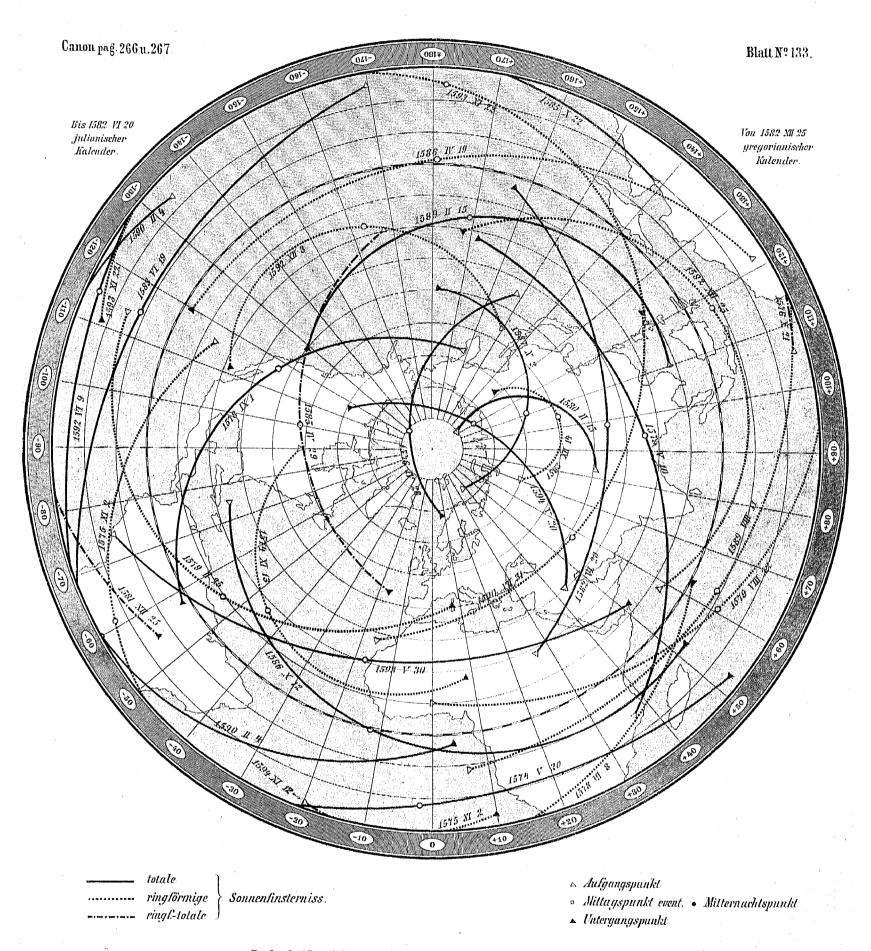
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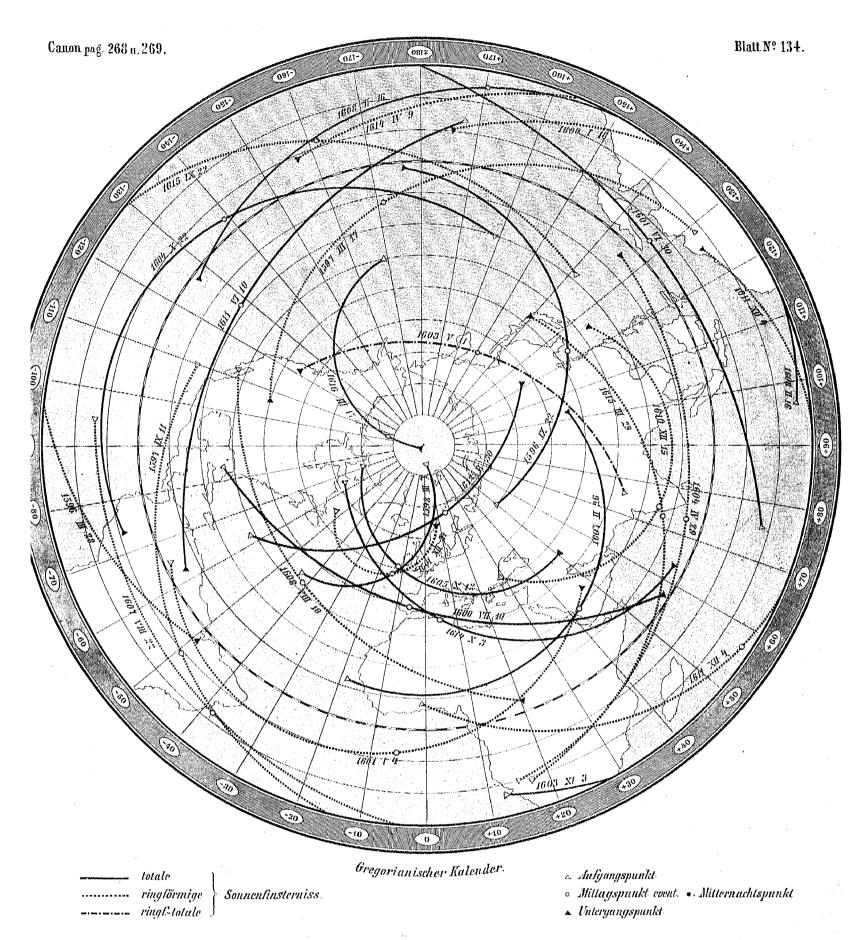


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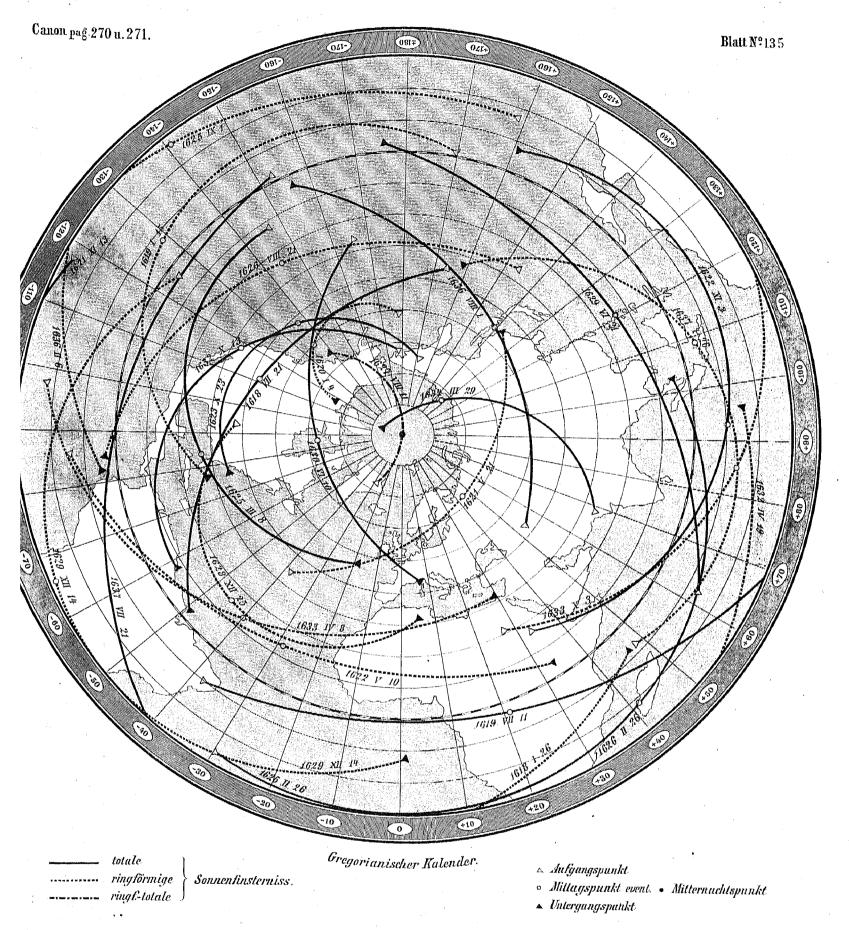


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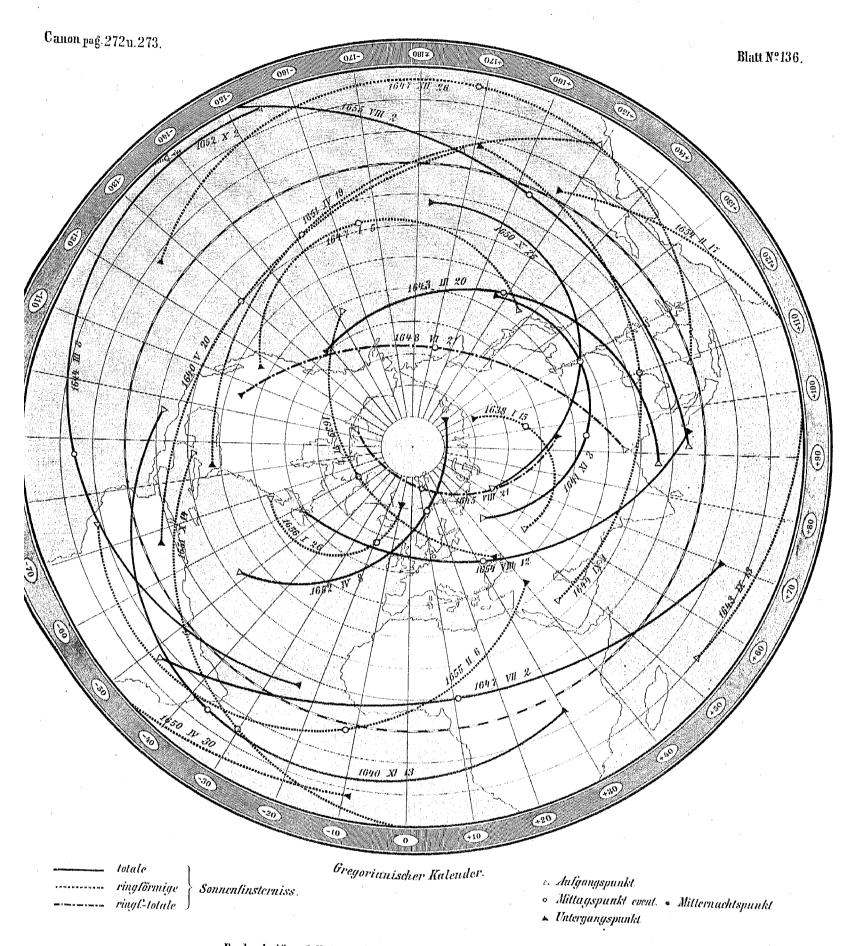


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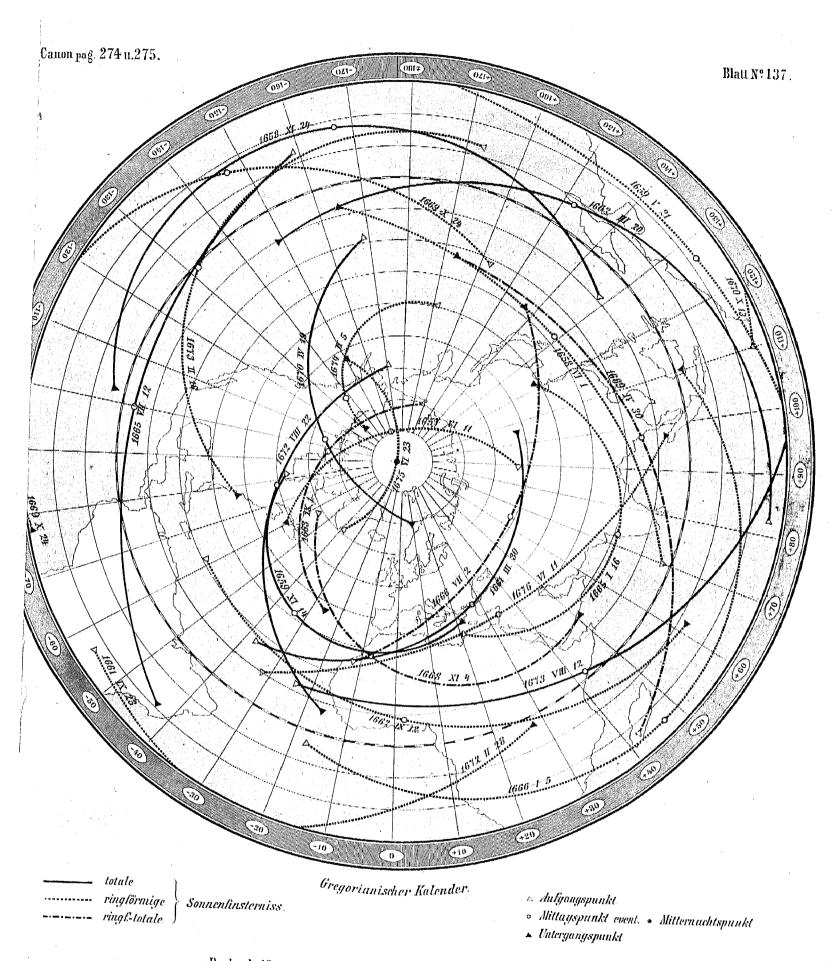
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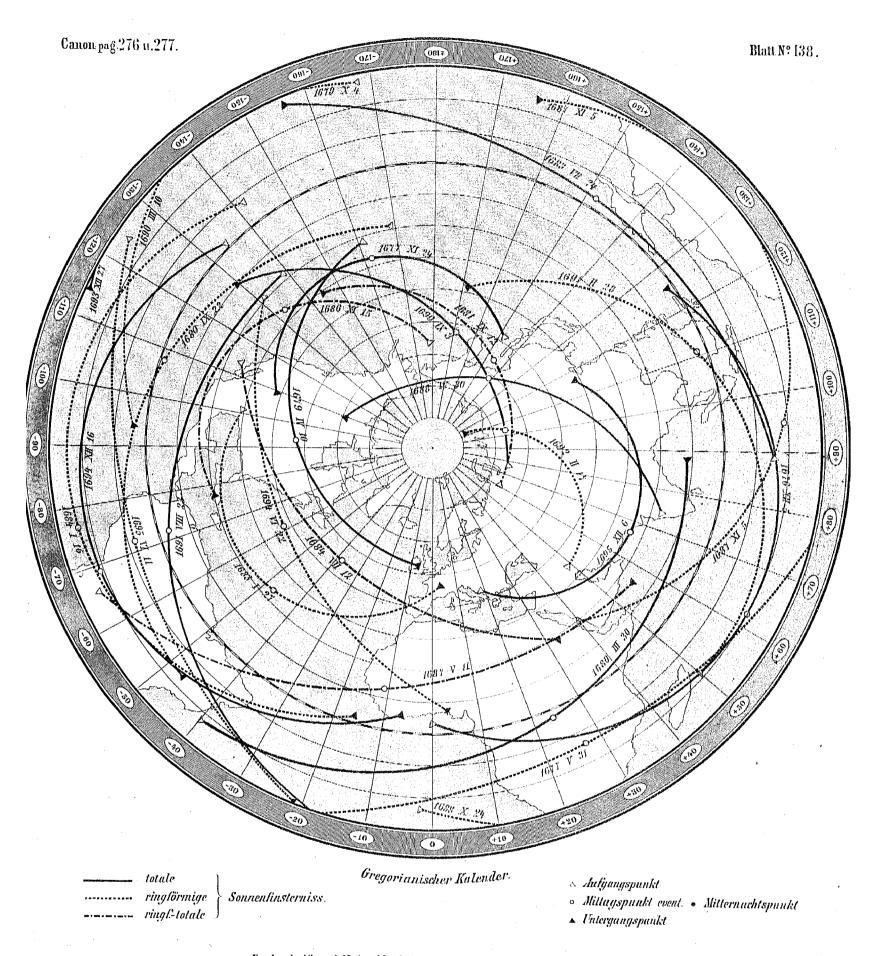


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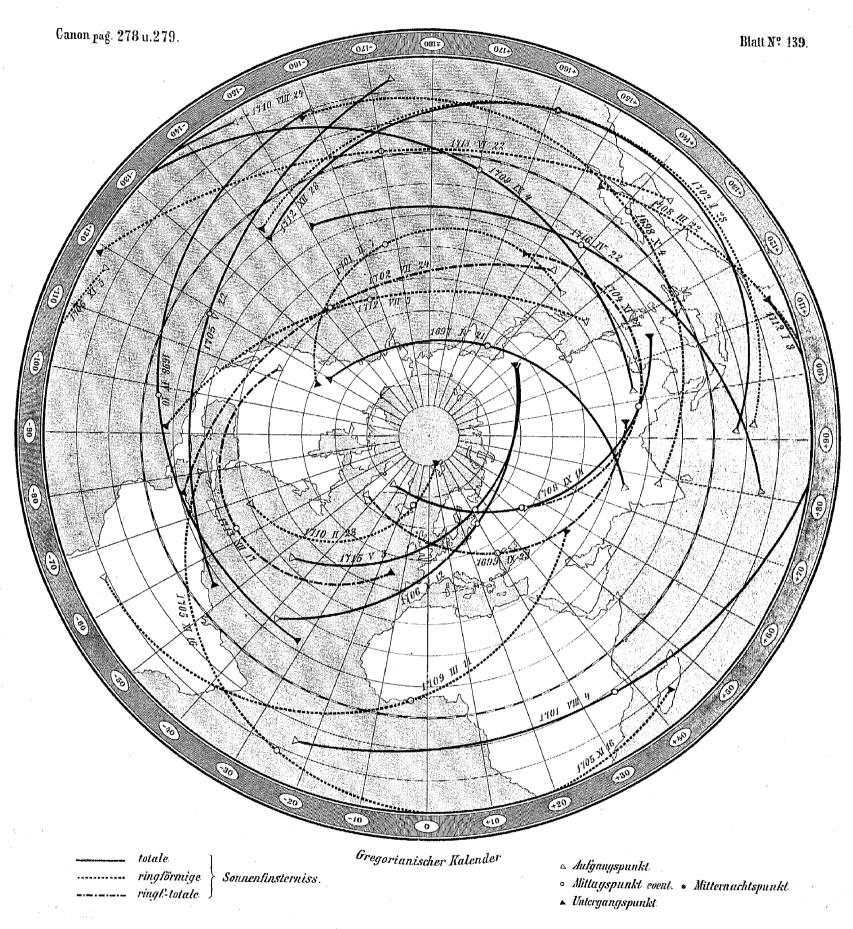


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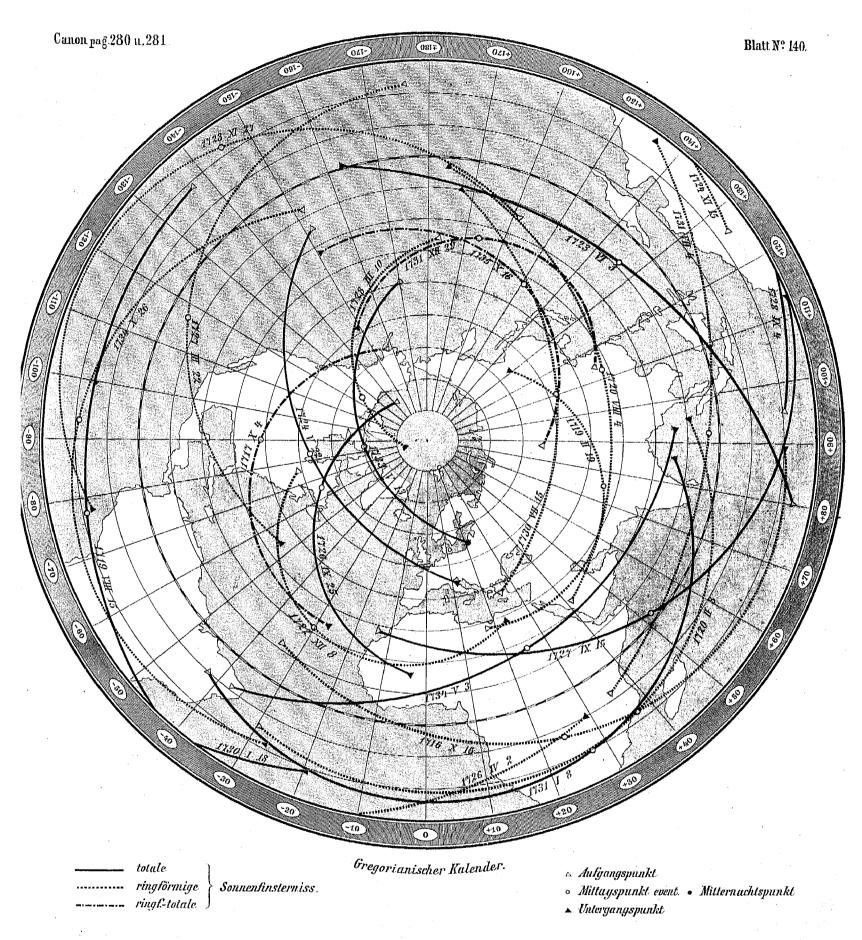
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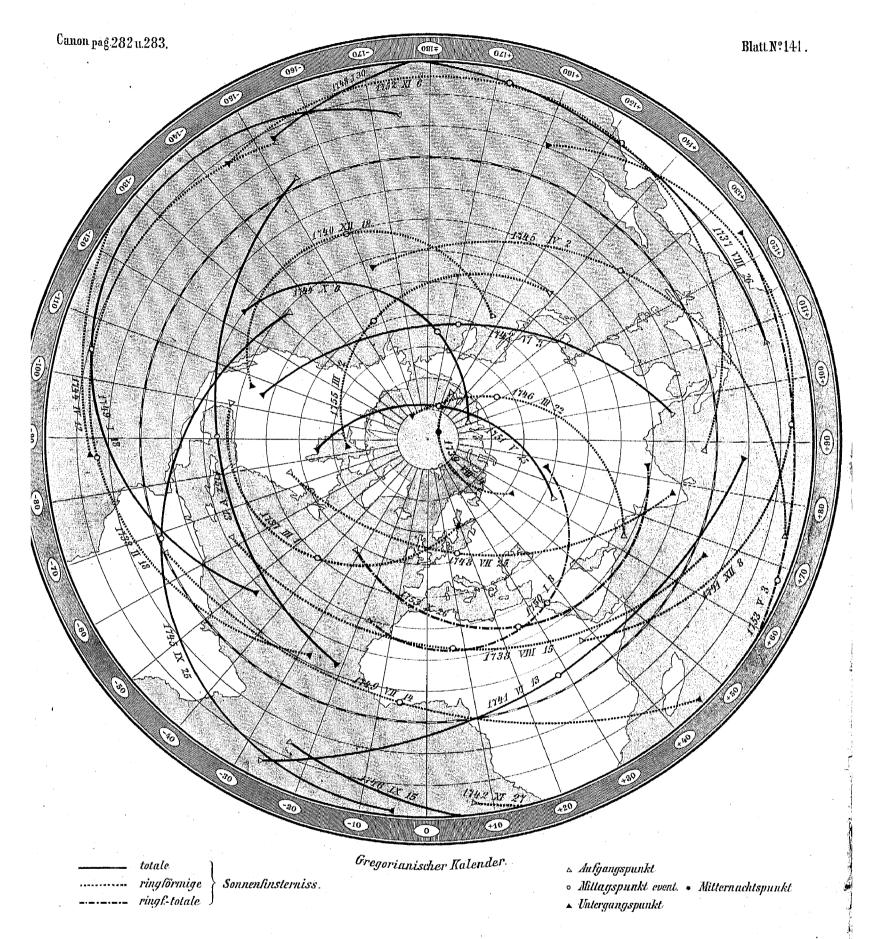
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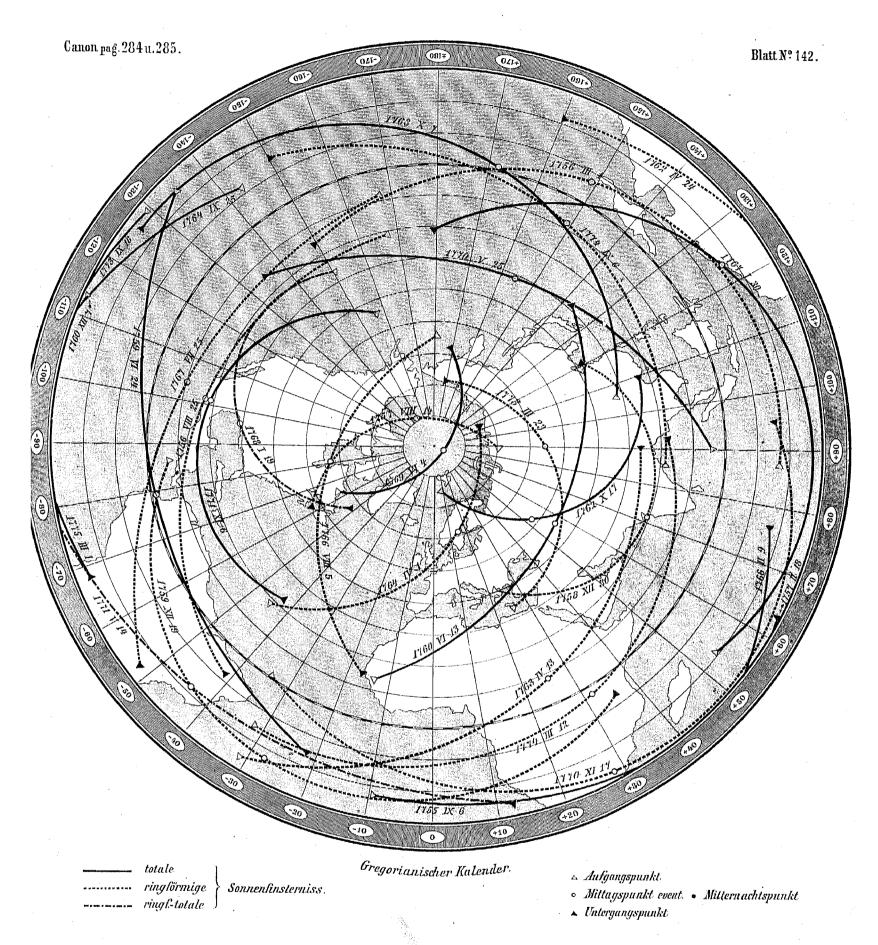
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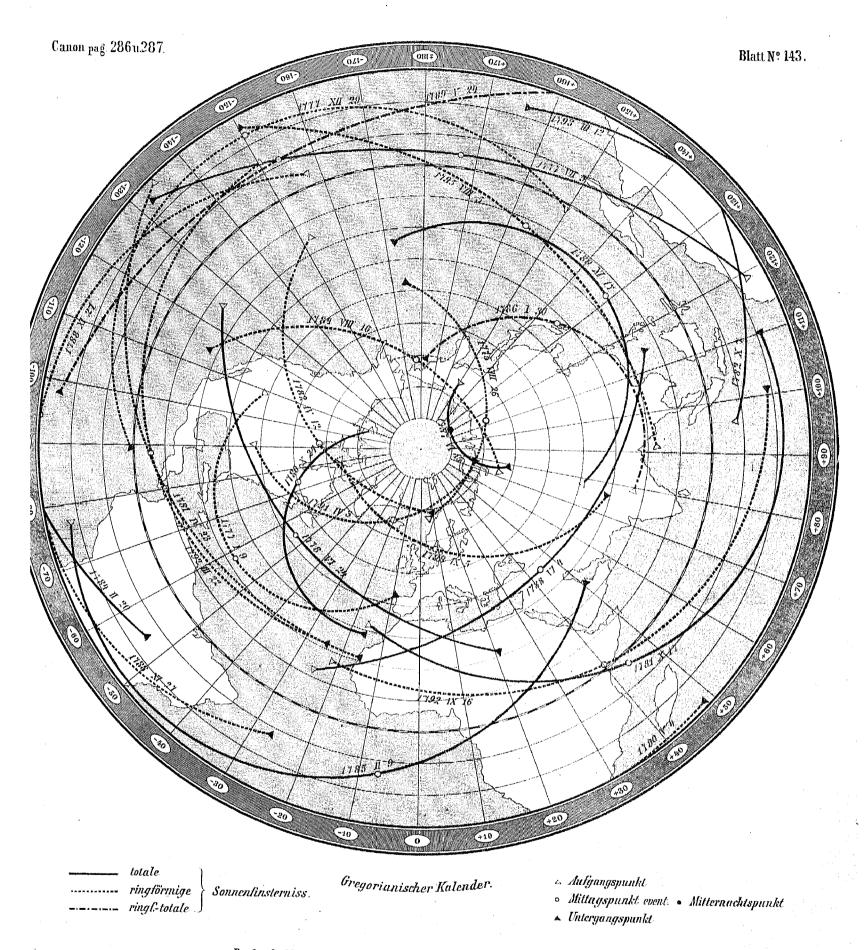
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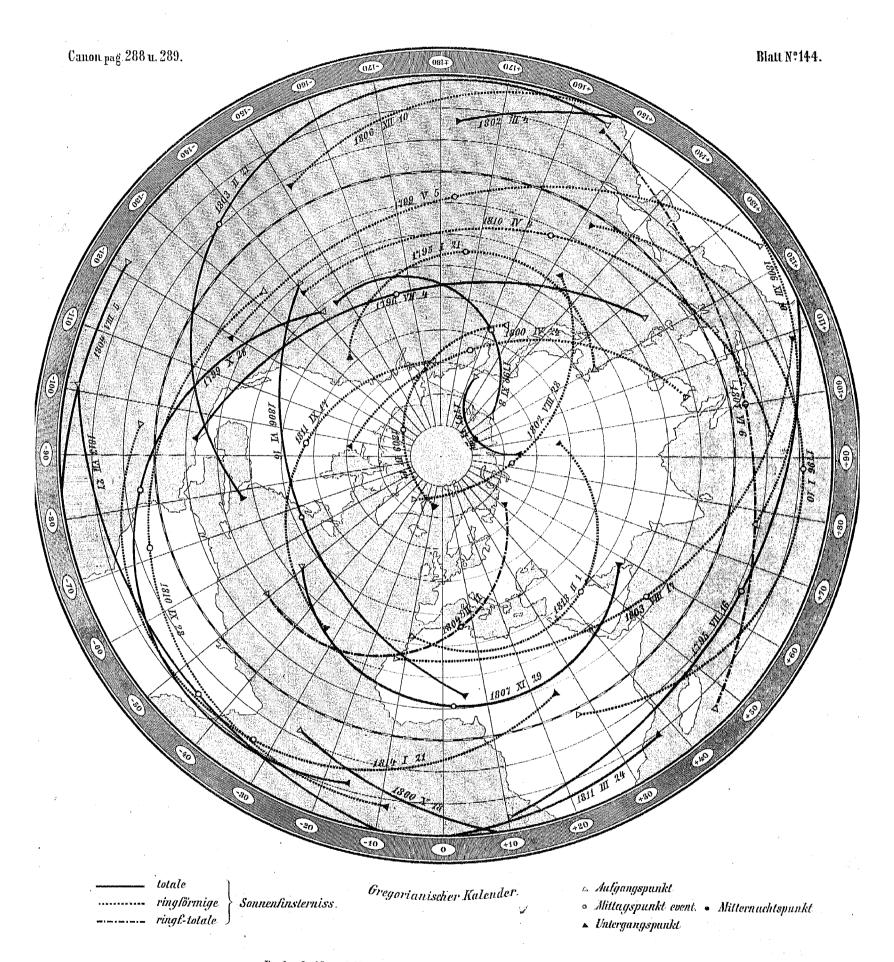
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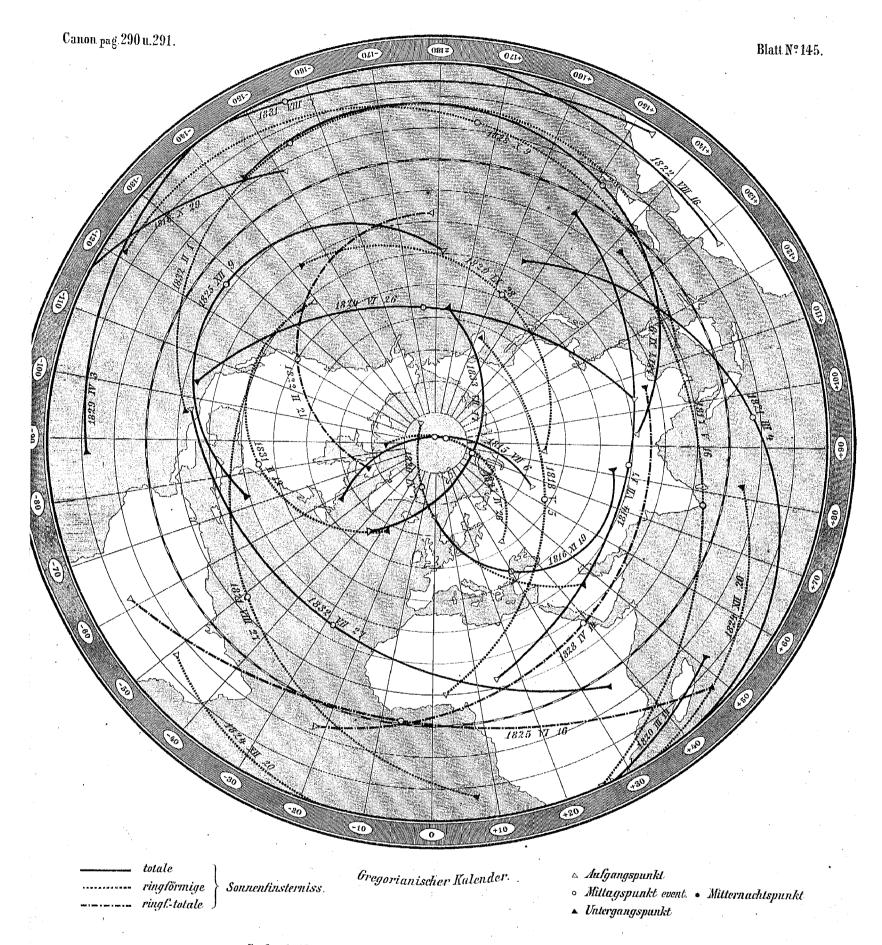


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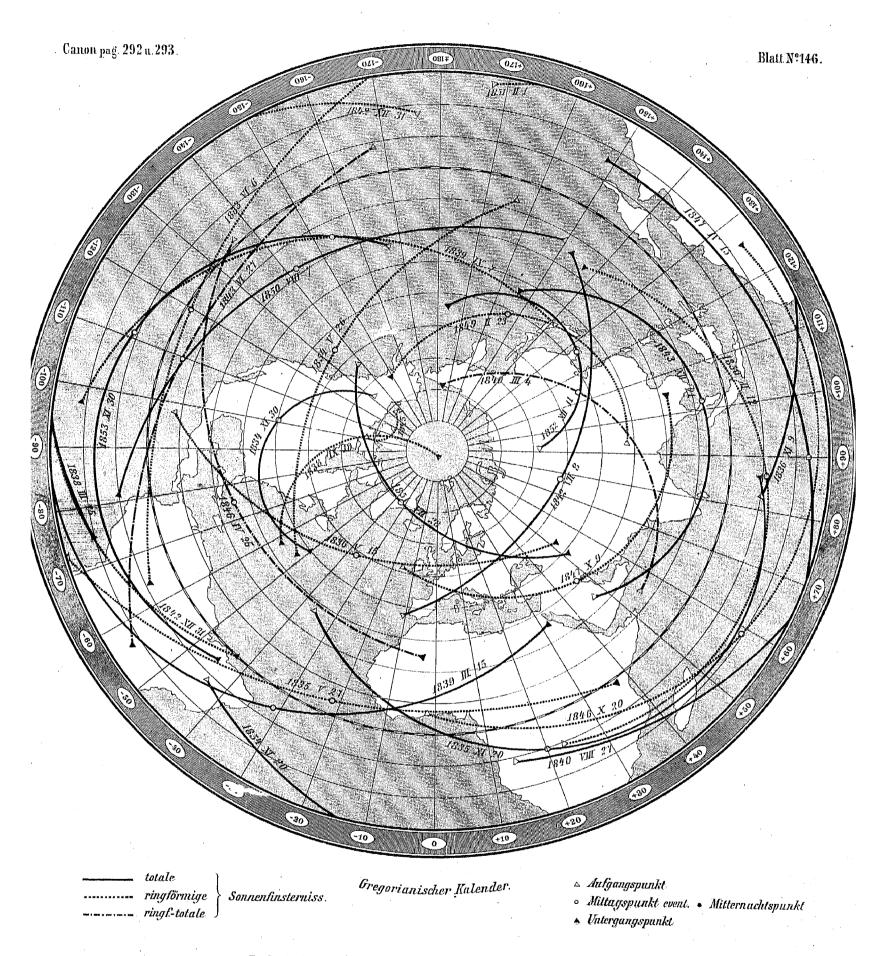


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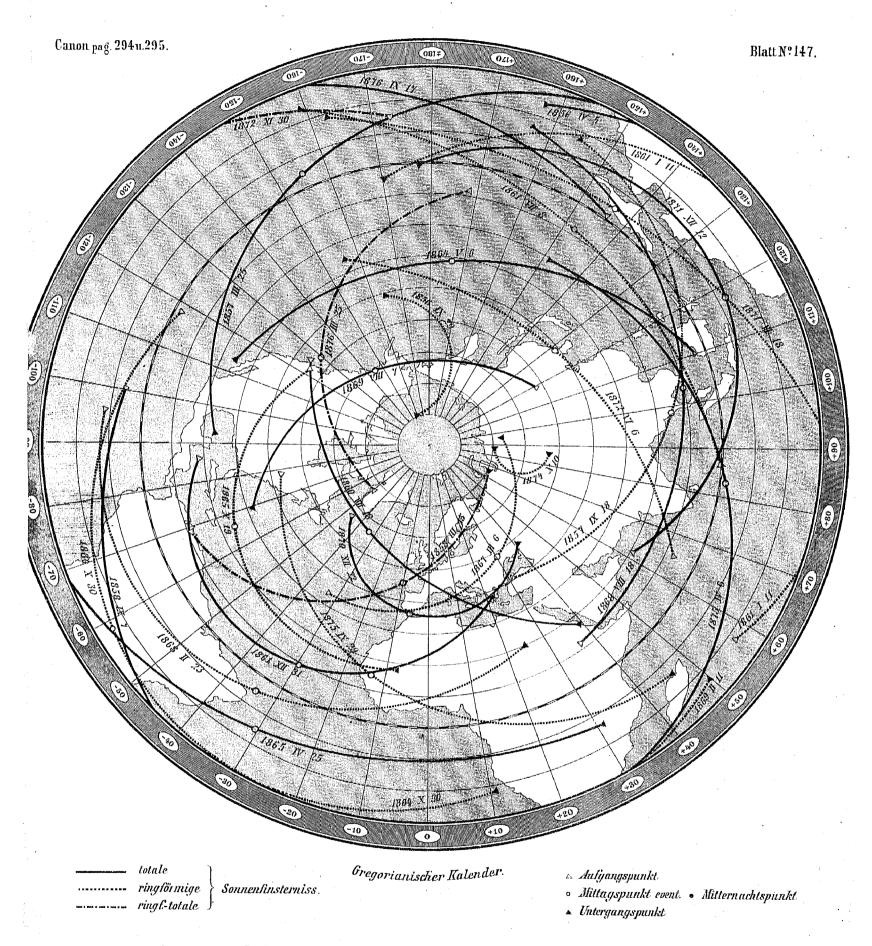
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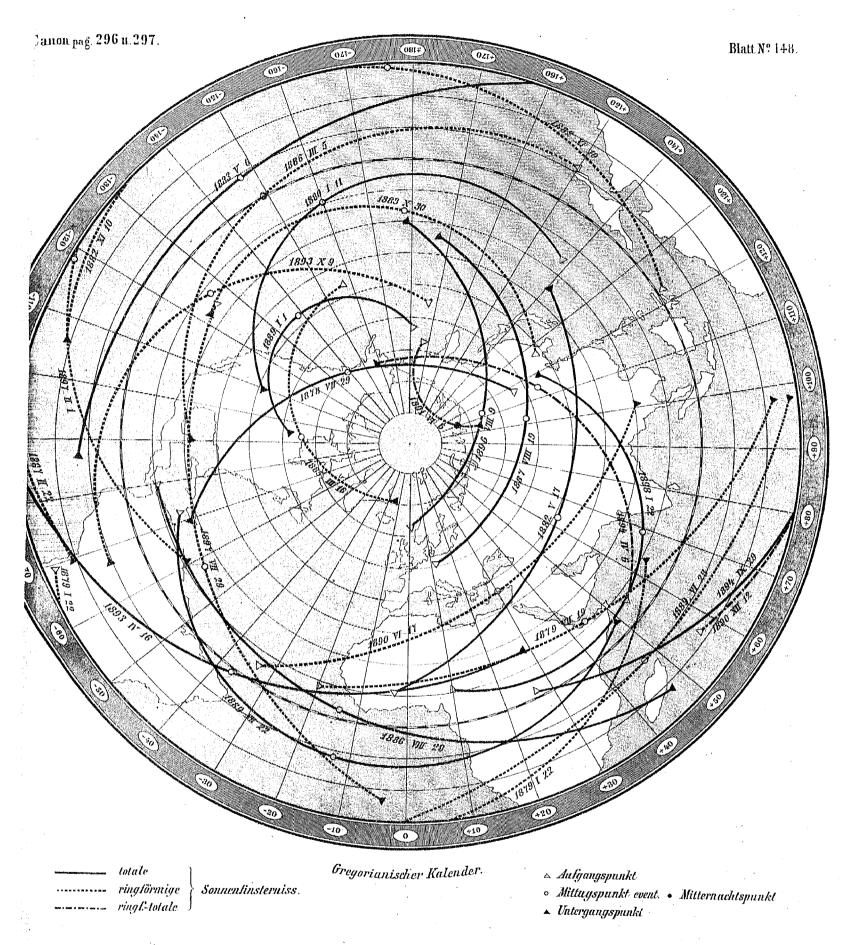
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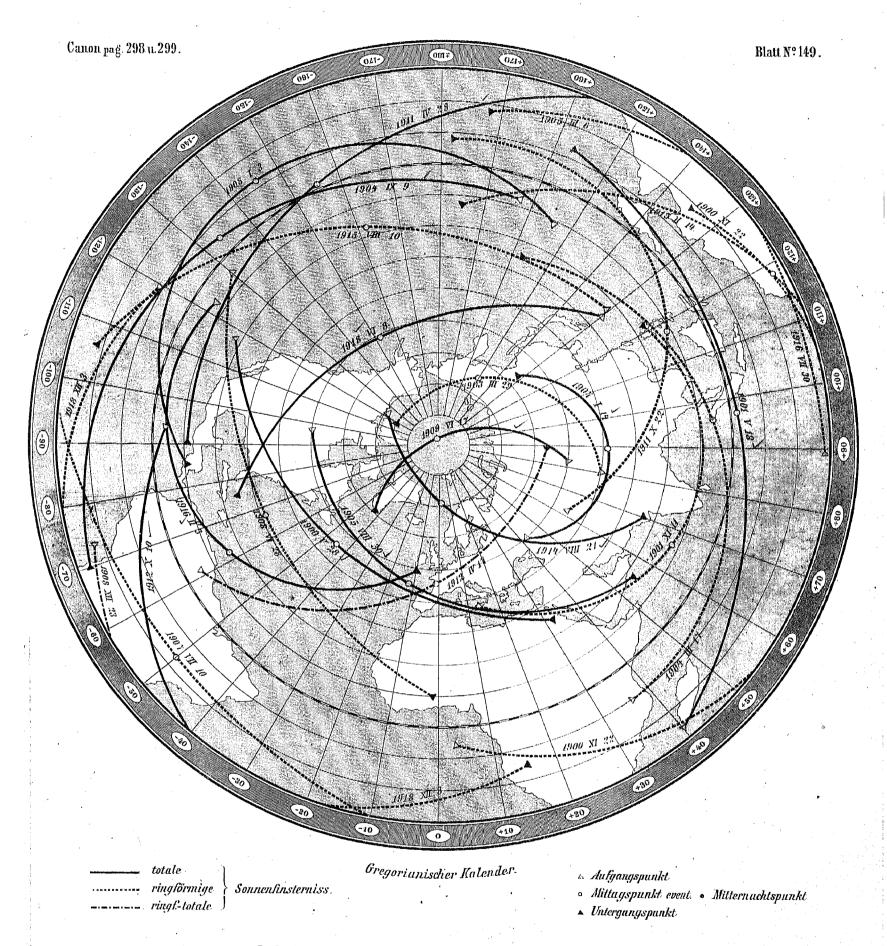


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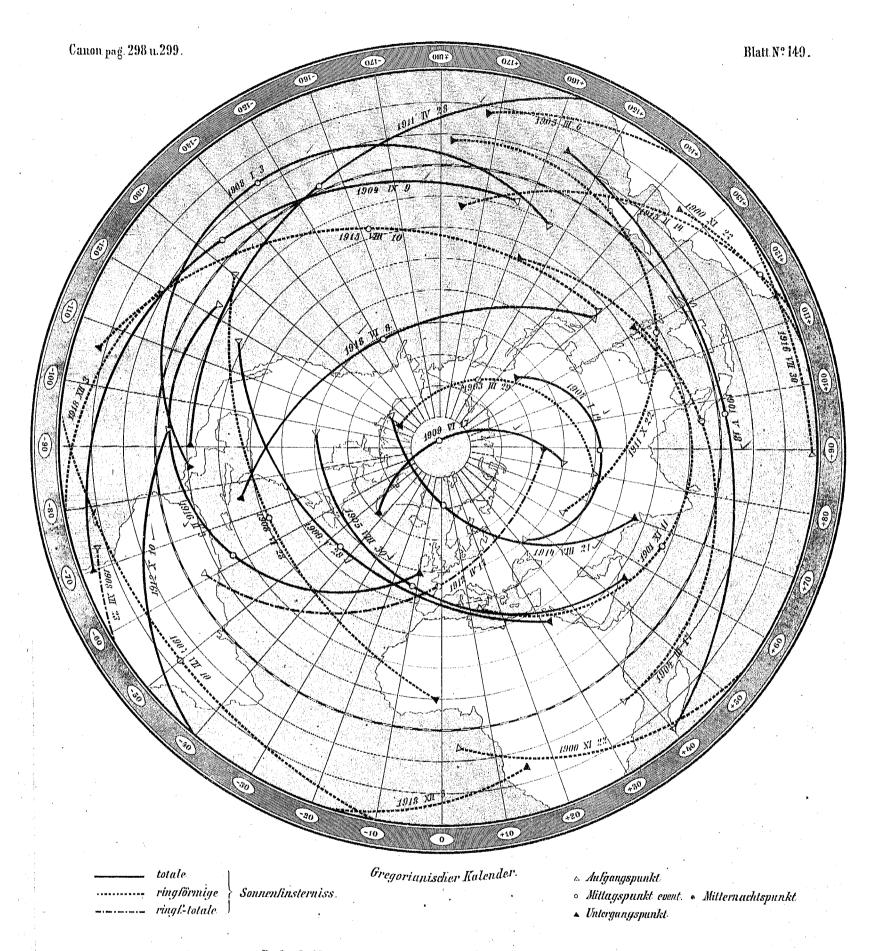


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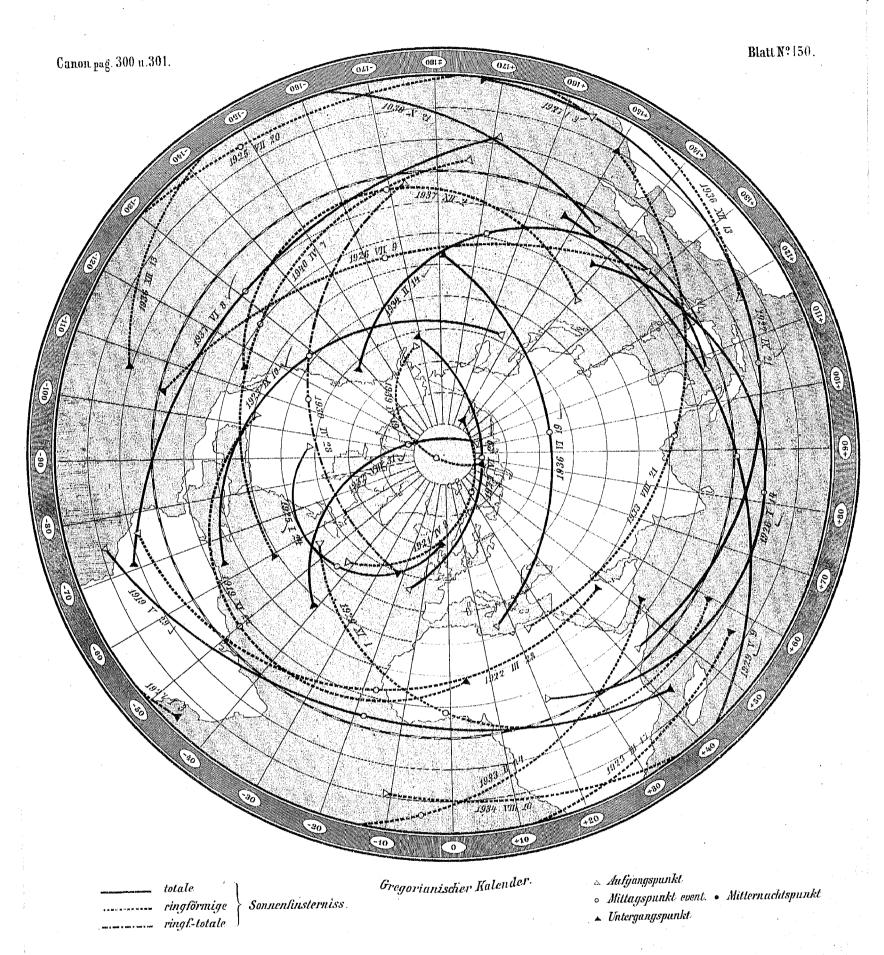
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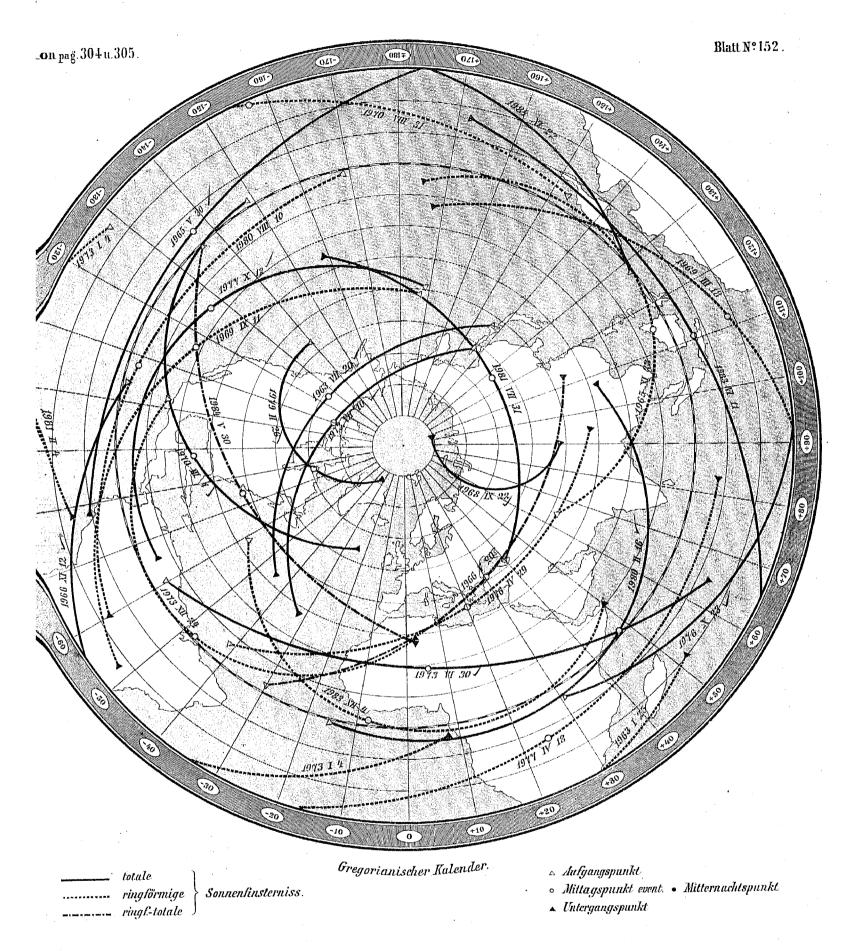


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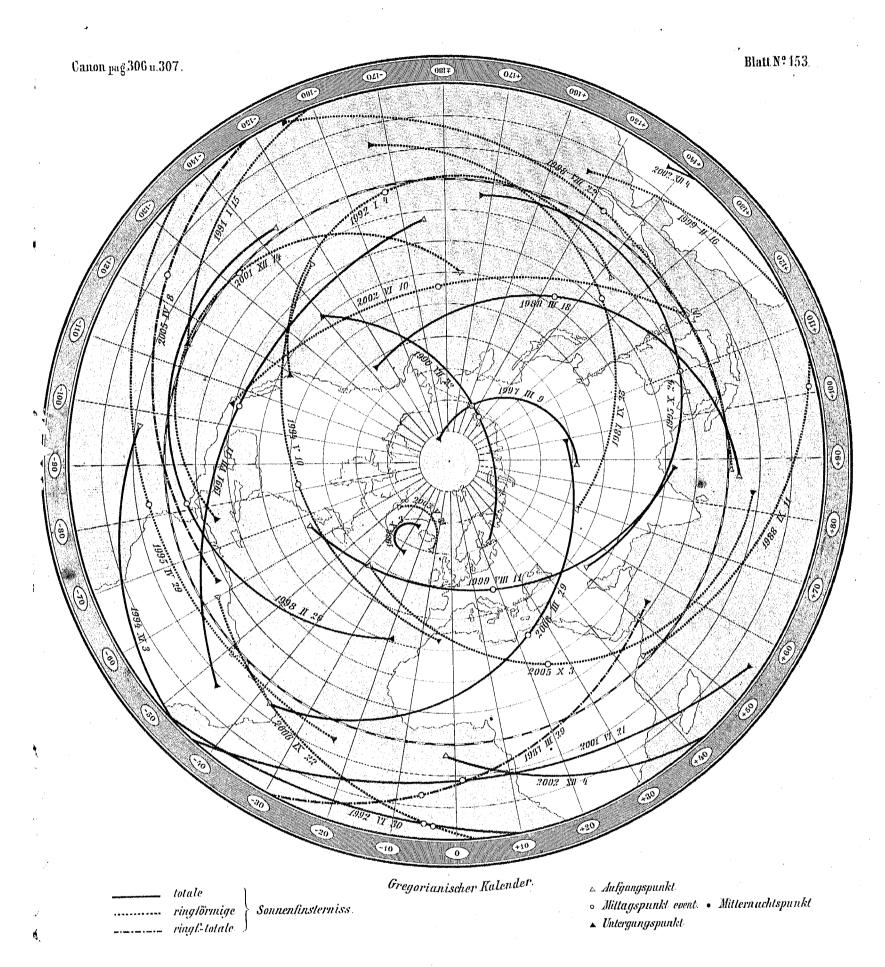
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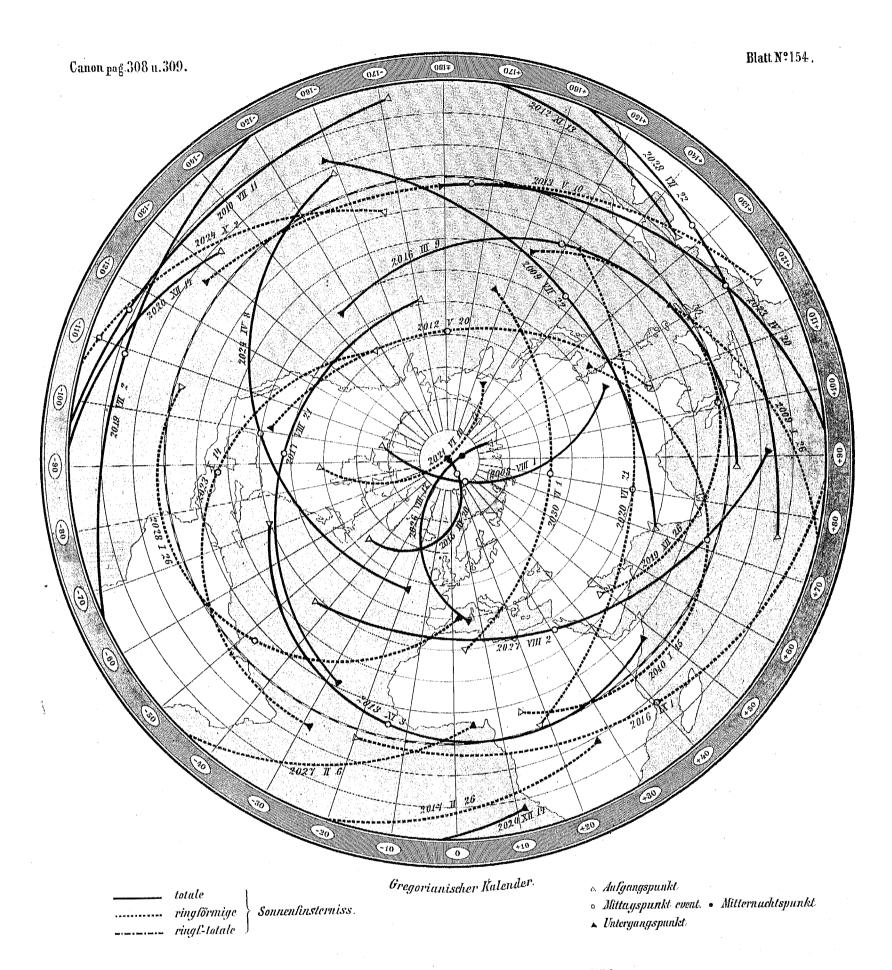
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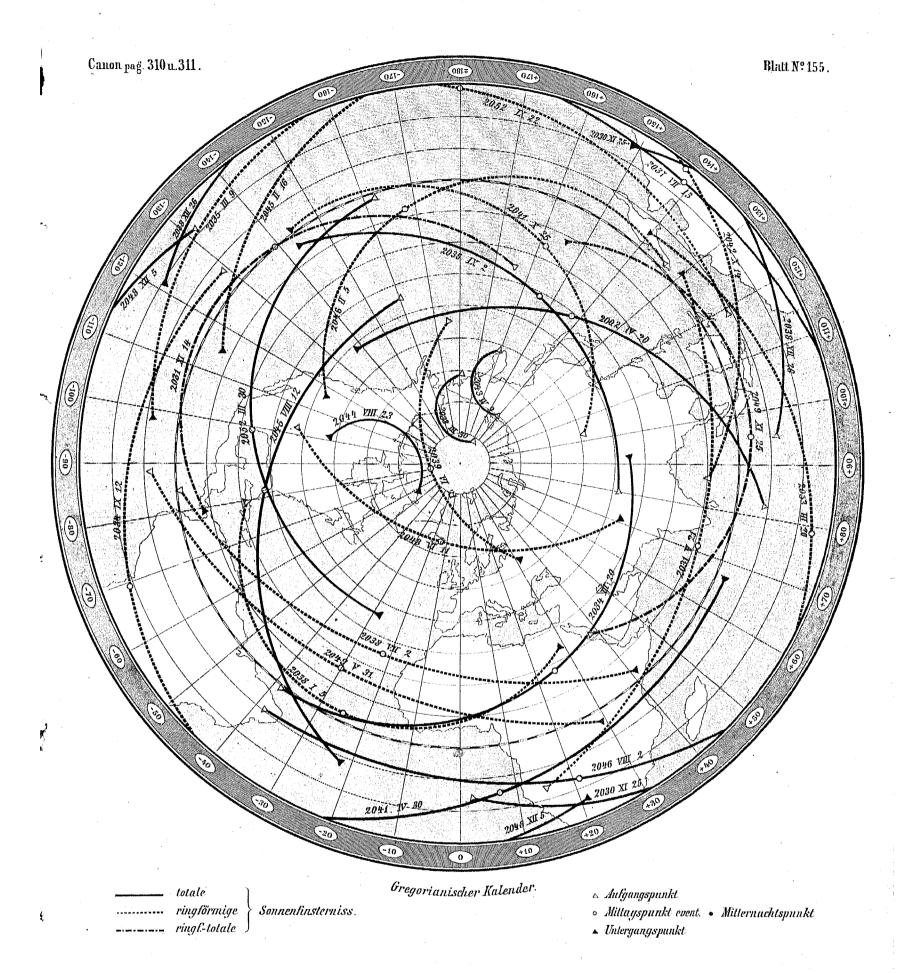
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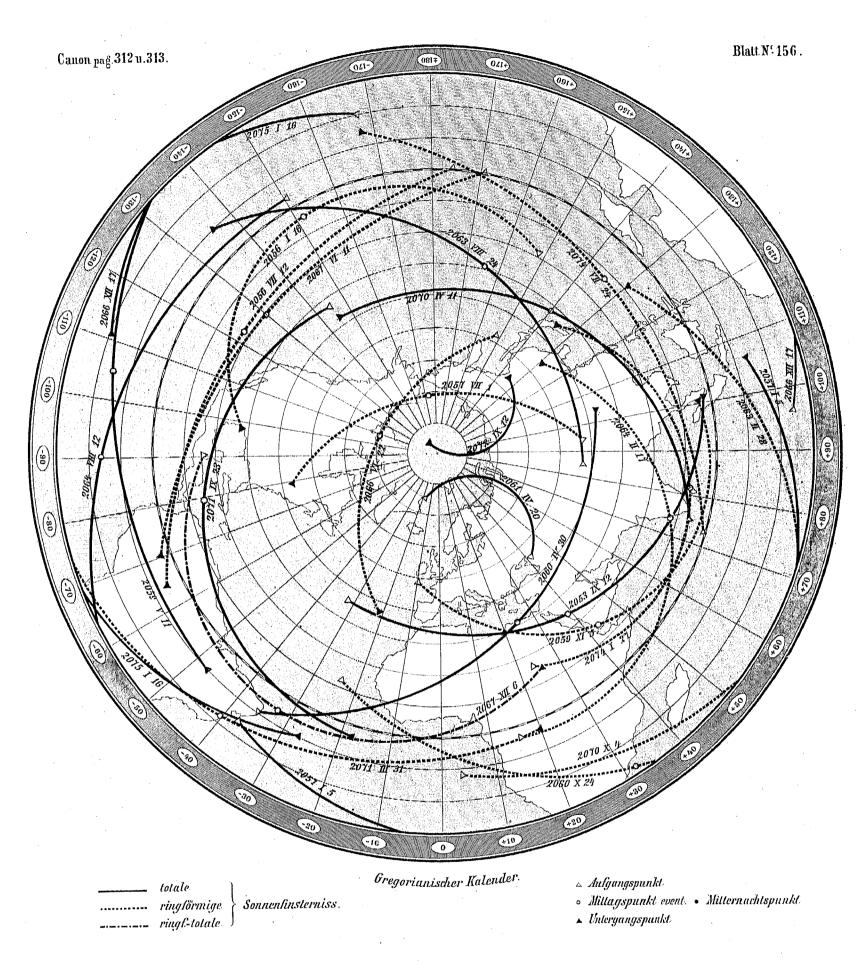
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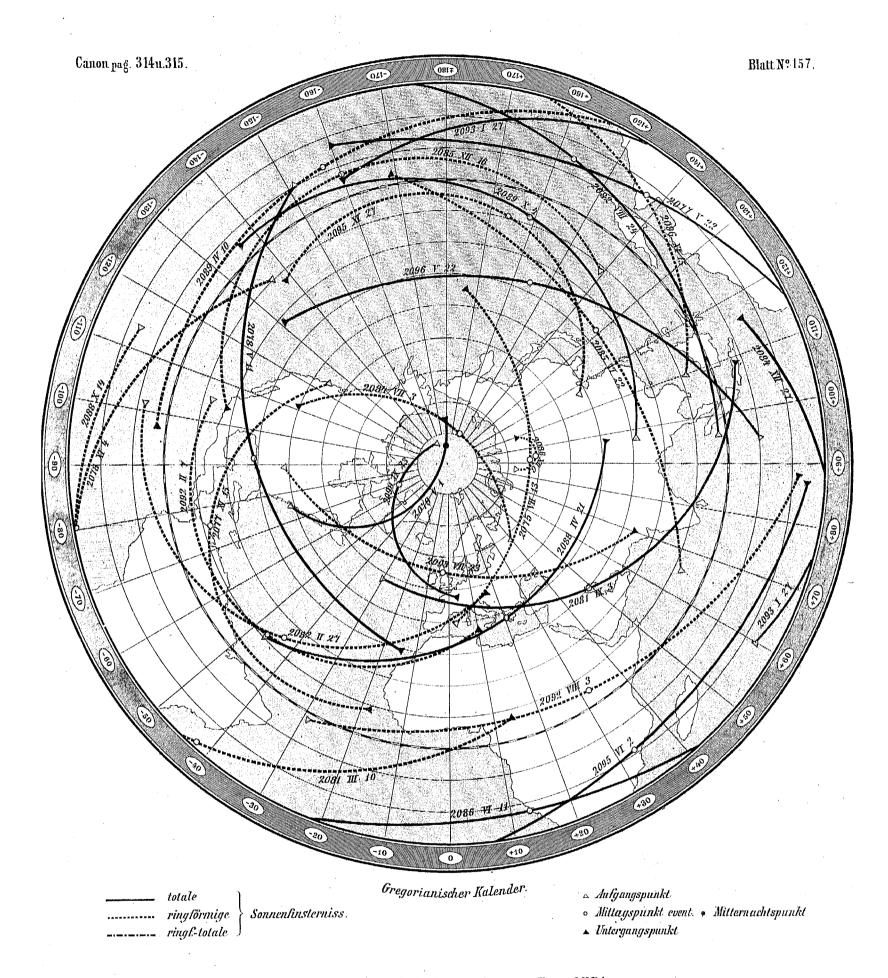


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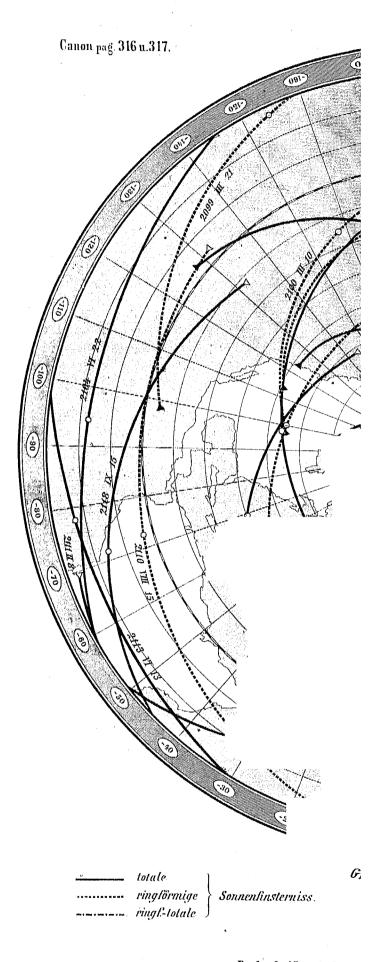
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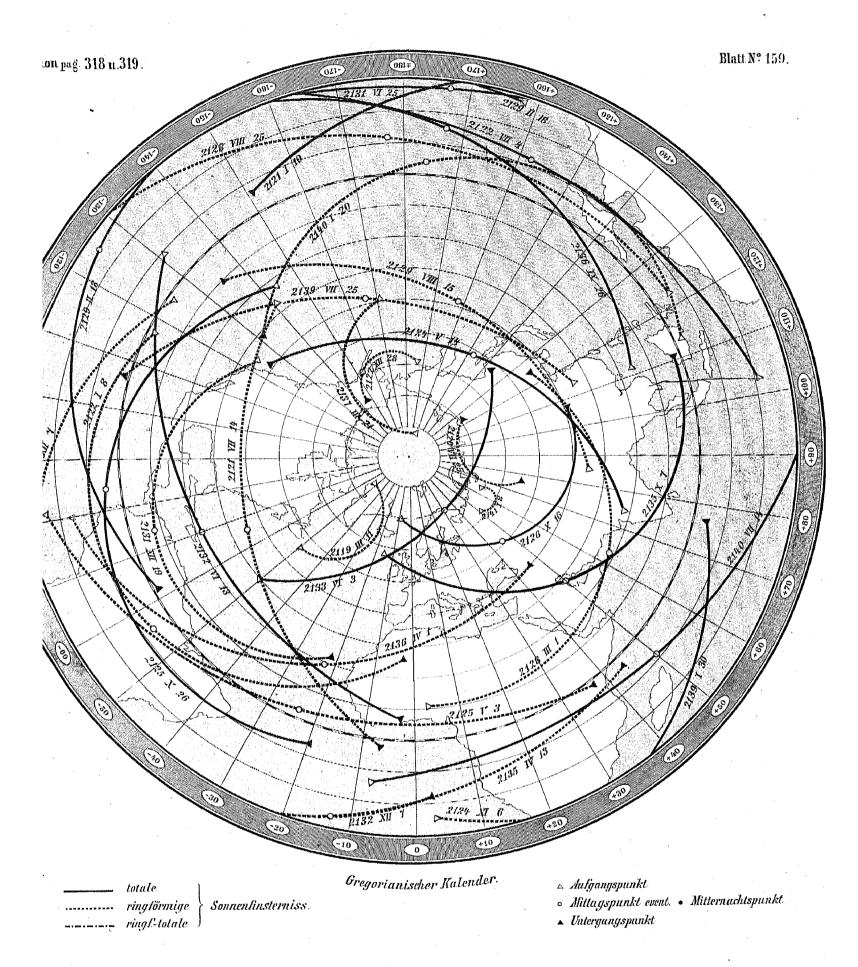


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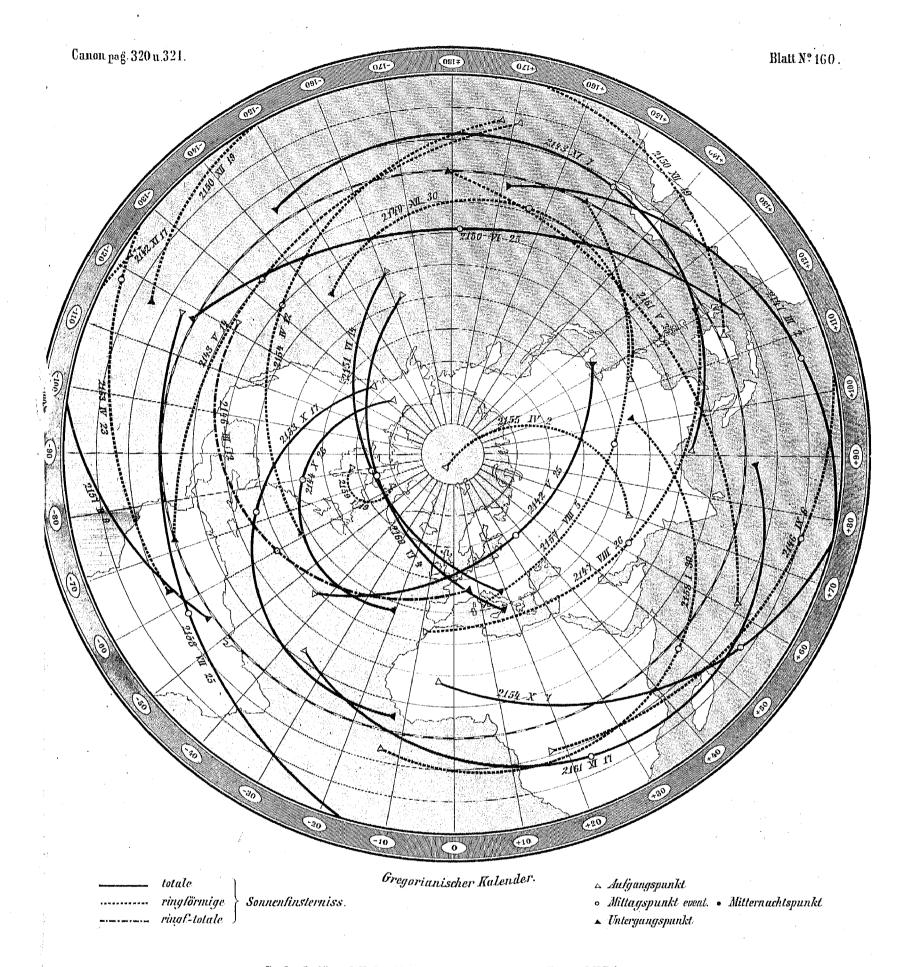
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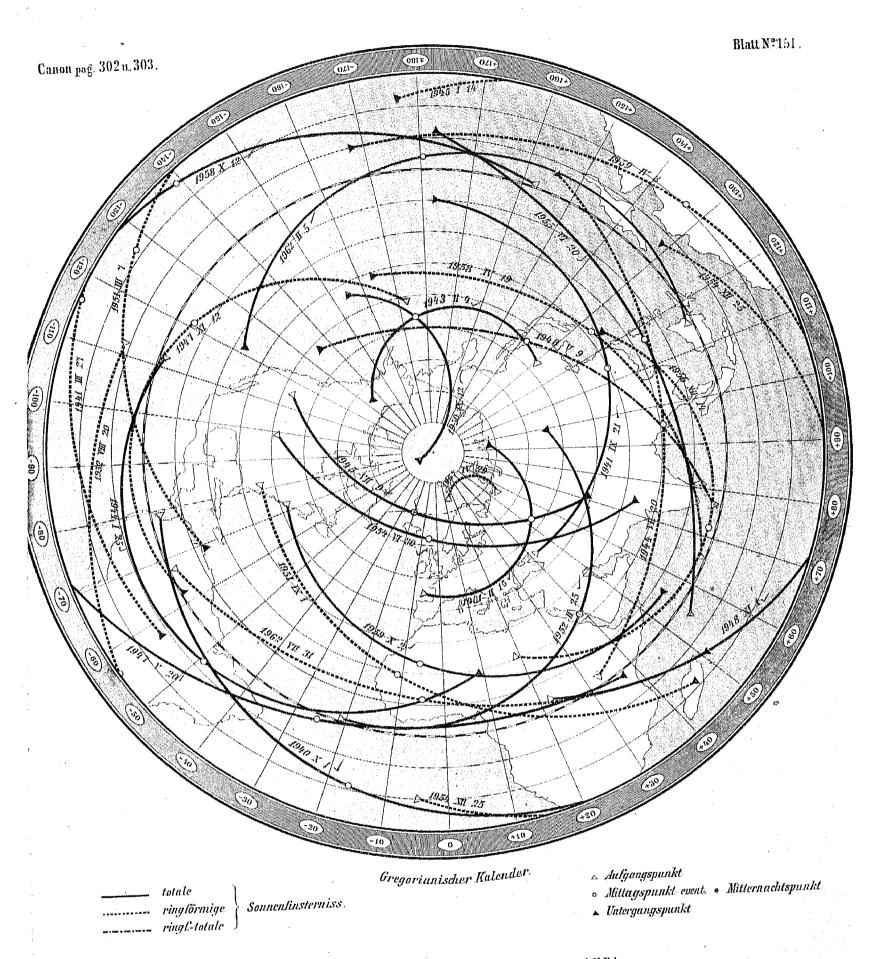


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Denkschriften d. Kais. Akad.d. Wiss. malh-naturw. Classe LH.Bd.